# REPORT ON A HELICOPTER-BORNE
# VERSATILE TIME DOMAIN ELECTROMAGNETIC (VTEM)
# GEOPHYSICAL SURVEY

## SERPENTINE NICKEL BLOCK

**Ontario, Canada**

2 · 37101

for

**Sedex Mining Corp.**

By

**Geotech Ltd.**

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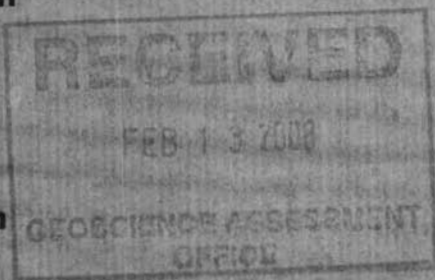Survey flown in September, 2007

Project 7085

October, 2007

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# REPORT ON A HELICOPTER-BORNE
# VERSATILE TIME DOMAIN ELECTROMAGNETIC SURVEY

Serpentine Nickel block, Ontario, Canada

## Executive Summary

During the period of September 3rd to 11th, 2007, Geotech Ltd. carried out a helicopter-borne geophysical survey for Sedex Mining Corp. over one block located south of Timmins, Ontario, Canada.

Principal geophysical sensors included a versatile time domain electromagnetic (VTEM) system and a caesium magnetometer. Ancillary equipment included a GPS navigation system and a radar altimeter. A total of 933 line-km were flown.

In-field data processing involved quality control and compilation of data collected during the acquisition stage, using the in-field processing centre established at Howard Johnson Hotel Timmins, in Ontario. Preliminary and final data processing, including generation of final digital data products were done at the office of Geotech Ltd. in Aurora, Ontario.

The processed survey results are presented as electromagnetic stacked profiles and the following grids,

- B-field time channel 3.286 ms
- total magnetic intensity
- second vertical magnetic derivative
- digital elevation model.

Digital data includes all electromagnetic and magnetic products plus positional, altitude and raw data.

# 1. INTRODUCTION

## 1.1 General Considerations

These services are the result of the Agreement made between Geotech Ltd. and Sedex Mining Corp. to perform a helicopter-borne geophysical survey over the Serpentine Nickel block in Ontario, Canada.

933 line-km of geophysical data were acquired during the survey.

John Keating acted on behalf of Sedex Mining Corp. during data acquisition and data processing phases of this project.

The survey block is as shown in Appendix A.

The crew was based in Timmins, Ontario for the acquisition phase of the survey, as shown in Section 2 of this report.

Survey flying was completed on September 11th, 2007. Preliminary data processing was carried out daily during the acquisition phase of the project. Final data presentation and data archiving was completed in the Aurora office of Geotech Ltd. by October, 2007.

## 1.2. Survey and System Specifications

The survey block was flown at nominal traverse line spacing of 75 metres, in north- south direction. Tie lines were flown perpendicular to traverse lines.

Where possible, the helicopter maintained a mean terrain clearance of 75 metres, which translated into an average height of 35 meters above ground for the bird-mounted VTEM system and 60 meters for the magnetic sensor.

The survey was flown using an Astar B2 helicopter, registration C-FXFU. The helicopter was operated by Gateway Helicopters Ltd. Details of the survey specifications may be found in Section 2 of this report.

### 1.3. Data Processing and Final Products

Data compilation and processing were carried out by the application of Geosoft OASIS Montaj and programs proprietary to Geotech Ltd.

Databases, grids and maps of final products are presented to Sedex Mining Corp.

The survey report describes the procedures for data acquisition, processing, final image presentation and the specifications for the digital data set.

### 1.4. Topographic Relief and Cultural Features

Serpentine Nickel block is located approximately 55 kilometres south of Timmins, Ontario. The block is inside the following Townships: Nursey, Semple, Sothman, Hutt and Halliday.

Topographically, the survey area exhibits a moderate relief, with elevation ranging from 350 metres to 410 metres above sea level. The block is included in NTS-041P14 of the National Topographic System of Canada.

Swamp areas, lakes and rivers are observed in the survey area.

Power line activity is detected by the 60 Hz power line monitor. Hence, special care is recommended in identifying cultural features that might be recorded in the data.

## 2. DATA ACQUISITION

### 2.1. Survey Area

The survey block (see location map, Appendix A) and general flight specifications are as follows:

| Survey block | Line spacing (m) | Area (Km²) | Line-km | Flight direction | Line number |
|---|---|---|---|---|---|
| Serpentine Nickel | 75 | 68.9 | 903.5 | N0°E | L24020 - 25630 |
| | 750 | | 106.0 | N90°E | T24640 - 24790 |

Table 1 - Survey block

Survey block boundaries co-ordinates are provided in Appendix B.

### 2.2. Survey Operations

Survey operations were based in Timmins, Ontario for the acquisition phase of the survey. The block was flown between September 3rd to 11th, 2007 performing eleven flights as shown in Table 2.

The crew was housed at Howard Johnson Hotel in Timmins.

Serpentine Nickel block was flown as part of a larger survey on behalf of Sedex Mining Corp.

| Date | Crew Location | Flight # | Block | Km flown | Comments |
|---|---|---|---|---|---|
| 02-Sep-07 | Timmins | | | | No production due to weather |
| 03-Sep-07 | Timmins | 82, 83 | Serpentine Nickel | 151 | Production |
| 04-Sep-07 | Timmins | 84,85,86 | Serpentine Nickel | 229 | Production |
| 05-Sep-07 | Timmins | 87,88,89,90 | Serpentine Nickel | 340 | Production |
| 06-Sep-07 | Timmins | | | | No production due to weather |
| 07-Sep-07 | Timmins | | | | No production due to weather |
| 08-Sep-07 | Timmins | | | | No production due to weather |
| 09-Sep-07 | Timmins | | | | No production due to weather |
| 10-Sep-07 | Timmins | | | | No production due to weather |
| 11-Sep-07 | Timmins | 91,92 | Serpentine Nickel | 216 | Serpentine Nickel completed |
| 12-Sep-07 | Timmins | 94 | Nickel South | 108 | Production |
| 13-Sep-07 | Timmins | 95 | Nickel South | 11 | Limited production due to weather |
| 14-Sep-07 | Timmins | 96, 97 | Nickel South | 236 | Production |

| 15-Sep-07 | Timmins | 98, 99 | Nickel South | 216 | Production |
|---|---|---|---|---|---|
| 16-Sep-07 | Timmins | 100 - 102 | Nickel South | 390 | Production |
| 17-Sep-07 | Timmins | 105, 106 | Nickel South & North | 131 | Nickel South completed |
| 18-Sep-07 | Timmins | 107 | Nickel North | 113 | Production |
| 19-Sep-07 | Timmins | 108, 109 | Nickel North | 236 | Production |
| 20-Sep-07 | Timmins | 110, 111 | Nickel North | 284 | Production |
| 21-Sep-07 | Timmins | 112 - 116 | Nickel North | 475 | Production |
| 22-Sep-07 | Timmins | | | | No production due to weather. |
| 23-Sep-07 | Timmins | 117 - 120 | Nickel North | 516 | Production |
| 24-Sep-07 | Timmins | 121 - 123 | Nickel North | 380 | Production |
| 25-Sep-07 | Timmins | 124 - 126 | Nickel North | 377 | Production |
| 26-Sep-07 | Timmins | 127 - 128 | Nickel North | 279 | Production |
| 27-Sep-07 | Timmins | 129, 130 | Nickel North | 177 | Nickel North completed |

Table 2 – Survey summary.

## 2.3. Flight Specifications

The nominal EM sensor terrain clearance was 35 m (EM bird height above ground, i.e. helicopter is maintained 75 m above ground). Nominal survey speed was 75 km/hour. The data recording rates of the data acquisition was 0.1 second for electromagnetic and magnetometer, 0.2 second for altimeter and GPS data. This translates to a geophysical reading about every 2 metres along flight track. Navigation was assisted by a GPS receiver and data acquisition system, which reports GPS co-ordinates as latitude/longitude and directs the pilot over a pre-programmed survey grid.

The operator was responsible for monitoring of the system integrity. He also maintained a detailed flight log during the survey, tracking the times of the flight as well as any unusual geophysical or topographic feature.

On return of the aircrew to the base camp the survey data was transferred from a compact flash card (PCMCIA) to the data processing computer.

## 2.4. Aircraft and Equipment

### 2.4.1. Survey Aircraft

An Astar B2 helicopter, registration C-FXFU, owned and operated by Gateway Helicopters Ltd., was used for the survey. Installation of the geophysical and ancillary equipment was carried out by Geotech Ltd.

### 2.4.2. Electromagnetic System

The electromagnetic system was a Geotech Time Domain EM (VTEM) system. The configuration is as indicated in Figure 1 below.
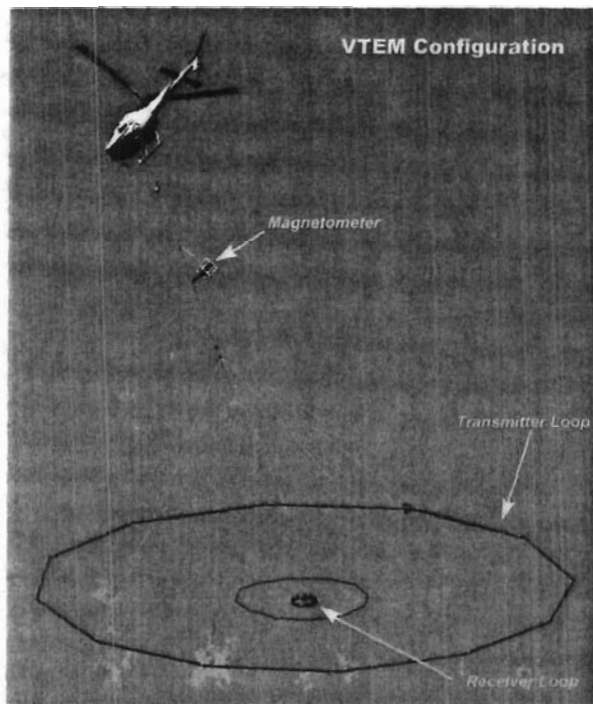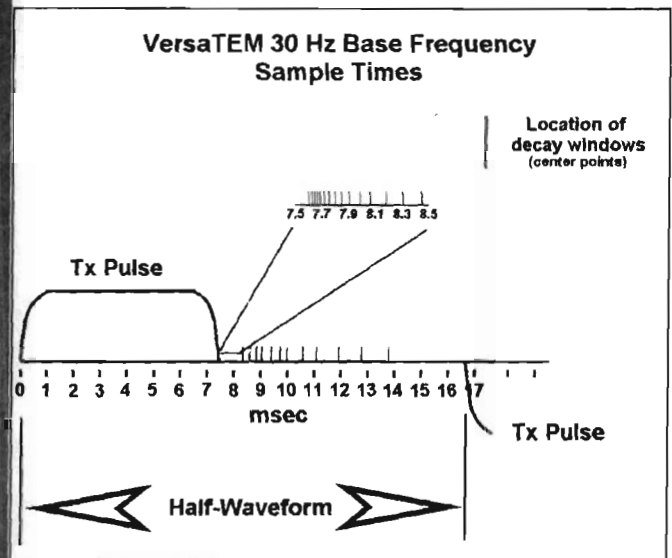


Figure 1 – VTEM configuration



Figure 2 – Sample times

Receiver and transmitter coils are concentric and Z-direction oriented.
The receiver decay recording scheme is shown in Figure 2.

Twenty-four measurement gates were used in the range from 120 μs to 6578 μs, as shown in Table 3.

| Array Index | VTEM Decay Sampling scheme | | | |
|---|---|---|---|---|
| | ( Microseconds ) | | | |
| | Time Gate | Start | End | Width |
| 10 | 120 | 110 | 131 | 21 |
| 11 | 141 | 131 | 154 | 24 |
| 12 | 167 | 154 | 183 | 29 |
| 13 | 198 | 183 | 216 | 34 |
| 14 | 234 | 216 | 258 | 42 |
| 15 | 281 | 258 | 310 | 53 |
| 16 | 339 | 310 | 373 | 63 |
| 17 | 406 | 373 | 445 | 73 |
| 18 | 484 | 445 | 529 | 84 |
| 19 | 573 | 529 | 628 | 99 |
| 20 | 682 | 628 | 750 | 123 |
| 21 | 818 | 750 | 896 | 146 |
| 22 | 974 | 896 | 1063 | 167 |
| 23 | 1151 | 1063 | 1261 | 198 |
| 24 | 1370 | 1261 | 1506 | 245 |
| 25 | 1641 | 1506 | 1797 | 292 |
| 26 | 1953 | 1797 | 2130 | 333 |
| 27 | 2307 | 2130 | 2526 | 396 |
| 28 | 2745 | 2526 | 3016 | 490 |
| 29 | 3286 | 3016 | 3599 | 583 |
| 30 | 3911 | 3599 | 4266 | 667 |
| 31 | 4620 | 4266 | 5058 | 792 |
| 32 | 5495 | 5058 | 6037 | 979 |
| 33 | 6578 | 6037 | 7203 | 1167 |

Table 3 - VTEM decay sampling scheme

Transmitter specifications:

- Loop diameter: 26 m
- Number of turns: 4
- Loop axis orientation: Z axis
- Pulse frequency: 30 Hz
- Pulse width (on time): 7.2 ms

- Peak current: 208 Amp
- Duty cycle: 44%.
- Dipole moment: 441,700 NIA.

Receiver specifications:

- Loop diameter: 1.2 m
- Number of turns: 100
- Receiver effective area: 113 m$^2$
- loop axis orientation: Z axis
- Wave form: trapezoid.

Recording sampling rate was 10 samples per second.
A 60 Hz power line monitor data is also recorded.
EM measurements are recorded approximately 35 to 38 m bellow helicopter, according to flying conditions (cable length is 42 m).


### 2.4.3. Airborne magnetometer

The magnetic sensor utilized for the survey was a Geometrics optically pumped caesium vapour magnetic field sensor, mounted in a separated bird, towed 15 metres below the helicopter, as shown on figure 1. The sensitivity of the magnetic sensor is 0.02 nanoTesla (nT) at a sampling interval of 0.1 seconds. The magnetometer sends the measured magnetic field strength as nanoTeslas to the data acquisition system via the RS-232 port.


### 2.4.4. Ancillary Systems


#### 2.4.4.1. Radar Altimeter

A Terra TRA 3000/TRI 40 radar altimeter was used to record terrain clearance. The antenna was mounted beneath the bubble of the helicopter cockpit.


#### 2.4.4.2. GPS Navigation System

The navigation system used was a Geotech PC based navigation system utilizing a NovAtel's WAAS enable OEM4-G2-3151W GPS receiver, Geotech navigate software, a full screen display with controls in front of the pilot to direct the flight and an NovAtel GPS antenna mounted on the helicopter tail.

The co-ordinates of the block were set-up prior to the survey and the information was fed into the airborne navigation system.

### 2.4.4.3.    Digital Acquisition System

A Geotech data acquisition system recorded the digital survey data on an internal compact flash card.  Data is displayed on an LCD screen as traces to allow the operator to monitor the integrity of the system.  The data type and sampling interval as provided in table 4.

| DATA TYPE | SAMPLING |
|---|---|
| TDEM | 0.1 sec |
| Magnetometer | 0.1 sec |
| GPS Position | 0.2 sec |
| RadarAltimeter | 0.2 sec |

Table 4 - Sampling Rates

## 2.4.5. Base Station

A combined magnetometer/GPS base station was utilized on this project. A Geometrics Caesium vapour magnetometer was used as a magnetic sensor with a sensitivity of 0.001 nT. The base station was recording the magnetic field together with the GPS time at 1 Hz on a base station computer.

The base station magnetometer sensor was installed where the crew was housed, 150 metres north of the Howard Johnson Hotel, away from electric transmission lines and moving ferrous objects such as motor vehicles.

The magnetometer base station's data was backed-up to the data processing computer at the end of each survey day.

## 3. PERSONNEL

The following Geotech Ltd. personnel were involved in the project.

Field

| | |
|---|---|
| Field Operation manager: | Shawn Grant |
| Crew chief: | Kyle Corriveau |
| Operators: | Tom Lilley |
| System Engineers: | Oleg Babishin |

The survey pilot and the mechanic engineer were employed directly by the helicopter operator – Gateway Helicopters Ltd.

| | |
|---|---|
| Pilots: | Joselyn V. |
| Engineer: | Andrew Mcgregor |

Office

| | |
|---|---|
| Project Manager/QC Geophysicist: | Harish Kumar |
| Data Processing / Reporting: | Marta Orta |

Data acquisition and processing phases were carried out under the supervision of Andrei Bagrianski, Surveys Manager. Overall management of the project was undertaken by Edward Morrison, President, Geotech Ltd.

# 4. DATA PROCESSING AND PRESENTATION

## 4.1. Flight Path

The flight path, recorded by the acquisition program as WGS 84 latitude/longitude, was converted into the UTM coordinate system in Oasis Montaj.

The flight path was drawn using linear interpolation between x,y positions from the navigation system. Positions are updated every second and expressed as UTM eastings (x) and UTM northings (y).

## 4.2. Electromagnetic Data

A three stage digital filtering process was used to reject major sferic events and to reduce system noise. Local sferic activity can produce sharp, large amplitude events that cannot be removed by conventional filtering procedures. Smoothing or stacking will reduce their amplitude but leave a broader residual response that can be confused with geological phenomena. To avoid this possibility, a computer algorithm searches out and rejects the major sferic events. The filter used was a 16 point non-linear filter.

The signal to noise ratio was further improved by the application of a low pass linear digital filter. This filter has zero phase shift which prevents any lag or peak displacement from occurring, and it suppresses only variations with a wavelength less than about 1 second or 20 metres. This filter is a symmetrical 1 sec linear filter.

The results are presented as stacked profiles of EM voltages for the time gates, in linear - logarithmic scale for both B-field and dB/dt response. Late time channels recorded 3.286 milliseconds after the termination of the impulse is also presented as contour colour image for B-field response.

Generalized modeling results of VTEM data, written by Geophysicist Roger Barlow, are shown in Appendix C.

Graphical representation of the VTEM output voltage of the receiver coil and the transmitter current is shown in Appendix D.

### 4.3. Magnetic Data

The processing of the magnetic data involved the correction for diurnal variations by using the digitally recorded ground base station magnetic values. The base station magnetometer data was edited and merged into the Geosoft GDB database on a daily basis. The aeromagnetic data was corrected for diurnal variations by subtracting the observed magnetic base station deviations.

Tie line levelling was carried out by adjusting intersection points along traverse lines. A micro-levelling procedure was applied to remove persistent low-amplitude components of flight-line noise remaining in the data.

The corrected magnetic data was interpolated between survey lines using a random point gridding method to yield x-y grid values for a standard grid cell size of approximately 0.2 cm at the mapping scale. The Minimum Curvature algorithm was used to interpolate values onto a rectangular regular spaced grid.

# 5. DELIVERABLES

## 5.1. Survey Report

The survey report describes the data acquisition, processing, and final presentation of the survey results.

The survey report is provided in five paper copies and digitally in PDF format.

## 5.2. Maps

Final maps were produced at a scale of 1:20,000. The coordinate/projection system used was NAD83, UTM zone 17 north. All maps show the flight path trace and topographic data. Latitude and longitude are also noted on maps.

The following maps are presented on paper,

- dB/dt profiles, Time Gates 0.234 – 6.578 ms in linear - logarithmic scale
- B-field profiles, Time Gates 0.234 – 6.578 ms in linear - logarithmic scale
- Total Magnetic intensity contours and colour image
- B-field time channel 3.286 ms contours and color image

## 5.3. Digital Data

Five copies of CD-ROMs were prepared.
There are two (2) main directories,

**Data**      contains databases, grids and maps, as described below.
**Report**      contains a copy of the report and appendices in PDF format.

- Databases in Geosoft GDB format, containing the following channels:

X:      X positional data (meters – NAD83, utm zone 17 north)
Y:      Y positional data (meters – NAD83, utm zone 17 north)
Lon:      Longitude data (degree – WGS84)
Lat:      Latitude data (degree – WGS84)

| | |
|---|---|
| Z: | GPS antenna elevation (meters - ASL) |
| Radar: | Helicopter terrain clearance from radar altimeter (meters - AGL) |
| DEM: | Digital elevation model (meters) |
| Gtime1: | GPS time (seconds of the day) |
| Mag1: | Raw Total Magnetic field data (nT) |
| Basemag: | Magnetic diurnal variation data (nT) |
| Mag2: | Total Magnetic field diurnal variation corrected data (nT) |
| Mag3: | Levelled Total Magnetic field data (nT) |
| SF[10]: | dB/dt 120 microsecond time channel ($pV/A/m^4$) |
| SF[11]: | dB/dt 141 microsecond time channel ($pV/A/m^4$) |
| SF[12]: | dB/dt 167 microsecond time channel ($pV/A/m^4$) |
| SF[13]: | dB/dt 198 microsecond time channel ($pV/A/m^4$) |
| SF[14]: | dB/dt 234 microsecond time channel ($pV/A/m^4$) |
| SF[15]: | dB/dt 281 microsecond time channel ($pV/A/m^4$) |
| SF[16]: | dB/dt 339 microsecond time channel ($pV/A/m^4$) |
| SF[17]: | dB/dt 406 microsecond time channel ($pV/A/m^4$) |
| SF[18]: | dB/dt 484 microsecond time channel ($pV/A/m^4$) |
| SF[19]: | dB/dt 573 microsecond time channel ($pV/A/m^4$) |
| SF[20]: | dB/dt 682 microsecond time channel ($pV/A/m^4$) |
| SF[21]: | dB/dt 818 microsecond time channel ($pV/A/m^4$) |
| SF[22]: | dB/dt 974 microsecond time channel ($pV/A/m^4$) |
| SF[23]: | dB/dt 1151 microsecond time channel ($pV/A/m^4$) |
| SF[24]: | dB/dt 1370 microsecond time channel ($pV/A/m^4$) |
| SF[25]: | dB/dt 1641 microsecond time channel ($pV/A/m^4$) |
| SF[26]: | dB/dt 1953 microsecond time channel ($pV/A/m^4$) |
| SF[27]: | dB/dt 2307 microsecond time channel ($pV/A/m^4$) |
| SF[28]: | dB/dt 2745 microsecond time channel ($pV/A/m^4$) |
| SF[29]: | dB/dt 3286 microsecond time channel ($pV/A/m^4$) |
| SF[30]: | dB/dt 3911 microsecond time channel ($pV/A/m^4$) |
| SF[31]: | dB/dt 4620 microsecond time channel ($pV/A/m^4$) |
| SF[32]: | dB/dt 5495 microsecond time channel ($pV/A/m^4$) |
| SF[33]: | dB/dt 6578 microsecond time channel ($pV/A/m^4$) |
| BF[10]: | B-field 120 microsecond time channel $(pV*ms)/(A* m^4)$ |
| BF[11]: | B-field 141 microsecond time channel $(pV*ms)/(A* m^4)$ |
| BF[12]: | B-field 167 microsecond time channel $(pV*ms)/(A* m^4)$ |
| BF[13]: | B-field 198 microsecond time channel$(pV*ms)/(A* m^4)$ |
| BF[14]: | B-field 234 microsecond time channel $(pV*ms)/(A* m^4)$ |
| BF[15]: | B-field 281 microsecond time channel $(pV*ms)/(A* m^4)$ |
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| BF[18]: | B-field 484 microsecond time channel $(pV*ms)/(A* m^4)$ |
| BF[19]: | B-field 573 microsecond time channel $(pV*ms)/(A* m^4)$ |

| | |
|---|---|
| BF[20]: | B-field 682 microsecond time channel $(pV*ms)/(A*m^4)$ |
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| BF[31]: | B-field 4620 microsecond time channel $(pV*ms)/(A*m^4)$ |
| BF[32]: | B-field 5495 microsecond time channel $(pV*ms)/(A*m^4)$ |
| BF[33]: | B-field 6578 microsecond time channel $(pV*ms)/(A*m^4)$ |
| PLM: | Power line monitor |

Electromagnetic B-field and dB/dt data is found in array channel format between indexes 10 – 33, as described above.

- Database VTEM_waveform.gdb in Geosoft GDB format, containing the following channels:

| | |
|---|---|
| Time: | Sampling rate interval, 10.416 microseconds |
| Volt: | output voltage of the receiver coil (volt) |

- Grids in Geosoft GRD format, as follow,

| | |
|---|---|
| BF3286_bb: | B-field channel 3.286 ms $(pV*ms)/(A*m4)$ |
| Mag_bb: | Total magnetic intensity (nT) |
| MagVD2_bb: | Second vertical magnetic derivative $(nT/m^2)$ |
| DEM_bb: | Digital elevation model (m) |
| | Where, |
| | bb represents the block name (Ex: Serpentine Nickel) |

A Geosoft .GRD file has a .GI metadata file associated with it, containing grid projection information.
Grid cell size of 15 meters was used.

- Maps at 1:20,000 scale in Geosoft MAP format, as follow,

  | | |
  |---|---|
  | BfieldProf_*bb*: | B-field profiles, time channels 0.234 – 6.578 ms |
  | dBdtProf_*bb*: | dB/dt profiles, time channels 0.234 – 6.578 ms |
  | BF3286_*bb*: | B-field time channel 3.286 ms contours and color image |
  | MAG_*bb*: | Total Magnetic intensity contours and colour image |
  | | Where, |
  | | *bb* represents the block name (Ex: Serpentine Nickel) |

- Google Earth file *FP_SerpentineNickel.kml* showing the flight path of the block.

  Free version of Google Earth software can be downloaded from,
  http://earth.google.com/download-earth.html

- A *readme.txt* file describing the content of digital data, as described above.

# 6.    CONCLUSIONS

A helicopter-borne versatile time domain electromagnetic (VTEM) geophysical survey has been completed over the Serpentine Nickel block, located south of Timmins, Ontario, Canada.

The total area coverage is 68.9 km$^2$. Total survey line coverage is 933 line kilometres. Principal sensors included a Time Domain EM system and a magnetometer. Results have been presented as stacked profiles and contour colour images at a scale of 1:20,000.

Final data processing at the office of Geotech Ltd. in Aurora, Ontario was carried out under the supervision of Andrei Bagrianski, Surveys Manager.

Several EM anomalies were identified. Further investigation is recommended in describing each group of anomalies using modeling techniques and ground verification.
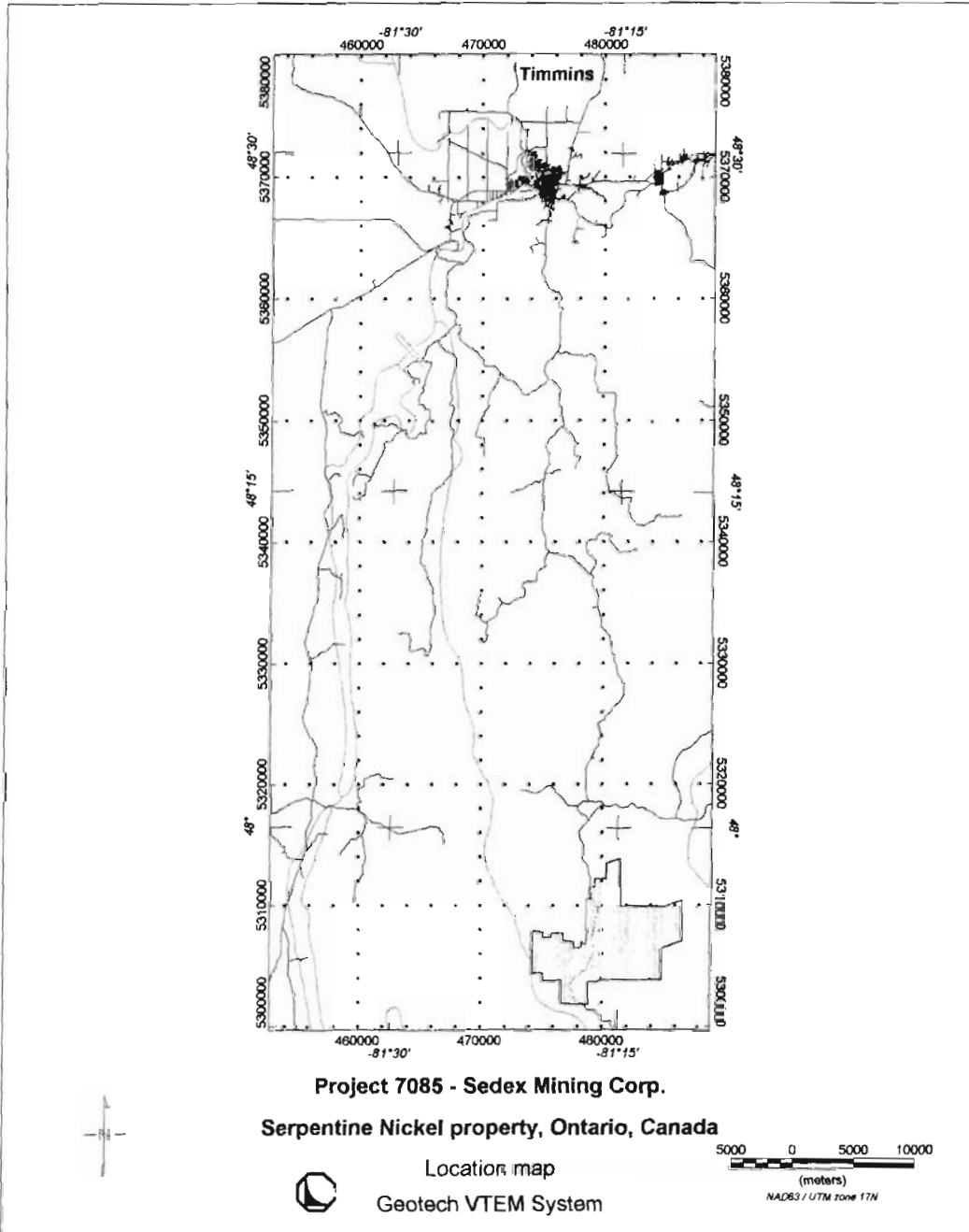
Respectfully submitted,

Marta Orta,
**Geotech Ltd.**
October 2007

# APPENDIX A

## SURVEY BLOCK LOCATION MAP



**Project 7085 - Sedex Mining Corp.**

**Serpentine Nickel property, Ontario, Canada**

Location map

Geotech VTEM System

# APPENDIX B

## SURVEY BLOCK COORDINATES
(NAD83, UTM zone 17 north)

### Serpentine Nickel Block

| X | Y |
|---|---|
| 480348 | 5313431 |
| 481534 | 5313832 |
| 481551 | 5309924 |
| 485125 | 5309891 |
| 486577 | 5310358 |
| 486594 | 5307052 |
| 484924 | 5306451 |
| 484924 | 5303845 |
| 479898 | 5303845 |
| 479530 | 5303662 |
| 478862 | 5303678 |
| 478862 | 5301808 |
| 476741 | 5301875 |
| 476741 | 5303795 |
| 475155 | 5303745 |
| 475172 | 5304413 |
| 474320 | 5304413 |
| 474337 | 5307853 |
| 475205 | 5307720 |
| 475202 | 5307325 |
| 475850 | 5307293 |
| 475840 | 5307673 |
| 476794 | 5307646 |
| 476805 | 5307035 |
| 477685 | 5306971 |
| 477695 | 5306515 |
| 478333 | 5306515 |
| 478333 | 5306922 |
| 478870 | 5306831 |
| 478864 | 5310542 |
| 479095 | 5310467 |
| 479084 | 5311524 |
| 479470 | 5311508 |
| 479460 | 5312189 |
| 480361 | 5312184 |

# APPENDIX C

# MODELING VTEM DATA

# MODELING VTEM DATA

## Introduction

The VTEM system is based on a concentric or central loop design, whereby, the receiver is positioned at the centre of a 26.1 meters diameter transmitter loop that produces a dipole moment up to 625,000 NIA at peak current. The wave form is a bi-polar, modified square wave with a turn-on and turn-off at each end. With a base frequency of 30 Hz, the duration of each pulse is approximately 7.3 milliseconds followed by an off time where no primary field is present.

During turn-on and turn-off, a time varying field is produced (dB/dt) and an electro-motive force (emf) is created as a finite impulse response. A current ring around the transmitter loop moves outward and downward as time progresses. When conductive rocks and mineralization are encountered, a secondary field is created by mutual induction and measured by the receiver at the centre of the transmitter loop.

Measurements are made during the off-time, when only the secondary field (representing the conductive targets encountered in the ground) is present.

Late in 2006, Geotech Ltd. incorporated a B-Field measurement in the VTEM system. The B-Field measurements have the advantage of containing more spectral energy at low spectral frequencies than the dB/dt measurements, hence, greater amplitudes and accuracies when encountering targets with higher conductances (> 500 Siemens). The converse is true at higher spectral frequencies where dB/dt measurements are best applied. The B-field is most widely used in nickel exploration where a small percentage of targets are extremely conductive (> 2500 Siemens) and less resolvable or invisible (below the noise threshold) using dB/dt measurements.

Efficient modeling of the results can be carried out on regularly shaped geometries, thus yielding close approximations to the parameters of the measured targets. The following is a description of a series of common models made for the purpose of promoting a general understanding of the measured results.

## Variation of Plate Depth

Geometries represented by plates of different strike length, depth extent, dip, plunge and depth below surface can be varied with characteristic parameters like conductance of the target, conductance of the host and conductivity/thickness and thickness of the overburden layer.

Diagrammatic models for a vertical plate are shown in figures A and G at two different depths, all other parameters remaining constant. With this transmitter-receiver geometry, the classic **M** shaped response is generated. Figure A shows a plate where the top is near surface. Here, amplitudes of the duel peaks are higher and symmetrical with the zero centre positioned directly above the plate. Most important is the separation distance of the peaks. This distance is small when the plate is near surface and widens with a linear relationship as the plate (depth to top) increases. Figure G shows a much deeper plate where the separation distance of the peaks is much wider and the amplitudes of the channels have decreased.

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## Variation of Plate Dip

As the plate dips and departs from the vertical position, the peaks become asymmetrical. Figure B shows a near surface plate dipping 80°. Note that the direction of dip is toward the high shoulder of the response and the top of the plate remains under the centre minimum.

As the dip increases, the aspect ratio (Min/Max) decreases and this aspect ratio can be used as an empirical guide to dip angles from near 90° to about 30°. The method is not sensitive enough where dips are less than about 30°. Figure E shows a plate dipping 45° and, at this angle, the minimum shoulder starts to vanish. In Figure D, a flat lying plate is shown, relatively near surface. Note that the twin peak anomaly has been replaced by a symmetrical shape with large, bell shaped, channel amplitudes which decay relative to the conductance of the plate.

Figure H shows a special case where two plates are positioned to represent a synclinal structure. Note that the main characteristic to remember is the centre amplitudes are higher (approximately double) compared to the high shoulder of a single plate. This model is very representative of tightly folded formations where the conductors where once flat lying.

## Variation of Prism Depth

Finally, with prism models, another algorithm is required to represent current on the plate. A plate model is considered to be infinitely thin with respect to thickness and incapable of representing the current in the thickness dimension. A prism model is constructed to deal with this problem, thereby, representing the thickness of the body more accurately.

Figures C, F and I show the same prism at increasing depths. Aside from an expected decrease in amplitude, the side lobes of the anomaly show a widening with deeper prism depths of the bell shaped early time channels.
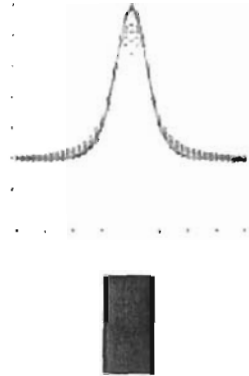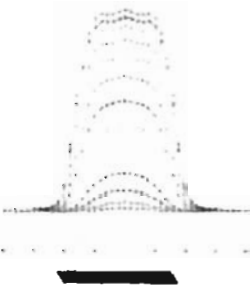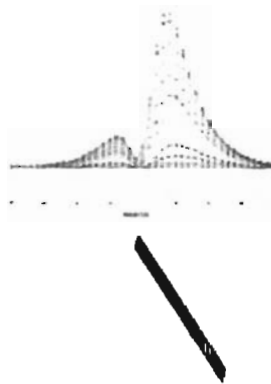
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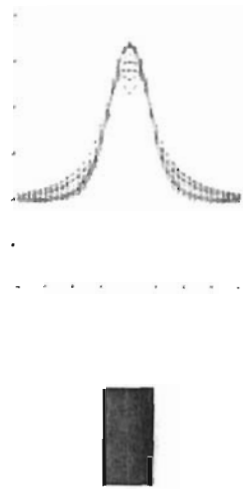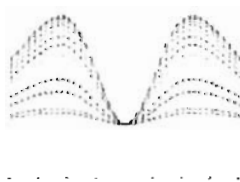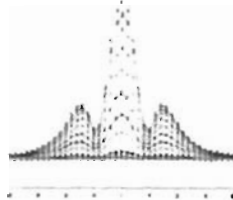
# A

# B

# C

# D

# E

# F

# G

# H

# I

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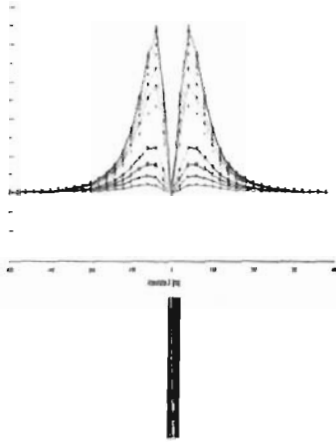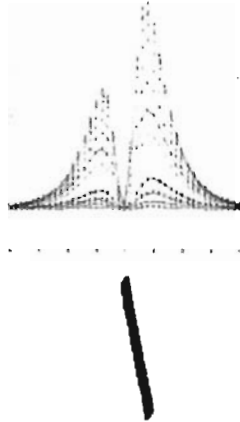
## General Modeling Concepts

A set of models has been produced for the Geotech VTEM® system with explanation notes (see models A to I above). The reader is encouraged to review these models, so as to get a general understanding of the responses as they apply to survey results. While these models do not begin to cover all possibilities, they give a general perspective on the simple and most commonly encountered anomalies.

When producing these models, a few key points were observed and are worth noting as follows:

- For near vertical and vertical plate models, the top of the conductor is always located directly under the centre low point between the two shoulders in the classic **M** shaped response.

- As the plate is positioned at an increasing depth to the top, the shoulders of the **M** shaped response, have a greater separation distance.

- When faced with choosing between a flat lying plate and a prism model to represent the target (broad response) some ambiguity is present and caution should be exercised.

- With the concentric loop system and Z-component receiver coil, virtually all types of conductors and most geometries are most always well coupled and a response is generated (see model H). Only concentric loop systems can map this type of target.

The modelling program used to generate the responses was prepared by EMIGMA from PetRos Eikon Inc. and is one of a very few that can model a wide range of targets in a conductive half space.

Geotech currently employs a variety of software to model VTEM data. A first approach is being implemented by Geotech proprietary algorithms to identify and characterize the targets. Detailed interpretation follows by the utilization of Maxwell from EMIT as well as EM-Flow from Encom accordingly.

## General Interpretation Principals

Magnetics

The total magnetic intensity responses reflect major changes in the magnetite and/or other magnetic minerals content in the underlying rocks and unconsolidated overburden. Precambrian rocks have often been subjected to intense heat and pressure during structural and metamorphic events in their history. Original signatures imprinted on these rocks at the time of formation have, it most cases, been modified, resulting in low magnetic susceptibility values.

The amplitude of magnetic anomalies, relative to the regional background, helps to assist in identifying specific magnetic and non-magnetic rock units (and conductors) related to, for example, mafic flows, mafic to ultramafic intrusives, felsic intrusives, felsic volcanics and/or sediments etc. Obviously, several geological sources can produce the same magnetic response. These ambiguities can be reduced considerably if basic geological information on the area is available to the geophysical interpreter.

In addition to simple amplitude variations, the shape of the response expressed in the wave length and the symmetry or asymmetry, is used to estimate the depth, geometric parameters and magnetization of the anomaly. For example, long narrow magnetic linears usually reflect mafic flows or intrusive dyke features. Large areas with complex magnetic patterns may be produced by intrusive bodies with significant magnetization, flat lying magnetic sills or sedimentary iron formation. Local isolated circular magnetic patterns often represent plug-like igneous intrusives such as kimberlites, pegmatites or volcanic vent areas.

Because the total magnetic intensity (TMI) responses may represent two or more closely spaced bodies within a response, the second derivative of the TMI response may be helpful for distinguishing these complexities. The second derivative is most useful in mapping near surface linears and other subtle magnetic structures that are partially masked by nearby higher amplitude magnetic features. The broad zones of higher magnetic amplitude, however, are severely attenuated in the vertical derivative results. These higher amplitude zones reflect rock units having strong magnetic susceptibility signatures. For this reason, both the TMI and the second derivative maps should be evaluated together.

Theoretically, the second derivative, zero contour or colour delineates the contacts or limits of large sources with near vertical dip and shallow depth to the top. The vertical gradient map also aids in determining contact zones between rocks with a susceptibility contrast, however, different, more complicated rules of thumb apply.

**Concentric Loop EM Systems**

Concentric systems with horizontal transmitter and receiver antennae produce much larger responses for flat lying conductors as contrasted with vertical plate-like conductors. The amount of current developing on the flat upper surface of targets having a substantial area in this dimension, are the direct result of the effective coupling angle, between the primary magnetic field and the flat surface area. One therefore, must not compare the amplitude/conductance of responses generated from flat lying bodies with those derived from near vertical plates; their ratios will be quite different for similar conductances.

Determining dip angle is very accurate for plates with dip angles greater than 30°. For angles less than 30° to 0°, the sensitivity is low and dips can not be distinguished accurately in the presence of normal survey noise levels.

A plate like body that has near vertical position will display a two shoulder, classic **M** shaped response with a distinctive separation distance between peaks for a given depth to top.

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It is sometimes difficult to distinguish between responses associated with the edge effects of flat lying conductors and poorly conductive bedrock conductors. Poorly conductive bedrock conductors having low dip angles will also exhibit responses that may be interpreted as surfacial overburden conductors. In some situations, the conductive response has line to line continuity and some magnetic correlation providing possible evidence that the response is related to an actual bedrock source.

The EM interpretation process used, places considerable emphasis on determining an understanding of the general conductive patterns in the area of interest. Each area has different characteristics and these can effectively guide the detailed process used.
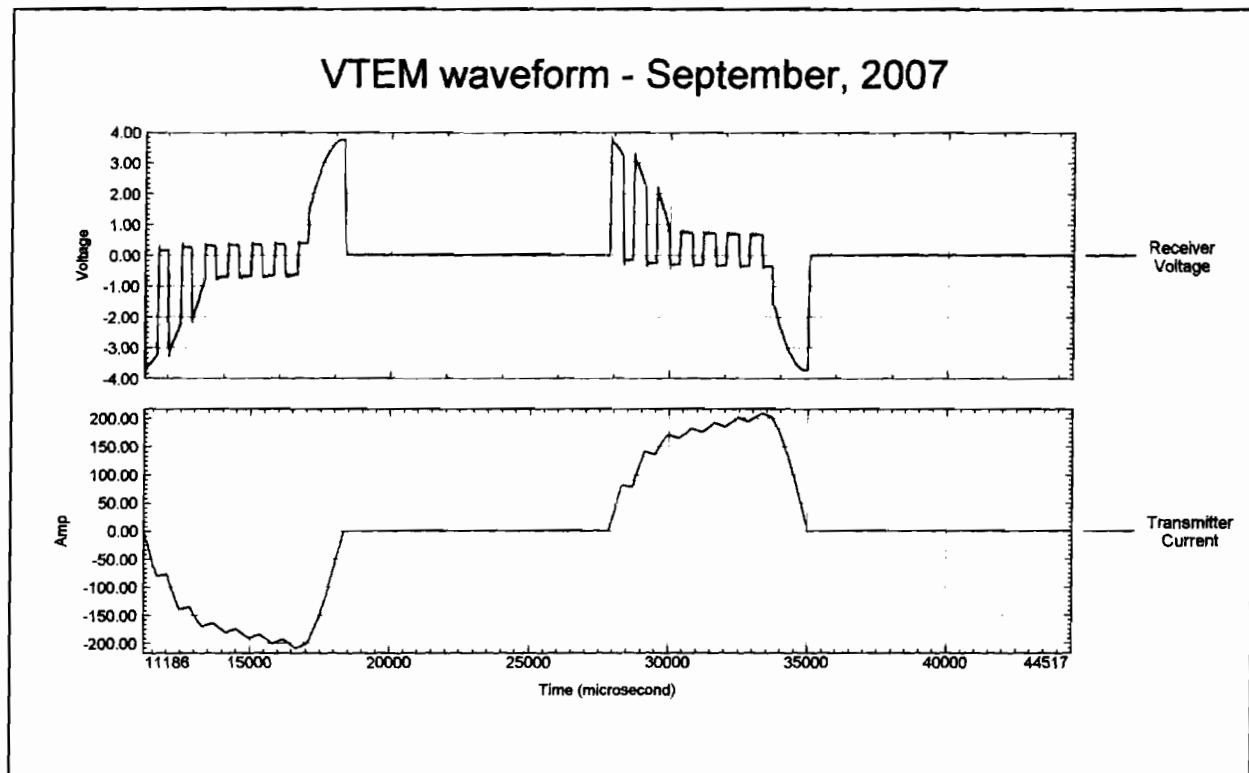
The first stage is to determine which time gates are most descriptive of the overall conductance patterns. Maps of the time gates that represent the range of responses can be very informative.

Next, stacking the relevant channels as profiles on the flight path together with the second vertical derivative of the TMI is very helpful in revealing correlations between the EM and Magnetics.

Next, key lines can be profiled as single lines to emphasize specific characteristics of a conductor or the relationship of one conductor to another on the same line. Resistivity Depth sections can be constructed to show the relationship of conductive overburden or conductive bedrock with the conductive anomaly.

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# APPENDIX D

# VTEM WAVE FORM



VTEM waveform - September, 2007

# APPENDIX E

# GEOPHYSICAL MAPS

## B-field 3.286 ms
### (pV*ms)/(A*m^4)

0.0036  0.0073  0.0148  0.0303  0.0619  0.1285  0.2586  0.5283  1.0796  2.2060

**Project 7085 - Sedex Mining Corp.**

**Serpentine Nickel property, Ontario, Canada**

B-Field Time Channel 3.286 ms

Geotech VTEM System

1000    0    1000    2000
(meters)
NAD83 / UTM zone 17N

**TMI**
[nT]

| 56525 | 56601 | 56647 | 56697 | 56746 | 56791 | 56835 | 56889 | 56952 | 57033 | 57149 | 57332 | 58022 |

## Project 7085 - Sedex Mining Corp.

### Serpentine Nickel property, Ontario, Canada

Total Magnetic Intensity

Geotech VTEM System

1000    0    1000    2000
(meters)
NAD83 / UTM zone 17N