

REPORT ON A HELICOPTER-BORNE MAGNETIC AND ELECTROMAGNETIC SURVEY

"featuring the AeroQuest AeroTEM® System"



Bannockburn Property
Bannockburn Township, Matachewan Area, Ontario

for

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TABLE OF CONTENTS

1.	INTRODUCTION	1
2.	SURVEY AREAS	1
3.	SURVEY SPECIFICATIONS AND PROCEDURES	3
4.	AIRCRAFT AND EQUIPMENT	5
5.	PERSONNEL	10
6.	DELIVERABLES	10
7.	DATA PROCESSING AND PRESENTATION	11

Figures

- Figure 1-2:** Location Maps
- Figure 3:** The EM and Mag Birds
- Figure 4:** The Instrument Rack
- Figure 5:** Schematic of Tx and Rx waveforms

Appendices

- Appendix 1:** Interpretation Report by J. Rudd
- Appendix 2:** Survey Block Co-ordinates
- Appendix 3:** Description of Database Fields
- Appendix 4:** Technical Paper entitled "Mineral Exploration with the AeroTEM System"
- Appendix 5:** Instrumentation Specification Sheet

Author's Statement of Qualifications

MAPS

The results of the survey are presented in a series of black line and colour maps at a scale of 1:10,000. Map products are as follows:

- Plate 1. Flight path with EM anomaly centres.
- Plate 2. Total Magnetic Intensity (TMI) colour grid w/line contours and anomaly centres.
- Plate 3. Z1 On-time, Z5 On-time,, and Z0 Off-time EM profiles and anomaly centres.
- Plate 4. Z0 Off-time EM colour grid w/line contours and anomaly centres.

All the maps show the flight path, claims fabric, and skeletal topography, and EM anomalies represented by conductance classified symbols. An anomaly identifier label and the estimated conductance in siemens are posted alongside the anomaly symbol. Colour contour maps show colour fill plus superimposed line contours.

DIGITAL DATA on DVD-ROM

The results of the survey are archived on a single DVD-ROM as Geosoft GDB (binary) database(s) as well as Geosoft maps and magnetic grids. A *readme.txt* file may be found on the DVD which describes the contents in more detail.

For the reader's convenience, a copy of Geosoft's Oasis Montaj Ver 6.0 Free Interface is included on the DVD. To install the interface, unzip the two files and follow the instructions in the PDF format (Adobe Reader) guide.

The DVD also contains a digital version of this report in PDF (Adobe Acrobat) format including the technical paper by Balch, et al, which is re-printed in the appendix of this report. Adobe Acrobat Reader Ver 5.0 has been included on the DVD.

REPORT ON A HELICOPTER-BORNE MAGNETIC AND ELECTROMAGNETIC SURVEY

**Bannockburn Property
Bannockburn Township, Matachewan Area, Ontario**

1. INTRODUCTION

This report describes a helicopter-borne geophysical survey carried out on behalf of Mustang Minerals Corp. on the Bannockburn Property, in Bannockburn Township, in the Matachewan area of Ontario.

Principal geophysical sensors included AeroQuest's exclusive AeroTEM[®] time domain helicopter electromagnetic system and a high sensitivity cesium vapour magnetometer. Ancillary equipment included a GPS navigation system with GPS base station, radar altimeter, video recorder, and a base station magnetometer. Raw streaming EM data, consisting of 126 channels of Z and X component sampled at 300 times per second during both on-current and off-current times, was recorded. A second RMS "analogue" acquisition system recorded 6 Z-component and one X-component channels of semi-processed EM data at 7.5 times per second, in addition to recording GPS position, magnetic field, and terrain clearance.

The Bannockburn Property was acquired by Mustang Minerals Corp. for its potential to host both economic Kambalda-style nickel-copper (Ni-Cu) mineralisation and Mount Keith-style Ni-Cu mineralisation.

Appendix 1 lists the UTM corner co-ordinates for the survey area and provides a list of claims covered by the survey. The total line kilometres (unwindowed) flown was 2368.2 km. The survey flying described in this report took place on April 20 - May 11, 2004.

Bedrock EM anomalies were interpreted and graded according to the estimated conductance. This report describes the survey, the data processing and presentation and includes an interpretation report, prepared separately by Mr. S. Balch, in the appendix.

2. SURVEY AREA

The Bannockburn survey block occupies the west half of Bannockburn Township, as well as parts of Montrose, Doon, Midlothian, Zavitz, Argyle and Hincks Townships. The block lies approximately 62 km south-southeast of the city of Timmins and 17 km west of the village of Matachewan (Figure 1). Primary access to the block is via Provincial Highway 566 which crosses the block in two places. Further access to the area is by numerous logging roads and trails connected to the north to Timmins and Hwy 144 and south to Shining Tree and Hwy 560. The property is centred at 48°00'N latitude, 80°55'W longitude.

3. SURVEY SPECIFICATIONS AND PROCEDURES

The survey specifications are summarised in the following table:

Area Name	Line Spacing (m)	Line Direction	Unwindowed Total Survey (km)	Windowed Total Survey (km)	Dates Flown (2004)
Bannockburn	50/100	N-S & E-W	2368.2	2038.8	Apr 25-May 11

The unwindowed kilometres flown is calculated by adding up the survey and control (tie) line lengths as presented in the database. The windowed kilometres is determined in the same manner but after masking the database with an outline of the claims boundary. All the survey lines flown in both the UTM grid North/South and East/West direction. The control (tie) lines were flown perpendicular to the survey lines.

Nominal EM bird terrain clearance was ~30m (100 ft). The magnetometer sensor was mounted in a smaller bird connected to the tow rope 21 metres above the EM bird and 17 metres below the helicopter. Nominal survey speed was 75 km/hr. Scan rates for data acquisition was 0.1 second for the magnetometer, electromagnetics and altimeter and 0.2 second for the GPS determined position. This translates to a geophysical reading about every 2-3 metres along flight track.

Navigation was assisted by a GPS receiver and the RMS data acquisition system which reports GPS co-ordinates as NAD27 latitude/longitude and directs the pilot over a pre-programmed survey grid. The x-y-z position of the aircraft, as reported by the GPS, is recorded at 0.2 second intervals.

Unlike frequency domain electromagnetic systems, the AeroTEM[®] system has negligible drift due to thermal expansion. The system static offset is removed by high altitude zero calibration lines and employing local levelling lines.

The operator was responsible for ensuring the instrument was properly warmed up prior to departure and that the instruments operated properly throughout the flight. He also maintained a detailed flight log during the survey noting the times of the flight as well as any unusual geophysical or topographic features.

On return of the aircrew to the base camp, the RMS acquisition system survey data on FlashCard was downloaded to the data processing work station. The MDAS recorded data, on removable hard-drive, was also downloaded to the processing station and archived onto DVD. In-field processing included flight preparation, transfer of the RMS acquired data to Geosoft GDB database format and production of preliminary EM, magnetic contour, and flight path maps. Survey lines which showed excessive deviation from the intended flight path were re-flown.

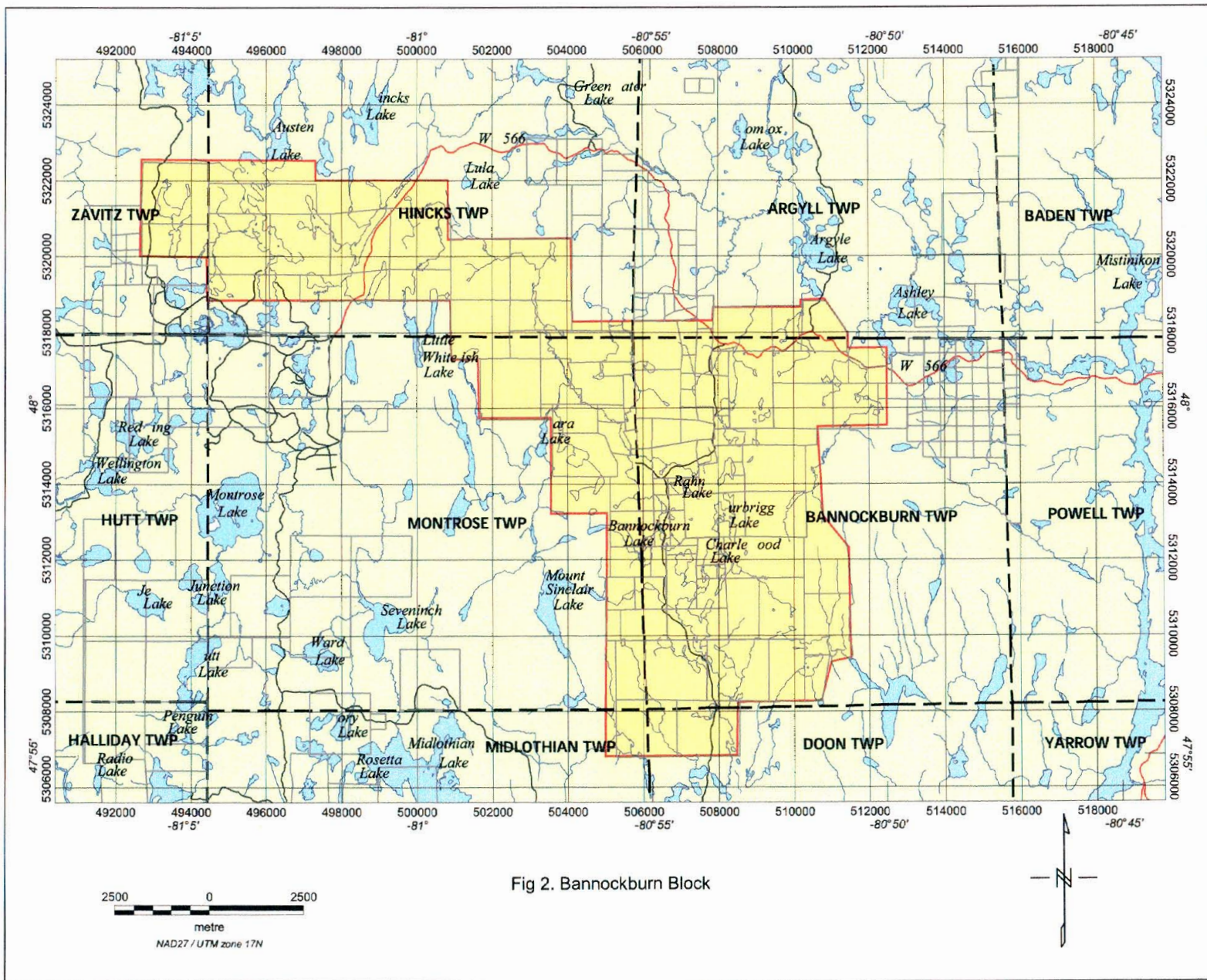


Fig 2. Bannockburn Block

4. AIRCRAFT AND EQUIPMENT

4.1 Aircraft

A Eurocopter (Aerospatiale) AS350B2 "A-Star" helicopter - registration C-FAVI was used as survey platform. The helicopters was owned and operated by Abitibi Helicopters Ltd., LaSarre, P.Q. Installation of the geophysical and ancillary equipment was carried out by AeroQuest Limited at the Gateway Helicopters Base in North Bay, Ont. then ferried to the survey area. The survey aircraft was flown at a nominal terrain clearance of 220 ft (70 m).

4.2 Magnetometer

The AeroQuest airborne survey system employed the Geometrics G-823A cesium vapour magnetometer sensor installed in a two metre towed bird airfoil attached to the main tow line, 17 metres below the helicopter. The sensitivity of the magnetometer is 0.001 nanoTesla at a 0.1 second sampling rate. The nominal ground clearance of the magnetometer bird was 51 metres (170 ft.). The magnetics data is recorded at 10Hz by the RMS DGR-33.



Fig.3 The mag bird (foreground) and EM bird

4.3 Electromagnetic System

The electromagnetic system employed was an AeroQuest AeroTEM[®] Time Domain towed bird system. A triangular transmitter on-time pulse of 1.150 millisecond is employed, at a base frequency of 150 Hz. During every tx on-off cycle (300 per second), 126 contiguous channels of raw x and z component (as well as a transmitter current monitor, itx) of the received waveform are measured. Each channel width is 26.455 microsec starting at the beginning of the Tx pulse on. This 126 channel data is referred to as the raw streaming data.

The AeroTEM system has two separate EM data recording streams, the conventional RMS DGR-33 and the MDAS system.



Fig.4 Instrument Rack

RMS DGR-33 Acquisition System

In addition to the magnetics, altimeter and position data, six time channels of on-board real time processed off-time EM decay in the Z direction and one in the X direction are recorded by the RMS DGR-33 acquisition system at 7.5 samples per second. These channels are derived by a real-time binning, stacking and filtering procedure on the raw streaming data. The RMS data (Z1 to Z6, X1) is also sent to the analogue chart recorder and is often referred to as the analogue data.

The channel window timing of the RMS DGR-33 6 channel system is described in the table below.

RMS Channel	Start time (microsec)	End time (microsec)	Width (microsec)	Streaming Channels	Noise tolerance
Z1, X1	1269.8	1322.8	52.9	48-50	20 ppb
Z2	1322.8	1455.0	132.2	50-54	20 ppb
Z3	1428.6	1587.3	158.7	54-59	15 ppb
Z4	1587.3	1746.0	158.7	60-65	15 ppb
Z5	1746.0	2063.5	317.5	66-77	10 ppb
Z6	2063.5	2698.4	634.9	78-101	10 ppb

MDAS Acquisition System

The 126 channels of raw streaming are recorded by the MDAS acquisition system onto a removable hard drive. The streaming data may undergo post-survey processing to yield 33 stacked and binned on-time and off-time channels at a 10 Hz sample rate. The timing of those reduced streaming channels is described in the following table.

Processed Channel	Measured Channels	Start (microsec)	Stop (microsec)	Mid (microsec)	Width (microsec)
1 ON	24	634.9	661.4	648.1	26.5
2 ON	25	661.4	687.8	674.6	26.5
3 ON	26	687.8	714.3	701.1	26.5
4 ON	27	714.3	740.7	727.5	26.5
5 ON	28	740.7	767.2	754.0	26.5
6 ON	29	767.2	793.7	780.4	26.5
7 ON	30	793.7	820.1	806.9	26.5
8 ON	31	820.1	846.6	833.3	26.5
9 ON	32	846.6	873.0	859.8	26.5
10 ON	33	873.0	899.5	886.2	26.5
11 ON	34	899.5	925.9	912.7	26.5
12 ON	35	925.9	952.4	939.2	26.5
13 ON	36	952.4	978.8	965.6	26.5
14 ON	37	978.8	1005.3	992.1	26.5
15 ON	38	1005.3	1031.7	1018.5	26.5
16 ON	39	1031.7	1058.2	1045.0	26.5
0 OFF	44	1164.0	1190.5	1177.2	26.5
1 OFF	45	1190.5	1216.9	1203.7	26.5
2 OFF	46	1216.9	1243.4	1230.2	26.5
3 OFF	47	1243.4	1269.8	1256.6	26.5
4 OFF	48	1269.8	1296.3	1283.1	26.5
5 OFF	49	1296.3	1322.8	1309.5	26.5
6 OFF	50	1322.8	1349.2	1336.0	26.5
7 OFF	51	1349.2	1375.7	1362.4	26.5
8 OFF	52	1375.7	1402.1	1388.9	26.5
9 OFF	53	1402.1	1428.6	1415.3	26.5
10 OFF	54	1428.6	1455.0	1441.8	26.5
11 OFF	55	1455.0	1481.5	1468.3	26.5
12 OFF	56	1481.5	1507.9	1494.7	26.5
13 OFF	57-60	1507.9	1640.2	1574.1	132.3
14 OFF	61-68	1613.8	1825.4	1719.6	211.6
15 OFF	69-84	1825.4	2248.7	2037.0	423.3
16 OFF	85-116	2248.7	3095.2	2672.0	846.6

T

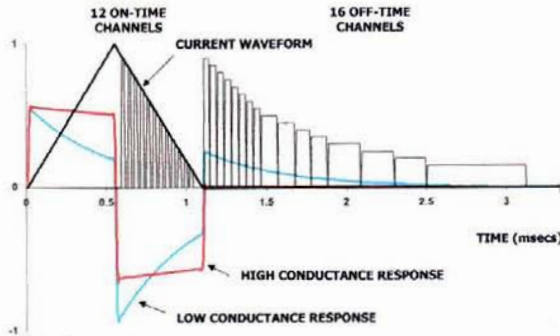


Fig. 5 Schematic of Tx and Rx waveforms

The current AeroTEM[®] Transmitter Dipole moment is 38.8 kNIA. The AeroTEM[®] bird was towed 38 metres (125 ft) below the helicopter. More technical details of the system may be found in the technical paper in the Appendix.

4.4 Ancillary Systems

Magnetometer and GPS Base Station

An integrated GPS and magnetometer base station was set up to monitor the static position GPS errors to permit differential post-processing and to record the diurnal variations of the earth's magnetic field. Each sensor, GPS and magnetic, receiver/signal processor was attached to a dedicated laptop computer for purposes of instrument control and/or data display and recording. The laptops were, in turn, linked together to provide a common recording time reference using the GPS clock.

The base magnetometer was a Scintrex CS-2 cesium precession magnetometer coupled with a Picodas MEP-710 frequency counter/decoupler. Data logging and magnetometer control was provided by the Picodas *basemag.exe* software. The logging was configured to measure at 1.0 second intervals. Digital recording resolution was 0.1 nT. The sensor was placed on a tripod away from potential noise sources outside of the lodge. A continuously updated profile plot of the base station values was available for viewing on the base station display.

The GPS base station employed a Leica Mx9212 12 channel GPS receiver with external antenna mounted near the magnetometer sensor. Although the GPS receiver was controlled by the Picodas *cdu510.exe* software, logging was not engaged as the aircraft employed a real-time differential GPS receiver. The base GPS was used only for the GPS clock for synchronisation purposes.

RRadar Altimeter

A Terra TRA 3500/TRI-30 radar altimeter was used to record terrain clearance. The antenna was mounted on the outside of the helicopter beneath the cockpit. The recorded data represented the height of the antenna, i.e. helicopter, above the ground. The Terra altimeter has an altitude accuracy of +/- 1.5 metres.

Video Tracking and Recording System

A high resolution colour VHS/8mm video camera was used to record the helicopter ground flight path along the survey lines. The video is digitally annotated with GPS position and time and can be used to verify ground positioning information and cultural causes of anomalous geophysical data.

GPS Navigation System

The navigation system consisted of an Ag-Nav Inc. AG-NAV2 GPS navigation system comprising a PC based acquisition system, navigation software, a deviation indicator in front of the aircraft pilot to direct the flight, a full screen display with controls in front of the operator, a Trimble AgGPS132 WAAS enabled GPS receiver mounted on the instrument rack and a Trimble antenna mounted on the magnetometer bird.

WAAS (Wide Area Augmentation System) consists of approximately 25 ground reference stations positioned across the United States that monitor GPS satellite data. Two master stations, located on either coast, collect data from the reference stations and create a GPS correction message. This correction accounts for GPS satellite orbit and clock drift plus signal delays caused by the atmosphere and ionosphere. The corrected differential message is then broadcast through one of two geostationary satellites, or satellites with a fixed position over the equator. The corrected position has a published accuracy of under 3 metres. A recent static ground test of the Trimble WAAS GPS yielded a standard deviation in x and y of under 0.6 metres and for z under 1.5 metres over a two hour period.

Survey co-ordinates are set-up prior to survey and the information is fed into the airborne navigation system. The co-ordinate system employed in the survey design was NAD83 UTM. The real-time differentially corrected GPS positional data was recorded by the RMS DGR-33 in NAD83 latitude and longitude at 0.2 second intervals directly in the analogue geophysical data file. The datum of the recorded latitude/longitude depended on the datum defined in the navigation file used to guide the survey aircraft.

Digital Acquisition System

The RMS Instruments DGR33A data acquisition system was used to collect and record the analogue data stream, i.e. the geophysical and positional data, including processed 6 channel EM, magnetic, radar altimeter, GPS position, and time. The data was recorded on 128Mb capacity FlashCard. The RMS output was also directed to a thermal chart recorder.

The AeroTEM received waveform sampled during on and off-time at 126 channels per decay, 300 times per second, was logged in parallel by the proprietary MDAS data acquisition system. The channel sampling commences at start of the Tx cycle and the width of each channel is 26.445 microseconds. The streaming data was recorded on a removable hard-drive and was later backed-up onto DVD-ROM on the field-processing computer.

5. PERSONNEL

The following AeroQuest personnel were involved in the project

Field -

Party Chief: Bert Simon

Data Processor: Chris Balch

Operator: Marcus Watson

Office-

Data Processing and Report: Neil Fiset/Matt Holden/Steve Balch

Interpretation: Steve Balch

The survey pilot, Kevin Jackson, was employed directly by the helicopter operator - Abitibi Helicopters Ltd.

6. DELIVERABLES

The report includes a set of four geophysical maps plotted at 1:10,000 scale. The map types are as follows:

- Plate 1. Flight path with EM anomaly centres.
- Plate 2. Total Magnetic Intensity (TMI) colour grid w/line contours and anomaly centres.
- Plate 3. Z1 On-time, Z5 On-time, and Z0 Off-time EM profiles and anomaly centres.
- Plate 4. Z0 Off-time EM colour grid w/line contours and anomaly centres.

The block was divided into an A, B, and C sheet. An additional sheet, "D", covers the east-west flying with flight path and EM profiles. The basic map coordinate/projection system used to create the maps was NAD27 Canada Mean Universal Transverse Mercator Zone 17. For reference, the latitude and longitude are also noted on the maps.

All the maps show flight path trace with time reference fiducials marked at a 10 second interval, skeletal topography, claims fabric, and conductor picks represented by an anomaly symbol classified according to estimated conductance. The anomaly symbol is accompanied by postings denoting the conductance as well as an anomaly identifier label. The anomaly symbol legend may be found in the margin of the maps. Colour contour maps show colour fill plus superimposed line contours.

The geophysical profile data is archived digitally in a Geosoft GDB binary format database. The binary database contains both the processed streaming data and the RMS data.

The Geosoft database included is as follows (filename extension is ".gdb"):

<u>Area</u>	<u>RMS & Streaming Data</u>
Bannockburn	Bannockburn.gdb

A description of the various channels found in this database may be found in the appendices of this report.

An archive CD complements the hard copy report and maps. It contains the digital database as well as the geophysical maps and grids in Geosoft format.

7. DATA PROCESSING AND PRESENTATION

All in-field and post-field data processing was carried out using Geosoft Montaj as well as AeroQuest proprietary data processing software. Plotting was on a 36 inch wide HP650C ink-jet plotter.

7.1 Base Map

The geophysical maps accompanying this report are based on positioning in the datum of NAD27 Canada Mean. The survey geodetic GPS positions have been map projected using the Universal Transverse Mercator projection in Zone 17.

A summary of the map datum and projection specifications are as follows:

Ellipse: Clark 1866

Ellipse major axis: 6378206.4m eccentricity: 0.082271854

Datum: North American 1927 - Canada Mean

Datum Shifts (x,y,z) : 10, -158, -187 metres

Map Projection: Universal Transverse Mercator Zone 17 (Central Meridian 81°W)

Central Scale Factor: 0.9996

False Easting, Northing: 500,000m, 0m

The skeletal topography, provided by Mustang Minerals Corp., was derived from the digital Ontario Base Map (OBM) 1:20,000 map series. The claims fabric was downloaded from the MNDM website in NAD83 then reprojected to NAD27 Canada Mean before merging with the topographic data.

7.2 Flight Path & Terrain Clearance

The position of the survey helicopter was directed by use of the Global Positioning System (GPS). Positions were updated five times per second (5Hz) and expressed as NAD27 latitude and longitude calculated from the raw pseudorange derived from the C/A code signal.

The instantaneous GPS flight path, after conversion to NAD27 Canada Mean UTM co-ordinates, is drawn using linear interpolation between the x/y positions. The time reference fiducials are drawn on the map at appropriate intervals and are used to reference the digital data files to the plan map.

The raw Digital Terrain Mode (DTM) was derived by simply taking the satellite position altitude and subtracting the radar altimeter. The calculated values are relative and are not tied into to surveyed geodetic heights.

7.3 Electromagnetic Data

The raw streaming data, sampled at a rate of 38,400 Hz (126 channels, 300 times per second) was reprocessed using a proprietary software algorithm developed by Mr. Steve Balch. Processing began with a segmenting and synchronisation procedure that isolates the relevant portion of the flight and pre-processes the time series to ensure data synchronisation is maintained. The pre-processed segment was then partially stacked and tested for high noise events, including sferics, which are skipped during the main stacking procedure. The coefficients for the waveform deconvolution process were also determined.

During the main processing algorithm, data were stacked for 40 full-cycles or 0.2 seconds. Deconvolution of the system waveform, primary field removal during the on-time, and system transient removal during the off-time were performed ahead of the stacking. The data were then binned into the 16 On-time and 17 Off-time channels and their base levels corrected. The resulting profiles were then filtered using a filter with 11 coefficients. An overburden stripped response was generated by subtracting the off-time response from the on-time response for the X1 to X16 and Z1 to Z16 channels.

The final processing step was to merge the processed EM data back into a Geosoft GDB file with the GPS position, altimeter, levelled magnetics, etc. data. The EM fiducial is used to synchronise the two datasets. The processed channels are labelled in the database as ZOn1 to ZOn16, ZOff0 to ZOff16, XOn1 to XOn16, and XOff0 to XOff16. The overburden stripped channels are labelled Z1Obr to Z16Obr and X1Obr to X16Obr. In the database, the processed AeroTEM EM channels are expressed as nT/sec. To convert to parts per billion (ppb), multiply by 6.96. Conductors were interpreted based on a close visual examination of the EM profiles and taking into account the magnetic data along with geological and geochemical data provided by the client. A report of that interpretation may be found in the Appendices.

Conductors were interpreted based on a close visual examination of the EM profiles and taking into account the magnetic data along with geological and geochemical data provided by the client. A report of that interpretation may be found in the Appendices.

At each conductor pick, the on-time and off-time conductance have been calculated based on a conventional vertical thin sheet model and where the channel response satisfies a threshold of 5.0 nT/s on-time and 2.5 nT/s off-time. From these calculated values, an interpreted conductance (COND) value has been assigned to each anomaly. The assigned value is determined from the off-time response, unless there are 16 off-time channels with nT/s >2.0 in the response. In that event the assigned value is taken from the on-time because of the higher conductance. In the case of conductors marked by a double peak type response (thin, shallow sources) where the EM coupling is a minima over or near the conductor axis, the conductance value (COND) is derived from the higher response area adjacent to the axis. For each interpreted conductor, the number of off-time channels of response (from channels ZOff1-ZOff16) above the threshold is also noted.

Each conductor pick has been given an identification letter label and has also been classified according to a set of seven ranges of conductance values. The anomalies were then plotted on the plan maps with one of seven symbols reflecting that classification level. Adjacent to the map symbol is posted the identifier label as well as the interpreted conductance values in siemens. The maximum possible number of off-time channels is 16 given the first channel of the 17 processed channels is not included.

With regard to the six channel off-time data recorded by the RMS DGR-33, after a lag correction then a two stage digital filtering process was used to remove any residual short wavelength noise. Sharp large amplitude events were removed with a 0.4 sec non-linear filter. The signal to noise ratio was further improved by the application of a low pass linear digital filter. This filter has zero phase shift which prevents any lag or peak displacement from occurring, and it suppresses only variations with a wavelength less than about 1.0 seconds or 30 metres. This filter is referred to as a 1.0 sec linear filter. The raw channels are denoted in the database with the suffix "raw", e.g. z1raw, x1raw, etc. The filtered channels are indicated by the "f" suffix, e.g. z1f, x1f, etc.

During the high elevation checks, an internal 5 second wide calibration pulse in all EM channels was generated in order to ensure that the gain of the system remained constant and within specifications.

7.4 **Magnetic Data**

Prior to any levelling the magnetic data was subjected to a lag correction of -0.1 seconds and a spike removal filter. The filtered aeromagnetic data were then corrected for diurnal variations using the magnetic base station and the intersections of the tie lines. No corrections for the regional reference field (IGRF) were applied. The corrected profile data were interpolated on to a grid using a random grid technique with a grid cell size of 25 metres. The final levelled grid provided the basis for threading the presented contours which have a minimum contour interval of 20 nT.

Respectfully submitted,



Neil Fiset, B.Sc.,
AeroQuest Limited
August 18, 2004

APPENDIX 1

Interpretation Report by S. Balch

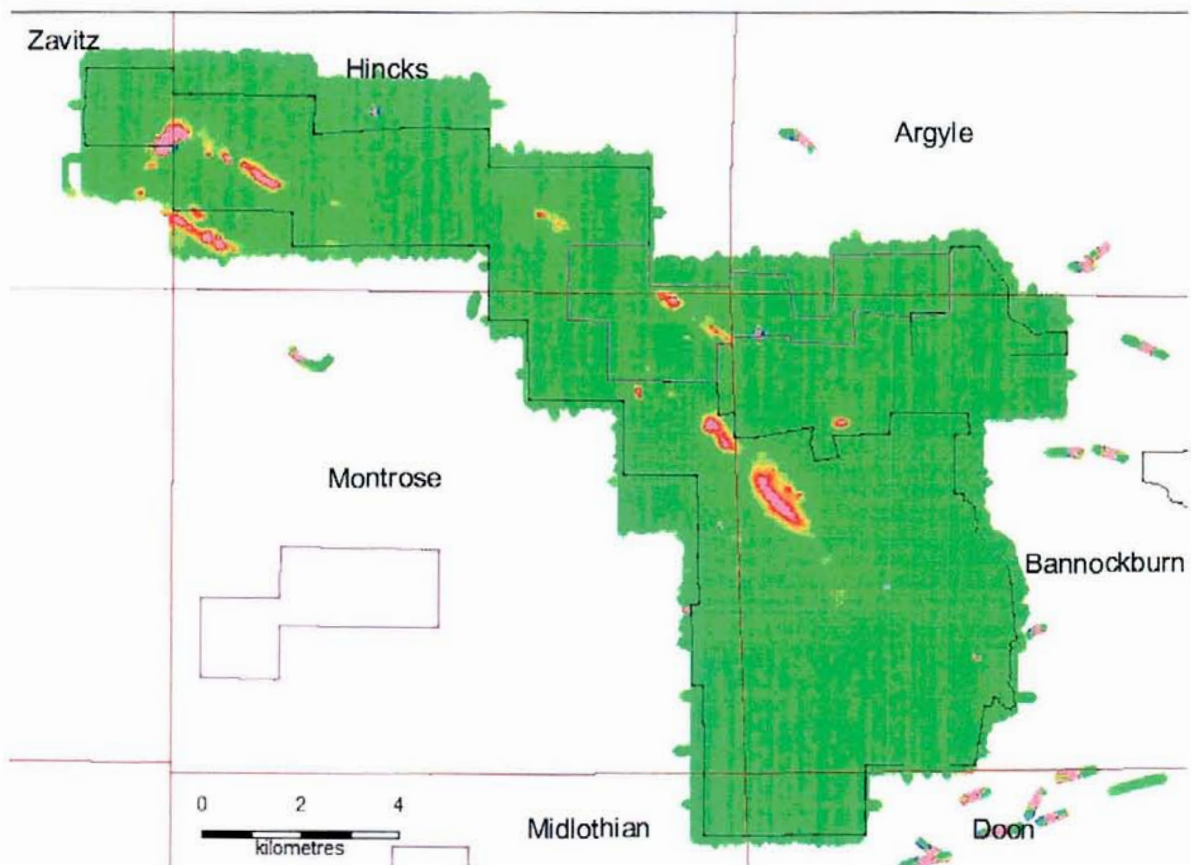
INTERPRETATION REPORT

Summary of an AeroTEM Airborne Geophysical Survey

On the Bannockburn Property

For

Mustang Minerals Corp



By

S.J. Balch

June 20, 2004

Introduction

Aeroquest Limited flew an AeroTEM helicopter electromagnetic and magnetometer survey over the Bannockburn Property owned by Mustang Minerals Corp during May and June of 2004. The main purpose of the survey was to characterize the nickel-copper-precious metals (Ni-Cu-PGMs) intersections of the known mineralization and to detect new Ni-Cu-PGM mineralization. The second purpose of the survey was to identify any other conductive targets that have the potential to be a mineralizing system and to characterize these targets as well.

The AeroTEM survey comprised a total of 2450 line kilometres. Over the known mineralization the line spacing was 50 m in both directions. Over the remainder of the property the line spacing was 100 m in a north to south line direction.

Background

Mustang Minerals Corp (Mustang) is exploring for Ni-Cu-PGM mineralization within ultramafic flows that are often termed Kambalda-type komatiitic lava flows. The geologic model assumes that nickel-sulphide within the ultramafic flow can erode the base of the host rock to form thickened zones of massive sulphide. This is a primary exploration target. It is also possible for nickel-sulphide to invade the country rock as veins or splays. This is also a primary exploration target. Lower percent nickel-sulphide can also occur within the ultramafic host. If the nickel tenor is high enough, it is possible to have economic concentrations within the host without requiring the concentration mechanisms of erosion or splaying. This is a secondary exploration target.

The geophysical signatures of Kambalda-type Ni-Cu-PGM mineralization will vary depending upon the nature of the target, but there are three general models that closely follow the geological ones. The most common model is a target of high conductance occurring within an area of highly anomalous magnetic field. The assumption is that the nickel-sulphide is highly conductive and occurs within the highly magnetic ultramafic. The second geophysical model is a high conductance target without an associated magnetic field high, but close to one. Here the geological model is massive nickel-sulphide splays that have exited the ultramafic host and entered the country rock. The third geophysical model is broad conductive trends that occur within a strong magnetic field high. This is the ultramafic host model with elevated nickel-sulphide where the concentration of sulphide is relatively low but the nickel tenor is elevated.

Results

At Bannockburn, AeroTEM has identified magnetic and conductive trends that satisfy two of the three geological models. In addition a number of interesting targets have been identified that are unlikely to represent nickel-sulphide within an ultramafic host, but nonetheless are of great interest. All of the targets are described below by zone.

The total magnetic field image is shown in Figure 1 for the entire property. An early time Z-axis EM response is shown in Figure 2. The total number of conductive trends on the property is estimated to be about 12 depending on how the trends are subdivided. This range provides an excellent framework for follow-up because the target areas are well defined.

B-Zone

The B-Zone is characterized by low percent sulphide within an ultramafic flow that extends for a distance of 1.2 km. The zone averages 1-2 S of conductance and appears to be rather uniform throughout. On some lines the conductance (and also the amplitude) increases slightly at the margins of the ultramafic suggesting a slight enhancement of sulphide at the contact, but in general the center of the ultramafic shows the highest conductance. The magnetic field over the B-Zone is shown in Figure 3, while the mid on-time EM response is shown in Figure 4. AeroTEM on-time profiles are shown in Figure 5 along with the total magnetic field and estimated conductance. The average conductance of the B-Zone at 1-2 S extends across distances of 200 m or more. This puts an estimate for conductivity of less than 0.01 S/m (10 ohm-m). Despite the high amplitude responses noted in the AeroTEM (and previous MegaTEM) survey, the B-Zone is a relatively poor conductor. The center of the B-Zone is listed in Table 1 for the east-west AeroTEM flight lines. Boreholes drilled in the vicinity of lines 3380 to 3431 would test the typical style of mineralization within the B-Zone. The possibility of an economic deposit would be tied more to a change in the sulphide tenor than to an increase in sulphide content (and hence an increase in metal concentration).

Line	Conductance (S)	East (m)	North (m)	Comments
3230	0.67	506376	5314467	North limit of B-Zone. Mineralization on eastern side of ultramafic.
3241	0.63	506362	5314437	Mineralization of eastern side of ultramafic.
3250	1.22	506336	5314373	Mineralization extends throughout ultramafic.
3262	1.06	506380	5314332	Mineralization centered within ultramafic.
3270	1.07	506322	5314263	Conductance rises near edges of zone.
3280	1.24	506345	5314226	
3290	1.17	506342	5314183	Conductance highest in center of ultramafic.
3300	1.36	506332	5314128	Broad zone of conductance with magnetics.
3310	1.42	506345	5314076	Broad zone of conductance with magnetics.
3320	1.65	506375	5314026	Broad zone of conductance with magnetics.
3330	1.67	506359	5313981	Broad zone of conductance with magnetics.
3340	2.03	506380	5313928	Broad zone of conductance with magnetics.
3350	1.81	506433	5313882	Broad zone of conductance with magnetics.
3360	1.83	506480	5313827	Broad zone of conductance with magnetics.
3372	2.01	506553	5313779	Broad zone of conductance with magnetics.
3380	2.22	506569	5313729	Broad zone of conductance with magnetics.
3390	2.40	506613	5313673	Broad zone of conductance with magnetics.
3400	2.15	506629	5313620	Broad zone of conductance with magnetics.
3410	2.21	506663	5313579	Broad zone of conductance with magnetics.
3420	2.11	506674	5313538	Broad zone of conductance with magnetics.
3431	2.07	506750	5313479	Broad zone of conductance with magnetics.
3440	1.85	506759	5313437	Broad zone of conductance with magnetics.
3450	1.85	506712	5313382	Broad zone of conductance with magnetics.
3460	1.54	506968	5313324	Broad zone of conductance with magnetics.
3470	1.51	506944	5313276	Broad zone of conductance with magnetics.
3480	1.15	506952	5313225	Broad zone of conductance with magnetics.
3490	1.12	507064	5313169	Broad zone of conductance with magnetics.
3500	0.95	507143	5313128	Broad zone of conductance with magnetics.
3510	0.90	507219	5313084	Broad zone of conductance with magnetics.
3520	1.77	507075	5313031	Obvious trend of increasing conductance to the west at depth.

3530	1.70	507180	5312974	Obvious trend of increasing conductance to the west at depth.
3540	2.31	507165	5312927	South termination of B-Zone.

Table 1. B-Zone conductor picks.

B-Zone Splay

The B-Zone splays into a small secondary zone at the southwest margin of the ultramafic unit. Based on the low conductance values (ranging from 0.40 to 1.24 S) it is unlikely that higher grade mineralization would be intersected within this splay. The approximate axis of the B-Zone splay is summarized in Table 2.

Line	Conductance (S)	East (m)	North (m)	Comments
3460	0.97	506538	5313327	Low conductance splay of the B-Zone.
3470	0.97	506559	5313262	Low conductance splay of the B-Zone.
3481	0.80	506553	5313233	Low conductance splay of the B-Zone.
3490	0.93	506606	5313191	Low conductance splay of the B-Zone.
3500	1.24	506682	5313138	Low conductance splay of the B-Zone.
3510	0.40	506577	5313080	Low conductance splay of the B-Zone.

Table 2. B-Zone splay conductor picks.

C-Zone

The C-Zone shows the highest conductance of any of the targets within the main ultramafic under exploration within the Bannockburn Property. On line 3380, for example, the peak conductance is 7 S, still low for pyrrhotite-rich massive sulphide, but much higher than the B-Zone. Given the narrow intersections of the C-Zone relative to the B-Zone, the conductivity of the C-Zone ranges from 0.1-1.0 S/m, or from ten to one hundred times greater than that of the B-Zone.

The C-Zone was flown with both north-south and east-west flight lines. Although the mineralization is thought to be trending east-west, the responses from the east-west flight lines produce a higher conductance and appear to be more diagnostic. A likely explanation is that flight line 3380 is located directly over the axis of the C-Zone. But it might also be possible that the C-Zone mineralization has both an east-west component and one that is north-south. It is recommended that the conductor picks be more closely matched to the geology and that some drilling be considered in an east-west direction to test for a possible north-south orientation to the mineralization. If the C-Zone is fault controlled there could be portions of the mineralization located along the fault margins (that are proposed to be oriented north-south).

Line	Conductance (S)	East (m)	North (m)	Comments
3372	2.54	507220	5313775	Emergence of C-Zone on east-west lines. No magnetic association.
3380	7.03	507165	5313732	Higher conductance response.
3390	2.89	507121	5313674	Edge of C-Zone.
1450	1.56	507067	5313697	Should be surrounded by low percent sulphide.
1455	2.48	507116	5313720	Slight north dip.
1460	2.58	507168	5313696	Thin sub-vertical response.
1465	2.99	507219	5313758	Small discrete response.

1470 2.61 507267 5313664 Very deep response (100+ m).

Table 3. C-Zone conductor picks.

D-Zone

The D-Zone is likely related to low percent sulphide located along the eastern margin of the ultramafic unit. There appear to be 2 zones defining this trend with an interruption between flight lines 3300 and 3330. The conductance range of the D-Zone is 0.12-1.41 S. Given its smaller thickness relative to the B-Zone the mineralization of the D-Zone is probably similar and would give rise to a similar conductivity. No drilling recommendations can be made with regards to the D-Zone unless there is a possibility that the nickel tenor is greater along the eastern margin of the ultramafic. Conductor picks for the D-Zone are listed in Table 4.

Line	Conductance (S)	East (m)	North (m)	Comments
3262	0.38	506938	5314322	North limit of D-Zone
3270	0.12	506922	5314264	Conductor centered within ultramafic splay.
3280	0.16	506911	5314228	Centered within magnetic response.
3290	0.12	506935	5314179	Probable pinching of the mineralization.
3300	0.78	506915	5314132	Lower amplitude, higher conductance.
3330	0.85	506901	5313975	Re-emergence of D-Zone.
3340	0.74	506867	5313927	D-Zone.
3350	0.85	506898	5313863	D-Zone. Strong magnetic association.
3360	0.73	506904	5313831	D-Zone. Strong magnetic association.
3372	1.19	506968	5313778	D-Zone conductance up marginally.
3380	1.41	506958	5313735	D-Zone amplitude dropping.

Table 4. D-Zone conductor picks.

I-Zone

The I-Zone is not related to nickel sulphide within an ultramafic. The zone is best described as having an east to west strike direction (300 m), moderate conductance, and no magnetic association. The eastern limit of the trend appears to be the most conductive (8-10 S). Lines 1540-1545 have the highest amplitude. Ground prospecting is recommended on the latter two lines, with a possible drill target suggested near 1545-1555 if the area is thought to be favourable for VMS style mineralization.

Line	Conductance (S)	East (m)	North (m)	Comments
1525	1.86	507815	5315218	Moderate conductance target with no magnetic association.
1530	1.60	507867	5315225	Thin conductor dipping to the south, low conductance and no magnetic association.
1535	1.37	507921	5315227	Two closely spaced conductors with no magnetic association.
1540	4.07	507966	5315235	Good amplitude, moderate conductance target, showing current migration to the south, with no magnetic association.
1545	5.32	508018	5315233	Good amplitude, moderate conductance target,

1550	8.27	508070	5315224	showing current migration to the south, with no magnetic association.
1555	10.65	508122	5315229	Moderate amplitude, good conductance target, thick, no magnetic association.
1560	3.21	508164	5315231	Moderate amplitude, good conductance target, no magnetic association. Low amplitude, low conductance target representing the eastern termination of the I-Zone, with no magnetic association.

Table 5. I-Zone conductor picks.

J-Zone

The J-Zone is a southeast trending conductor that dips to the northeast and extends from flight lines 1170 to 1320. The zone has no magnetic association. To the northwest the zone is dipping steeply to the northeast and is thin. Toward the southeast the zone dips to the northeast at a shallow angle (within 30° of surface). The cause for the conductor is unknown, but it has the same trend as the main ultramafic unit at Bannockburn.

Line	Conductance (S)	East (m)	North (m)	Comments
1170	0.50	504268	5317707	Low conductance target dipping to the northeast.
1180	0.64	504366	5317679	Low conductance target dipping to the northeast.
1190	1.69	504469	5317663	Low conductance target dipping to the northeast.
1200	1.29	504560	5317622	Low conductance target dipping to the northeast.
1210	1.29	504668	5317616	Low conductance target dipping to the northeast.
1220	0.27	504766	5317522	Low conductance target dipping to the northeast, very low amplitude.
1240	0.13	504966	5317462	Low conductance target dipping to the northeast, very low amplitude.
1250	0.18	505076	5317375	Low conductance target, thin and possibly sub-vertical, very low amplitude.
1260	0.09	505175	5317322	Low conductance target, thin and possibly sub-vertical or south dipping, very low amplitude.
1270	0.76	505266	5317232	Low conductance target, thin and possibly sub-vertical or south-dipping, very low amplitude.
1280	1.17	505370	5317131	Low conductance target dipping to the northeast, very low amplitude.
1290	3.00	505471	5317001	Moderate conductance target, dipping at a shallow angle to the northeast. Conductor pick represents upper edge.
1300	2.61	505566	5316947	Moderate conductance target, dipping at a shallow angle to the northeast. Conductor pick represents upper edge.

1310	2.93	505664	5316870	Moderate conductance target, dipping at a shallow angle to the northeast. Conductor pick represents upper edge.
1320	3.09	505768	5316873	Moderate conductance target, dipping at a shallow angle to the northeast. Conductor pick represents upper edge.

Table 6. J-Zone conductor picks.

K-Zone

The K-Zone is a trend of conductors with little or no magnetic association, oriented southeast and having low conductance. The conductor is dipping to the northeast, often at a shallow angle. Ground prospecting is suggested to explain this feature. It appears to be along strike of the J-Zone conductor.

Line	Conductance (S)	East (m)	North (m)	Comments
920	0.33	501765	5319449	North dipping conductor, thin, low conductance, with low amplitude magnetic field response.
930	1.65	501866	5319351	Conductor dipping at a shallow angle to the north, having low conductance and magnetic association (low amplitude). Pick represents upper edge of conductor.
940	2.14	501967	5319334	Conductor dipping at a shallow angle to the north, having low conductance and magnetic association (low amplitude). Pick represents upper edge of conductor.
950	1.37	502069	5319290	Conductor dipping at a shallow angle to the north, having low conductance and magnetic association (low amplitude). Pick represents upper edge of conductor. EM response has very low amplitude.
960	1.20	502168	5319251	Sub-vertical to north dipping, thin conductor with no magnetic response.
970	1.37	502263	5319221	Sub-vertical to north dipping, thin conductor with no magnetic response.
980	1.78	502369	5319120	Conductor dipping at a shallow angle to the north, having low conductance and magnetic association (low amplitude). Pick represents upper edge of conductor. EM response has very low amplitude.
990	1.09	502464	5319125	Weak amplitude target having low conductance and no magnetic association.
1000	1.26	502567	5319120	Weak amplitude target having low conductance and no magnetic association.

Table 7. K-Zone conductor picks.

L-Zone

The L-Zone is a shallow, moderate conductance target that dips to the northeast. The zone strikes to the southeast and is sub-parallel to the J- and K-zones. It is possible that the shallow dipping conductors, such as the L-Zone, represent sedimentary cover and are not bedrock conductors. This possibility should be reviewed because most of the shallow dipping conductors have the same strike direction, and could be formational.

Line	Conductance (S)	East (m)	North (m)	Comments
330	4.0	495865	5320375	Northeast dipping.
340	3.0	495970	5320297	Northeast dipping sheet.
350	2.1	496070	5320217	25 m estimated depth.
360	3.0	496175	5320099	Northeast dipping, no magnetic association.
370	1.7	496264	5320075	50 m estimated depth.
380	7.4	496374	5320020	50 m estimated depth.
390	6.7	496469	5319984	35 m estimated depth.
400	3.0	496573	5319936	75 m estimated depth.
410	2.2	496670	5319923	100 m estimated depth.

Table 8. L-Zone conductor picks.

M-Zone

The M-Zone is a high-amplitude, good conductance target that shows considerable thickness on some flight lines (e.g. 180). The strike direction is to the northeast on the western lines, and southeast on the eastern lines suggesting a possible fold nose. The northeast trending portion has an associated magnetic response while the southeast trending portion does not. The zone could represent two conductor trends, in which case the northeast trending section of the western most lines is of greater interest, owing to its apparent thickness, and magnetic association.

Line	Conductance (S)	East (m)	North (m)	Comments
210	12.5	494670	5321037	Shallow (~25 m) dipping to the north steeply.
200	14.2	494568	5321087	North dipping, magnetic association, two conductors present.
190	30.6	494472	5321061	50 m estimated depth.
190	57.6	494468	5321211	
180	45.4	494370	5320951	<25 m below surface.
180	18.0	494368	5321198	65 m estimated depth.
170	43.0	494270	5320877	<20 m below surface.
160	35.0	494165	5320802	<20 m below surface.
150	27.7	494073	5320847	60 m estimated depth, dipping north.

Table 9. M-Zone conductor picks.

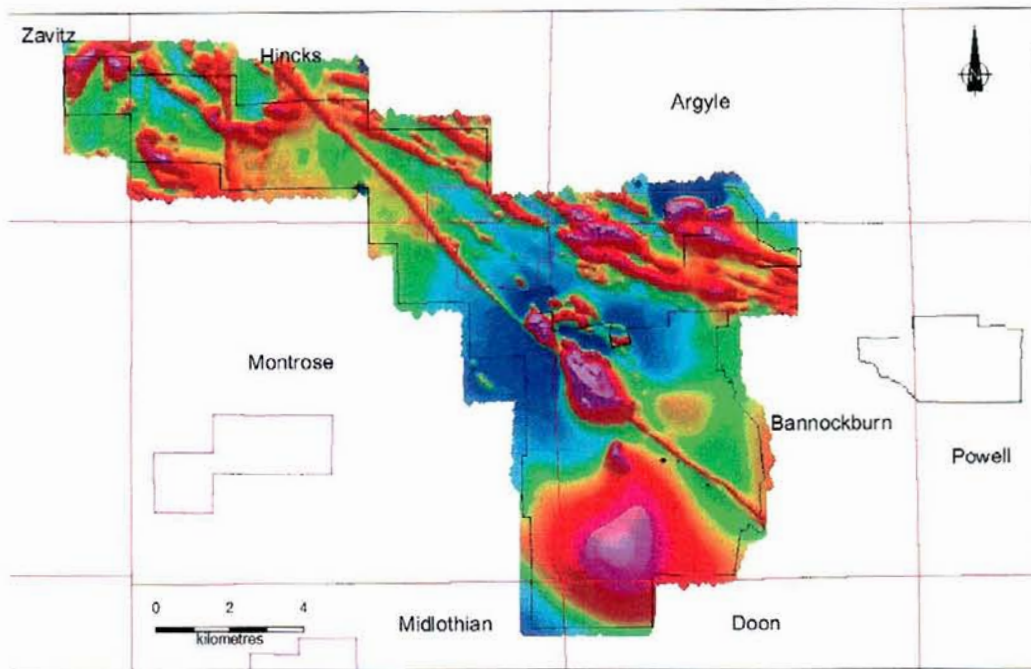


Figure 2 Bannockburn Property Map (NAD27, Z17)

Figure 1. Total magnetic field over the Bannockburn Property.

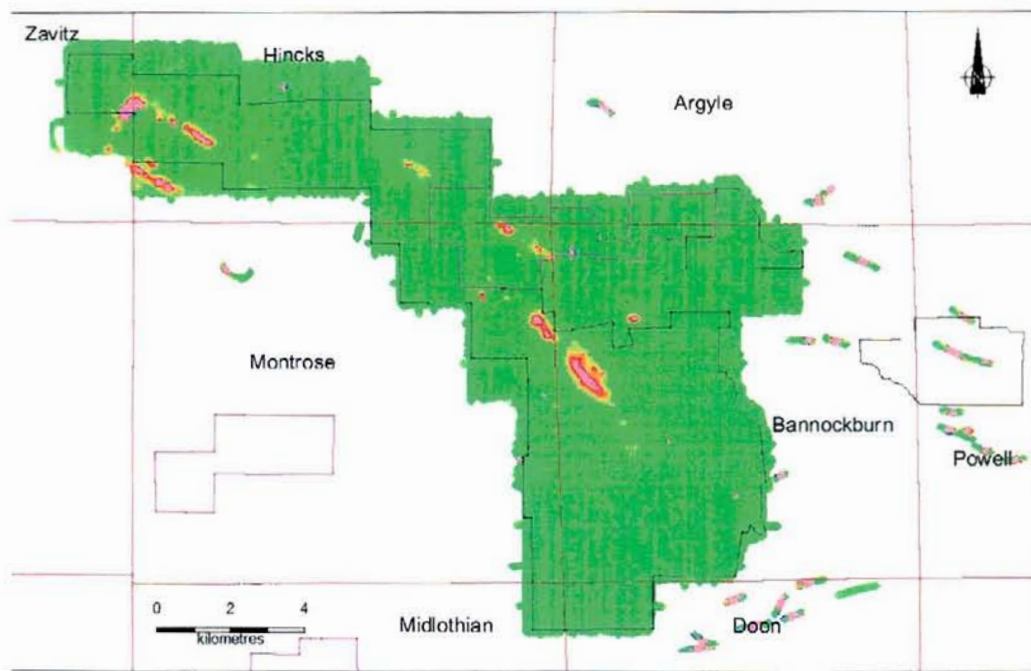


Figure 2 Bannockburn Property Map (NAD27, Z17)

Figure 2. Mid time-channel (channel 7) on-time EM response, Bannockburn Property.

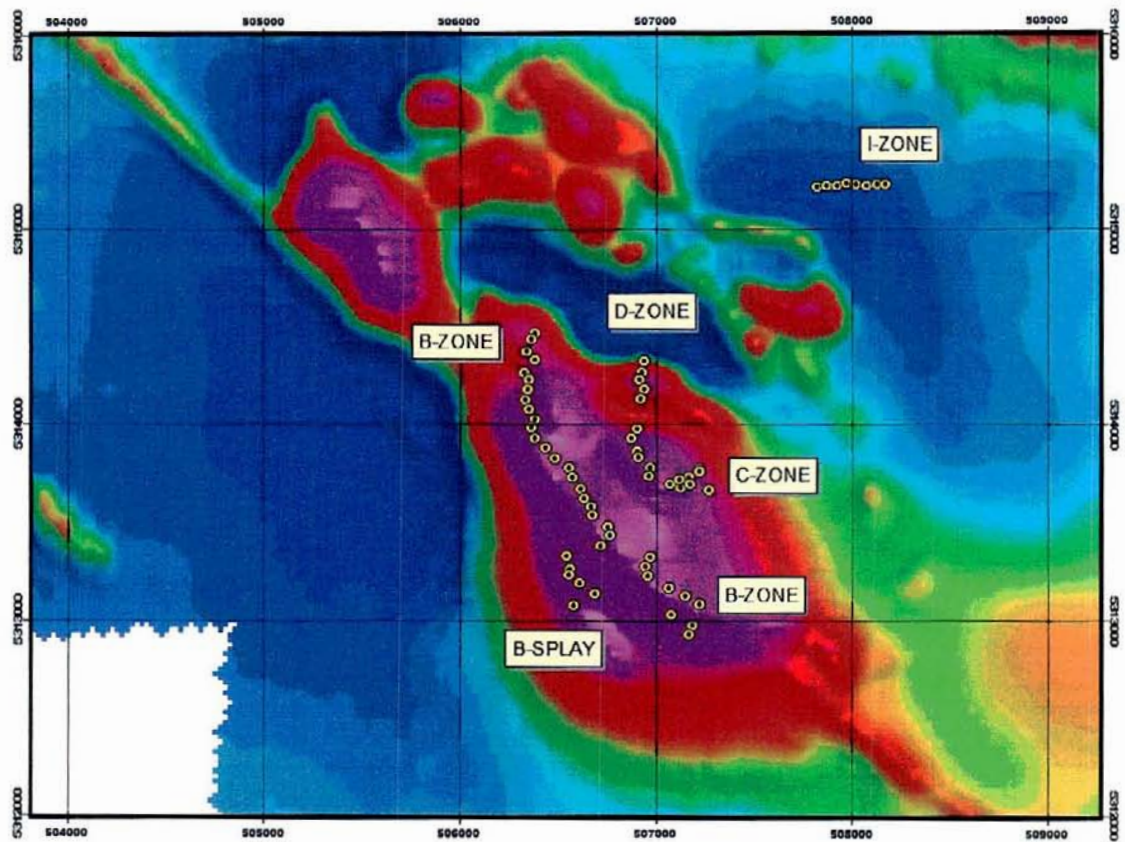


Figure 3. The B-Zone at Bannockburn is a conductive trend oriented along the central axis of a strongly magnetic ultramafic unit. To the northeast are the D- and C-Zones. To the southwest is the B-Zone splay.

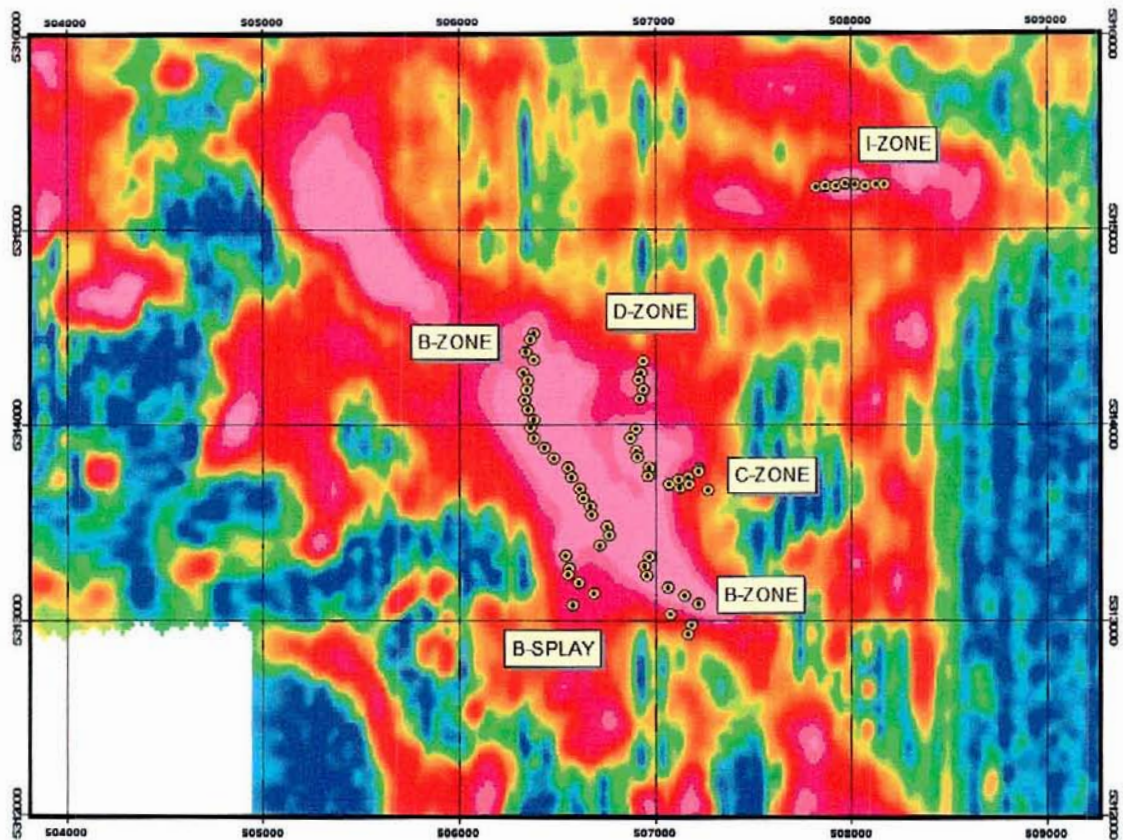


Figure 4. Early off-time EM response for the Bannockburn B-Zone, D-Zone, C-Zone, and B-Zone splay. The B-Zone is defined as a high amplitude, moderate conductance target with a substantial thickness but low conductivity. The thickness of the B-Zone may account for the high apparent conductance as noted in several borehole surveys where modeling is performed using thin plates.

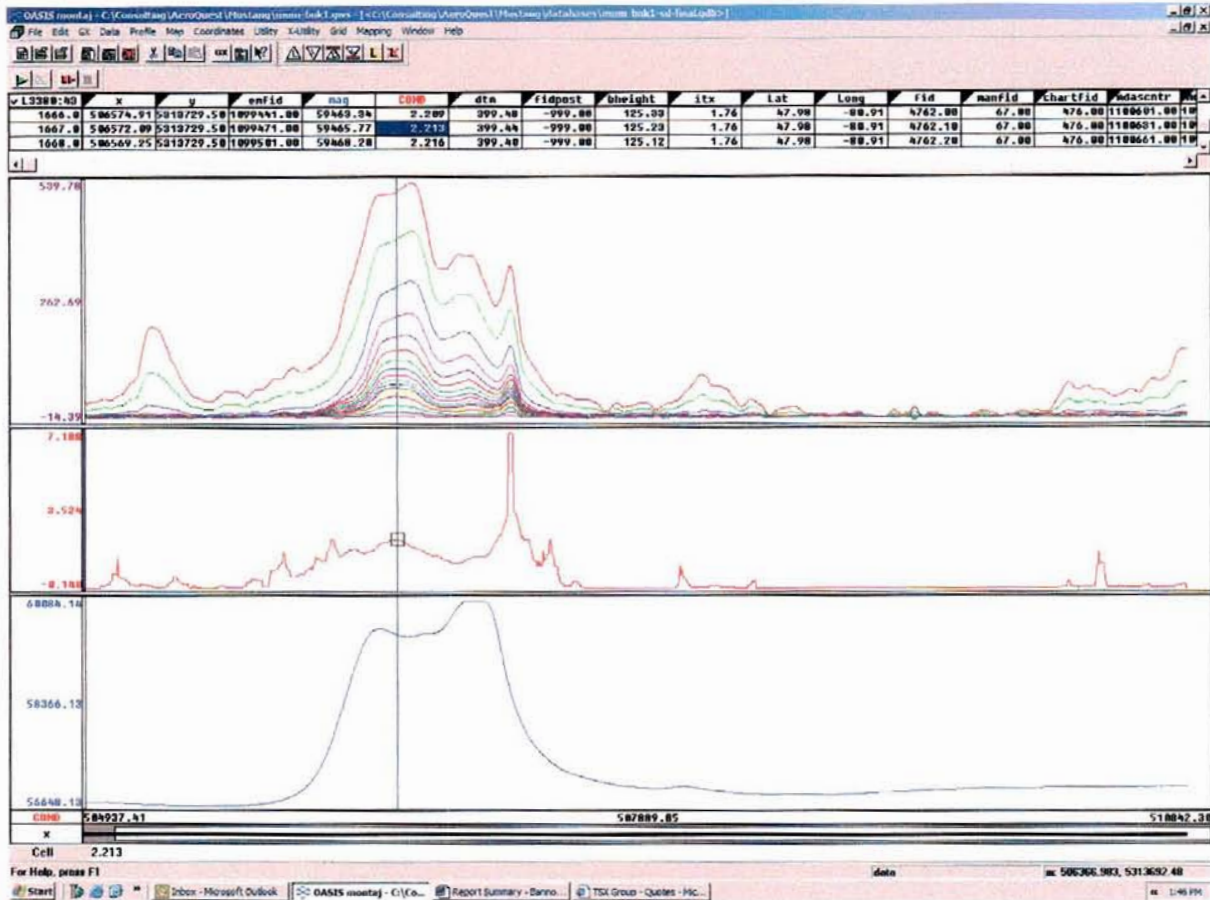


Figure 5. The above AeroTEM Z-axis off-time profiles are typical of the B-Zone. The conductance range is fairly constant from 1-2 S (conductivity range is 0.01-0.05 S/m). The conductor occurs within the ultramafic and there is a close association between higher amplitude magnetic field and conductive response. Note the C-Zone conductor to the east. This target has a higher conductance (7 S) and a much higher conductivity (1-5 S/m). There is no magnetic association with the C-Zone as it occurs outside of the ultramafic.

APPENDIX 2

Block corner co-ordinates (UTM Zone 17 - NAD27 Canada Mean)

Bannockburn Survey Block Outline (UTM E and N in metres)			
504979	5306826	504124	5318283
505036	5313239	507829	5318312
503554	5313210	507857	5318654
503554	5315747	510195	5318654
501644	5315747	510195	5318853
501616	5317286	510822	5318882
500903	5317286	511449	5317970
500875	5318853	511449	5317571
494405	5318853	512475	5317599
494405	5319993	512475	5315547
492638	5320022	510622	5315519
492666	5322559	510765	5313153
497312	5322530	511449	5312326
497312	5322017	511506	5309419
500818	5322017	510964	5309305
500818	5320450	510708	5308279
504095	5320478	508484	5308251
		508456	5306854

Claims Listing (The nearby Powell Property, consisting of 4 claims, is described in a separate report)

Mustang-Outokumpu Option				Mustang Claims 100%			
Claim	Units	Township	Due Date	Claim	Units	Township	Due Date
L1198911	8	BANNOCKBURN	April 11, 2008	P3009881	15	ZAVITZ	June 25, 2005
L1198912	4	BANNOCKBURN	April 7, 2008	L3009882	14	HINCKS	June 25, 2005
L1198913	1	BANNOCKBURN	April 7, 2008	L3016327	16	HINCKS	June 25, 2005
L1198916	4	BANNOCKBURN	April 11, 2008	L3016328	16	HINCKS	June 25, 2005
L1198917	1	BANNOCKBURN	April 11, 2008	L3016329	16	HINCKS	June 26, 2005
L1203764	1	BANNOCKBURN	April 11, 2008	L3016330	12	HINCKS	June 26, 2005
L1206090	1	BANNOCKBURN	April 7, 2008	L3016331	16	HINCKS	June 26, 2005
L1207453	1	BANNOCKBURN	May 1, 2008	L3016332	8	HINCKS	June 26, 2005
L1218700	2	BANNOCKBURN	May 15, 2008	L3016333	16	HINCKS	June 26, 2005
L1218720	1	BANNOCKBURN	March 24, 2008	L3016334	16	HINCKS	June 26, 2005
L1218721	11	BANNOCKBURN	March 24, 2007	L3016335	16	HINCKS	June 26, 2005
L1218722	6	BANNOCKBURN	March 24, 2007	L3012786	16	MONTROSE	June 26, 2005
L1218723	1	BANNOCKBURN	March 24, 2008	L3000658	1	MONTROSE	June 26, 2005
L1218724	1	BANNOCKBURN	March 24, 2008	L3012783	8	BANNOCKBURN	June 26, 2005
L1218725	7	BANNOCKBURN	March 24, 2008	L3012784	12	BANNOCKBURN	June 26, 2005
L1218727	7	BANNOCKBURN	March 24, 2008	L3012785	14	BANNOCKBURN	June 26, 2005
L1218728	1	BANNOCKBURN	March 24, 2008	L3005407	6	MONTROSE	June 26, 2005
L1218729	2	BANNOCKBURN	March 24, 2008	L3005408	2	MONTROSE	June 26, 2005
L1218730	1	BANNOCKBURN	March 24, 2008	L3012782	12	MONTROSE	June 26, 2005
L1218731	1	BANNOCKBURN	March 24, 2008	L3005402	12	BANNOCKBURN	June 26, 2005
L1218732	11	BANNOCKBURN	March 24, 2008	L3005598	12	BANNOCKBURN	June 26, 2005
L1218736	1	BANNOCKBURN	March 24, 2008	L3005399	8	ARGYLE	June 26, 2005
L1228144	8	BANNOCKBURN	October 15, 2007	L3005400	10	BANNOCKBURN	June 26, 2005
L1228145	16	BANNOCKBURN	October 15, 2007	L3005401	4	BANNOCKBURN	June 26, 2005
L1228146	16	BANNOCKBURN	October 15, 2007	L3011799	2	MONTROSE	Nov. 10, 2005
L1228147	8	BANNOCKBURN	October 15, 2007	L3011800	6	MONTROSE	Nov. 10, 2005
L1228148	6	BANNOCKBURN	October 15, 2007	L3011803	6	BANNOCKBURN	Nov. 10, 2005
L1228149	6	BANNOCKBURN	October 15, 2007	L3011773	1	BANNOCKBURN	Nov. 10, 2005
L1218726	1	MONTROSE	March 24, 2007	L3011840	12	BANNOCKBURN	Nov. 10, 2005
L1228150	8	MONTROSE	October 15, 2006	L3011861	4	BANNOCKBURN	Nov. 10, 2005
Total	143			L3011863	12	BANNOCKBURN	Nov. 10, 2005
				L1167018	5	BANNOCKBURN	Nov 10, 2005
				L1199159	12	BANNOCKBURN	Nov. 10, 2005
				L1199955	12	BANNOCKBURN	Nov. 10, 2005
				L3011885	6	BANNOCKBURN	Nov. 10, 2005
				Total	356		

Mustang-Phoenix Matachewan Mines Option

Claim	Township	Due Date
L1195039	Argyle	2004-Oct-31
L1239119	Argyle	2005-Apr-30
L1239120	Argyle	2005-Apr-30
L1199659	Bannockburn	2005-May-31
L1222268	Bannockburn	2005-Apr-30
L3002220	Hincks	2006-May-17
L3009235	Hincks	2005-Jun-25
L3009236	Hincks	2005-Jun-25
L1242852	Montrose	2004-Oct-31
L3002221	Montrose	2006-May-17

Patented Claims

Claim Number	Township
MR17999	Montrose
MR18000	Montrose
MR18001	Montrose
L373374	Montrose
L374737	Montrose
L374738	Montrose
L374739	Montrose
L374741	Montrose
L374742	Montrose
L374743	Montrose
L374744	Montrose
L374745	Montrose

APPENDIX 3

Description of Database Fields (Geosoft GDB database)

Column	Description
x	Zone 17 UTM Easting in metres (NAD27-Canada Mean)
y	Zone 17 UTM Northing in metres (NAD27-Canada Mean)
x83	Zone 17 UTM Easting in metres (NAD83)
y83	Zone 17 UTM Northing in metres (NAD83)
lat	Latitude in decimal degrees (NAD27-Canada Mean)
long	Longitude in decimal degrees (NAD27-Canada Mean)
lat83	Latitude in decimal degrees (NAD83)
long83	Longitude in decimal degrees (NAD83)
fiducial	Time reference fiducial in seconds
manfid	Manual Fiducial
chartfid	Chart Recorder Fiducial
emfid	Fiducial counter for streaming data synchronisation
utctime	UTC Time in seconds of the day
rtctime	Local (System) time in HH:MM:SS
fltno	Flight number
date	Date in YY/MM/DD format
galtf	GPS Altitude in metres
ralt	Radar Altimeter in metres
bheight	Terrain clearance of EM bird in feet
dtm	Raw Digital Terrain Model in metres
basemag	Base Station magnetic field in nT
rawmag	Raw total magnetic intensity in nT
mag	Diurnally corrected Total Magnetic Intensity in nT
magtie	Final levelled Total Magnetic Intensity in nT
x1	Raw RMS Off-Time EM-X component of channel 1 in ppb
z1raw-z6raw	Raw RMS Off-Time EM-Z component of channels 1 to 6 in ppb
x1f	Smoothed RMS Off-Time EM-X component of channel 1 in ppb
z1f-z6f	Smoothed RMS Off-Time EM-Z component of channels 1 to 6 in ppb
ZOn1-ZOn16	Processed Streaming On-Time Z component Channels 1-16 in nT/sec
ZOff0-ZOff16	Processed Streaming Off-Time Z component Channels 0-16 in nT/sec
XOn1-XOn16	Processed Streaming On-Time X component Channels 1-16 in nT/sec
XOff0-XOff16	Processed Streaming Off-Time X component Channels 0-16 in nT/sec
Z1Obr-ZObr16	Overburden stripped Z component response Channels 1-16 in nT/sec
X1Obr-XObr16	Overburden stripped X component response Channels 1-16 in nT/sec
ZOff17-ZOff22	Special weighted combination channels in nT/sec (see note below)

anum	Index number of conductor pick
anomlabel	Letter label of conductor pick
nchan	No of off-time (or on-time) channels with response over 2.5nT/sec
on_con	On-time conductance in siemens
off_con	Off-time conductance in siemens
Aclass	Classification from 1-7 based on conductance of pick
cond	Interpreted conductance in siemens

Weighted channels:

ZOff17: $0.25*ch44 + 0.50*ch45 + 0.25*ch46$

ZOff18 : $(ch46+ch47)/2$

ZOff19 : $(ch48+ch49+ch50+ch51)/4$

ZOff20 : $(ch52..ch59)/8$

ZOff21 : $(ch60..ch75)/16$

ZOff22 : $(ch76..ch107)/32$

In the databases the Survey lines, Tie Lines, and High Altitude/Internal Q coil lines are prefixed with an "L" or "Line", "T" or "Tie", and "S" or "Test", respectively.

APPENDIX 4 Technical Paper

Mineral Exploration with the AeroTEM System

S.J. Balch, W.P. Boyko, G. Black, and R.N. Pedersen, AeroQuest Limited, Presented at the SEG Int'l Exposition and 72nd Annual Meeting, Salt Lake City, Utah, October 6-11, 2002

Mineral Exploration with the AeroTEM System

S.J. Balch, W.P. Boyko, G. Black, and R.N. Pedersen, AeroQuest Limited.

Summary

AeroTEM is a concentric-loop time-domain EM system designed for mineral exploration and geologic mapping. The high dipole moment of the transmitter in combination with the unique *superimposed dipole* coil geometry allows the system to achieve a depth of exploration similar to fixed-wing systems, but with the resolution and target response symmetry that is typical of conventional helicopter-towed EM systems. AeroTEM has flown over 20,000 line-km since its introduction in 1999. Ground follow-up geophysical surveys and drilling programs have confirmed the depth of exploration to be in excess of 200 m with high spatial resolution of target conductors confirmed. The compact, rigid system geometry should provide for a true on-time measurement of secondary fields from highly conductive sources often associated with Ni-Cu-PGE mineralization, thereby gaining a considerable advantage over all towed-receiver fixed-wing airborne EM systems, which are known to be blind to such targets (Hanneson, 1998).

Introduction

Airborne EM systems, as they have evolved since the 1940s generally fall into one of two categories, namely, (1) the loosely coupled towed-bird systems on fixed-wing aircraft, and (2) the rigid transmitter-receiver configuration towed by helicopters (e.g., Fountain, 1998). The fixed-wing systems operate in the time domain and are characterized by a wideband high-moment transmitter to maximize depth penetration, especially in a resistive environment. The rigid helicopter systems operate in the frequency domain and are characterized by multiple narrow-band low-moment transmitters and closely spaced receivers to maximize spatial resolution and provide moderate depth penetration. Thus one system seeks to maximize signal while the other strives to minimize noise, both attempting to increase the signal-to-noise-ratio...this being the *only* determining factor of an EM system's level of performance.

The AeroTEM system is a wide-band time-domain EM design that draws on the rigid design of the frequency-domain systems and the high-moment transmitter design of the fixed-wing platforms. The system attempts to both maximize signal and minimize noise by incorporating the two major advantages of airborne EM systems: transmitter power and rigid coil geometry. As Duckworth (1993) so succinctly states, the optimum coupling to a target by a transmitter-receiver coil pair is achieved by only two possible coil configurations. The first optimum coupling is



Figure 1. The AeroTEM airborne electromagnetic system.

achieved when the coil separation is 0.6 times the distance to the target the second optimum coupling is achieved when the coils are coincident. Because target depth cannot be known a priori, the coincident coil geometry is obviously preferred.

Method

The system (Figure 1) consists of a 3-axis receiver coil mounted centrally within a large 5-m diameter transmitter loop. The transmitter waveform is a triangular current pulse of 1.15 ms duration at a base frequency of 150 Hz with a peak current of 260 A for a total transmitter moment of 40,000 Am². The mutually orthogonal receiver coils are mounted with the X-axis along the flight line, transverse, and Z vertical. System waveforms and typical conductor responses are shown in Figure 2.

The system is towed 40 m below the helicopter at a nominal terrain clearance of 30 m. The present transmitter produces a peak primary field of 300 nT vertically below the transmitter at ground level. Because *both* the transmitter and receiver are located close to the ground, AeroTEM produces a stronger target response in the upper 50 m of the earth compared to a fixed-wing aircraft with a peak dipole moment of 500,000 Am² and a peak primary field of 55 nT at ground surface.

The strength of the primary field from an EM transmitter decreases rapidly with distance from the transmitter location. High moment transmitters on fixed-wing aircraft, such as GEOTEM, tend to have better depth penetration because the strength of the primary field even at 300 m

The AeroTEM System

is sufficiently high to energize a conductor and produce a measurable secondary field. Large loop ground EM systems have even greater depth penetration, owing to the lower rate at which the primary field falls off with distance from the transmitter for distances on the order of the loop dimensions. The strength of the primary field from the AeroTEM transmitter is compared with that of some common systems in Figure 3.

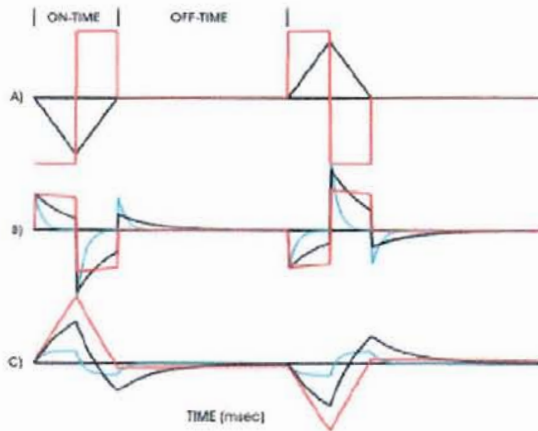


Figure 2. The AeroTEM system is characterized by a) a triangular current pulse at the transmitter and a step response at the receiver. The dB/dt response in b) and the B-field in c) are shown for conductor time constants of 0.1 ms (blue), 0.5 ms (black) and 5 ms (red).

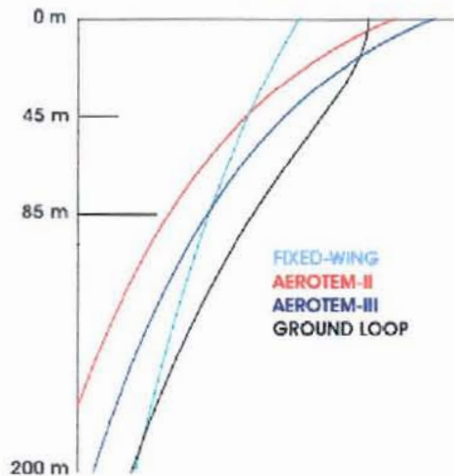


Figure 3: Primary field strength versus depth is compared for fixed wing ($500,000\text{Am}^2$), AeroTEM-II ($40,000\text{Am}^2$), AeroTEM-III ($80,000\text{Am}^2$) and ground moving-loop (diameter 100 m, 15 A current, single turn) surface to 200 m.

Although the fixed-wing and ground EM systems gain an advantage in primary field at depth, this energy is diffused over a larger volume, thus reducing their effectiveness in energizing smaller conductors. For large loop ground EM systems, this is especially a problem where large regional conductors can mask the more subtle responses of smaller isolated targets.

Example One: Spatial Resolution

The vertical (Z-axis) component produces responses that are independent of the flight line direction. The close proximity of the transmitter and receiver coils produces very sharp anomaly edges. These two factors combine to produce images of the Z component channels that have high spatial resolution.

In the following example, the amplitude of the earliest off-time channel for the Z component receiver coil is shown in Figure 4. The survey was conducted for Nuinsco Resources in the Lac Rocher area of Quebec during an exploration program for Ni-Cu-PGE deposits.

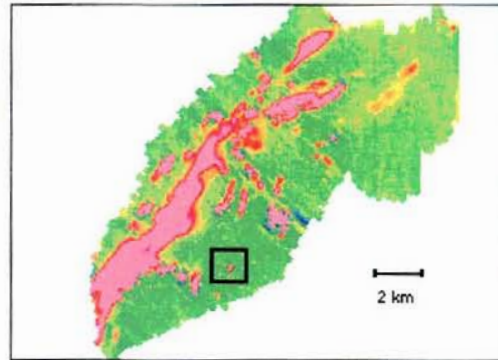


Figure 4. Color image of the earliest time channel, AeroTEM Z component. The black outline represents a conductor response from a near-surface target of limited strike extent.

One discrete anomaly detected from the Lac Rocher survey, and represented by the black outline in Figure 4, is shown in profile format in Figure 5. The approximate lateral extent of the conductor response is 50 m on the earliest time channel (width at half-maximum). The narrow response of this isolated conductor compares favorably with the spatial resolution achieved with conventional HEM systems.

The AeroTEM System

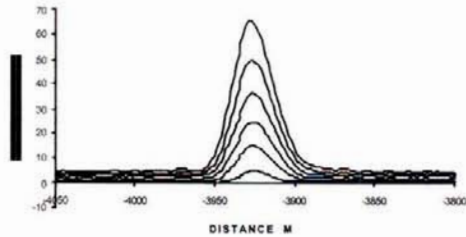


Figure 5: The high spatial resolution of AeroTEM is demonstrated by the EM response of an isolated conductor. The width of the response is less than 50 m on the earliest time channel (peak amplitude at half-maximum).

Example Two: Air borne - Ground Comparison

Aurogin Resources, in joint venture with Heron Mines, flew an 800 line-km AeroTEM survey over the Belledune Property in New Brunswick in the search for Cu-Zn-Pb deposits. Several AeroTEM airborne EM conductors were identified from that survey over two separate areas.

A ground follow-up program of Crone Pulse EM was conducted over one selected target in Area Two. The AeroTEM early-time Z component response is shown in Figure 6. The anomaly subjected to the ground follow-up program is outlined in black (Figure 6).

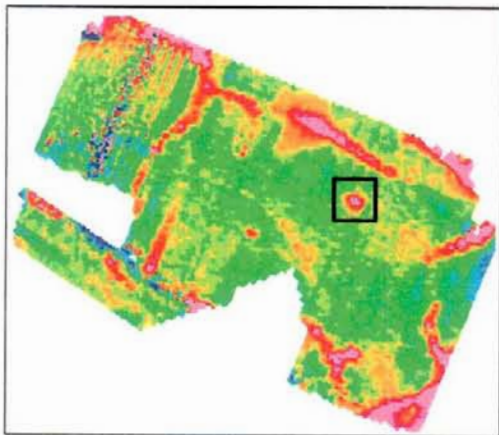


Figure 6: Early-time Z component AeroTEM response over the Belledune Survey Area Two. A detailed ground follow-up survey was centered over the response outlined in black.

An expanded view of the airborne response is shown in Figure 7. The Crone early-time response is shown in Figure 8. The conductor was located within an area of favorable geology. Modeling of the Crone response suggested a sub-horizontal conductor dipping at 25° below the horizontal and located approximately 100 m below surface. The AeroTEM response also suggested a flat-lying conductor because of the symmetric Z component response.

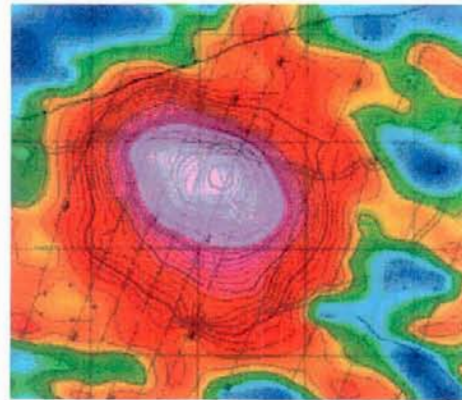


Figure 7: AeroTEM earliest time-channel Z component response, Belledune Property, New Brunswick. The survey was flown with a line spacing of 100 m.

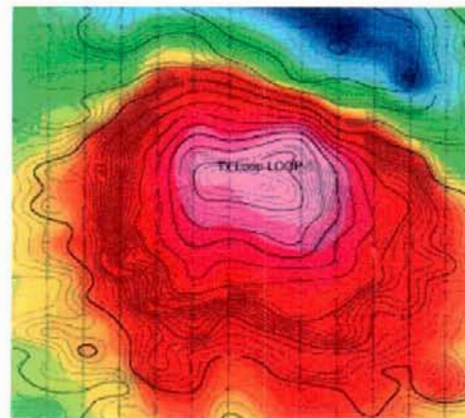


Figure 8: Crone Pulse EM vertical component, amplitude of time channel 10, from the Belledune Property, New Brunswick. The survey was performed in-loop with a 100 m line spacing.

The AeroTEM System

Two boreholes were drilled to then evaluate the EM responses and both intersected up to 15 sulphide containing significant Au-Ag-Cu within a volcanic rhyolite. Downhole Pulse EM surveys confirmed the intersection of a conductor approximately 170 m downhole, coincident with the intersected mineralization, and corresponding to a vertical depth of 145 m. The peak response in the earliest AeroTEM time channel was 90 ppb, or roughly 200 times above the system noise level. The peak response in the Crone survey was 110 nT/s, about 200 times above the system noise level. This is an example of a drilling program that could have proceeded directly from the airborne survey without the added expense of ground geophysics.

Example Three: Air borne Air borne Comparison

Nuinsco Resources conducted GEOTEM and AeroTEM surveys over the Lac Rocher property covering both the known mineralized area and a larger area of unexplored claims. In one area of the survey both GEOTEM (Figure 9) and AeroTEM (Figure 10) recorded responses that were coincident with a large magnetic anomaly.

Both systems clearly show a distinct, multi-channel anomaly. Nuinsco drilled the conductor in 1999 and intersected 2.2 m of massive sulphide at a depth of 200 m below surface. The AeroTEM peak response was 3 ppb or 10 times the system noise level, while the GEOTEM peak response was 400 ppm or 40 times system noise level. While noise levels are dependent upon the level of filtering, the higher apparent signal-to-noise-ratio of the GEOTEM response can be attributed to its higher moment transmitter and the depth of the conductor.

Conclusions

AeroTEM shows a high spatial resolution, due to its unique coil configuration. The system produces responses that compare well with existing ground and airborne systems. The present depth of exploration is estimated to be up to 250 m with a typical noise level of +/-0.5 ppb.

Improvements to the system will come in the form of larger transmitter moments, decreased noise levels and the development of true on-time measurements through full waveform recording. There are numerous advantages of using helicopter-towed time-domain systems with a depth penetration approaching that of the fixed-wing platforms. The success of these systems will no doubt be dictated by the perceived needs of the mineral exploration industry for such techniques.

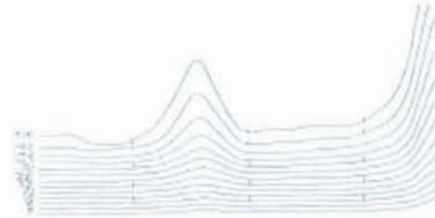


Figure 9: GEOTEM Z component response over a deep conductor at Lac Rocher.

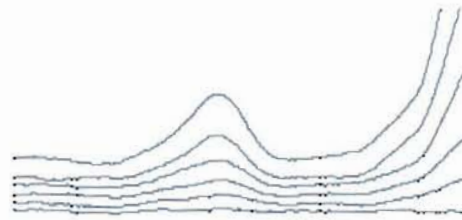


Figure 10: AeroTEM Z component response over a deep conductor at Lac Rocher.

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Acknowledgments

AeroQuest wishes to thank Nuinsco Resources and Aurogin Resources for permission to publish the survey data from their respective properties.

APPENDIX 5 Instrumentation Specification Sheets



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AEROTEM Helicopter Electromagnetic System

System Characteristics

Transmitter: Triangular Pulse Shape Base Frequency 30 or 150 Hz.
Tx On Time - 5,750 (30Hz) or 1,150 (150Hz) microsec.
Tx Off Time - 10,915 (30Hz) or 2,183 (150Hz) microsec.
Loop Diameter - 5 m.
Peak Current - 250 A.
Peak Moment - 38,800 NIA.
Typical Z Axis Noise at Survey Speed = 8 ppb peak.
Sling Weight: 270 Kg.
Length of Tow Cable: 40 m.
Bird Survey Height: 30 m or less nominal.

Receiver

Three Axis Receiver Coils (x, y, z) positioned at centre of transmitter loop.
Selectable Time Delay to start of first channel 21.3, 42.7, or 64.0 msec.

Analogue Display & Acquisition

Six Channels per Axis.
Analogue (RMS) Channel Widths: 52.9, 132.3, 158.7, 158.7, 317.5, 634.9 microsec.
Recording & Display Rate = 10 readings per second.
MDAS Digital recording at 126 sample per decay curve at a maximum of 300 curves per second (26.455 microsec channel width).

System Considerations

Comparing a fixed wing time domain transmitter with a typical moment of 500,000 NIA flying at an altitude of 120 m with a Helicopter TDEM at 30 m, notwithstanding, the substantial moment loss in the airframe of the fixed wing, the same penetration by the lower flying helicopter system would only require a sixty-fourth of the moment. Clearly the AeroTEM system with nearly 40,000 NIA has more than sufficient moment.

The airframe of the fixed wing presents a response to the towed bird, which must be compensated for dynamically. This problem is non-existent for AeroTEM since transmitter and receiver positions are fixed. The AeroTEM system is completely portable, and can be assembled at the survey site within half a day.

NEIL Fiset

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Author's Statement of Qualifications

I, Neil Fiset, of 15 Valley Ridge St., Nepean, Ont., do hereby certify that :

1. I hold a Bachelor of Science degree in Geology(1976) from the University of New Brunswick, Fredericton, New Brunswick.
2. I am a member of the Canadian Exploration Geophysicists Society.
3. Since 1976 I have been an employee of Scintrex Limited, Noranda Exploration Co. Ltd., JvX Ltd. and the United Nations.
5. I have been a self-employed consultant since 1996.
4. I am presently a consulting Geophysicist, practising in Canada and overseas.
5. Permission is granted to Mustang Minerals Corp. to use this report in a prospectus or other financial offering.
6. I have not received, directly or indirectly, nor do I expect to receive any interest, direct or indirect, in the properties of Mustang Minerals Corp. or any affiliate thereof, nor do I beneficially own, directly or indirectly, any securities in Mustang Minerals Corp. or any affiliate thereof

Signed on this 18th day of August, 2004 at Nepean, Ont.



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