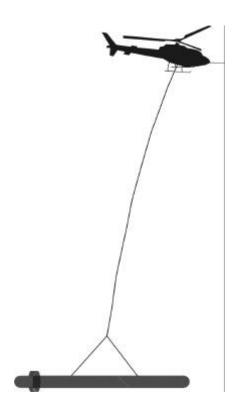


Report #06040

DIGHEM SURVEY
FOR
Q-GOLD (ONTARIO) LTD.
MINE CENTER / BAD VERMILION LAKE:
BLOCKS A, B & C.
FORT FRANCES, ONTARIO, CANADA

NTS: 52C/9,10,15,16



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August 18, 2006

#### SUMMARY

This report describes the logistics, data acquisition, processing and presentation of results of a DIGHEM airborne geophysical survey carried out for Q-Gold (Ontario) Ltd., over three blocks located near Fort Frances, Ontario. Total coverage of the survey blocks amounted to 1516 km. The survey was flown from May 6 to May 26, 2006.

The purpose of the survey was to detect zones of conductive mineralization and to provide information that could be used to map the geology and structure of the survey areas. This was accomplished by using a DIGHEM multi-coil, multi-frequency electromagnetic system, supplemented by a high sensitivity cesium magnetometer. The information from these sensors was processed to produce maps that display the magnetic and conductive properties of the survey areas. A GPS electronic navigation system ensured accurate positioning of the geophysical data with respect to the base maps.

The survey data were processed and compiled in the Fugro Airborne Surveys Toronto office. Map products and digital data were provided in accordance with the scales and formats specified in the Survey Agreement.

The survey properties contain several anomalous features, many of which are considered to be of moderate to high priority as exploration targets. Most of the inferred bedrock conductors appear to warrant further investigation using appropriate surface exploration techniques. Areas of interest may be assigned priorities on the basis of supporting

geophysical, geochemical and/or geological information. After initial investigations have been carried out, it may be necessary to re-evaluate the remaining anomalies based on information acquired from the follow-up program.

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# **APPENDICES**

- A. List of Personnel
- B. Background InformationC. Data Archive Description
- D. EM Anomaly ListE. Data Processing Flowcharts
- F. Glossary

#### 1. INTRODUCTION

A DIGHEM electromagnetic survey was flown for Q-Gold (Ontario) Ltd., from May 6 to May 26, 2006 over survey blocks located near Fort Frances, Ontario. The survey areas can be located on NTS map sheets 52C/9,10,15,16 (Figure 2).

Survey coverage consisted of approximately 1516 line-km, including 110 line-km of tie lines. Flight lines were flown in an azimuthal direction of 029°/209° for Area A, 120°/300° for Area B and 0°/180° for Area C with a line separation of 100 meters for Area A and 200 metres for Areas B and C. Tie lines were flown orthogonal to the traverse lines with a line separation 2000 metres in Areas B and C. Boundary tie lines were flown parallel to the area boundaries in Area A.

The survey employed the DIGHEM electromagnetic system. Ancillary equipment consisted of a magnetometer, radar and barometric altimeter, video camera, analog and digital recorders, and an electronic navigation system. The instrumentation was installed in an AS350B2 turbine helicopter, registration C-FZTA, that was provided by Questral Helicopters Ltd. The helicopter flew at an average airspeed of 120 km/h with an EM sensor height of approximately 30 metres.

In some portions of the survey area, the steep topography forced the pilot to exceed normal terrain clearance for reasons of safety. It is possible that some weak conductors

may have escaped detection in areas where the bird height exceeded 120 m. In difficult areas where near-vertical climbs were necessary, the forward speed of the helicopter was reduced to a level that permitted excessive bird swinging. This problem, combined with the severe stresses to which the bird was subjected, gave rise to aerodynamic noise levels that are slightly higher than normal on some lines. Where warranted, reflights were carried out to minimize these adverse effects.

Due to the presence of cultural features in the survey area, any interpreted conductors that occur in close proximity to cultural sources, should be confirmed as bedrock conductors prior to drilling.



Figure 1: Fugro Airborne Surveys RESOLVE EM bird with AS350-B3

# 2. SURVEY OPERATIONS

The base of operations for the survey was established at Fort Frances, Ontario. The survey areas can be located on NTS map sheets 52C/9,10,15,16 (Figures 2 through 4).

Table 2-1 lists the corner coordinates of the survey areas in NAD 83, UTM Zone 15 N, central meridian 93° W.

Table 2-1

Block	Corners	Corners X-UTM (E) Y-U	
06040-1	1	520000	5389800
Area A	2	526477	5401485
	3	529368	5399484
	4	524000	5389800
06040-2	1	516800	5393400
Area B	2	520325	5398867
	3	526517	5401537
	4	535038	5397050
	5	532489	5393279
	6	529810	5394690
	7	526670	5390025
	8	523405	5390016
06040-3	1	525000	5402800
Area C	2	541000	5402800
	3	541000	5399600
	4	537000	5399600
	5	537000	5398600
	6	535000	5398600
	7	535000	5397600
	8	525000	5397600

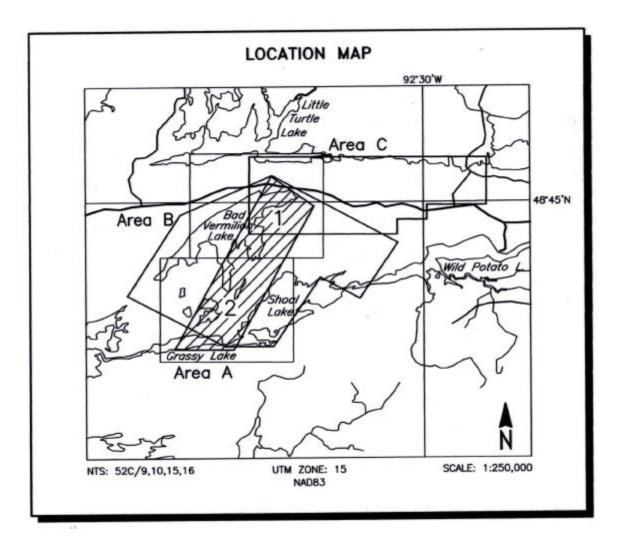


Figure 2 Location Map and Sheet Layout Survey Area A Job # 06040

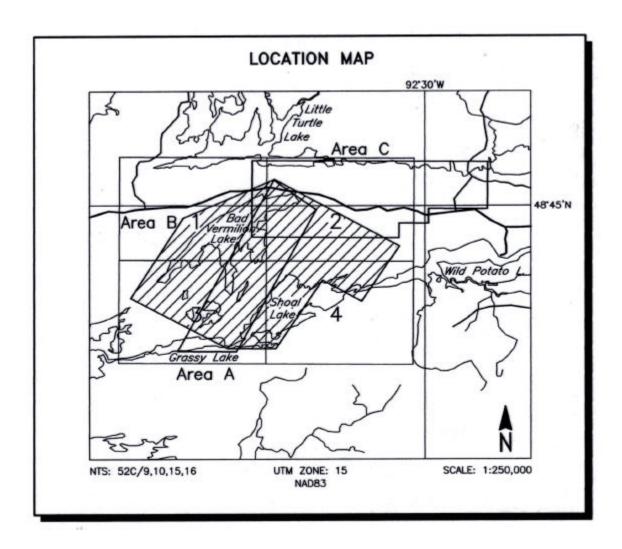


Figure 3 Location Map and Sheet Layout Survey Area B Job # 06040

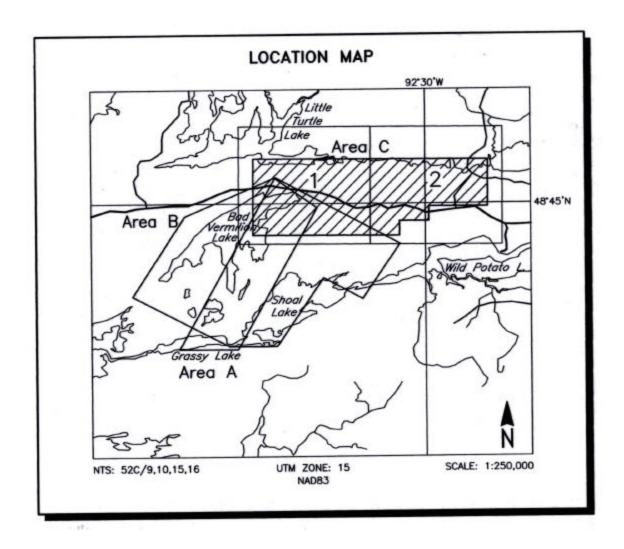


Figure 4
Location Map and Sheet Layout
Survey Area C
Job # 06040

The survey specifications were as follows:

Parameter	Specifications
Traverse line direction	Area A: 029°/209°
	Area B: 120°/300°
	Area C: 0°/180°
Traverse line spacing	Area A 100 m;
	Area B and C 200 m;
Tie line direction	Area A:various
	Area B and C 90°/270°
Tie line spacing	All areas 2000 m
Sample interval	10 Hz, 3.3 m @ 120 km/h
Aircraft mean terrain clearance	58 m
EM sensor mean terrain clearance	30 m
Mag sensor mean terrain clearance	30 m
Average speed	120 km/h
Navigation (guidance)	±5 m, Real-time GPS
Post-survey flight path	±2 m, Differential GPS

#### 3. SURVEY EQUIPMENT

This section provides a brief description of the geophysical instruments used to acquire the survey data and the calibration procedures employed. The geophysical equipment was installed in an AS350B2 helicopter. This aircraft provides a safe and efficient platform for surveys of this type.

# **Electromagnetic System**

Model: DIGHEM

Type: Towed bird, symmetric dipole configuration operated at a nominal

survey altitude of 30 metres. Coil separation is 8 metres for 900 Hz, 1000 Hz, 5500 Hz and 7200 Hz, and 6.3 metres for the 56,000 Hz coil-

pair.

Coil orientations, frequencies and dipole moments	Atm <sup>2</sup>	orientation	<u>1</u>	<u>nominal</u>	<u>actual</u>
·	211	coaxial	/	1000 Hz	1113 Hz
	211	coplanar	/	900 Hz	870 Hz
	67	coaxial	/	5500 Hz	5692 Hz
	56	coplanar	/	7200 Hz	7238 Hz
	15	coplanar	/	56,000 Hz	55,470 Hz
Channels recorded:	5 in-phase channels 5 quadrature channels 2 monitor channels				
Sensitivity:	0.12 pp 0.12 pp 0.24 pp		00 00 00	Hz Cp	

Sample rate: 10 per second, equivalent to 1 sample every 3.3 m, at a survey speed of 120 km/h.

The electromagnetic system utilizes a multi-coil coaxial/coplanar technique to energize conductors in different directions. The coaxial coils are vertical with their axes in the flight direction. The coplanar coils are horizontal. The secondary fields are sensed simultaneously by means of receiver coils that are maximum coupled to their respective transmitter coils. The system yields an in-phase and a quadrature channel from each transmitter-receiver coil-pair.

## In-Flight EM System Calibration

Calibration of the system during the survey uses the Fugro AutoCal automatic, internal calibration process. At the beginning and end of each flight, and at intervals during the flight, the system is flown up to high altitude to remove it from any "ground effect" (response from the earth). Any remaining signal from the receiver coils (base level) is measured as the zero level, and is removed from the data collected until the time of the next calibration. Following the zero level setting, internal calibration coils, for which the response phase and amplitude have been determined at the factory, are automatically triggered – one for each frequency. The on-time of the coils is sufficient to determine an accurate response through any ambient noise. The receiver response to each calibration coil "event" is compared to the expected response (from the factory calibration) for both phase angle and amplitude, and any phase and gain corrections are automatically applied to bring the data to the correct value.

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In addition, the outputs of the transmitter coils are continuously monitored during the

survey, and the gains are adjusted to correct for any change in transmitter output.

Because the internal calibration coils are calibrated at the factory (on a resistive halfspace)

ground calibrations using external calibration coils on-site are not necessary for system

calibration. A check calibration may be carried out on-site to ensure all systems are

working correctly. All system calibrations will be carried out in the air, at sufficient altitude

that there will be no measurable response from the ground.

The internal calibration coils are rigidly positioned and mounted in the system relative to

the transmitter and receiver coils. In addition, when the internal calibration coils are

calibrated at the factory, a rigid jig is employed to ensure accurate response from the

external coils.

Using real time Fast Fourier Transforms and the calibration procedures outlined above,

the data are processed in real time, from measured total field at a high sampling rate, to in-

phase and quadrature values at 10 samples per second.

Airborne Magnetometer

Model:

Fugro AM102 processor with Scintrex

CS2 sensor

Type: Optically pumped cesium vapour

Sensitivity: 0.01 nT

Sample rate: 10 per second

The magnetometer sensor is housed in the EM bird, 28 m below the helicopter.

# **Magnetic Base Station**

#### **Primary**

Model: Fugro CF1 base station with timing

provided by integrated GPS.

Sensor type: Scintrex CS3

Counter specifications: Accuracy: ±0.1 nT

Resolution: 0.01 nT Sample rate 1 Hz

GPS specifications: Model: Marconi Allstar

Type: Code and carrier tracking of L1 band,

12-channel, C/A code at 1575.42 MHz

Sensitivity: -90 dBm, 1.0 second update

Accuracy: Manufacturer's stated accuracy for differential

corrected GPS is 2 metres

Environmental

Monitor specifications: Temperature:

Accuracy: ±1.5°C max
Resolution: 0.0305°C
Sample rate: 1 Hz

• Range: -40°C to +75°C

Barometric pressure:

Model: Motorola MPXA4115A

• Accuracy: ±3.0° kPa max (-20°C to 105°C temp. ranges)

Resolution: 0.013 kPaSample rate: 1 Hz

• Range: 55 kPa to 108 kPa

## Refer to Figure 5



Figure 5: CF1 Magnetic Base Station Set-up

<u>Backup</u>

Model: GEM Systems GSM-19T

Type: Digital recording proton precession

Sensitivity: 0.10 nT

Sample rate: 3 second intervals

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A digital recorder is operated in conjunction with the base station magnetometer to record

the diurnal variations of the earth's magnetic field. The clock of the base station is

synchronized with that of the airborne system, using GPS time, to permit subsequent

removal of diurnal drift. The Fugro CF1 magnetometer was the primary magnetic base

station. It was set-up at two locations throughout the duration of the survey: Sand Pit from

May 14 until May 20, 2006 and Sand Pit 2 from May 21 to May 26, 2006. The first location

was at 48° 44' 48.35358" N, 92° 35' 25.96713" W (WGS84); and the second location was

at 48° 44' 54.06034" N, 92° 35' 25.96713" W (WGS84).

The GEM Systems magnetometer was the back-up magnetic base station. It was set-up

at three locations throughout the survey: Fort Frances Airport from May 8 to May 14,

2006; Sand Pit from May 14 to May 20, 2006; and Sand Pit 2 from May 20 to May 26,

2006. The first location was at 48° 44' 48.35358" N, 92° 35' 25.96713" W (WGS84); the

second location was at 48° 44' 54.06034" N, 92° 35' 25.96713" W (WGS84); and the third

location was at 48° 44' 54.06034" N, 92° 35' 25.96713" W (WGS84).

**Navigation (Global Positioning System)** 

Airborne Receiver for Real-time Navigation & Guidance

Model: Ashtech Glonass GG24 with PNAV 2100 interface

Type: SPS (L1 band), 24-channel, C/A code at 1575.42 MHz,

S code at 0.5625 MHz, Real-time differential.

Sensitivity: -132 dBm, 0.5 second update

Accuracy: Manufacturer's stated accuracy is better than 5 metres

real-time

Antenna: Mounted on tail of aircraft

#### Primary Base Station for Post-Survey Differential Correction

Model: Ashtech Z-Surveyor

Type: Code and carrier tracking of L1 band, 12-channel, dual

frequency C/A code at 1575.2 MHz, and L2 P-code

1227 MHz

Sample rate: 0.5 second update

Accuracy: Manufacturer's stated accuracy for differential corrected

GPS is better than 1 metre



Figure 6: GPS Base Station Set-up

## Secondary GPS Base Station

Model: Marconi Allstar OEM, CMT-1200

Type: Code and carrier tracking of L1 band, 12-channel, C/A code

at 1575.42 MHz

Sensitivity: -90 dBm, 1.0 second update

Accuracy: Manufacturer's stated accuracy for differential corrected GPS

is 2 metres.



Figure 7: CF1 GPS Base Station Set-up

The Ashtech GG24 is a line of sight, satellite navigation system that utilizes time-coded signals from at least four of forty-eight available satellites. Both Russian GLONASS and American NAVSTAR satellite constellations are used to calculate the position and to provide real time guidance to the helicopter. For flight path processing an Ashtech Z-surveyor was used as the mobile receiver. A similar system was used as the primary base station receiver. The mobile and base station raw XYZ data were recorded, thereby permitting post-survey differential corrections for theoretical accuracies of better than 2 metres. A Marconi Allstar GPS unit, part of the CF1, was used as a secondary (back-up) base station.

- 3.10 -

Each base station receiver is able to calculate its own latitude and longitude. For this

survey, the primary GPS station was set up at two locations at the Fort Frances Airport.

The first location was located at latitude 48° 39' 01.64387" N, longitude 93° 26' 09.44240"

W at an elevation of 311.886 metres above the ellipsoid from May 11 to May 12, 2006.

The second location was located at latitude 48° 39' 01.76630" N, longitude 93° 26'

09.42006" W at an elevation of 308.827 metres above the ellipsoid from May 17 to May

26, 2006. The secondary GPS unit was set-up at three locations Fort Frances Airport from

May 8 to May 14, 2006; Sand Pit from May 8 to May 20, 2006; and Sand Pit 2 from May

21 to May 26, 2006. Fort Frances Airport is located at latitude 48° 39' 01.76630" N,

longitude 93° 26' 09.42006" W at an ellipsoidal elevation of 308.83 metres. Sand Pit is

located at latitude 48° 44' 48.35358" N, longitude 92° 35' 25.96713" W at an ellipsoidal

elevation of 337.37 metres. Sand Pit 2 is located at latitude 48° 44' 54.06034" N,

longitude 92° 35' 25.96713" W at an ellipsoidal elevation of 336.38 metres. The GPS

records data relative to the WGS84 ellipsoid, which is the basis of the revised North

American Datum (NAD83). Conversion software is used to transform the WGS84

coordinates to the NAD83 UTM system displayed on the maps.

Radar Altimeter

Manufacturer:

Honeywell/Sperry

Model:

AA 330 or RT220

Type:

Short pulse modulation, 4.3 GHz

- 3.11 -

Sensitivity: 0.3 m

Sample rate: 2 per second

The radar altimeter measures the vertical distance between the helicopter and the ground.

This information is used in the processing algorithm that determines conductor depth.

### **Barometric Pressure and Temperature Sensors**

Model: DIGHEM D 1300

Type: Motorola MPX4115AP analog pressure sensor

AD592AN high-impedance remote temperature sensors

Sensitivity: Pressure: 150 mV/kPa

Temperature: 100 mV/°C or 10 mV/°C (selectable)

Sample rate: 10 per second

The D1300 circuit is used in conjunction with one barometric sensor and up to three temperature sensors. Two sensors (baro and temp) are installed in the EM console in the aircraft, to monitor pressure (1KPA) and internal operating temperatures (2TDC).

# **Digital Data Acquisition System**

Manufacturer: Fugro

Model: Helidas

- 3.12 -

Recorder: Compact Flash Cards

The stored data are downloaded to the field workstation PC at the survey base, for verification, backup and preparation of in-field products.

# **Video Flight Path Recording System**

Type: Sony DXC-101

Recorder: Sanyo

Format: NTSC (VHS)

Fiducial numbers are recorded continuously and are displayed on the margin of each image. This procedure ensures accurate correlation of data with respect to visible features on the ground.

#### 4. QUALITY CONTROL AND IN-FIELD PROCESSING

Digital data for each flight were transferred to the field workstation, in order to verify data quality and completeness. A database was created and updated using Geosoft Oasis Montaj and proprietary Fugro Atlas software. This allowed the field personnel to calculate, display and verify both the positional (flight path) and geophysical data on a screen or printer. Records were examined as a preliminary assessment of the data acquired for each flight.

In-field processing of Fugro survey data consists of differential corrections to the airborne GPS data, verification of EM calibrations, drift correction of the raw airborne EM data, spike rejection and filtering of all geophysical and ancillary data, verification of flight videos, calculation of preliminary resistivity data, diurnal correction, and preliminary leveling of magnetic data.

All data, including base station records, were checked on a daily basis, to ensure compliance with the survey contract specifications. Reflights were required if any of the following specifications were not met.

Flight Path - No lines to exceed ±25% departure from nominal line spacing over a continuous distance of more than 1 km, except for reasons of safety.

Clearance - Mean terrain sensor clearance of 30 m, ±10 m, except where precluded by safety considerations, e.g., restricted or populated

areas, severe topography, obstructions, tree canopy, aerodynamic

limitations, etc.

Airborne Mag - Aerodynamic magnetometer fourth difference is not to exceed 1.6 nT over a distance of more than 1 km.

Base Mag - Diurnal variations not to exceed 10 nT over a straight line time chord

of 1 minute.

Spheric pulses may occur having strong peaks but narrow widths.
 The EM data area considered acceptable when their occurrence is less than 10 spheric events exceeding the stated noise specification for a given frequency per 100 samples continuously over a distance of 2,000 metres.

	Coil	Peak to Peak Noise Envelope		
Frequency	Orientation	(ppm)		
1000 Hz	vertical coplanar	5.0		
900 Hz	horizontal coplanar	10.0		
5500 Hz	vertical coaxial	10.0		
7200 Hz	horizontal coplanar	20.0		
56,000 Hz	horizontal coplanar	40.0		

#### 5. DATA PROCESSING

# Flight Path Recovery

The final flight path is produced by applying the following procedures:

- Data quality checks
- Differential post-processing of data
- Projecting the raw latitudes/longitudes into UTM coordinates
- Flight path and speed checks

Initially the raw data are checked for gaps and data quality. The raw range data from at

least four satellites are simultaneously recorded by both the base and mobile GPS units.

The geographic positions of both units, relative to the model ellipsoid, are calculated from

this information.

Differential corrections, which are obtained from the base station, are applied next to the

mobile unit data to provide a post-flight track of the aircraft, accurate to within 2 m. The

processed data are then projected from latitude/longitude coordinates into UTM X/Y

coordinates. Finally the flight path and speed of the flight path are checked to determine

if there are any spikes or gaps in the data.

The corrected WGS84 latitude/longitude coordinates are transformed to the coordinate system used on the final maps. Images or plots are then created to provide a visual check of the flight path.

# **Electromagnetic Data**

The final EM data are produced by applying the following procedures:

- Data quality checks
- Filtering
- Lag correction
- Resistivity and depth calculations
- Leveling of the in-phase and quadrature EM channels

EM data are processed at the recorded sample rate of 10 samples/second. Initially the data quality is checked to insure the data is within the stated noise and spheric specifications. Spheric rejection median and hanning filters are then applied to reduce noise to acceptable levels. All EM data are lagged by 10 scans (1 second).

EM test profiles are then created to allow the interpreter to select the most appropriate EM anomaly picking controls for a given survey area. The EM picking parameters depend on several factors but are primarily based on the dynamic range of the resistivities within the survey area, and the types and expected geophysical responses of the targets being sought.

Anomalous electromagnetic responses are selected and analysed by computer to provide a preliminary electromagnetic anomaly map. The automatic selection algorithm is intentionally oversensitive to assure that no meaningful responses are missed. Using the preliminary map in conjunction with the multi-parameter stacked profiles, the interpreter then classifies the anomalies according to their source and eliminates those that are not substantiated by the data. The final interpreted EM anomaly map includes bedrock, surficial and cultural conductors. A map containing only bedrock conductors can be generated, if desired.

## **Apparent Resistivity**

Apparent resistivity maps portray all of the information for a given frequency over the entire survey area. The large dynamic range afforded by the multiple frequencies makes the apparent resistivity parameter an excellent mapping tool. Broad conductors, which more closely approximate a half-space model, will be maximum coupled to the horizontal (coplanar) coil-pair and should be more evident on the resistivity parameter. Resistivity maps, therefore, may be more valuable than the electromagnetic anomaly maps, in areas where broad or flat-lying conductors are considered to be of importance.

The inputs to the resistivity algorithm are the in-phase and quadrature amplitudes of the secondary field. The algorithm calculates the apparent resistivity in ohm-meters, and the apparent height of the bird above the conductive source. Any difference between the apparent height and the true height, as measured by the radar altimeter, is called the

pseudo-layer and reflects the difference between the real geology and a homogeneous halfspace. This difference is often attributed to the presence of a highly resistive upper layer. Any errors in the altimeter reading, caused by heavy tree cover, are included in the pseudo-layer and do not affect the resistivity calculation. The apparent depth estimates, however, will reflect the altimeter errors. Apparent resistivities calculated in this manner may differ from those calculated using other models.

In areas where the effects of magnetic permeability or dielectric permittivity have suppressed the in-phase responses, the calculated resistivities will be erroneously high.

Various algorithms and inversion techniques can be used to partially correct for the effects of permeability and permittivity.

Apparent resistivity maps portray all of the information for a given frequency over the entire survey area. This full coverage contrasts with the electromagnetic anomaly map, which provides information only over interpreted conductors. The large dynamic range afforded by the multiple frequencies makes the apparent resistivity parameter an excellent mapping tool.

The preliminary apparent resistivity maps and images are carefully inspected to identify any lines or line segments that might require base level adjustments. Subtle changes between in-flight calibrations of the system can result in line-to-line differences that are more recognizable in resistive (low signal amplitude) areas. Manual leveling adjustments are carried out to eliminate or minimize resistivity differences that can be attributed, in part,

to changes in operating temperatures. These leveling adjustments are very subtle, and do not result in the degradation of discrete anomalies.

After the manual leveling process is complete, revised resistivity grids are created. The resulting grids can be subjected to a microleveling technique in order to smooth the data for contouring.

The calculated resistivities for the 3 coplanar frequencies are included in the XYZ archives. Values are in ohm-metres on all final products.

# Dielectric Permittivity and Magnetic Permeability Corrections<sup>1</sup> (Optional)

In resistive areas having magnetic rocks, the magnetic and dielectric effects will both generally be present in high-frequency EM data, whereas only the magnetic effect will exist in low-frequency data.

The magnetic permeability is first obtained from the EM data at the lowest frequency, because the ratio of the magnetic response to conductive response is maximized and because displacement currents are negligible. The homogeneous half-space model is used. The computed magnetic permeability is then used along with the in-phase and quadrature response at the highest frequency to obtain the relative dielectric permittivity, again using the homogeneous half-space model. The highest frequency is used because

the ratio of dielectric response to conductive response is maximized. The resistivity can then be determined from the measured in-phase and quadrature components of each frequency, given the relative magnetic permeability and relative dielectric permittivity.

# **Resistivity-depth Sections (optional)**

The apparent resistivities for all frequencies can be displayed simultaneously as coloured resistivity-depth sections. Usually, only the coplanar data are displayed as the close frequency separation between the coplanar and adjacent coaxial data tends to distort the section. The sections can be plotted using the topographic elevation profile as the surface. The digital terrain values, in metres a.m.s.l., can be calculated from the GPS Z-value or barometric altimeter, minus the aircraft radar altimeter.

Resistivity-depth sections can be generated in three formats:

- (1) Sengpiel resistivity sections, where the apparent resistivity for each frequency is plotted at the depth of the centroid of the in-phase current flow<sup>2</sup>; and,
- (2) Differential resistivity sections, where the differential resistivity is plotted at the differential depth<sup>3</sup>.

<sup>1</sup> Huang, H. and Fraser, D.C., 2001 Mapping of the Resistivity, Susceptibility, and Permittivity of the Earth Using a Helicopter-borne Electromagnetic System: Geophysics 106 pg 148-157.

Sengpiel, K.P., 1988, Approximate Inversion of Airborne EM Data from Multilayered Ground: Geophysical Prospecting 36, 446-459.

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Huang, H. and Fraser, D.C., 1993, Differential Resistivity Method for Multi-frequency Airborne EM Sounding: presented at Intern. Airb. EM Workshop, Tucson, Ariz.

(3) Occam<sup>4</sup> or Multi-layer<sup>5</sup> inversion.

Both the Sengpiel and differential methods are derived from the pseudo-layer half-space model. Both yield a coloured resistivity-depth section that attempts to portray a smoothed approximation of the true resistivity distribution with depth. Resistivity-depth sections are most useful in conductive layered situations, but may be unreliable in areas of moderate to high resistivity where signal amplitudes are weak. In areas where in-phase responses have been suppressed by the effects of magnetite, or adversely affected by cultural features, the computed resistivities shown on the sections may be unreliable.

Both the Occam and multi-layer inversions compute the layered earth resistivity model that would best match the measured EM data. The Occam inversion uses a series of thin, fixed layers (usually 20 x 5m and 10 x 10m layers) and computes resistivities to fit the EM data. The multi-layer inversion computes the resistivity and thickness for each of a defined number of layers (typically 3-5 layers) to best fit the data.

# **Total Magnetic Field**

The final leveled total field is produced by applying the following procedures:

Data quality checks

-

Constable et al, 1987, Occam's inversion: a practical algorithm for generating smooth models from electromagnetic sounding data: Geophysics, 52, 289-300.

Huang H., and Palacky, G.J., 1991, Damped least-squares inversion of time domain airborne EM data based on singular value decomposition: Geophysical Prospecting, 39, 827-844.

- Lag correction
- Checking and applying the diurnal data
- IGRF Correction
- Leveling of the total magnetic field

The quality of the magnetic data are checked by using a fourth difference editing routine looking specifically for spikes and noise in the data. The noise levels are maintained within the stated specifications. Narrow spikes are removed manually guided by the fourth difference calculation and the resulting small gaps are interpolated using an Akima spline.

A magnetic lag test is flown to calculate the positional lag that develops between the time a reading is made and the time it is recorded in the data. A large metallic body such as railway tracks, a bridge, buildings or a distinct magnetic anomaly is flown over along a single line, at survey altitude, in opposite directions. This allows the time constant value that will line-up the magnetic anomaly peaks or troughs that are produced to be determined. A lag of 17 scans (1.7 seconds) is applied to all the magnetic data in this survey. This time shift constant is then added to the data of lines flown in one direction and subtracted from the data of lines flown in the opposite direction.

A GEM proton precession magnetometer and a Fugro CF1 cesium vapour magnetometer were operated at the survey base to record diurnal variations of the earth's magnetic field.

The clock of the base station was synchronized with that of the airborne system to permit subsequent removal of diurnal drift. The diurnal field was filtered before the corrections

were applied to the magnetic data. The diurnally corrected magnetic data were then corrected for regional variations in the magnetic field, based on the International Geomagnetic Reference Field (IGRF). This IGRF correction is calculated based on the magnetometer's height, gps position and date for each reading. This calculated regional value is then subtracted from each magnetic field reading. This results in removing regional variations from the data enhancing the local variations. Then the average IGRF value in the survey area, 57865 nT, was added back to the magnetic field.

The IGRF corrected magnetic data were then leveled using tie and traverse line intercepts.

Manual adjustments were applied to any lines that required leveling, as indicated by shadowed images of the gridded magnetic data.

# **Calculated Vertical Magnetic Gradient**

The diurnally-corrected total magnetic field data were subjected to a processing algorithm that enhances the response of magnetic bodies in the upper 500 m and attenuates the response of deeper bodies. The resulting vertical gradient map provides better definition and resolution of near-surface magnetic units. It also identifies weak magnetic features that may not be evident on the total field map. However, regional magnetic variations and changes in lithology may be better defined on the total magnetic field map.

# **EM Magnetite (optional)**

The apparent percent magnetite by weight is computed wherever magnetite produces a negative in-phase EM response. This calculation is more meaningful in resistive areas.

## Residual Magnetic Intensity (optional)

The residual magnetic intensity (RMI) is derived from the total magnetic field (TMF), the diurnal, and the regional magnetic field. The total magnetic intensity is measured in the aircraft, the diurnal is measured from the ground station, and the regional magnetic field is calculated from the international geo-referenced magnetic field (IGRF). The low frequency component of the diurnal is extracted from the filtered ground station data and removed from the TMF. The average of the diurnal is then added back in to obtain the resultant total magnetic intensity. The regional magnetic field, calculated for the specific survey location and the time of the survey, is then removed from the resultant total magnetic intensity to yield the residual magnetic intensity.

# **Magnetic Derivatives (optional)**

The total magnetic field data can be subjected to a variety of filtering techniques to yield maps or images of the following:

second vertical derivative reduction to the pole/equator

magnetic susceptibility with reduction to the pole

upward/downward continuations

analytic signal

enhanced magnetics

All of these filtering techniques improve the recognition of near-surface magnetic bodies, with the exception of upward continuation. Any of these parameters can be produced on request.

## **Digital Elevation**

The radar altimeter values (ALTR – aircraft to ground clearance) are subtracted from the differentially corrected and de-spiked GPS-Z values to produce profiles of the height above the ellipsoid along the survey lines. These values are gridded to produce contour maps showing approximate elevations within the survey area. The calculated digital terrain data are then tie-line leveled and adjusted to mean sea level. Any remaining subtle line-to-line discrepancies are manually removed. After the manual corrections are applied, the digital terrain data are filtered with a microleveling algorithm.

The accuracy of the elevation calculation is directly dependent on the accuracy of the two input parameters, ALTR and GPS-Z. The ALTR value may be erroneous in areas of

heavy tree cover, where the altimeter reflects the distance to the tree canopy rather than the ground. The GPS-Z value is primarily dependent on the number of available satellites. Although post-processing of GPS data will yield X and Y accuracies in the order of 1-2 metres, the accuracy of the Z value is usually much less, sometimes in the ±10 metre range. Further inaccuracies may be introduced during the interpolation and gridding process.

Because of the inherent inaccuracies of this method, no guarantee is made or implied that the information displayed is a true representation of the height above sea level. Although this product may be of some use as a general reference, <u>THIS PRODUCT MUST NOT BE USED FOR NAVIGATION PURPOSES</u>.

# **Contour, Colour and Shadow Map Displays**

The geophysical data are interpolated onto a regular grid using a modified Akima spline technique. The resulting grid is suitable for image processing and generation of contour maps. The grid cell size is 20% of the line interval.

Colour maps are produced by interpolating the grid down to the pixel size. The parameter is then incremented with respect to specific amplitude ranges to provide colour "contour" maps.

Monochromatic shadow maps or images are generated by employing an artificial sun to cast shadows on a surface defined by the geophysical grid. There are many variations in the shadowing technique. These techniques can be applied to total field or enhanced magnetic data, magnetic derivatives, resistivity, etc. The shadowing technique is also used as a quality control method to detect subtle changes between lines.

## **Multi-channel Stacked Profiles**

Distance-based profiles of the digitally recorded geophysical data are generated and plotted at an appropriate scale. These profiles also contain the calculated parameters that are used in the interpretation process. These are produced as worksheets prior to interpretation, and are also presented in the final corrected form after interpretation. The profiles display electromagnetic anomalies with their respective interpretive symbols. Table 5-1 shows the parameters and scales for the multi-channel stacked profiles.

In Table 5-1, the log resistivity scale of 0.06 decade/mm means that the resistivity changes by an order of magnitude in 16.6 mm. The resistivities at 0, 33 and 67 mm up from the bottom of the digital profile are respectively 1, 100 and 10,000 ohm-m.

**Table 5-1. Multi-channel Stacked Profiles** 

Channel		Sca	ale
Name (Freq)	Observed Parameters	Units	s/mm
MAG	total magnetic field (fine)	2.5	nT
MAG	total magnetic field (coarse)	25	nT
ALTBIRDM	EM sensor height above ground	6	m
CXI1000	vertical coaxial coil-pair in-phase (1000 Hz)	4	ppm
CXQ1000	vertical coaxial coil-pair quadrature (1000 Hz)	4	ppm
CPI900	horizontal coplanar coil-pair in-phase (900 Hz)	4	ppm
CPQ900	horizontal coplanar coil-pair quadrature (900 Hz)	4	ppm
CXI5500	vertical coaxial coil-pair in-phase (5500 Hz)	8	ppm
CXQ5500	vertical coaxial coil-pair quadrature (5500 Hz)	8	ppm
CPI7200	horizontal coplanar coil-pair in-phase (7200 Hz)	8	ppm
CPQ7200	horizontal coplanar coil-pair quadrature (7200 Hz)	8	ppm
CPI56K	horizontal coplanar coil-pair in-phase (56,000 Hz)	10	ppm
CPQ56K	horizontal coplanar coil-pair quadrature (56,000 Hz)	10	ppm
CXSP	coaxial spherics monitor		
CPPL	coplanar powerline monitor		
CPSP	coplanar spherics monitor		
	Computed Parameters		
DIFI ( mid freq.)	difference function in-phase from CXI and CPI	4	ppm
DIFQ (mid freq.)	difference function quadrature from CXQ and CPQ	4	ppm
RES900	log resistivity	.06	decade
RES7200	log resistivity	.06	decade
RES56K	log resistivity	.06	decade
DEP900	apparent depth	6	m
DEP7200	apparent depth	6	m
DEP56K	apparent depth	6	m
CDT	conductance	1	grade

- 6.1 -

6. PRODUCTS

This section lists the final maps and products that have been provided under the terms of

the survey agreement. Other products can be prepared from the existing dataset, if

requested. These include magnetic enhancements or derivatives, percent magnetite,

resistivities corrected for magnetic permeability and/or dielectric permittivity, digital terrain,

resistivity-depth sections, inversions, and overburden thickness. Most parameters can be

displayed as contours, profiles, or in colour.

**Base Maps** 

Base maps of the survey area were produced by scanning published topographic maps to

a bitmap (.bmp) format. This process provides a relatively accurate, distortion-free base

that facilitates correlation of the navigation data to the map coordinate system. The

topographic files were combined with geophysical data for plotting the final maps. All

maps were created using the following parameters:

Projection Description:

Datum: NAD83 Ellipsoid: GRS80

Projection: UTM (Zone: 15N)

Central Meridian: 93 W
False Northing: 0
False Easting: 500000
Scale Factor: 0.9996

WGS84 to Local Conversion: Molodensky

Datum Shifts: DX:0 DY:0 DZ:0

The following parameters are presented on 8 map sheets for all three areas, at a scale of

1:10,000. All maps include flight lines and topography, unless otherwise indicated.

Preliminary products are not listed.

## **Final Products**

	No. of Map Sets	
	Blackline	Colour
EM Anomalies	2	
Total Magnetic Field		2
Calculated Vertical Magnetic Gradient		2
Apparent Resistivity 900 Hz		2
Apparent Resistivity 7200 Hz		2

### **Additional Products**

Digital Archive (see Archive Description)

Survey Report

Multi-channel Stacked Profiles

Flight Path Video (VHS)

1 CD-ROM
2 copies
All lines
1 cassette

## 7. SURVEY RESULTS

### **General Discussion**

Tables 7-1 through 7-3 summarize the EM responses in the survey areas, with respect to conductance grade and interpretation. The apparent conductance and depth values shown in the EM Anomaly list appended to this report have been calculated from "local" inphase and quadrature amplitudes of the Coaxial 5500 Hz frequency. The picking and interpretation procedure relies on several parameters and calculated functions. For this survey, the Coaxial 5500 Hz responses and the mid-frequency difference channels were used as two of the main picking criteria. The 7200 Hz coplanar results were also weighted to provide picks over wider or flat-dipping sources. The quadrature channels provided picks in areas where the in-phase responses might have been suppressed by magnetite.

The anomalies shown on the electromagnetic anomaly maps are based on a near-vertical, half plane model. This model best reflects "discrete" bedrock conductors. Wide bedrock conductors or flat-lying conductive units, whether from surficial or bedrock sources, may give rise to very broad anomalous responses on the EM profiles. These may not appear on the electromagnetic anomaly map if they have a regional character rather than a locally anomalous character.

## **TABLE 7-1 EM ANOMALY STATISTICS**

# Mine Center / Bad Vermilion Lake Area A

CONDUCTOR GRADE	CONDUCTANCE RANGE NUMBE SIEMENS (MHOS) RESPO	
7 6 5 4 3 2 1	>100 50 - 100 20 - 50 10 - 20 5 - 10 1 - 5 <1 INDETERMINATE	0 0 0 2 1 131 225 273
TOTAL		632
CONDUCTOR MODEL	MOST LIKELY SOURCE	NUMBER OF RESPONSES
D B S H E L	DISCRETE BEDROCK CONDUCTOR DISCRETE BEDROCK CONDUCTOR CONDUCTIVE COVER ROCK UNIT OR THICK COVER EDGE OF WIDE CONDUCTOR CULTURE	2 27 522 49 1 31
TOTAL		632

(SEE EM MAP LEGEND FOR EXPLANATIONS)

## **TABLE 7-2 EM ANOMALY STATISTICS**

# Mine Center / Bad Vermilion Lake Area B

CONDUCTOR GRADE	CONDUCTANCE RANGE SIEMENS (MHOS)		
7 6 5 4 3 2 1	>100 50 - 100 20 - 50 10 - 20 5 - 10 1 - 5 <1 INDETERMINATE	0 0 0 2 6 233 459 427	
TOTAL		1127	
CONDUCTOR MODEL	MOST LIKELY SOURCE	NUMBER OF RESPONSES	
D B S H E L	DISCRETE BEDROCK CONDUCTOR DISCRETE BEDROCK CONDUCTOR CONDUCTIVE COVER ROCK UNIT OR THICK COVER EDGE OF WIDE CONDUCTOR CULTURE	17 42 920 132 2 14	
TOTAL		1127	

(SEE EM MAP LEGEND FOR EXPLANATIONS)

## **TABLE 7-3 EM ANOMALY STATISTICS**

# Mine Center / Bad Vermilion Lake Area C

CONDUCTOR GRADE	CONDUCTANCE RANGE SIEMENS (MHOS)	NUMBER OF RESPONSES
7 6 5 4 3 2 1	>100 50 - 100 20 - 50 10 - 20 5 - 10 1 - 5 <1 INDETERMINATE	0 0 1 8 17 230 261 292
TOTAL		809
CONDUCTOR MODEL	MOST LIKELY SOURCE	NUMBER OF RESPONSES
B S H L	DISCRETE BEDROCK CONDUCTOR CONDUCTIVE COVER ROCK UNIT OR THICK COVER CULTURE	5 558 41 205
TOTAL		632

(SEE EM MAP LEGEND FOR EXPLANATIONS)

These broad conductors, which more closely approximate a half-space model, will be maximum coupled to the horizontal (coplanar) coil-pair and should be more evident on the resistivity parameter. Resistivity maps, therefore, may be more valuable than the electromagnetic anomaly maps, in areas where broad or flat-lying conductors are considered to be of importance. Contoured resistivity maps, based on the 900 Hz and 7200 Hz coplanar data, are included with this report.

Excellent resolution and discrimination of conductors was accomplished by using a fast sampling rate of 0.1 sec and by employing a "common" frequency (5500/7200 Hz) on two orthogonal coil-pairs (coaxial and coplanar). The resulting difference channel parameters often permit differentiation of bedrock and surficial conductors, even though they may exhibit similar conductance values.

Anomalies that occur near the ends of the survey lines (i.e., outside the survey area), should be viewed with caution. Some of the weaker anomalies could be due to aerodynamic noise, i.e., bird bending, which is created by abnormal stresses to which the bird is subjected during the climb and turn of the aircraft between lines. Such aerodynamic noise is usually manifested by an anomaly on the coaxial in-phase channel only, although severe stresses can affect the coplanar in-phase channels as well.

## **Magnetics**

A Fugro CF-1 cesium vapour magnetometer was operated at the survey base to record diurnal variations of the earth's magnetic field. The clock of the base station was synchronized with that of the airborne system to permit subsequent removal of diurnal drift.

A GEM Systems GSM-19T proton precession magnetometer was also operated as a backup unit.

The total magnetic field data have been presented as contours on the base maps using a contour interval of 5 nT where gradients permit. The maps show the magnetic properties of the rock units underlying the survey areas.

The total magnetic field data have been subjected to a processing algorithm to produce maps of the calculated vertical gradient. This procedure enhances near-surface magnetic units and suppresses regional gradients. It also provides better definition and resolution of magnetic units and displays weak magnetic features that may not be clearly evident on the total field maps.

There is some evidence on the magnetic maps that suggests that the survey areas have been subjected to deformation and/or alteration. These structural complexities are evident on the contour maps as variations in magnetic intensity, irregular patterns, and as offsets or changes in strike direction.

If a specific magnetic intensity can be assigned to the rock type that is believed to host the target mineralization, it may be possible to select areas of higher priority on the basis of the total field magnetic data. This is based on the assumption that the magnetite content of the host rocks will give rise to a limited range of contour values that will permit differentiation of various lithological units.

The magnetic results, in conjunction with the other geophysical parameters, have provided valuable information that can be used to effectively map the geology and structure in the survey areas.

# **Apparent Resistivity**

Apparent resistivity maps, which display the conductive properties of the survey areas, were produced from the 900 Hz and 7200 Hz coplanar data. The maximum resistivity values, which are calculated for each frequency, are 3,000 and 10,000 ohm-m respectively. These cutoffs eliminate the erratic higher resistivities that would result from unstable ratios of very small EM amplitudes.

In general, the resistivity patterns show moderately good agreement with the magnetic trends. This suggests that many of the resistivity lows are probably related to bedrock features, rather than conductive overburden. There are some areas, however, where contour patterns appear to be strongly influenced by conductive surficial material.

There are other resistivity lows in the area. Some of these are quite extensive and often reflect "formational" conductors that may be of minor interest as direct exploration targets. However, attention may be focused on areas where these zones appear to be faulted or folded or where anomaly characteristics differ along strike.

## **Electromagnetic Anomalies**

The EM anomalies resulting from this survey appear to fall within one of three general categories. The first type consists of discrete, well-defined anomalies that yield marked inflections on the difference channels. These anomalies are usually attributed to conductive sulphides or graphite and are generally given a "B", "T" or "D" interpretive symbol, denoting a bedrock source.

The second class of anomalies comprises moderately broad responses that exhibit the characteristics of a half-space and do not yield well-defined inflections on the difference channels. Anomalies in this category are usually given an "S" or "H" interpretive symbol. The lack of a difference channel response usually implies a broad or flat-lying conductive source such as overburden. Some of these anomalies could reflect conductive rock units, zones of deep weathering, or the weathered tops of kimberlite pipes, all of which can yield "non-discrete" signatures.

The effects of conductive overburden are evident over portions of the survey area(s). Although the difference channels (DIFI and DIFQ) are extremely valuable in detecting bedrock conductors that are partially masked by conductive overburden, sharp undulations in the bedrock/overburden interface can yield anomalies in the difference channels which may be interpreted as possible bedrock conductors. Such anomalies usually fall into the "S?" or "B?" classification but may also be given an "E" interpretive symbol, denoting a resistivity contrast at the edge of a conductive unit.

The "?" symbol does not question the validity of an anomaly, but instead indicates some degree of uncertainty as to which is the most appropriate EM source model. This ambiguity results from the combination of effects from two or more conductive sources, such as overburden and bedrock, gradational changes, or moderately shallow dips. The presence of a conductive upper layer has a tendency to mask or alter the characteristics of bedrock conductors, making interpretation difficult. This problem is further exacerbated in the presence of magnetite.

In areas where EM responses are evident primarily on the quadrature components, zones of poor conductivity are indicated. Where these responses are coincident with magnetic anomalies, it is possible that the in-phase component amplitudes have been suppressed by the effects of magnetite. Poorly-conductive magnetic features can give rise to resistivity anomalies that are only slightly below or slightly above background. If it is expected that poorly-conductive economic mineralization could be associated with magnetite-rich units, most of these weakly anomalous features will be of interest. In areas where magnetite

causes the in-phase components to become negative, the apparent conductance and depth of EM anomalies will be unreliable. Magnetite effects usually give rise to overstated (higher) resistivity values and understated (shallow) depth calculations.

The third class consists of cultural anomalies which are usually given the symbol "L" or "L?". Anomalies in this category can include telephone or power lines, pipelines, railways, fences, metal bridges or culverts, buildings and other metallic structures.

It is impractical to assess the relative merits of EM anomalies on the basis of conductance. It is recommended that an attempt be made to compile a suite of geophysical "signatures" over any known areas of interest. Anomaly characteristics are clearly defined on the multiparameter geophysical data profiles that are supplied as one of the survey products.

## Mine Center/ Bad Vermilion Lake

Area A was flown as an infill area within Area B but with a tighter line spacing; 100m vs. 200m; and with the traverse lines flown perpendicular from those in area B. As expected, these two blocks reveal the same anomalous zones but the zones within Area A yield more detail due to the tighter line spacing. As result of the two different line directions, there are some subtle differences with respect to anomaly shapes between the two areas.

A regional scale paged sized geology map was provide by Q-Gold (Ontario) Ltd. and was used as an aid to the geophysical interpretation.

#### Areas A and B

Many of the resistivity patterns appear to be strongly influenced by conductive overburden such as swamps, streams and lakes. However, there are areas where good correlation exists between the resistivity and magnetic patterns. This suggests the resistivity data is also responding to bedrock and structural features.

A large magnetic low was mapped near the center of the survey block, labelled as M1, on the EM anomaly maps. It strikes in an approximate 30°/210° direction and extends for over 8500 metres. This magnetic low is coincident with a resistive unit identified on both the 7200 Hz and 900 Hz resistivity maps. This zone is also well defined on the calculated vertical magnetic gradient map as a region of low relief magnetic patterns. However, a few weakly magnetic linears are mapped within this unit trending in an approximate 30°/210° direction. There appear to be a few subtle crosscutting breaks within the magnetic patterns across this zone. Many of these breaks are better defined within the Area A datasets due to the different line direction and tighter line spacing.

Several gold showing and two mines, Foley Mine and Golden Star Mine, are identified on the geology map that occur either within this low magnetic and resistive unit or along its margins. Further work should be undertaken to determine the relationship of these two mines and the gold showings with the geophysical datasets.

Several long narrow linear magnetic features are located southeast of this central zone. Many trend parallel with this zone but towards the southern extents of the survey block, the magnetic trends display an east/west strike direction. As well, near the northeast edge of the survey area, the magnetic features yield a trend angle closer to a NE/SW direction. The conductive trends generally parallel the magnetic strike directions.

Along the northwest flank of Zone M1, a narrow linear magnetic and conductive trend has been mapped. This feature may be mapping a structure break, shear zone or contact between differing rock types.

Northwest of Zone M1 the calculated vertical magnetic gradient data becomes more active, as several moderately well defined magnetic trends have been identified which strike approximately in a 30°/210° direction. Several north/south trending structural breaks can be inferred from the magnetic data. Many other crosscutting features are also evident within the data that yield various strike directions. A few of the more predominate inferred breaks have been identified on the EM anomaly maps, some of which are coincident with conductive trends.

Near the western edge of the survey block a magnetic dyke-like feature has been mapped. It is located along the edge of Bad Vermilion Lake and extends across the survey block striking in an approximate NE/SW direction. Near the northern edge of Area B and into Area C, the strike direction changes to become east/west.

#### Area C

The magnetic data displays a predominate east/west strike direction within the northern portion of the survey block. The magnetic data is also quite active within this region as evident by both the calculated vertical gradient data and the total field magnetic data. Several crosscutting breaks of various strike directions can be inferred from the magnetic data. There appears to be at least three north/south trending magnetic features that parallel the line direction. Two have been identified on the EM anomaly map and are evident in the total field magnetic data. The third is a weak response, it is located along line 30150, and is best highlighted in the vertical magnetic gradient data.

Near the southern edge of the survey block, the magnetic patterns become less active and the magnetic amplitudes are much lower. Most of the magnetic trends yield a strike direction of approximately 60°/240°.

The resistivity data appears to be strongly influenced by conductive surficial material similar to Areas A and B. The EM data is contaminated by the numerous cultural features in the area. These cultural features include buildings, power lines and railway tracks.

A highly conductive narrow linear trend is mapped trending east/west along the northern edge of the survey block. This feature corresponds the Quetico Fault as identified on the geology map.

The Mine Centre is located near the intersection of line 30160 and tie line 39010. It is located along an east/west magnetic unit near the contact between a weakly conductive unit and a resistive unit. The Mine Center is also located in close proximity to two crosscutting features. The first break trends in an approximate 130°/310° direction as inferred from the magnetic datasets. The second feature yields a north/south trend direction and appears as a subtle magnetic high within the calculated vertical magnetic dataset. It is coincident with line 30150. Several other gold showings are marked on the geology map and are in close proximity to the east/west trending magnetic linear features.

### 8. CONCLUSIONS AND RECOMMENDATIONS

This report provides a very brief description of the survey results and describes the equipment, data processing procedures and logistics of the survey.

The survey was successful in locating several anomalous conductive and/or magnetic zones that may warrant additional work. The various maps included with this report display the magnetic and conductive properties of the survey areas. It is recommended that a complete assessment and detailed evaluation of the survey results be carried out, in conjunction with all available geophysical, geological and geochemical information. Particular reference should be made to the multi-parameter data profiles that clearly define the characteristics of the individual anomalies.

Many of the conductive anomalies have been attributed to conductive overburden but some do coincide with magnetic gradients that may reflect contacts, faults or shears. Such structural breaks are considered to be of particular interest as they may have influenced mineral deposition within the survey area.

The interpreted bedrock conductors and anomalous targets defined by the survey should be subjected to further investigation, using appropriate surface exploration techniques.

Anomalies that are currently considered to be of moderately low priority may require upgrading if follow-up results are favourable.

- 8.2 -

It is also recommended that image processing of existing geophysical data be considered,

in order to extract the maximum amount of information from the survey results. Current

software and imaging techniques often provide valuable information on structure and

lithology, which may not be clearly evident on the contour and colour maps. These

techniques can yield images that define subtle, but significant, structural details.

Respectfully submitted,

FUGRO AIRBORNE SURVEYS CORP.

Douglas Garrie Geophysicist

DGG/sdp

R06040

### APPENDIX A

#### LIST OF PERSONNEL

The following personnel were involved in the acquisition, processing, interpretation and presentation of data, relating to a DIGHEM airborne geophysical survey carried out for Q-Gold (Ontario) Ltd., near Fort Frances, Ontario.

David Miles Manager, Helicopter Operations

Emily Farquhar Manager, Data Processing and Interpretation

Jazz Bola Senior Geophysical Operator

Sheli Droszio Field Geophysicist

Geo Rawlings Pilot (Questral Helicopters Ltd.)
Roger Morrow Pilot (Questral Helicopters Ltd.)
Allan Savard Pilot (Questral Helicopters Ltd.)
Russell Imrie Geophysical Data Processor
Lesley Minty Geophysical Data Processor
Douglas Garrie Interpretation Geophysicist

Lyn Vanderstarren Drafting Supervisor

Susan Pothiah Word Processing Operator

Albina Tonello Secretary/Expeditor

The survey consisted of 1516 km of coverage, flown from May 6 to May 26, 2006.

All personnel are employees of Fugro Airborne Surveys, except for the pilots who are employees of Questral Helicopters Ltd.

APPENDIX B

BACKGROUND INFORMATION

#### **APPENDIX B**

#### BACKGROUND INFORMATION

## **Electromagnetics**

Fugro electromagnetic responses fall into two general classes, discrete and broad. The discrete class consists of sharp, well-defined anomalies from discrete conductors such as sulphide lenses and steeply dipping sheets of graphite and sulphides. The broad class consists of wide anomalies from conductors having a large horizontal surface such as flatly dipping graphite or sulphide sheets, saline water-saturated sedimentary formations, conductive overburden and rock, kimberlite pipes and geothermal zones. A vertical conductive slab with a width of 200 m would straddle these two classes.

The vertical sheet (half plane) is the most common model used for the analysis of discrete conductors. All anomalies plotted on the geophysical maps are analyzed according to this model. The following section entitled **Discrete Conductor Analysis** describes this model in detail, including the effect of using it on anomalies caused by broad conductors such as conductive overburden.

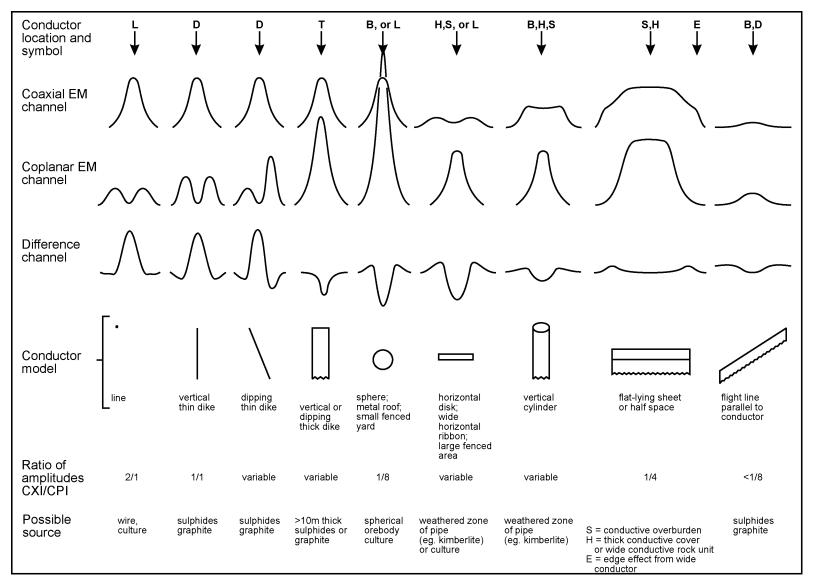
The conductive earth (half-space) model is suitable for broad conductors. Resistivity contour maps result from the use of this model. A later section entitled **Resistivity Mapping** describes the method further, including the effect of using it on anomalies caused by discrete conductors such as sulphide bodies.

# **Geometric Interpretation**

The geophysical interpreter attempts to determine the geometric shape and dip of the conductor. Figure B-1 shows typical HEM anomaly shapes which are used to guide the geometric interpretation.

# **Discrete Conductor Analysis**

The EM anomalies appearing on the electromagnetic map are analyzed by computer to give the conductance (i.e., conductivity-thickness product) in siemens (mhos) of a vertical sheet model. This is done regardless of the interpreted geometric shape of the conductor. This is not an unreasonable procedure, because the computed conductance increases as the electrical quality of the conductor increases, regardless of its true shape. DIGHEM anomalies are divided into seven grades of conductance, as shown in Table B-1. The conductance in siemens (mhos) is the reciprocal of resistance in ohms.



Typical HEM anomaly shapes Figure B-1

The conductance value is a geological parameter because it is a characteristic of the conductor alone. It generally is independent of frequency, flying height or depth of burial, apart from the averaging over a greater portion of the conductor as height increases. Small anomalies from deeply buried strong conductors are not confused with small anomalies from shallow weak conductors because the former will have larger conductance values.

**Table B-1. EM Anomaly Grades** 

Anomaly Grade	Siemens
7	> 100
6	50 - 100
5	20 - 50
4	10 - 20
3	5 - 10
2	1 - 5
1	< 1

Conductive overburden generally produces broad EM responses which may not be shown as anomalies on the geophysical maps. However, patchy conductive overburden in otherwise resistive areas can yield discrete anomalies with a conductance grade (cf. Table B-1) of 1, 2 or even 3 for conducting clays which have resistivities as low as 50 ohm-m. In areas where ground resistivities are below 10 ohm-m, anomalies caused by weathering variations and similar causes can have any conductance grade. The anomaly shapes from the multiple coils often allow such conductors to be recognized, and these are indicated by the letters S, H, and sometimes E on the geophysical maps (see EM legend on maps).

For bedrock conductors, the higher anomaly grades indicate increasingly higher conductances. Examples: the New Insco copper discovery (Noranda, Canada) yielded a grade 5 anomaly, as did the neighbouring copper-zinc Magusi River ore body; Mattabi (copper-zinc, Sturgeon Lake, Canada) and Whistle (nickel, Sudbury, Canada) gave grade 6; and the Montcalm nickel-copper discovery (Timmins, Canada) yielded a grade 7 anomaly. Graphite and sulphides can span all grades but, in any particular survey area, field work may show that the different grades indicate different types of conductors.

Strong conductors (i.e., grades 6 and 7) are characteristic of massive sulphides or graphite. Moderate conductors (grades 4 and 5) typically reflect graphite or sulphides of a less massive character, while weak bedrock conductors (grades 1 to 3) can signify poorly connected graphite or heavily disseminated sulphides. Grades 1 and 2 conductors may not respond to ground EM equipment using frequencies less than 2000 Hz.

The presence of sphalerite or gangue can result in ore deposits having weak to moderate conductances. As an example, the three million ton lead-zinc deposit of Restigouche

Mining Corporation near Bathurst, Canada, yielded a well-defined grade 2 conductor. The 10 percent by volume of sphalerite occurs as a coating around the fine grained massive pyrite, thereby inhibiting electrical conduction. Faults, fractures and shear zones may produce anomalies that typically have low conductances (e.g., grades 1 to 3). Conductive rock formations can yield anomalies of any conductance grade. The conductive materials in such rock formations can be salt water, weathered products such as clays, original depositional clays, and carbonaceous material.

For each interpreted electromagnetic anomaly on the geophysical maps, a letter identifier and an interpretive symbol are plotted beside the EM grade symbol. The horizontal rows of dots, under the interpretive symbol, indicate the anomaly amplitude on the flight record. The vertical column of dots, under the anomaly letter, gives the estimated depth. In areas where anomalies are crowded, the letter identifiers, interpretive symbols and dots may be obliterated. The EM grade symbols, however, will always be discernible, and the obliterated information can be obtained from the anomaly listing appended to this report.

The purpose of indicating the anomaly amplitude by dots is to provide an estimate of the reliability of the conductance calculation. Thus, a conductance value obtained from a large ppm anomaly (3 or 4 dots) will tend to be accurate whereas one obtained from a small ppm anomaly (no dots) could be quite inaccurate. The absence of amplitude dots indicates that the anomaly from the coaxial coil-pair is 5 ppm or less on both the in-phase and quadrature channels. Such small anomalies could reflect a weak conductor at the surface or a stronger conductor at depth. The conductance grade and depth estimate illustrates which of these possibilities fits the recorded data best.

There are a number of factors that can produce an error in the depth estimate, including the averaging of topographic variations by the altimeter, overlying conductive overburden, and the location and attitude of the conductor relative to the flight line. Conductor location and attitude can provide an erroneous depth estimate because the stronger part of the conductor may be deeper or to one side of the flight line, or because it has a shallow dip. A heavy tree cover can also produce errors in depth estimates. This is because the depth estimate is computed as the distance of bird from conductor, minus the altimeter reading. The altimeter can lock onto the top of a dense forest canopy. This situation yields an erroneously large depth estimate but does not affect the conductance estimate.

Dip symbols are used to indicate the direction of dip of conductors. These symbols are used only when the anomaly shapes are unambiguous, which usually requires a fairly resistive environment.

A further interpretation is presented on the EM map by means of the line-to-line correlation of bedrock anomalies, which is based on a comparison of anomaly shapes on adjacent lines. This provides conductor axes that may define the geological structure over portions of the survey area. The absence of conductor axes in an area implies that anomalies could not be correlated from line to line with reasonable confidence.

The electromagnetic anomalies are designed to provide a correct impression of conductor quality by means of the conductance grade symbols. The symbols can stand alone with geology when planning a follow-up program. The actual conductance values are printed in the attached anomaly list for those who wish quantitative data. The anomaly ppm and depth are indicated by inconspicuous dots which should not distract from the conductor patterns, while being helpful to those who wish this information. The map provides an interpretation of conductors in terms of length, strike and dip, geometric shape, conductance, depth, and thickness. The accuracy is comparable to an interpretation from a high quality ground EM survey having the same line spacing.

The appended EM anomaly list provides a tabulation of anomalies in ppm, conductance, and depth for the vertical sheet model. No conductance or depth estimates are shown for weak anomalous responses that are not of sufficient amplitude to yield reliable calculations.

Since discrete bodies normally are the targets of EM surveys, local base (or zero) levels are used to compute local anomaly amplitudes. This contrasts with the use of true zero levels which are used to compute true EM amplitudes. Local anomaly amplitudes are shown in the EM anomaly list and these are used to compute the vertical sheet parameters of conductance and depth.

#### **Questionable Anomalies**

The EM maps may contain anomalous responses that are displayed as asterisks (\*). These responses denote weak anomalies of indeterminate conductance, which may reflect one of the following: a weak conductor near the surface, a strong conductor at depth (e.g., 100 to 120 m below surface) or to one side of the flight line, or aerodynamic noise. Those responses that have the appearance of valid bedrock anomalies on the flight profiles are indicated by appropriate interpretive symbols (see EM legend on maps). The others probably do not warrant further investigation unless their locations are of considerable geological interest.

#### The Thickness Parameter

A comparison of coaxial and coplanar shapes can provide an indication of the thickness of a steeply dipping conductor. The amplitude of the coplanar anomaly (e.g., CPI channel) increases relative to the coaxial anomaly (e.g., CXI) as the apparent thickness increases, i.e., the thickness in the horizontal plane. (The thickness is equal to the conductor width if the conductor dips at 90 degrees and strikes at right angles to the flight line.) This report refers to a conductor as thin when the thickness is likely to be less than 3 m, and thick when in excess of 10 m. Thick conductors are indicated on the EM map by parentheses "( )". For base metal exploration in steeply dipping geology, thick conductors can be high priority targets because many massive sulphide ore bodies are thick. The system cannot

sense the thickness when the strike of the conductor is subparallel to the flight line, when the conductor has a shallow dip, when the anomaly amplitudes are small, or when the resistivity of the environment is below 100 ohm-m.

## **Resistivity Mapping**

Resistivity mapping is useful in areas where broad or flat lying conductive units are of interest. One example of this is the clay alteration which is associated with Carlin-type deposits in the south west United States. The resistivity parameter was able to identify the clay alteration zone over the Cove deposit. The alteration zone appeared as a strong resistivity low on the 900 Hz resistivity parameter. The 7,200 Hz and 56,000 Hz resistivities showed more detail in the covering sediments, and delineated a range front fault. This is typical in many areas of the south west United States, where conductive near surface sediments, which may sometimes be alkalic, attenuate the higher frequencies.

Resistivity mapping has proven successful for locating diatremes in diamond exploration. Weathering products from relatively soft kimberlite pipes produce a resistivity contrast with the unaltered host rock. In many cases weathered kimberlite pipes were associated with thick conductive layers that contrasted with overlying or adjacent relatively thin layers of lake bottom sediments or overburden.

Areas of widespread conductivity are commonly encountered during surveys. These conductive zones may reflect alteration zones, shallow-dipping sulphide or graphite-rich units, saline ground water, or conductive overburden. In such areas, EM amplitude changes can be generated by decreases of only 5 m in survey altitude, as well as by increases in conductivity. The typical flight record in conductive areas is characterized by in-phase and quadrature channels that are continuously active. Local EM peaks reflect either increases in conductivity of the earth or decreases in survey altitude. For such conductive areas, apparent resistivity profiles and contour maps are necessary for the correct interpretation of the airborne data. The advantage of the resistivity parameter is that anomalies caused by altitude changes are virtually eliminated, so the resistivity data reflect only those anomalies caused by conductivity changes. The resistivity analysis also helps the interpreter to differentiate between conductive bedrock and conductive overburden. For example, discrete conductors will generally appear as narrow lows on the contour map and broad conductors (e.g., overburden) will appear as wide lows.

The apparent resistivity is calculated using the pseudo-layer (or buried) half-space model defined by Fraser (1978)<sup>6</sup>. This model consists of a resistive layer overlying a conductive

Resistivity mapping with an airborne multicoil electromagnetic system: Geophysics, v. 43, p.144-172

half-space. The depth channels give the apparent depth below surface of the conductive material. The apparent depth is simply the apparent thickness of the overlying resistive layer. The apparent depth (or thickness) parameter will be positive when the upper layer is more resistive than the underlying material, in which case the apparent depth may be quite close to the true depth.

The apparent depth will be negative when the upper layer is more conductive than the underlying material, and will be zero when a homogeneous half-space exists. The apparent depth parameter must be interpreted cautiously because it will contain any errors that might exist in the measured altitude of the EM bird (e.g., as caused by a dense tree cover). The inputs to the resistivity algorithm are the in-phase and quadrature components of the coplanar coil-pair. The outputs are the apparent resistivity of the conductive half-space (the source) and the sensor-source distance. The flying height is not an input variable, and the output resistivity and sensor-source distance are independent of the flying height when the conductivity of the measured material is sufficient to yield significant in-phase as well as quadrature responses. The apparent depth, discussed above, is simply the sensor-source distance minus the measured altitude or flying height. Consequently, errors in the measured altitude will affect the apparent depth parameter but not the apparent resistivity parameter.

The apparent depth parameter is a useful indicator of simple layering in areas lacking a heavy tree cover. Depth information has been used for permafrost mapping, where positive apparent depths were used as a measure of permafrost thickness. However, little quantitative use has been made of negative apparent depths because the absolute value of the negative depth is not a measure of the thickness of the conductive upper layer and, therefore, is not meaningful physically. Qualitatively, a negative apparent depth estimate usually shows that the EM anomaly is caused by conductive overburden. Consequently, the apparent depth channel can be of significant help in distinguishing between overburden and bedrock conductors.

# Interpretation in Conductive Environments

Environments having low background resistivities (e.g., below 30 ohm-m for a 900 Hz system) yield very large responses from the conductive ground. This usually prohibits the recognition of discrete bedrock conductors. However, Fugro data processing techniques produce three parameters that contribute significantly to the recognition of bedrock conductors in conductive environments. These are the in-phase and quadrature difference channels (DIFI and DIFQ, which are available only on systems with "common" frequencies on orthogonal coil pairs), and the resistivity and depth channels (RES and DEP) for each coplanar frequency.

The EM difference channels (DIFI and DIFQ) eliminate most of the responses from conductive ground, leaving responses from bedrock conductors, cultural features (e.g., telephone lines, fences, etc.) and edge effects. Edge effects often occur near the

perimeter of broad conductive zones. This can be a source of geologic noise. While edge effects yield anomalies on the EM difference channels, they do not produce resistivity anomalies. Consequently, the resistivity channel aids in eliminating anomalies due to edge effects. On the other hand, resistivity anomalies will coincide with the most highly conductive sections of conductive ground, and this is another source of geologic noise. The recognition of a bedrock conductor in a conductive environment therefore is based on the anomalous responses of the two difference channels (DIFI and DIFQ) and the resistivity channels (RES). The most favourable situation is where anomalies coincide on all channels.

The DEP channels, which give the apparent depth to the conductive material, also help to determine whether a conductive response arises from surficial material or from a conductive zone in the bedrock. When these channels ride above the zero level on the depth profiles (i.e., depth is negative), it implies that the EM and resistivity profiles are responding primarily to a conductive upper layer, i.e., conductive overburden. If the DEP channels are below the zero level, it indicates that a resistive upper layer exists, and this usually implies the existence of a bedrock conductor. If the low frequency DEP channel is below the zero level and the high frequency DEP is above, this suggests that a bedrock conductor occurs beneath conductive cover.

## **Reduction of Geologic Noise**

Geologic noise refers to unwanted geophysical responses. For purposes of airborne EM surveying, geologic noise refers to EM responses caused by conductive overburden and magnetic permeability. It was mentioned previously that the EM difference channels (i.e., channel DIFI for in-phase and DIFQ for quadrature) tend to eliminate the response of conductive overburden.

Magnetite produces a form of geological noise on the in-phase channels. Rocks containing less than 1% magnetite can yield negative in-phase anomalies caused by magnetic permeability. When magnetite is widely distributed throughout a survey area, the in-phase EM channels may continuously rise and fall, reflecting variations in the magnetite percentage, flying height, and overburden thickness. This can lead to difficulties in recognizing deeply buried bedrock conductors, particularly if conductive overburden also exists. However, the response of broadly distributed magnetite generally vanishes on the in-phase difference channel DIFI. This feature can be a significant aid in the recognition of conductors that occur in rocks containing accessory magnetite.

# **EM Magnetite Mapping**

The information content of HEM data consists of a combination of conductive eddy current responses and magnetic permeability responses. The secondary field resulting from conductive eddy current flow is frequency-dependent and consists of both in-phase and quadrature components, which are positive in sign. On the other hand, the secondary field

resulting from magnetic permeability is independent of frequency and consists of only an in-phase component which is negative in sign. When magnetic permeability manifests itself by decreasing the measured amount of positive in-phase, its presence may be difficult to recognize. However, when it manifests itself by yielding a negative in-phase anomaly (e.g., in the absence of eddy current flow), its presence is assured. In this latter case, the negative component can be used to estimate the percent magnetite content.

A magnetite mapping technique, based on the low frequency coplanar data, can be complementary to magnetometer mapping in certain cases. Compared to magnetometry, it is far less sensitive but is more able to resolve closely spaced magnetite zones, as well as providing an estimate of the amount of magnetite in the rock. The method is sensitive to 1/4% magnetite by weight when the EM sensor is at a height of 30 m above a magnetitic half-space. It can individually resolve steep dipping narrow magnetite-rich bands which are separated by 60 m. Unlike magnetometry, the EM magnetite method is unaffected by remanent magnetism or magnetic latitude.

The EM magnetite mapping technique provides estimates of magnetite content which are usually correct within a factor of 2 when the magnetite is fairly uniformly distributed. EM magnetite maps can be generated when magnetic permeability is evident as negative inphase responses on the data profiles.

Like magnetometry, the EM magnetite method maps only bedrock features, provided that the overburden is characterized by a general lack of magnetite. This contrasts with resistivity mapping which portrays the combined effect of bedrock and overburden.

# The Susceptibility Effect

When the host rock is conductive, the positive conductivity response will usually dominate the secondary field, and the susceptibility effect will appear as a reduction in the inphase, rather than as a negative value. The in-phase response will be lower than would be predicted by a model using zero susceptibility. At higher frequencies the in-phase conductivity response also gets larger, so a negative magnetite effect observed on the low frequency might not be observable on the higher frequencies, over the same body. The susceptibility effect is most obvious over discrete magnetite-rich zones, but also occurs over uniform geology such as a homogeneous half-space.

Magnetic susceptibility and permeability are two measures of the same physical property. Permeability is generally given as relative permeability,  $\mu_r$ , which is the permeability of the substance divided by the permeability of free space (4  $\pi$  x 10<sup>-7</sup>). Magnetic susceptibility k is related to permeability by  $k=\mu^r-1$ . Susceptibility is a unitless measurement, and is usually reported in units of 10<sup>-6</sup>. The typical range of susceptibilities is -1 for quartz, 130 for pyrite, and up to 5 x 10<sup>-5</sup> for magnetite, in 10<sup>-6</sup> units (Telford et al, 1986).

High magnetic susceptibility will affect the calculated apparent resistivity, if only conductivity is considered. Standard apparent resistivity algorithms use a homogeneous half-space model, with zero susceptibility. For these algorithms, the reduced in-phase response will, in most cases, make the apparent resistivity higher than it should be. It is important to note that there is nothing wrong with the data, nor is there anything wrong with the processing algorithms. The apparent difference results from the fact that the simple geological model used in processing does not match the complex geology.

# **Measuring and Correcting the Magnetite Effect**

Theoretically, it is possible to calculate (forward model) the combined effect of electrical conductivity and magnetic susceptibility on an EM response in all environments. The difficulty lies, however, in separating out the susceptibility effect from other geological effects when deriving resistivity and susceptibility from EM data.

Over a homogeneous half-space, there is a precise relationship between in-phase, quadrature, and altitude. These are often resolved as phase angle, amplitude, and altitude. Within a reasonable range, any two of these three parameters can be used to calculate the half space resistivity. If the rock has a positive magnetic susceptibility, the in-phase component will be reduced and this departure can be recognized by comparison to the other parameters.

The algorithm used to calculate apparent susceptibility and apparent resistivity from HEM data, uses a homogeneous half-space geological model. Non half-space geology, such as horizontal layers or dipping sources, can also distort the perfect half-space relationship of the three data parameters. While it may be possible to use more complex models to calculate both rock parameters, this procedure becomes very complex and time-consuming. For basic HEM data processing, it is most practical to stick to the simplest geological model.

Magnetite reversals (reversed in-phase anomalies) have been used for many years to calculate an "FeO" or magnetite response from HEM data (Fraser, 1981). However, this technique could only be applied to data where the in-phase was observed to be negative, which happens when susceptibility is high and conductivity is low.

# **Applying Susceptibility Corrections**

Resistivity calculations done with susceptibility correction may change the apparent resistivity. High-susceptibility conductors, that were previously masked by the susceptibility effect in standard resistivity algorithms, may become evident. In this case the susceptibility corrected apparent resistivity is a better measure of the actual resistivity of the earth. However, other geological variations, such as a deep resistive layer, can also reduce the in-phase by the same amount. In this case, susceptibility correction would not be the best method. Different geological models can apply in different areas of the same

data set. The effects of susceptibility, and other effects that can create a similar response, must be considered when selecting the resistivity algorithm.

## Susceptibility from EM vs Magnetic Field Data

The response of the EM system to magnetite may not match that from a magnetometer survey. First, HEM-derived susceptibility is a rock property measurement, like resistivity. Magnetic data show the total magnetic field, a measure of the potential field, not the rock property. Secondly, the shape of an anomaly depends on the shape and direction of the source magnetic field. The electromagnetic field of HEM is much different in shape from the earth's magnetic field. Total field magnetic anomalies are different at different magnetic latitudes; HEM susceptibility anomalies have the same shape regardless of their location on the earth.

In far northern latitudes, where the magnetic field is nearly vertical, the total magnetic field measurement over a thin vertical dike is very similar in shape to the anomaly from the HEM-derived susceptibility (a sharp peak over the body). The same vertical dike at the magnetic equator would yield a negative magnetic anomaly, but the HEM susceptibility anomaly would show a positive susceptibility peak.

# **Effects of Permeability and Dielectric Permittivity**

Resistivity algorithms that assume free-space magnetic permeability and dielectric permittivity, do not yield reliable values in highly magnetic or highly resistive areas. Both magnetic polarization and displacement currents cause a decrease in the in-phase component, often resulting in negative values that yield erroneously high apparent resistivities. The effects of magnetite occur at all frequencies, but are most evident at the lowest frequency. Conversely, the negative effects of dielectric permittivity are most evident at the higher frequencies, in resistive areas.

The table below shows the effects of varying permittivity over a resistive (10,000 ohm-m) half space, at frequencies of 56,000 Hz (DIGHEM<sup>V</sup>) and 102,000 Hz (RESOLVE).

# Apparent Resistivity Calculations Effects of Permittivity on In-phase/Quadrature/Resistivity

Freq	Coil	Sep	Thres	Alt	ln	Quad	Арр	App Depth	Permittivity
•	Con	•							1 Cillitativity
(Hz)		(m)	(ppm)	(m)	Phase	Phase	Res	(m)	
56,000	CP	6.3	0.1	30	7.3	35.3	10118	-1.0	1 Air
56,000	CP	6.3	0.1	30	3.6	36.6	19838	-13.2	5 Quartz
56,000	CP	6.3	0.1	30	-1.1	38.3	81832	-25.7	10 Epidote
56,000	CP	6.3	0.1	30	-10.4	42.3	76620	-25.8	20 Granite
56,000	CP	6.3	0.1	30	-19.7	46.9	71550	-26.0	30 Diabase

56,000	СР	6.3	0.1	30	-28.7	52.0	66787	-26.1	40 Gabbro
102,000	СР	7.86	0.1	30	32.5	117.2	9409	-0.3	1 Air
102,000	CP	7.86	0.1	30	11.7	127.2	25956	-16.8	5 Quartz
102,000	СР	7.86	0.1	30	-14.0	141.6	97064	-26.5	10 Epidote
102,000	СР	7.86	0.1	30	-62.9	176.0	83995	-26.8	20 Granite
102,000	СР	7.86	0.1	30	-107.5	215.8	73320	-27.0	30 Diabase
102,000	СР	7.86	0.1	30	-147.1	259.2	64875	-27.2	40 Gabbro

Methods have been developed (Huang and Fraser, 2000, 2001) to correct apparent resistivities for the effects of permittivity and permeability. The corrected resistivities yield more credible values than if the effects of permittivity and permeability are disregarded.

# **Recognition of Culture**

Cultural responses include all EM anomalies caused by man-made metallic objects. Such anomalies may be caused by inductive coupling or current gathering. The concern of the interpreter is to recognize when an EM response is due to culture. Points of consideration used by the interpreter, when coaxial and coplanar coil-pairs are operated at a common frequency, are as follows:

- 1. Channels CXPL and CPPL monitor 60 Hz radiation. An anomaly on these channels shows that the conductor is radiating power. Such an indication is normally a guarantee that the conductor is cultural. However, care must be taken to ensure that the conductor is not a geologic body that strikes across a power line, carrying leakage currents.
- 2. A flight that crosses a "line" (e.g., fence, telephone line, etc.) yields a centre-peaked coaxial anomaly and an m-shaped coplanar anomaly. When the flight crosses the cultural line at a high angle of intersection, the amplitude ratio of coaxial/coplanar response is 2. Such an EM anomaly can only be caused by a line. The geologic body that yields anomalies most closely resembling a line is the vertically dipping thin dike. Such a body, however, yields an amplitude ratio of 1 rather than 2. Consequently, an m-shaped coplanar anomaly with a CXI/CPI amplitude ratio of 2 is virtually a guarantee that the source is a cultural line.
- A flight that crosses a sphere or horizontal disk yields centre-peaked coaxial and coplanar anomalies with a CXI/CPI amplitude ratio (i.e., coaxial/coplanar) of 1/8. In the absence of geologic bodies of this geometry, the most likely conductor is a

<sup>&</sup>lt;sup>8</sup> See Figure B-1 presented earlier.

metal roof or small fenced yard. Anomalies of this type are virtually certain to be cultural if they occur in an area of culture.

- 4. A flight that crosses a horizontal rectangular body or wide ribbon yields an m shaped coaxial anomaly and a centre-peaked coplanar anomaly. In the absence of geologic bodies of this geometry, the most likely conductor is a large fenced area.<sup>5</sup> Anomalies of this type are virtually certain to be cultural if they occur in an area of culture.
- 5. EM anomalies that coincide with culture, as seen on the camera film or video display, are usually caused by culture. However, care is taken with such coincidences because a geologic conductor could occur beneath a fence, for example. In this example, the fence would be expected to yield an m-shaped coplanar anomaly as in case #2 above. If, instead, a centre-peaked coplanar anomaly occurred, there would be concern that a thick geologic conductor coincided with the cultural line.
- 6. The above description of anomaly shapes is valid when the culture is not conductively coupled to the environment. In this case, the anomalies arise from inductive coupling to the EM transmitter. However, when the environment is quite conductive (e.g., less than 100 ohm-m at 900 Hz), the cultural conductor may be conductively coupled to the environment. In this latter case, the anomaly shapes tend to be governed by current gathering. Current gathering can completely distort the anomaly shapes, thereby complicating the identification of cultural anomalies. In such circumstances, the interpreter can only rely on the radiation channels and on the camera film or video records.

# **Magnetic Responses**

The measured total magnetic field provides information on the magnetic properties of the earth materials in the survey area. The information can be used to locate magnetic bodies of direct interest for exploration, and for structural and lithological mapping.

The total magnetic field response reflects the abundance of magnetic material in the source. Magnetite is the most common magnetic mineral. Other minerals such as ilmenite, pyrrhotite, franklinite, chromite, hematite, arsenopyrite, limonite and pyrite are also magnetic, but to a lesser extent than magnetite on average.

<sup>&</sup>lt;sup>9</sup> It is a characteristic of EM that geometrically similar anomalies are obtained from: (1) a planar conductor, and (2) a wire which forms a loop having dimensions identical to the perimeter of the equivalent planar conductor.

#### - Appendix B.14 -

In some geological environments, an EM anomaly with magnetic correlation has a greater likelihood of being produced by sulphides than one which is non-magnetic. However, sulphide ore bodies may be non-magnetic (e.g., the Kidd Creek deposit near Timmins, Canada) as well as magnetic (e.g., the Mattabi deposit near Sturgeon Lake, Canada).

Iron ore deposits will be anomalously magnetic in comparison to surrounding rock due to the concentration of iron minerals such as magnetite, ilmenite and hematite.

Changes in magnetic susceptibility often allow rock units to be differentiated based on the total field magnetic response. Geophysical classifications may differ from geological classifications if various magnetite levels exist within one general geological classification. Geometric considerations of the source such as shape, dip and depth, inclination of the earth's field and remanent magnetization will complicate such an analysis.

In general, mafic lithologies contain more magnetite and are therefore more magnetic than many sediments which tend to be weakly magnetic. Metamorphism and alteration can also increase or decrease the magnetization of a rock unit.

Textural differences on a total field magnetic contour, colour or shadow map due to the frequency of activity of the magnetic parameter resulting from inhomogeneities in the distribution of magnetite within the rock, may define certain lithologies. For example, near surface volcanics may display highly complex contour patterns with little line-to-line correlation.

Rock units may be differentiated based on the plan shapes of their total field magnetic responses. Mafic intrusive plugs can appear as isolated "bulls-eye" anomalies. Granitic intrusives appear as sub-circular zones, and may have contrasting rings due to contact metamorphism. Generally, granitic terrain will lack a pronounced strike direction, although granite gneiss may display strike.

Linear north-south units are theoretically not well-defined on total field magnetic maps in equatorial regions due to the low inclination of the earth's magnetic field. However, most stratigraphic units will have variations in composition along strike that will cause the units to appear as a series of alternating magnetic highs and lows.

Faults and shear zones may be characterized by alteration that causes destruction of magnetite (e.g., weathering) that produces a contrast with surrounding rock. Structural breaks may be filled by magnetite-rich, fracture filling material as is the case with diabase dikes, or by non-magnetic felsic material.

Faulting can also be identified by patterns in the magnetic total field contours or colours. Faults and dikes tend to appear as lineaments and often have strike lengths of several kilometres. Offsets in narrow, magnetic, stratigraphic trends also delineate structure. Sharp contrasts in magnetic lithologies may arise due to large displacements along strikeslip or dip-slip faults.

## Gamma Ray Spectrometry

Radioelement concentrations are measures of the abundance of radioactive elements in the rock. The original abundance of the radioelements in any rock can be altered by the subsequent processes of metamorphism and weathering.

Gamma radiation in the range that is measured in the thorium, potassium, uranium and total count windows is strongly attenuated by rock, overburden and water. Almost all of the total radiation measured from rock and overburden originates in the upper .5 metres. Moisture in soil and bodies of water will mask the radioactivity from underlying rock. Weathered rock materials that have been displaced by glacial, water or wind action will not reflect the general composition of the underlying bedrock. Where residual soils exist, they may reflect the composition of underlying rock except where equilibrium does not exist between the original radioelement and the products in its decay series.

Radioelement counts (expressed as counts per second) are the rates of detection of the gamma radiation from specific decaying particles corresponding to products in each radioelements decay series. The radiation source for uranium is bismuth (Bi-214), for thorium it is thallium (TI-208) and for potassium it is potassium (K-40).

The uranium and thorium radioelement concentrations are dependent on a state of equilibrium between the parent and daughter products in the decay series. Some daughter products in the uranium decay are long lived and could be removed by processes such as leaching. One product in the series, radon (Rn-222), is a gas which can easily escape. Both of these factors can affect the degree to which the calculated uranium concentrations reflect the actual composition of the source rock. Because the daughter products of thorium are relatively short lived, there is more likelihood that the thorium decay series is in equilibrium.

Lithological discrimination can be based on the measured relative concentrations and total, combined, radioactivity of the radioelements. Feldspar and mica contain potassium. Zircon, sphene and apatite are accessory minerals in igneous rocks that are sources of uranium and thorium. Monazite, thorianite, thorite, uraninite and uranothorite are also sources of uranium and thorium which are found in granites and pegmatites.

In general, the abundance of uranium, thorium and potassium in igneous rock increases with acidity. Pegmatites commonly have elevated concentrations of uranium relative to thorium. Sedimentary rocks derived from igneous rocks may have characteristic signatures that are influenced by their parent rocks, but these will have been altered by subsequent weathering and alteration.

Metamorphism and alteration will cause variations in the abundance of certain radioelements relative to each other. For example, alterative processes may cause

#### - Appendix B.16 -

uranium enrichment to the extent that a rock will be of economic interest. Uranium anomalies are more likely to be economically significant if they consist of an increase in the uranium relative to thorium and potassium, rather than a sympathetic increase in all three radioelements.

Faults can exhibit radioactive highs due to increased permeability which allows radon migration, or as lows due to structural control of drainage and fluvial sediments which attenuate gamma radiation from the underlying rocks. Faults can also be recognized by sharp contrasts in radiometric lithologies due to large strike-slip or dip-slip displacements. Changes in relative radioelement concentrations due to alteration will also define faults.

Similar to magnetics, certain rock types can be identified by their plan shapes if they also produce a radiometric contrast with surrounding rock. For example, granite intrusions will appear as sub-circular bodies, and may display concentric zonations. They will tend to lack a prominent strike direction. Offsets of narrow, continuous, stratigraphic units with contrasting radiometric signatures can identify faulting, and folding of stratigraphic trends will also be apparent.

APPENDIX C

DATA ARCHIVE DESCRIPTION

#### **APPENDIX C**

#### ARCHIVE DESCRIPTION

Reference: CCD02465

Disc 1 of 1

Archive Date: August 25, 2006

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This archive contains FINAL 2006 DATA ARCHIVES of the airborne EM and magnetometer survey conducted by FUGRO AIRBORNE SURVEYS CORP. over the Mine Centre/Bad Vermilion Lake Area, Ontario on behalf of Q Gold (Ontario) Ltd. from May 14 to May 25. Area A files have the suffix 'A'and line numbers start with 1. Area B files have the suffix 'B' and line numbers that start with 2. Area C files have the suffix 'C' and its line numbers start with 3.

Job # 06040

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****** Disc 1 of 1 ******
\README.TXT - this file
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#### GRIDS\GEOSOFT

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Grids in Geosoft binary (I*4)
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CVG-\*.GRD - Calculated Vertical Gradient of MAG-\*.GRD nT/m area \*

MAG-\*.GRD - Horizontally Enhanced Residual Magnetic Intensity nT area \*

RES56K-\*.GRD - Apparent Resistivity 55600 kHz coplanar area \*
RES900-\*.GRD - Apparent Resistivity 875 Hz coplanar area \*
RES7200-\*.GRD - Apparent Resistivity 7144 Hz coplanar area \*

DTM-\*.GRD - Digital Terain Model area \*

#### GRIDS\JPEGS

Grids with topo in jpeg format with the coordinate registration JGW files

CVG-\*.JPEG - Calculated Vertical Gradient of MAG-\*.GRD nT/m area \*

MAG-\*.JPEG - Horizontally Enhanced Residual Magnetic Intensity nT area \*

RES56K-\*.JPEG - Apparent Resistivity 55600 kHz coplanar area \* RES900-\*.JPEG - Apparent Resistivity 875 Hz coplanar area \* RES7200-\*.JPEG - Apparent Resistivity 7144 Hz coplanar area \*

DTM-\*.JPEG - Digital Terain Model area \*

#### GRIDS\GEOTIFFS

#### Grids in Geotiff format

```
TOPO*1.TIF - Topo Map area * Map Sheet 1
TOPO*2.TIF - Topo Map area * Map Sheet 2
TOPO*3.TIF - Topo Map area * Map Sheet 3
TOPO*4.TIF - Topo Map area * Map Sheet 4
```

#### - Appendix C.2 -

TOPO\*001.TIF - Topo Map area \*

37 - DEP56K

```
LINEDATA\
     AN06040-*.XYZ - EM Anomaly listing in Geosoft XYZ Format area *
     AN06040.TXT
                     - Text file documenting the contents of AN06040-*.XYZ
     ARC-06040.XYZ
                     - Geosoft ASCII Format final archive all areas
REPORT\
     06040-REP.PDF - Report in PDF format
______
The ARC-06040.XYZ file contains the following data channels:
1 - X
                       UTM EASTING NAD 83 ZONE 15N (METRES)
 2 - Y
                      UTM NORTHING NAD 83 ZONE 15N (METRES)
 3 - FID
                     FIDUCIAL
4 - Z
                     HEIGHT OF BIRD ABOVE WGS84 SPHEROID (METRES)
5 - ALTBIRD RADAR ALTIMETER HEIGHT OF BIRD ABOVE GROUND (METRES)

6 - DTM
                     DIGITAL TERRAIN MODEL (Z-ALTBIRD)(METRES)
6 - DTM
7 - MAGRAW
                     RAW TOTAL MAGNETIC INTENSITY (nT)
8 - DIURNAL
                     DIURNAL MAGNETIC VARIATION (nT)
9 - MAGLD
                      LAGGED DIURNAL CORRECTED TOTAL MAGNETIC INTENSITY (nT)
10 - IGRF
                 I NTERNATIONAL GEOMAGNETIC REFERENCE FIELD (nT)
11 - MAG
                     LEVELED IGRF PLANE REMOVED TOTAL MAGNETIC INTENSITY (nT)
12 - CPI900_R
                      UNLEVELED COPLANAR INPHASE 870 Hz (PPM)
13 - CPQ900_R
                      UNLEVELED COPLANAR QUADRATURE 870 Hz (PPM)
14 - CXI1000_R
                      UNLEVELED COAXIAL INPHASE 1128 Hz (PPM)
15 - CXQ1000_R
                      UNLEVELED COAXIAL OUADRATURE 1128 Hz (PPM)
                      UNLEVELED COAXIAL INPHASE 5692 Hz (PPM)
16 - CXI5500_R
17 - CXQ5500_R
                      UNLEVELED COAXIAL QUADRATURE 5692 Hz (PPM)
18 - CPI7200_R
                      UNLEVELED COPLANAR INPHASE 7238 Hz (PPM)
19 - CPQ7200_R
                      UNLEVELED COPLANAR QUADRATURE 7238 Hz (PPM)
20 - CPI56K_R
                      UNLEVELED COPLANAR INPHASE 55470 Hz (PPM)
21 - CPQ56K_R
                      UNLEVELED COPLANAR QUADRATURE 55470 Hz (PPM)
22 - CPI900
                     LEVELED COPLANAR INPHASE 870 Hz (PPM)
23 - CPQ900
                      LEVELED COPLANAR QUADRATURE 870 Hz (PPM)
                    LEVELED COAXIAL INPHASE 1128 Hz (PPM)
LEVELED COAXIAL QUADRATURE 1128 Hz (PPM)
24 - CXI1000
25 - CXQ1000
26 - CXI5500
                     LEVELED COAXIAL INPHASE 5692 Hz (PPM)
27 - CXQ5500
                      LEVELED COAXIAL QUADRATURE 5692 Hz (PPM)
28 - CPI7200
                     LEVELED COPLANAR INPHASE 7238 Hz (PPM)
29 - CPQ7200
                     LEVELED COPLANAR QUADRATURE 7238 Hz (PPM)
30 - CPI56K
                      LEVELED COPLANAR INPHASE 55470 Hz (PPM)
31 - CPQ56K
                      LEVELED COPLANAR QUADRATURE 55470 Hz (PPM)
32 - RES900
                     APPARENT RESISTIVITY 870 Hz COPLANAR (OHM*M)
33 - RES7200
                     APPARENT RESISTIVITY 7238 Hz COPLANAR (OHM*M)
34 - RES56K
                     APPARENT RESISTIVITY 55470 Hz COPLANAR (OHM*M)
35 - DEP900
                     APPARENT DEPTH 870 Hz COPLANAR (M)
36 - DEP7200
                     APPARENT DEPTH 7238 Hz COPLANAR (M)
```

APPARENT DEPTH 55470 Hz COPLANAR (M)

### - Appendix C.3 -

4 1	DT TOUR	DI TOUR MINDED
40 -	CXSP	COAXIAL SPHERICS MONITOR
39 -	CPSP	COPLANAR SPHERICS MONITOR
38 -	CPPL	COPLANAR POWERLINE MONITOR

41 - FLIGHT FLIGHT NUMBER 42 - DATE DATE YYYY/MM/DD

\_\_\_\_\_\_

All EM data in the archive is presented in the standard normalization convention for the coplanar coils. The ratio of coplanar to coaxial amplitudes for the same frequency is 4:1 over a layered earth.

Resistivity is calculated using a proprietary pseudo-layer half-space algorithm.

\_\_\_\_\_\_

The coordinate system for all grids and XYZ files is projected as follows

Datum NAD 83 Spheroid GRS-80 Projection UTM Central meridian 93 West False easting 500000 False northing Scale factor 0.9996 Northern parallel N/ABase parallel N/A

WGS84 to local conversion method Molodensky

Delta X shift +0
Delta Y shift +0
Delta Z shift +0

\_\_\_\_\_\_

If you have any problems with this archive please contact

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# **APPENDIX D**

**EM ANOMALY LIST** 

\_\_\_\_\_

EM Anomaly List

				 	   CX 55		CP 7	200 HZ	CP	900 HZ	Vertical		   Mag. Corr	
Labe:	l Fid	Interp		YUTM	Real	Quad	Real	Quad	Real	~	!	DEPTH*		ļ
			m	m	ppm	ppm	ppm	ppm	ppm	n ppm	siemens	m	NT	
LINE	10011		FLIGHT	17	 						 I		 	
A	928.9	H	520373	5390398	9.6	1.4	68.1	19.0	26.8	21.8			i o	İ
В	897.6	S	520926	5391398	4.0	12.8	9.6	9.0	0.3	1.7			i o	j
ĺС	850.4	H	521756	5392910	18.1	13.9	301.6	138.9	27.9	110.4	2.1	15	22	İ
D	802.4		522601	5394415	5.4	7.9	66.8	140.8	1.2	22.3	i		25	İ
E	784.8	S	522864	5394925	15.6	17.4	115.8	304.1	1.2	46.8	1.3	10	j o	j
F	764.0	S	523189	5395489	7.7	23.8	250.2	467.5	2.3	82.7	0.4	0	95	İ
G	730.2	S	523700	5396422	10.3	23.6	65.5	227.2	1.7	34.1	j		j o	j
Н	700.4	S	524165	5397239	9.2	9.7	113.4	184.6	3.7	34.2	1.2	18	j o	j
İΙ	589.5	S	525906	5400402	1.8	5.6	179.3	192.1	13.2	43.7	j		j o	j
jЈ	552.7	S	526380	5401284	2.2	10.6	37.5	44.0	46.3	12.3	i		j o	į
K	547.2	L	526431	5401381	16.8	13.2	24.5	30.7	5.7	15.0	j		0	į
LINE	10020		FLIGHT	 12	 I						 I		 I	
A	1399.8	S?	520355	5390169	33.9	60.7	258.5	336.5	15.6	94.2	1.1	0	0	l I
l B	1405.2		520440	5390329	15.3	17.3	105.3	85.7	18.3	46.1	1.3	10	] 0	
I C	1429.9		520440	5391030	6.5	8.6	37.8	106.7	2.0	16.2	0.8	2	0	
D D	1439.4		5210041	5391322	6.8	18.3	29.3	86.2	0.5	11.7	0.4	0	26	-
E	1449.4		521175	5391642	6.7	16.2	5.5	39.9	1.3	5.9	0.5	0	1 0	
F	1463.9		521450	5392125	9.7	21.5	238.5	419.0	4.5	74.8	0.6	5	j 0	l
l G	1488.1		521862	5392866	47.4	43.5	720.5	490.1	78.1	276.5	2.4	6	j 0	l
H	1495.1		521989	5393092	17.1	16.5	192.3	244.6	5.5	65.6	1.6	9	0	
II	1513.6		522309	5393674	0.0	6.2	20.5	107.2	1.0	13.7	l		0   6	
<del> </del>   J	1522.4		522460	5393953	8.7	9.8	11.6	89.5	1.6	12.1	 		] 0 ] 9	
K	1535.1		522689	5394347	10.8	27.7	31.6	177.9	1.9	24.9	! 		i o	
L	1552.1		522994	5394907	8.6	17.5	30.5	95.4	1.3	14.5	! 		14	
M	1568.5		523304	5395477	10.8	39.0	298.8	457.6	6.1	100.3	0.4	0	55	
N N	1586.6		523627	5396039	8.8	12.9	4.6	20.9	0.5	3.3	0.4 		16	
0	1602.4		523905	5396536	1.2	6.5	15.1	55.2	1.2	8.3	 		16	
l P	1621.6		524250	5397172	13.7	21.6	101.4	232.7	1.9	38.0	0.9	7	1 0	
I Q	1704.6		525801	5400007	7.6	24.5	161.3	294.1	6.5	55.9	0.4	2	0	
Q  R	1727.5		526200	5400708	1.6	3.5	26.3	108.7	12.7	15.6	0.4 		0	
ls	1746.3		526542	5401321	2.1	6.7	42.4	34.0	33.7	8.0	 		] 0	
T	1747.3		526561	5401353	18.4	16.0	42.4	34.0	33.7	8.5	1.9	0	0	i
	10021				 ı									
!	10031		FLIGHT		12 -	05 0	160 5	204 6	0 0	60.3		0		ļ
A	1043.4		520464	5390137	13.5		168.5		9.9	60.3	0.7	9	0	
В	1077.9	S	520976	5391057	5.0	3.3	18.7	156.1	5.7	24.8			0	

CX = COAXIAL

\*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

CP = COPLANAR

Note: EM values shown above are local amplitudes

EM Anomaly List

					   CX 55	00 HZ	CP 7	'200 HZ	CP	900 HZ	   Vertica	 l Dike	   Mag. Corr	I
Labe	l Fid	Interr	NTUX c	YUTM	Real	Ouad	Real	Ouad	Real		!	DEPTH*		i
			m	m	ppm	ppm	ppm	ppm	ppm	~	siemens	m	NT	j
LT TATE	10021		FLIGHT	17	 I						 I			
!	10031	a			0.4	00 7	040 0	260 7	2 0	70.0	0	0	1 15	
C	1098.0		521288	5391620	9.4	23.7		360.7	3.2	72.9	0.5	0	15	
D	1111.9		521509	5392031	10.0	12.9		320.8	10.8	58.4	1.0	13	0	
E	1171.3		522388	5393606	4.5	23.9		131.6	0.9	17.7			16	
F	1181.1		522541	5393883	0.3	6.0		152.9	2.5	21.1			0	
G	1190.6		522686	5394155	5.0	20.7		121.7	1.0	17.2			8	
H	1217.8		523100	5394875	3.3	10.9	12.5	77.3	1.7	19.0			0	ļ
ļΙ	1233.5		523322	5395287	54.9	66.5		389.0		176.7	1.8	2	0	ļ
J	1256.7		523681	5395904	4.9	14.7	5.6	57.0	0.4	7.9			13	ļ
K	1266.2		523812	5396184	8.9	8.5	15.0	62.9	0.6	8.9			9	ļ
L	1276.2		523966	5396470	1.3	3.3	36.0	96.2	1.3	14.7			21	
M	1287.5		524134	5396771	12.2		194.1		1.4	73.7	0.5	0	11	
N	1298.2		524303	5397082	5.0	11.5		124.2	2.6	21.0	0.4	8	5	
0	1305.0	S	524420	5397293	9.3	17.0	31.1	83.8	3.6	11.6	0.7	4	10	
P	1326.4	H	524806	5397968	8.7	1.9	17.5	19.9	6.9	12.6			0	
Q	1397.3	S	525978	5400089	15.4	29.0	171.4	264.4	3.6	66.2	0.8	10	16	
R	1401.3	L	526044	5400195	3.3	32.5	77.4	301.2	2.1	48.5	0.1	0	0	ĺ
s	1441.0		526683	5401338	3.3	7.6	32.5	11.9	46.6	21.6	3.3	1	0	į
LITNE	10040		FLIGHT	13	 I						 		 	
A	2596.6	B?	520474	5389943	27.2	53.2	429.8	518.5	17 1	136.7	0.9	0	0	i
lB	2612.5	н	520681	5390331	11.5	15.7		109.1	8.5	45.1	1.0	5	0	ł
C	2639.5		521077	5391049	5.4		107.8		4.2	31.2	0.8	10	0	-
l D	2655.1		521342	53915049	22.2	48.7		489.2		92.9	0.8	0	0	-
E	2669.8		521595	5391971	15.1	27.9		350.5	7.7	86.1	0.8	1	0	
F	2696.1		522074	5392825	37.5	31.6			108.1		2.4	12	0	
G	2725.0		522561	5393746	12.4	42.7		205.2	1.2	30.1	0.4	0	14	
H	2723.0		522595	5393740	0.0	0.8	56.4	205.2	1.1	30.1	0.4		0	
H	2727.0	S S	522815	5393809	0.0	8.8	8.5	80.1		10.6			0	
											!	17	!	
J	2773.6	H	523413	5395248	31.4		216.0	39.9	39.0	90.1	4.9		21	
K	2793.7		523733	5395845		8.1	6.4	31.3	3.1	4.8	0.4	18	11	ļ
L	2799.9		523845	5396031	10.7	13.0	17.2	95.9	2.0	12.7	1.1	18	10	
M	2811.5	S	524042	5396380	4.3	3.5	20.5	60.3	2.4	9.5			13	
N	2820.1		524195	5396641	4.1		119.4	291.1	1.4	45.7	0.2	0	19	
0	2834.2		524406	5397041	13.9	39.6	86.4	321.1	0.0	47.3	0.5	0	29	ļ
P	2846.2		524572	5397362	13.0		161.1		3.6	53.2	0.8	7	34	ļ
Q	2864.9		524886	5397917	2.6	7.8	43.6	27.6	9.7	17.7			0	
R	2915.6		525802	5399568	0.9	2.1	10.6	13.1	7.4	5.7			0	ļ
S	2935.4	L	526161	5400224	34.6	24.2	165.4	285.7	33.7	81.2	3.0	7	0	

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					   CX 55	00 HZ	CP 7	200 HZ	 CP	900 HZ	   Vertica	 l Dike	   Mag. Corr	 
Labe	el Fid	Inter	MTUX q	YUTM	Real	Quad	Real	Quad	Real	Quad	COND	DEPTH*	į -	į
j			m	m	ppm	ppm	ppm	ppm	ppm	n ppm	siemens	m	NT	į
!	10040		FLIGHT		ļ									ļ
T	2970.6	L	526778	5401342	19.3	0.2	50.5	16.2	76.3	55.4			0	I
LINE	10050		FLIGHT	13	 						 			
A	3465.4	S?	520537	5389885	11.4	25.8	277.4	87.5	10.7	69.7	0.6	0	14	
В	3449.8	H	520801	5390359	1.4	0.0	50.4	14.2	11.1	20.5			0	
C	3425.6	S	521174	5391041	5.8	14.5	120.1	232.6	5.4	39.8	0.4	0	11	
D	3411.9	S	521396	5391420	7.9	33.5	324.1	558.4	3.2	105.6	0.3	0	17	
E	3392.8	S	521702	5391980	16.9	51.5	495.0	744.3	11.0	158.2	0.5	0	0	
F	3376.8	B?	521929	5392379	8.0	31.2	138.9	255.4	3.3	48.4	0.3	0	12	
G	3358.9	H	522154	5392802	34.0	32.2	262.9	236.0	87.6	282.0	2.1	10	0	
H	3331.5	S	522562	5393523	0.7	4.0	68.9	115.9	3.2	16.8			9	
Ī	3316.9	S	522782	5393924	5.4	20.7	14.9	137.7	1.1	19.1	0.3	0	0	į
J	3284.7	S	523285	5394824	9.9	18.5	324.4	515.4	7.5	104.0	0.7	16	0	į
K	3264.2	H	523618	5395441	46.9	70.8	805.4	899.9	36.0	251.5	1.4	3	j o	į
ļь	3247.2	S?	523900	5395941	8.1	14.7	19.8	82.2	2.0	11.4	0.6	0	14	į
ĺМ	3226.8	S	524206	5396502	6.2	14.6	66.4	218.2	1.9	31.3	0.5	1	j 20	į
N	3208.0	D	524491	5397010	1.5	9.3	6.6	20.4	1.1	2.7			i o	İ
ĺО	3194.0	S	524697	5397387	0.0	20.8	60.6	172.4	0.9	26.9			26	İ
P	3177.3	S	524981	5397895	6.6	8.2	97.5	101.8	3.0	26.8	0.9	29	j 8	į
ĺQ	3126.9	S	525788	5399364	1.3	8.4	31.0	75.6	2.8	12.9			i o	İ
Ŕ	3107.5	S	526115	5399930	8.7	19.0	6.5	32.3	0.1	6.0	0.6	1	i o	i
İs	3095.4	L	526288	5400280	29.5	25.6	112.6	221.2	59.3	54.6	2.2	5	i o	i
T	3074.8	S	526585	5400805	2.9	7.7	12.9	38.2	15.3	5.2			i o	į
ับ	3046.9	L	526872	5401314	13.1	8.7	22.7	7.8	36.2	15.1	2.3	0	0	į
	10060		FLIGHT	1 2	 I						 I			
A	3558.0	Н	520983	5390469	3.2	6.4	49.0	61.8	12.2	17.3	0.4	26	1 0	ļ
l B	3556.0	S	520963	5391059	1 4.2	3.7		126.3	2.7	22.0	0.4   1.1	20	1 0	
l C	3577.9	S	521320	5391059	4.2	13.3	143.3	284.2	1.9	48.6	0.4	0	l 8	
I D	3602.9	S	521496	5391365	21.8	28.7		473.7	5.9	86.6	1.2	9	1 42	- !
1											l .		ļ.	
E  F	3618.0	H	522009	5392301	32.8	26.6		617.0		254.5	2.4	12	11	-
	3637.9	H	522319	5392852		7.7		195.0		144.9	5.0	25 0	0   5	
G	3659.8	S	522682	5393515	4.0	18.1	15.3	92.5	1.4	12.1	0.2	-	5	ļ
H	3685.9	S	523127	5394345	12.0		131.8			60.5	0.4	0	!	- !
I	3701.0	H	523401	5394826	15.9	12.6	297.4	130.5	23.9	88.6	2.0	23	0	ļ
J	3718.4	S	523716	5395407	21.1		394.6	532.0		118.7	1.2	7	26	ļ
K	3732.5	S?	523944	5395810	10.8	12.4	8.0		0.5	6.9	1.1	13	41	ļ
L	3747.7	S	524214	5396291	6.9	17.4	40.7	109.1	0.6	17.2	0.5	0	0	

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

    Labe	l Fid	Inter	XUTM m	YUTM m	   CX 55   Real   ppm	OO HZ Quad ppm	CP 7 Real	200 HZ Quad ppm	CP Real	~	Vertica COND	 l Dike DEPTH* m	Mag. Corr       NT	     
	10060		FLIGHT	12							 I			
M	3770.0	D	524618	5397020	1.9	8.2	13.5	34.1	1.8	7.6	l I		0	ļ
N N	3776.5	S	524727	5397020	7.1	21.4	28.5	111.4	0.5	14.4	0.4	0	0	
0	3770.3	S	525111	5397892	14.1	33.2	83.4	186.0	0.9	31.8	0.4	0	14	
l P	3831.3	S	525659	5398869	3.1	21.5	146.9	367.3	3.5	60.9	0.0	0	0	
Q Q	3853.9	S	526069	5399616	8.7	13.7	130.9	180.6	7.7	45.1	0.2	19	0	l
Q   R	3874.0	L	526427	5400300	40.4	23.6	38.7	78.9	87.3	91.0	3.9	7	0	
s	3892.5	L	526717	5400300	11.6	5.9	14.6	10.9	9.5	4.0	3.9	7		
S  T	3898.0	ь	526787	5400767	18.7	11.4	73.6	63.8	11.4	28.6	3.1   2.9	2	160	
T	3090.0		520707	5400916	10. <i>/</i>		/3.0	03.0		40.0	2.9 			ا 
LINE	10070		FLIGHT	13	1									J
A	4580.9	H	521068	5390412	18.7	28.1	151.0	166.1	15.9	61.8	1.0	8	0	İ
В	4556.8	S	521442	5391086	9.5	21.6	144.3	347.3	1.6	54.6	0.6	0	0	j
C	4549.8	S?	521544	5391268	2.1	2.8	13.4	57.9	1.4	8.8	j		0	j
D	4522.8	B?	521920	5391950	30.8	25.8	120.4	171.8	15.8	41.3	2.3	13	0	j
E	4512.6	H	522069	5392225	30.1	27.5	655.6	421.6	103.7	264.3	2.1	8	0	j
F	4488.6	H	522403	5392828	22.8	19.3	441.9	381.4	38.6	201.7	2.1	16	0	į
Ġ	4465.9	S	522733	5393418	10.5	19.8	12.0	89.8	0.8	12.3	0.7	0	0	į
Н	4428.0	S	523248	5394338	13.5	16.8	233.5	292.4	5.5	65.4	1.1	9	0	į
İI	4416.4	H	523417	5394651	10.0	9.0	219.8	68.6	33.8	84.2	1.5	30	0	į
jЈ	4392.2	S?	523812	5395364	21.8	23.4	46.5	132.8	2.6	18.9	1.5	0	13	į
K	4381.0	S?	524003	5395699	6.4	19.5	45.6	127.8	1.5	18.2	0.4	0	11	į
ļь	4371.7	S	524157	5395980	2.4	6.9	30.1	109.2	0.9	15.2	i		20	İ
M	4338.6	S	524693	5396946	14.1	23.1	179.0	308.7	3.2	55.1	0.9	5	22	İ
N	4328.4	S	524852	5397250	6.1	18.6	63.9	230.9	0.8	33.1	0.4	0	15	j
jo	4319.3	S	525001	5397521	6.8	12.3	52.8	178.3	0.5	25.2	0.6	14	5	j
P	4308.2	S	525195	5397844	0.1	0.0	75.5	59.3	1.8	16.4	i		0	j
ĮQ	4300.5	S	525314	5398070	8.9	19.5	45.9	141.7	0.7	22.4	0.6	9	0	j
R	4284.0	S	525569	5398528	1.0	2.4	11.2	65.9	1.0	8.8	i		0	İ
s	4272.2	B?	525737	5398849	3.6	6.3	40.2	144.4	0.8	22.3	0.5	30	8	İ
Т	4264.5	B?	525852	5399066	4.9	25.4	44.7	251.0	1.3	35.5	0.2	0	0	İ
ប់	4232.8	S	526328	5399896	3.9	6.2	49.8	56.1	7.6	21.5	0.6	35	0	j
V	4208.0	L	526647	5400504	23.4		127.1	39.8	119.7	47.5	17.7	30	1740	j
W	4196.6	L	526774	5400737	48.0		121.9	136.2	52.0	42.6	2.0	0	0	j
X	4193.5	L	526820	5400796	0.0		121.9	87.6	52.0	42.6			36	j
Y	4189.6	L	526866	5400881	0.0		146.5		57.4	63.6			0	
	10000			12	 I						 I			 I
!	10080	a	FLIGHT		]	4 0	07 1	CO 2	2 (	11 0	 			
A	4688.4	S	520890	5389873	2.5	4.8	27.1	62.3	3.6	11.9			0	

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					   CX 55	00 HZ	CP 7	200 HZ	CP	900 HZ	Vertica	 l Dike	Mag. Corr	 
Labe	l Fid	Interp	XUTM	YUTM	Real	Quad	Real	Quad	Real	Quad	COND	DEPTH*		į
İ		_	m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	j
LINE	10080		FLIGHT	13	 						 			 
В	4706.1	Н	521121	5390294	8.6	11.8	225.3	166.4	15.5	66.4	0.9	21	j o	į
C	4735.1	S	521571	5391105	1.0	5.2	74.8	154.3	1.9	24.7	i		j o	į
D	4747.9	S	521781	5391482	4.3	6.8	35.1	82.1	1.3	12.3	0.6	5	0	į
E	4767.1	H	522099	5392075	19.2	3.2	160.4	1.3	92.2	108.8	18.1	23	0	į
F	4795.1	H	522529	5392834	18.8	20.5	408.2	341.0	20.5	125.0	1.4	9	0	ĺ
G	4814.1	S	522834	5393397	5.0	10.3	1.2	23.4	1.8	3.0	0.5	0	0	Ì
H	4850.2	H	523472	5394552	6.0	2.5	119.7	23.0	30.2	62.8	i		27	į
Ī	4872.7	S	523885	5395273	23.8	26.1	148.4	280.1	1.8	48.8	1.6	5	15	į
jЈ	4881.9	S	524053	5395588	22.0	27.1	189.9	165.0	4.3	48.5	1.3	0	12	į
K	4899.7	S	524376	5396174	3.7	6.6	41.3	74.4	2.2	12.6	0.5	0	19	ĺ
L	4922.6	S	524767	5396906	11.2	14.8	56.5	184.5	1.4	26.6	1.0	9	18	į
M	4940.6	S?	525067	5397440	11.6	8.7	28.3	69.9	0.7	11.2	1.9	5	j 11	į
N	4956.7	S	525352	5397931	2.5	6.2	131.1	169.7	3.7	36.7	j		0	į
o	4974.7	S	525638	5398453	3.0	5.6	8.0	46.8	0.5	6.8	j		j o	į
P	4986.1	S	525807	5398764	10.5	14.2	17.2	81.9	0.6	10.7	0.9	5	j 8	į
Q	5027.0	S	526450	5399930	7.9	9.5	36.2	43.7	6.9	17.1	1.0	24	j o	į
R	5042.0	L	526692	5400361	36.0	27.1	2.3	274.6	46.8	72.7	2.7	3	j o	į
s	5056.0	L	526881	5400705	9.5	5.4	63.9	38.5	11.4	12.7	2.5	10	j o	į
Т	5061.2	L	526967	5400851	4.4	8.5	85.9	88.9	31.3	33.7	0.5	11	0	j
LINE	10091		FLIGHT	17	 						 			ا
A	2078.0	S	521302	5390439	3.9	19.4	91.0	124.3	11.0	35.7	0.2	0	0	į
В	2054.8	S?	521662	5391068	3.5		121.6	264.3	3.3	43.1	0.8	44	0	į
ĺС	2047.5	S?	521761	5391262	9.6	3.8	50.8	105.9	1.7	15.9	4.0	26	j o	į
D	2040.9	S	521856	5391441	9.2	19.3	42.8	114.7	1.4	17.4	0.6	4	j o	į
E	2011.2	H	522281	5392220	31.2	21.2	742.8	342.3	101.5	276.1	3.0	15	28	Ì
F	1988.0	S	522617	5392823	32.0	34.7	531.1	493.9	27.3	168.3	1.7	5	23	į
Ġ	1968.7	S	522929	5393371	7.1	11.4	83.8	162.2	0.9	27.7	0.7	0	156	į
Н	1928.9		523570	5394542	16.8	19.0	334.4	309.0	12.0	92.7	1.3	17	0	į
İΙ	1907.7	S	523897	5395138	5.7		158.1	351.4	1.7	54.3	0.6	19	0	j
J	1893.8	S	524139	5395553	16.8	24.8	229.9	237.2	7.8	60.1	1.0	0	0	ĺ
K	1870.7	S	524521	5396237	3.3	5.5	30.4	78.7	0.8	12.5	0.5	31	0	j
Ĺ	1848.4	S?	524880	5396901	14.9	16.3	31.0	102.6	1.7	15.2	1.3	2	37	j
M	1840.0	S?	525014	5397135	4.1	9.4	12.0	58.7	0.9	8.3	0.4	0	0	j
N	1832.1	S?	525138	5397361	15.1	16.3		141.3	2.8	22.4	1.4	0	17	į
O	1813.0	S	525452	5397901	16.0		142.1	188.5	4.9	42.9	0.8	6	16	j
P	1781.2	S?	525901	5398744	12.8	21.2	39.8	144.2	1.9	20.8	0.8	0	22	j
Q	1739.0	S	526555	5399912	4.8	3.4	37.3	45.7	8.2	18.1	1.5	44	0	j

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

 					   CX 55	00 HZ	CP 7	 200 HZ	CP	900 HZ	Vertical	 l Dike	Mag. Corr	 
Labe	l Fid	Interp	XUTM	YUTM	Real	Quad	Real	Quad	Real	Quad	COND 1	DEPTH*		į
İ			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	İ
LINE	10091		FLIGHT	17	 						 			
R	1706.5	S	526985	5400721	6.0	6.7	53.8	61.6	12.5	22.1	1.0	24	0	ĺ
S	1699.0	L	527060	5400876	14.8	6.0	89.4	79.4	26.2	38.1	4.6	10	0	ĺ
LINE	10100		FLIGHT	17	 						 			
A	2196.4	B?	521211	5390032	12.7	34.5	144.8	322.3	2.2	54.8	0.5	0	30	į
В	2206.4	S	521361	5390319	14.2	8.4	156.5	140.3	5.6	40.6	2.7	21	0	ĺ
C	2220.9	S	521589	5390738	6.0	12.7	134.4	275.7	2.0	47.0	0.5	3	283	į
D	2239.0	S	521886	5391260	2.3	6.6	80.7	133.4	3.5	25.8	i		0	į
E	2267.1	H	522348	5392095	21.3	7.6	326.5	358.9	37.8	96.8	6.2	25	0	ĺ
F	2286.2	B?	522650	5392653	41.7	35.3	434.5	338.0	0.6	131.5	2.5	1	0	ĺ
G	2289.8	H	522707	5392756	18.5	13.9	439.4	338.0	29.7	133.9	2.2	14	26	İ
Н	2311.3	S	523056	5393380	7.6	7.7	162.0	233.1	2.7	46.8	1.2	15	139	į
İΙ	2337.2	S	523458	5394128	15.4	23.3	164.7	276.8	3.3	49.7	1.0	6	j 6	į
jЈ	2380.9	S	524174	5395399	3.7	3.7	48.1	122.3	2.6	18.8	0.9	42	j 15	į
K	2401.9	S?	524503	5396007	3.9	7.7	47.8	124.9	0.7	19.0	0.5	3	12	į
Ĺ	2429.6	S?	524964	5396814	10.5	18.3	68.1	143.9	2.3	22.4	0.7	0	24	į
М	2451.8	S	525327	5397435	0.9	4.7	73.4	154.9	1.4	26.8	i		12	į
N	2473.4	S?	525680	5398106	16.8	30.0	107.7		1.2	31.3	0.8	0	j 31	į
jo	2492.3	B?	526004	5398694	6.8	14.7	18.1	17.7	0.4	4.4	0.5	0	j 9	į
P	2498.4	S?	526094	5398873	0.0	14.9	64.0	134.8	1.5	21.7	i		j 5	į
ĺQ	2529.8	S	526654	5399882	1.5	3.2	8.5	19.8	6.1	4.7			j o	į
R	2561.3	L	527188	5400823	0.6	1.1	58.6	42.6	18.5	18.4			0	j
LINE	10110		FLIGHT	 17	 						 			
A	3138.6	S	521482	5390326	12.4	11.7	160.8	251.3	6.7	45.4	1.5	17	j 0	į
Ϊв	3127.2	S	521679	5390701	24.6	44.0	268.2	600.4	2.9	99.8	0.9	1	j o	į
İc	3106.4	S	522044	5391349	7.6	30.8	96.3	63.8	2.5	28.8	0.3	0	j o	į
D	3081.9		522453	5392078	18.0	9.7			27.0	56.0	3.4	27	j 5	į
E	3059.6	Н	522825	5392776	33.2	39.5	471.2	416.4	27.4	146.9	1.6	1	j o	į
F	3041.3	S	523166	5393360	0.0	0.0	34.1	41.2	2.7	9.2			141	j
Ġ	3021.2	S	523524	5394044	14.7	25.2	222.7	324.8	5.6	64.6	0.8	3	27	j
н	2968.8	S	524541	5395882	1.6	5.8	11.5	52.9	1.4	7.5			8	j
İI	2964.3		524622	5396033	7.1	6.9	4.2	29.5	1.6	3.3	1.2	24	0	j
jЈ	2946.3	S?	524935	5396566	5.3	8.0	17.7	46.8	0.1	7.3	0.7	3	7	j
K	2938.4	S	525057	5396793	13.4	5.1	76.4	160.1	1.3	25.2	4.8	26	29	j
ĹЪ	2922.9		525313	5397249	9.5	12.8	34.1	94.4	1.1	6.7	0.9	7	0	j
M	2916.4		525415	5397448	11.1	8.2		104.2	2.0	15.1	1.9	17	14	i
N	2905.6	S	525596	5397768	8.1		121.5		5.1	38.8	0.7	9	21	İ

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					   CX 55			200 HZ	CP	900 HZ	   Vertica		Mag. Corr	 ļ
Labe	el Fid	Interp		YUTM	Real	Quad	Real	Quad	Real		!	DEPTH*		ļ
I			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	
LINE	10110		FLIGHT	17	 						 			
0	2895.3	S	525769	5398090	18.6	25.3	24.4	70.9	1.6	11.0	1.1	0	19	
P	2876.9	S	526098	5398673	6.6	12.2	26.2	73.8	1.9	11.1	0.6	0	16	
Q	2860.6	S	526397	5399194	0.2	7.3	40.2	72.2	2.3	11.0			0	
R	2840.9	S	526730	5399814	1.6	4.0	2.2	32.0	14.1	11.0			0	
S	2819.0	L	527086	5400480	0.0	18.2	8.7	18.1	15.8	4.7			0	
T	2803.1	L	527302	5400858	6.8	1.6	14.6	30.9	3.0	10.2			0	
LINE	10120		FLIGHT	17	 						 			
A	3262.1	S	521604	5390346	8.5	14.7	171.8	154.2	5.1	41.2	0.7	7	0	i
В	3273.7	S	521807	5390698	16.3	14.3	69.9	129.0	3.6	18.7	1.8	3	j o	İ
ĺС	3288.7	S	522049	5391164	0.9	3.8	97.5	147.8	3.1	28.3	i		j o	į
D	3299.1	S	522234	5391484	2.6	18.6	26.6	54.1	3.8	8.8	i		8	i
E	3314.6	H	522499	5391990	0.0	7.1	24.2	90.0	16.5	14.8	j		10	į
F	3340.1	S	522935	5392749	0.2	5.9	77.8	80.1	4.0	21.3	i		11	ĺ
G	3361.0	S	523319	5393449	5.9	6.0	58.9	87.7	1.3	16.2	1.1	19	0	ĺ
H	3372.3	S	523531	5393841	8.7	14.4	161.7	238.3	4.0	46.8	0.7	6	30	ĺ
I	3386.1	S?	523791	5394309	4.8	3.4	20.4	53.6	0.5	8.5	1.5	42	12	ĺ
J	3394.7	S	523946	5394621	1.5	5.0	1.8	17.2	0.7	2.5			0	ĺ
K	3401.9	S?	524102	5394867	5.6	9.2	24.1	84.7	1.5	12.3	0.6	3	0	
L	3426.3	S	524564	5395705	2.6	4.4	3.9	19.0	1.6	2.7			0	
M	3456.6	S	525122	5396702	0.0	7.3	119.1	149.2	4.3	33.6			23	
N	3478.1	S	525518	5397420	7.5	1.3	50.4	86.7	1.3	17.0			0	
0	3487.6	H	525688	5397748	2.7	5.1	145.0	105.5	5.3	41.5			22	
P	3501.2	S	525943	5398181	0.9	6.3	31.8	73.2	2.9	12.4			0	
Q	3515.2	S	526195	5398645	10.9	16.1	193.2	247.3	4.1	54.6	0.9	1	32	
R	3532.1	S	526485	5399161	0.8	0.7	55.9	96.1	1.4	16.8			0	
S	3555.9	S	526886	5399905	5.2	8.0	60.8	93.6	14.5	30.9	0.7	32	0	ļ
T	3582.7	L	527342	5400708	6.8	0.5	22.7	20.5	5.3	8.9			0	
LINE	10130		FLIGHT	17	 						 			
A	4029.1	S	521697	5390340	16.9	13.9	195.4	212.2	9.6	43.3	1.9	17	0	į
В	4016.7	S	521949	5390761	16.1	25.3	336.7	412.4	7.4	102.1	0.9	5	0	i
C	4000.1	S	522224	5391264	7.2	9.2	123.3	232.0	2.7	38.9	0.9	17	0	į
D	3985.0	S?	522469	5391687	7.5	15.9	25.7	86.0	1.5	12.9	0.6	0	0	į
E	3973.1	S	522658	5392052	14.0	21.9	357.2	388.1	11.8	102.3	0.9	6	0	į
F	3950.9	S	522989	5392682	3.0	17.5		115.1	0.2	17.7	i		23	į
G	3944.3	S?	523115	5392889	17.4	38.7	57.1	196.2	2.1	25.8	0.7	0	12	į
Н	3931.5	S	523360	5393298	11.2	13.2		290.4	7.6	64.8	1.1	18	25	j

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

Label	Fid	Interp	XUTM	YUTM	CX 55	00 HZ Quad	CP 7 Real	200 HZ Quad	CP Real		Vertica   COND	l Dike DEPTH*	Mag. Corr	
		-	m	m	ppm	ppm	ppm	ppm	ppm		siemens	m	NT	j
LINE	10130		FLIGHT	17	 						 		 	
I	3906.5	S	523769	5394069	2.3	7.2	22.8	83.1	0.7	12.9			0	I
J	3900.4	S	523869	5394254	2.7	0.0	17.4	34.3	1.6	6.3			0	ĺ
K	3894.6	S	523971	5394434	2.7	10.3	9.4	59.7	0.8	7.5			0	ĺ
L	3884.3	S	524159	5394766	6.2	10.8	127.1	191.4	2.9	35.6	0.6	5	14	ĺ
M	3862.0	S	524565	5395496	1.2	2.6	33.1	71.8	3.5	11.5			10	ĺ
N	3836.4	S	525013	5396284	4.2	10.8	169.1	154.7	5.1	46.5	0.4	3	0	ĺ
0	3824.2	H	525223	5396661	17.9	10.9	73.5	48.3	9.0	26.4	2.8	18	7	ĺ
P	3796.1	S	525627	5397422	1.6	2.5	32.6	100.3	1.0	18.7			0	ĺ
Q	3773.0	S	526046	5398180	2.5	5.9	25.0	57.6	1.8	9.0			6	ĺ
R	3761.9	S	526252	5398538	0.6	7.6	63.6	118.5	1.5	20.7			18	ĺ
S	3758.1	S	526321		7.2	5.6	45.4	87.1	2.0	13.8	1.6	13	10	ĺ
T	3743.2	S	526590	5399117	7.8	7.2	67.9	124.5	1.2	21.5	1.3	19	0	ĺ
Ū	3715.6	H	526979	5399883	7.8	0.2	108.5	20.6	18.0	38.6			0	ĺ
V	3698.5	S?	527242	5400330	2.8	7.6	33.5	73.9	7.2	16.2			0	ĺ
M	3689.8	L	527354	5400517	2.9	0.6	21.9	26.2	1.9	4.2			251	İ
LINE	10140		FLIGHT	17	 						 			
A	4229.5	S	521646	5390012	4.2	8.7	13.0	40.1	0.9	6.0	0.5	6	8	ĺ
В	4246.5	S	521882	5390434	6.8	8.0	123.3	46.1	8.0	31.5	0.9	21	0	
C	4259.7	S	522094	5390804	19.2	13.1	181.2	120.7	9.2	45.7	2.5	14	0	1
D	4277.0	S?	522356	5391298	4.8	22.4	56.6	138.2	2.6	22.2	0.3	0	0	1
E	4300.3	S?	522726	5391959	11.4	20.1	70.0	130.3	1.2	24.0	0.7	0	78	
F	4304.8	S?	522796	5392086	9.6	9.4	105.8	214.9	0.5	36.0	1.3	18	0	
G	4334.4	S	523259	5392930	7.3	9.5	25.6	85.3	1.0	12.5	0.9	2	0	
H	4350.4	S	523528	5393434		8.1	105.5	155.0	3.4	31.1	0.5	21	0	
I	4391.2	S	524173	5394583	6.6	13.9	169.6	229.5	4.5	46.3	0.5	2	0	
J	4400.3	S	524310	5394857	5.6 1.8	19.0	19.5	61.4	0.5	9.5	0.3	0	0	
K	4421.2	S	524661	5395420			176.9		5.0	50.5			0	
	4441.0	S?	524996	5395992	5.7	22.5		225.5	0.5	30.9	0.3	0	15	
	4452.5		525164	5396356	16.9		162.6	188.0	10.4	43.3	0.9	12	15	
	4463.8		525344	5396691	21.0		155.9		8.0	47.4	2.0	10	6	
	4472.9		525498	5396963	5.6	5.4	66.9	64.8	4.0	18.0	1.1	23	0	
	4485.2		525725	5397346	1.1	8.1	35.2	94.6	0.8	15.1			7	
ı ~	4518.7		526261	5398344		7.9	4.0	25.0		4.0			0	
	4534.0		526526	5398819	2.6		103.4	181.4	1.2	35.9			6	
	4541.0		526649	5399040	10.5	13.0		118.2	1.9	20.9	1.0	1	9	
	4567.3		527085				102.8		19.3	37.7			0	
U	4583.8	S	527348	5400307	10.9	11.5	205.6	208.0	7.2	60.2	1.3	16	0	

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

  Labe	l Fid	Interp	MTUX c	YUTM m	CX 55   Real   ppm	00 HZ Quad ppm	CP 7 Real	200 HZ Quad ppm	CP Real ppm	~	Vertica COND	l Dike DEPTH* m	Mag. Corr     NT	
	10140 4593.0	L	FLIGHT 527476	17 5400518	   1.6	2.5	1.8	8.4	4.5	3.5	 		352	
LINE	10150		FLIGHT	17	 						 			
A	5021.8	S	522038	5390543	4.3	20.6	139.2	178.6	10.0	57.0	0.2	0	17	i
В	5009.0	S	522299	5390972	16.9	32.6		233.3	2.1	40.9	0.8	2	0	į
İc	4998.6	S	522472	5391311	3.1	7.6	37.0	89.8	1.6	14.1	i		0	į
D	4985.6	S	522720	5391739	4.6	0.0	20.0	42.6	1.9	7.5	i		j o	į
E	4971.2	S?	522973	5392199	10.9	21.1	44.9	140.7	1.0	20.4	0.7	0	j o	į
F	4955.0	S?	523244	5392686	12.7	3.0	11.6	4.2	4.9	2.7	i		0	į
Ġ	4950.5	S	523310	5392814	20.6	36.5	75.6	212.2	4.4	32.7	0.9	0	7	į
Н	4944.4	S?	523410	5392992	8.7	12.0	5.0	40.6	2.0	5.6	0.9	19	j o	į
İı	4938.0	S?	523519	5393164	3.4	14.5	14.3	18.5	1.9	5.1	i		0	į
jЈ	4929.8	S	523650	5393417	4.9	3.7	24.4	54.9	0.5	9.1	1.4	29	8	į
ĸ	4920.7	S	523801	5393708	16.0	19.0	208.3	228.1	4.8	54.5	1.2	3	32	į
ĹЪ	4895.6	S	524218	5394460	5.2	15.8	13.4	76.8	1.5	10.3	0.4	0	17	į
М	4867.8	S	524656	5395253	6.8	20.4	70.3	270.9	0.0	38.1	0.4	0	9	i
ĺи	4859.1	B?	524789	5395489	1.5	6.4		147.7	8.0	25.1			0	i
lо	4846.0	S?	524980	5395822	2.0	4.5	5.7	12.4	1.2	1.6			0	i
ĺР	4832.1	Н	525183	5396181	5.8		305.0	180.2	11.2	93.2	0.8	33	0	i
ĺQ	4818.3	H	525398	5396583	12.2		151.0	166.4	4.0	45.0	1.3	12	0	i
Ŕ	4806.0	S?	525568	5396899	13.5		146.1	165.3	3.1	42.0	0.7	0	11	i
s	4771.5	S	526174	5398002	1.4	3.2	4.8	27.6	2.4	2.2			7	i
T	4754.0	S?	526502	5398577	7.1	6.1	7.8	28.7	0.8	2.7	1.4	31	0	i
ĺΰ	4747.4	S	526641	5398788	0.0	0.5		120.3	2.5	25.5			0	i
ĺv	4740.3	B?	526758	5399018	6.5	9.2	59.0	81.7	0.8	16.5	0.8	0	19	i
w	4723.8	B?	527014		8.8	14.9	2.6	89.3	3.9	16.2	0.7	0	104	i
x	4707.4	H	527267	5399967	6.1	4.2	43.0	25.8	7.9	20.7	1.7	39	0	i
Y	4678.8	L	527607	5400559				6.3	3.3				204	İ
LINE	10160		FLIGHT	23	 						 			
A	851.3	S	521893	5390048	2.7	7.2	10.8	25.6	2.9	5.9	i		58	į
В	837.1	S	522134	5390481	22.9	18.2	168.6	165.0	20.9	75.1	2.2	20	0	j
C	821.7	S	522411	5390978	2.7		114.0	207.7	1.8	37.6			0	į
D	809.5	S	522629	5391366	1.6	8.9	5.4	48.5	1.2	6.4			0	į
E	797.3	S	522836	5391753	6.0	20.1	104.6	236.6	2.0	38.5	i		0	į
F	784.7	S	523052	5392152	9.2	8.5		179.9	5.5	29.9	1.4	13	j o	į
G	764.3	S	523391	5392768	20.5	39.5	303.9	566.4	4.3	101.4	0.8	0	0	i
Н	744.1	S	523740	5393389	2.6	14.3		79.1	2.9	11.0			8	į
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CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					   CX 55	00 HZ	CP 7	200 HZ	CP	900 HZ	Vertica	l Dike	Mag. Corr	
Labe	l Fid	Interp	MTUX	YUTM	Real	Quad	Real	Quad	Real	Quad	COND	DEPTH*		
			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	
LINE	10160		FLIGHT	23	 						 			
I	739.4	S	523813	5393523	8.8	20.3	32.5	140.6	1.8	19.6			0	
J	734.9	S	523878	5393649	16.4	10.0	80.6	304.3	2.0	45.1			0	
K	711.2	S	524269	5394336	4.0	10.8	20.5	81.2	0.4	11.5			0	
L	700.4		524468	5394674	2.2	9.6	3.4	17.7	2.1	3.4			6	
M	693.5	B?	524587	5394889	1.5	0.0	15.2	3.6	2.7	4.4			0	
N	688.9	S	524663	5395036	4.3	10.2	9.3	18.8	1.2	3.9			0	
0	672.5		524942	5395544	2.4	4.1	10.1	37.6	1.4	6.6			0	
P	666.6		525031	5395725	4.1	5.7	4.3	35.7	2.0	4.6			0	
Q	642.1		525450	5396476	6.1	0.7	53.2	6.3	6.4	18.4			0	
R	627.4		525696	5396930	10.5	14.1	300.3	394.2	21.9	90.8	1.0	22	0	
S	602.2		526109	5397660	13.0	36.4	363.1	688.7	4.5	123.8	0.5	1	0	
T	590.0		526345	5398084	7.5	18.7	29.9	75.7	1.8	10.8	0.5	0	7	
U	586.0		526425	5398225	1.4	6.5	9.6	26.5	1.5	4.2			0	
V	567.6	S	526774	5398842	5.9	13.6	69.0	117.7	1.3	22.4	0.5	6	0	
W	556.4		526970	5399215	1.6	5.5	3.9	31.8	2.4	4.6			0	
X	532.5	H	527386	5399977	5.6	6.8	55.8	31.5	7.1	25.4	0.9	31	64	
LINE	10170		FLIGHT	23	 						 			
A	945.7	S	521981	5390008	0.0	2.9	10.7	23.8	0.6	4.8			27	
В	957.3	S	522156	5390309	25.5	36.8	294.6	504.4	22.2	109.4	1.2	4	0	
C	980.9	S	522552	5391008	0.9	4.0	45.5	101.4	2.7	18.2			0	
D	1008.0	S?	523022	5391854	7.1	10.7	33.5	48.5	2.4	9.6	0.7	16	0	
E	1018.0	S	523199	5392166	9.3	11.9	162.3	186.6	5.5	43.7	1.0	5	0	
F	1040.7	S	523566	5392841	8.7	20.3	283.5	304.9	9.6	76.7	0.5	0	9	
G	1057.8		523831	5393318	11.3	27.3	38.8	141.3	1.3	20.3	0.6	0	6	
H	1073.1	S	524071	5393773	2.1	6.5	39.3	90.1	1.4	15.2			0	
I	1108.8		524673	5394863	0.0	1.7	15.9	46.2	0.5	7.9			6	
J	1159.5		525505	5396357	4.4	5.6	153.0	109.9	11.4	47.8	0.8	27	0	
K	1174.0		525748	5396799	4.5	7.6	170.3	135.8	13.9	58.3	0.6	16	24	
L	1192.6		526059	5397341	5.0	7.8	4.1	28.5	0.3	5.3			0	
M	1198.1		526148	5397503	5.7	18.4	107.7	284.1	1.9	43.9			26	
N	1205.7		526280	5397740	32.4	17.8	317.9	365.8	7.8	83.8	3.9	14	6	
0	1213.1		526410	5397978	4.8	3.0	67.7	118.6	1.8	20.5	1.8	42	13	
P	1226.5		526644	5398408	3.9	9.8	7.5	31.9	1.4	4.4			0	
Q	1243.7		526954	5398962	13.0	15.5	229.8	420.1	3.4	74.0	1.2	13	0	
R	1276.3	S	527479	5399914	7.7	2.7	58.7	4.5	8.1	19.5			0	

CX = COAXIAL

CP = COPLANAR

Note: EM values shown above are local amplitudes

\*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

					   CX 55	00 HZ	CP 7	200 HZ	CP	900 HZ	Vertica	 l Dike	Mag. Corr	 
Labe	l Fid	Interp	MTUX c	YUTM	Real	Quad	Real	Quad	Real	Quad	COND	DEPTH*		
			m	m	ppm	ppm	ppm	ppm	ppm	ndd p	siemens	m	NT	
LINE	10180		FLIGHT	23	 						 			 
İΑ	1683.3	S	522276	5390320	24.9	36.1	609.3	658.8	32.2	198.2	1.2	7	i o	i
В	1664.9		522633	5390975	9.8		116.0	185.5	2.1	34.6	2.8	38	0	i
lс	1633.5		523235	5392064	9.5		101.8		2.2	30.8	1.7	28	0	i
ĺЪ	1610.5		523632	5392802	2.0	5.2	250.6	363.2	8.7	73.2			14	i
E	1600.0	S	523836	5393149	8.1	13.0	61.2	134.4	2.0	20.2	0.7	12	j o	i
F	1582.8		524157	5393712	9.1	8.6	186.4	229.0	5.4	54.2	1.3	19	j o	i
Ġ	1553.5	S	524682	5394670	18.0	30.5	444.2	642.6	8.4	129.0	0.9	9	17	İ
Н	1541.3	S	524905	5395074	0.7	13.1	75.7	160.2	2.1	25.5	i		0	İ
İı	1530.7	S	525087	5395426	0.0	6.0	46.6	83.9	1.7	16.5	j		16	i
jЈ	1509.1	S?	525494	5396139	0.0	0.0	169.2	64.2	2.0	68.2	i		0	İ
ĸ	1506.0	S	525559	5396247	26.2	41.1	199.2	268.1	5.9	56.1	1.1	8	j 15	i
L	1489.8	S	525877	5396838	7.1	6.8	38.6	120.6	1.8	17.8	1.2	30	j 6	i
М	1481.2		526043	5397129	1.7	0.0	29.7	74.7	1.7	12.1			0	i
N	1472.5	S	526195	5397398	5.2	6.4	8.1	47.3	0.3	6.2			i o	i
ĺО	1464.0	S?	526351	5397680	3.1	17.9	86.6	134.9	1.3	25.8	0.2	0	j o	i
ĺР	1456.3	S	526507	5397941	6.3	8.2	69.8	96.5	2.8	18.7	i 0.8	5	j 10	i
ĺΩ	1428.3	S	527023	5398894	7.1	9.8	38.3	72.9	1.2	12.1	0.8	0	j o	i
Ŕ	1419.7	S?	527177	5399173	2.9	6.1	4.5	19.9	2.9	3.4			i o	i
s	1389.7	S	527676	5400092	0.0	4.4	0.0	108.1	0.0	6.1	i		164	İ
IT.TNE	10190		FLIGHT	23	 I						 I		 	 I
A	1902.3	S	522223	5390019	1.7	1.3	13.5	31.4	1.3	6.0			0	
lB	1916.2	S	522405	5390323	19.8	28.9	448.4	383.1	26.7	144.4	1.1	3	0	
İc	1938.6	S	522750	5390974	4.7	2.9	83.3	59.8	3.0	18.0			102	i
l D	1952.9		523023	5391436	2.7	7.5	21.0	71.0	6.9	10.7	i		0	i
E	1966.0		523258	5391879	9.2		193.3	225.9	5.3	54.6	1.4	14	12	
F	1979.4		523495	5392305	6.6	11.1	25.1	29.1	1.1	7.3	0.7	14	0	
Ġ	1994.9		523760	5392790	38.1	67.1		350.1	2.8	67.5	1.1	0	15	ł
Н	2012.8		524071	5393356	9.4		146.1	78.9	12.5	43.9	1.7	30	0	ł
II	2022.3		524238	5393663	10.6		192.3	65.2	14.0	57.5	1.7	27		l
J	2040.7	S	524567	5394274	12.9	8.7		382.3	6.2	74.6	2.3	30		
K	2068.1		525035	5395088	5.1	16.7		201.2	1.1	33.7	0.3	0	0	
L	2080.1		525227	5395439	2.2	2.4	25.6	79.3	1.9	12.1	0.5		11	
M	2095.2		525480	5395885	19.6	49.5	297.2	618.2		101.5	0.7	0	23	ł
N	2131.1		526093	5396981	2.3	0.4	12.7	59.5	0.1	7.7			0	ł
lo	2151.7		526422	5397597	8.5	13.6	15.6	68.6	3.7	8.9	0.7	8	1 0	ļ
l P	2160.4	S.	526557	5397866	1.6		145.8		4.0	41.8				l
											ı 		·	

CX = COAXIAL

CP = COPLANAR

Note: EM values shown above

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

    Labe 	l Fid	Inter	o XUTM m	YUTM m	   CX 55   Real   ppm	500 HZ Quad ppm	CP 7 Real	200 HZ Quad ppm	CP Real ppm	900 HZ Quad ppm	Vertica   COND   siemens	.l Dike DEPTH* m	Mag. Corr       NT	     
IT TNE	10190		 FLIGHT		 I						 I			
!	2172.2	S	526768	5398201	0.5	21 2	122.3	263.6	3.3	43.2	l I		1 0	ļ
Q  R	2172.2	S?	520700	5398641	0.0	1.5	22.5	79.1	2.1	12.0	 		0	-
ls	2107.5	S: S	527002	5398824	11.2	5.3	72.8	106.4	1.7	19.4	3.3	27	32	-
5   T	2205.0	S	527095	5399167	0.4	0.9	0.0	20.1	1.6	2.2	3.3		0	
lΩ	2213.1	S	527422	5399107	2.3	5.6	34.2	91.3	9.7	13.4	 			ł
lv	2227.0	S?	527422	5399834	11.2	30.9	155.8	328.7	45.4	53.1	0.5	0		ł
W	2235.9	s: S	527807	5400111	9.7	19.8		216.3	45.4	31.8	0.5	10	0	
LINE	10200		 FLIGHT	23	 						 			 
A	2644.0	S	522570	5390450	3.7	4.1	86.1	6.8	24.8	25.4	0.8	40	0	į
В	2628.8	S	522895	5391021	10.5	8.9	160.4	134.5	7.0	42.2	1.6	27	0	į
C	2616.7	S	523128	5391459	0.0	3.9	6.3	37.7	2.1	4.6	j		0	į
D	2607.6	S?	523305	5391781	12.8	25.8	202.3	207.0	1.7	54.9	0.7	0	0	į
E	2605.1	S	523354	5391868	6.7	9.4	203.8	207.0	7.0	54.9	0.8	8	30	į
F	2592.2	B?	523605	5392311	7.6	16.0	19.1	10.5	3.2	3.3	0.6	6	6	į
G	2583.5	S	523766	5392616	5.2	4.6	197.5	186.8	6.9	52.5	1.2	30	0	ĺ
Н	2569.1	S	524055	5393114	1.6	6.9	358.2	167.8	16.1	95.6	j		53	į
I	2523.9	S	524847	5394538	3.2	13.8	25.6	105.7	2.1	15.1	0.2	0	0	į
J	2511.5	S	525056	5394942	2.8	10.3	63.5	134.7	0.5	22.8	i		0	ĺ
K	2505.3	S?	525162	5395143	4.4	17.8	10.7	131.4	1.0	19.9	0.3	0	0	ĺ
L	2481.7	S	525588	5395892	6.9	14.8	16.5	97.1	0.7	13.1	0.5	0	0	
M	2456.7	S?	526050	5396688	3.3	5.9	20.9	92.3	1.5	13.4	0.5	18	0	ĺ
N	2451.2	S?	526150	5396874	6.4	12.1	18.4	56.5	1.6	9.1	0.6	0	0	ĺ
0	2444.9	S?	526269	5397084	1.8	9.6	6.9	14.3	1.1	0.5	i		0	ĺ
P	2430.7	S	526512	5397560	4.8	10.1	5.8	42.4	1.8	6.0	0.5	17	0	ĺ
Q	2424.4	S?	526633	5397757	12.0	34.8	120.0	283.6	4.4	44.9	0.5	0	0	
R	2414.0	S	526819	5398091	9.5	13.0	181.6	148.1	7.2	41.0	0.9	19	0	ĺ
S	2397.6	S	527099	5398613	1.9	2.4	4.9	43.6	0.4	5.6	i		0	ĺ
T	2390.6	S	527232	5398839	2.4	9.2	187.5	200.9	7.6	48.7	i		66	į
Ū	2372.2	S	527559	5399440	0.5	1.0	33.3	75.9	5.2	11.9	i		0	į
V	2348.8	S?	527935	5400148	25.3	61.6	42.5	246.9	39.4	33.2	0.7	0	0	İ
:	10210	<b>_</b>	FLIGHT		!	<b></b>	<b>-</b>	<b>-</b>	<b>_</b>	<b>_</b>	ļ	<b>_</b>	!	
A	2733.9	S?	522376	5389901	6.4	7.1	14.1	31.9	2.2	6.3			31	ļ
В	2758.0	H	522766	5390585	8.9		123.6	37.3	13.9	41.0	1.0	22	0	
C	2774.7	S	523059	5391121	10.4		133.4		4.4	32.6	1.6	21	221	
D	2806.7	S	523608	5392117	3.4		117.7		3.3	35.3	0.3	2	0	
E	2815.5	В	523758	5392371	0.0	0.0	68.7	0.0	30.4	27.9			22	[

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

    Labe	el Fid	Interp	XUTM	YUTM	   CX 55   Real	00 HZ Quad	CP 7	7200 HZ Quad	CP Real	900 HZ Quad	   Vertica   COND	 l Dike DEPTH*	Mag. Corr	   
İ			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	İ
LINE	10210		FLIGHT	23	 						 			 
F	2821.2	S	523848	5392532	13.6	9.8	199.4	194.0	5.9	54.4	2.1	17	j 0	į
G	2836.6	S	524100	5393004	10.4	10.3	251.9	274.8	8.0	70.5	1.3	18	21	į
Н	2875.8	S	524803	5394246	3.5	7.1	12.6	73.8	0.3	10.5	j		10	į
İΙ	2892.2	S	525078	5394783	0.5	0.3	36.2	74.6	3.6	13.3	j		0	į
J	2903.6	S	525277	5395149	1.5	0.5	16.3	42.5	1.8	7.3			0	
K	2924.6	S	525672	5395834	1.7	7.2	7.8	35.6	1.0	4.4			0	ĺ
L	2935.2	S	525874	5396190	5.9	5.4	1.1	18.9	2.4	3.3	1.2	41	0	Ì
M	2949.6	S	526147	5396680	2.6	10.3	40.5	146.9	1.2	22.4			5	
N	2960.9	S	526345	5397053	2.8	9.9	6.7	38.7	1.5	5.6			8	
0	2982.3	S	526720	5397735	0.5	3.7	11.4	59.0	0.9	9.0			0	
P	2989.6	S	526842	5397967	3.2	5.3	80.3	108.3	4.0	20.5	0.5	13	0	
Q	2995.8		526957	5398158	2.7	8.5	67.9	152.3	0.1	24.5			0	
R	3005.9		527121	5398465	2.9	1.9	12.4	3.9	5.3	3.7			68	
S	3018.1		527311	5398836	7.2		142.2		4.6	34.5	1.2	21	0	
T	3033.4	S	527580	5399286	14.8	27.1		339.7	7.1	77.4	0.8	0	0	
U	3038.4	S?	527673	5399442	7.2		134.7		3.9	45.9	0.9	18	0	
V	3046.5		527813		4.3	10.2		19.6	5.9	4.0	0.4	14	0	
W	3057.2	S	528000	5400026	8.5		222.2	419.8	9.9	76.4	0.5	4	0	
LINE	10220		FLIGHT		 						 			
A	3467.0	S?	522528	5389972	2.5	1.4	8.0	26.8	0.0	3.4			0	
В	3455.3	H	522758	5390357	17.0	12.7	290.5	94.2	18.7	82.7	2.2	18	0	
C	3429.0	S	523204	5391158	4.8	9.4	114.7	126.6	5.4	32.7	0.5	4	0	
D	3416.2	S?	523407	5391545	6.4	17.3	50.4	159.4	4.1	23.3	0.4	2	0	
E	3406.9	S	523558	5391820	2.8	5.3	6.8	41.7	2.3	6.0			0	
F	3396.5		523727	5392121	8.3	19.0		334.0	7.7	73.8	0.5	0	0	
G	3384.7	S	523921	5392475	14.3	37.5	107.7	256.8	2.1	39.7	0.6	0	0	
H	3371.8	S	524128	5392869	14.3	17.6	94.5		1.2	40.3	1.2	13	18	
I	3356.3	S	524426	5393368	0.0	2.1	12.3	41.2	2.5	7.0			0	
J	3329.6		524874	5394200	7.9	2.6	9.5	17.2	1.6	2.2			0	
K	3314.9		525118	5394632	1.3	2.3	14.0	44.6	1.0	6.8			5	
L	3301.6		525354	5395061	3.6	2.4	57.5	118.0	2.4	18.3			11	ļ
M	3276.5		525811	5395893	3.3	5.2	27.2	68.0	0.1	11.1	0.6	31	0	
N	3259.1	S	526137	5396478	0.6	5.9	20.2	109.7	1.0	16.1			6	
0	3254.4		526221	5396638	3.1	7.6	45.8	169.6	0.5	25.2	0.4	8	13	
P	3239.3		526500	5397137	4.2	4.8	19.1	86.2	1.6	12.8			0	
Q	3207.4	S	527096	5398184	0.0	2.0	3.3	23.4	1.1	3.5			6	
R	3202.5	S 	527174 	5398346	1.7	2.5	5.6	31.1	0.4	4.6	 		0	 

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

	    Labe	el Fid	Inter	 p XUTM	YUTM	   CX 55   Real	00 HZ Quad	CP 7	200 HZ Quad	CP Real	900 HZ Quad	   Vertica   COND	 l Dike DEPTH*	   Mag. Corr 	   
S 3191.1   B 527380 5398708   3.3   8.0   24.4   29.4   13.4   7.7   0.4   0   0   0   0   1   3176.8   S 527633 5399164   4.2   12.7   232.6   311.2   5.3   68.8   0.3   0   0   0   0   3166.7   S 527803 5399469   9.3   19.4   59.3   178.5   1.6   25.1   0.6   0   0   30   0   0   3153.1   S 528016 5399866   11.6   6.9   37.7   117.8   0.5   17.5   2.6   28   107   0   3145.8   S 528128   5400065   10.7   30.2   258.9   372.1   7.8   81.4   0.5   0   0   0   0   0   0   0   0   0				-		1					~	siemens	m	NT	İ
T	LINE	10220		FLIGHT	23	 						 			 
U 3166.7	S	3191.1	В	527380	5398708	3.3	8.0	24.4	29.4	13.4	7.7	0.4	0	0	
V 3153.1	T	3176.8	S	527643	5399154	4.2	12.7	232.6	311.2	5.3	68.8	0.3	0	0	
W 3145.8   S 528128   S400065   10.7   30.2   258.9   372.1   7.8   81.4   0.5   0   0   0       X 3138.0   S 528239   5400260   6.0   9.9   22.3   52.4   2.4   8.0   0.6   9   0   0       LINE 10230	U		S					59.3	178.5	1.6		0.6	0	30	
X   3138.0   S   52829   5400260   6.0   9.9   22.3   52.4   2.4   8.0   0.6   9   0	V	3153.1	S	528016	5399866		6.9			0.5	17.5	2.6	28	107	
LINE 10230   FLIGHT 23	W	3145.8	S					258.9	372.1	7.8	81.4	0.5	0	0	
LINE 10230	X	3138.0	S	528239	5400260					2.4	8.0	0.6	9	0	
B   3744   2   S   523329   5391184   8   8   3   7   3   183   1   150   1   5   3   49   6   1   4   17   110     C   3762   3   S   523608   5391701   0   2   4   3   2   4   13   8   1   6   1   7       0     D   3777   9   S   523854   5392142   23   3   25   8   204   8   349   6   3   0   65   5   1   5   5   21     E   3787   3   S   524000   5392556   3   2   8   1   131   4   259   7   1   5   4   7   2   2   2   0   8   11   30     F   3793   0   S   524000   5392556   3   2   8   1   131   4   259   7   1   5   4   7   2   0   4   2   3   0     G   3819   1   S   524471   5393242   0   9   12   2   18   6   96   5   1   3   13   1       6     H   3875   9   S   525352   5394838   3   7   0   6   15   0   59   6   0   0   7   8   9       0     I   3885   8   57   525513   5395137   4   4   14   3   67   9   16   2   0   0   5   2   2   2     K   3999   8   S   526352   5394585   1   0   2   3   3   3   10   0   1   8   17   2       0     K   3999   8   S   526429   5396785   1   0   2   3   4   0   12   7   1   5   2   8       0     K   4000   7   8   527405   5398548   0   0   4   1   16   9   16   8   10   9   8   2       0     M   4005   1   8   527476   5398647   1   0   2   3   3   1   1   2   2   2   2   8   7       0     M   4005   1   8   527476   5398647   1   0   2   3   3   1   1   2   2   2   2   8   7       0     M   4005   1   8   527476   5398647   1   0   2   3   3   1   1   1   2   2   2   2   2   8   7       0     M   4046   3   5   528991   5399799   16   3   14   6   107   9   174   1   4   3   2   2   1   1   1   1   1   1   1   1	LINE	10230		FLIGHT	23	 						 			 
C	A	3719.1	S	522929	5390480		8.6	115.2	108.3	16.8	38.4	1.0	22	0	ĺ
D	В	3744.2	S	523329	5391184	8.3	7.3	183.1	150.1	5.3	49.6	1.4	17	110	
E	C	3762.3	S	523608	5391701	0.2	4.3	2.4	13.8	1.6	1.7			0	
F   3793.0   S   524090   5392556   3.2   8.1   131.4   259.7   1.5   47.2   0.4   23   0   3819.1   S   524471   5393242   0.9   12.2   18.6   96.5   1.3   13.1       6     1   3875.9   S   525352   5394838   3.7   0.6   15.0   59.6   0.7   8.9       0     1   3885.8   S?   525513   5395137   4.4   14.3   67.9   162.0   0.5   26.2   0.3   0   6     0	D	3777.9	S	523854	5392142		25.8	204.8	349.6	3.0	65.5	1.5	5		
G	E		S							1.2		0.8	11	30	
H	F	3793.0	S	524090	5392556		8.1	131.4	259.7	1.5	47.2	0.4	23	0	
T	G		S	524471	5393242		12.2	18.6	96.5	1.3	13.1			6	
J 3905.7 S 525855 5395759   0.8 10.2 39.3 110.0 1.8 17.2     0	H	3875.9	S	525352	5394838	3.7	0.6	15.0	59.6	0.7	8.9			0	
K   3939.8   S   526429   5396785   1.0   2.3   4.0   12.7   1.5   2.8       0   0   0   0   0   0   0	Ι		S?							0.5		0.3	0	1	
L	J		S							1.8				0	
M	K	3939.8	S				2.3			1.5				0	
N	L	4000.7	В	527405						10.9				1	
LINE 10240	M	4005.1	В		5398647			31.7	12.2	27.2	8.7			1	
LINE 10240   FLIGHT 23	N		S									I		0	
A	0	4046.3	S	528091	5399779	16.3	14.6	107.9	174.1	4.3	29.1	1.7	16	22	
B	LINE	10240		FLIGHT	23	 						 			 
C       4417.8       S       523459       5391217       13.6       22.3       252.1       239.0       7.6       72.1       0.8       1       79         D       4406.0       S       523659       5391577       8.3       10.3       25.8       111.9       0.0       17.2       0.9       27       0         E       4388.4       S?       523977       5392117       8.0       14.3       38.7       78.9       2.5       12.4       0.7       0       10         F       4381.9       S       524093       5392325       10.1       17.8       45.7       92.3       3.0       16.0       0.7       0       14         G       4374.5       S?       524226       5392578       1.8       3.9       71.5       144.1       3.5       23.4         24         H       4363.2       S       524428       5392955       2.8       4.0       7.1       28.8       1.5       4.5         0         I       4356.0       S       524554       5393190       12.5       12.7       35.1       151.7       2.3       21.7       1.4       9 <td< td=""><td>A</td><td>4457.8</td><td>S</td><td>522773</td><td>5389974</td><td>2.5</td><td>4.4</td><td>11.9</td><td>32.7</td><td>1.7</td><td>5.3</td><td></td><td></td><td>63</td><td></td></td<>	A	4457.8	S	522773	5389974	2.5	4.4	11.9	32.7	1.7	5.3			63	
D       4406.0       S       523659       5391577       8.3       10.3       25.8       111.9       0.0       17.2       0.9       27       0         E       4388.4       S?       523977       5392117       8.0       14.3       38.7       78.9       2.5       12.4       0.7       0       10         F       4381.9       S       524093       5392325       10.1       17.8       45.7       92.3       3.0       16.0       0.7       0       14         G       4374.5       S?       524226       5392578       1.8       3.9       71.5       144.1       3.5       23.4         24         H       4363.2       S       524428       5392955       2.8       4.0       7.1       28.8       1.5       4.5         0         I       4356.0       S       524554       5393190       12.5       12.7       35.1       151.7       2.3       21.7       1.4       9       0         J       4349.3       S       524679       5393403       3.3       4.5       17.1       64.1       1.7       9.8       0.6       23       17 </td <td>В</td> <td>4445.0</td> <td>S</td> <td>522996</td> <td>5390369</td> <td>7.9</td> <td>9.9</td> <td>251.7</td> <td>116.1</td> <td>19.7</td> <td>79.5</td> <td>0.9</td> <td>18</td> <td>0</td> <td>ĺ</td>	В	4445.0	S	522996	5390369	7.9	9.9	251.7	116.1	19.7	79.5	0.9	18	0	ĺ
E       4388.4       S?       523977       5392117       8.0       14.3       38.7       78.9       2.5       12.4       0.7       0       10         F       4381.9       S       524093       5392325       10.1       17.8       45.7       92.3       3.0       16.0       0.7       0       14         G       4374.5       S?       524226       5392578       1.8       3.9       71.5       144.1       3.5       23.4         24         H       4363.2       S       524428       5392955       2.8       4.0       7.1       28.8       1.5       4.5         0       1         I       4356.0       S       524554       5393190       12.5       12.7       35.1       151.7       2.3       21.7       1.4       9       0         J       4349.3       S       524679       5393403       3.3       4.5       17.1       64.1       1.7       9.8       0.6       23       17         K       4308.3       S       525334       5394608       5.2       7.4       150.2       143.4       3.9       35.4       0.7       15 </td <td>C</td> <td>4417.8</td> <td>S</td> <td>523459</td> <td>5391217</td> <td></td> <td>22.3</td> <td>252.1</td> <td>239.0</td> <td>7.6</td> <td>72.1</td> <td>0.8</td> <td>1</td> <td>79</td> <td>ĺ</td>	C	4417.8	S	523459	5391217		22.3	252.1	239.0	7.6	72.1	0.8	1	79	ĺ
F       4381.9       S       524093       5392325       10.1       17.8       45.7       92.3       3.0       16.0       0.7       0       14         G       4374.5       S?       524226       5392578       1.8       3.9       71.5       144.1       3.5       23.4         24         H       4363.2       S       524428       5392955       2.8       4.0       7.1       28.8       1.5       4.5         0       0       1         I       4356.0       S       524554       5393190       12.5       12.7       35.1       151.7       2.3       21.7       1.4       9       0         J       4349.3       S       524679       5393403       3.3       4.5       17.1       64.1       1.7       9.8       0.6       23       17         K       4308.3       S       525334       5394608       5.2       7.4       150.2       143.4       3.9       35.4       0.7       15       0         L       4292.5       S?       525598       5395078       4.3       20.8       57.2       164.2       2.9       25.1      <	D	4406.0	S	523659	5391577	8.3	10.3	25.8	111.9	0.0	17.2	0.9	27	0	
G   4374.5   S?   524226   5392578   1.8   3.9   71.5   144.1   3.5   23.4       24     H   4363.2   S   524428   5392955   2.8   4.0   7.1   28.8   1.5   4.5       0     1   4356.0   S   524554   5393190   12.5   12.7   35.1   151.7   2.3   21.7   1.4   9   0   0     1   4349.3   S   524679   5393403   3.3   4.5   17.1   64.1   1.7   9.8   0.6   23   17     1	E	4388.4	S?	523977	5392117	8.0	14.3	38.7	78.9	2.5	12.4	0.7	0	10	
H     4363.2     S     524428     5392955     2.8     4.0     7.1     28.8     1.5     4.5       0	F	4381.9	S		5392325					3.0	16.0	0.7	0		j
I     4356.0     S     524554     5393190     12.5     12.7     35.1     151.7     2.3     21.7     1.4     9     0       J     4349.3     S     524679     5393403     3.3     4.5     17.1     64.1     1.7     9.8     0.6     23     17       K     4308.3     S     525334     5394608     5.2     7.4     150.2     143.4     3.9     35.4     0.7     15     0       L     4292.5     S?     525598     5395078     4.3     20.8     57.2     164.2     2.9     25.1       7	G	4374.5	S?	524226	5392578		3.9	71.5	144.1	3.5	23.4			24	j
J     4349.3     S     524679     5393403     3.3     4.5     17.1     64.1     1.7     9.8     0.6     23     17       K     4308.3     S     525334     5394608     5.2     7.4     150.2     143.4     3.9     35.4     0.7     15     0       L     4292.5     S?     525598     5395078     4.3     20.8     57.2     164.2     2.9     25.1       7	H		S		5392955		4.0			1.5	4.5			0	j
K       4308.3       S       525334       5394608               5.2       7.4       150.2       143.4       3.9       35.4               0.7       15               0          L       4292.5       S?       525598       5395078               4.3       20.8       57.2       164.2       2.9       25.1                 7	Ι	4356.0	S							2.3		1.4	9	1	j
L 4292.5 S? 525598 5395078   4.3 20.8 57.2 164.2 2.9 25.1     7	J	4349.3	S	524679	5393403					1.7	9.8	0.6	23	17	j
	K	4308.3	S	525334	5394608	5.2	7.4	150.2	143.4	3.9	35.4	0.7	15	0	j
M 4276.5 S? 525863 5395558   0.0 4.2 67.8 140.6 3.0 23.5     10	L	4292.5	S?	525598		4.3	20.8	57.2	164.2	2.9	25.1			7	j
	M	4276.5	S?	525863	5395558	0.0	4.2	67.8	140.6	3.0	23.5			10	j

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

  Labe] 	l Fid	Interp	XUTM m	YUTM m	CX 55   Real   ppm	00 HZ Quad ppm	CP 7 Real ppm	200 HZ Quad ppm	CP Real ppm	~	Vertica   COND   siemens	l Dike DEPTH* m	Mag. Corr     NT	
LINE	10240		FLIGHT	23	 						 		 	
N	4266.3	S	526035	5395866	0.0	2.7	17.3	86.6	1.7	11.4	i		j o	i
0	4235.5	S	526574	5396847	2.1	5.6	2.8	21.7	1.5	2.7	i		0	
LINE	10241		FLIGHT	24	 						 		 	
A	4496.9	S	527260	5398063	0.9	1.4	1.9	7.7	0.1	1.9	i		j o	į
В	4512.1	В	527516	5398487	1.2	0.2	24.4	11.4	15.0	8.7	i		62	į
C	4518.4	S	527622	5398673	5.3	8.4	22.6	93.8	7.0	10.6	0.6	10	0	į
D	4527.3		527767	5398935	5.4	19.2		103.6	0.2	13.5	0.3	0	84	į
E	4547.3	S	528058	5399508	7.8	5.0	117.5	166.2	7.6	33.2	2.0	38	5	į
F	4559.2	S	528243	5399872	5.1	11.6	177.5	188.2	13.2	59.0	0.5	15	j o	į
LINE	10250		FLIGHT	23	 						 		 	
A	4551.6	S	522867	5389970	5.6	6.0	14.2	24.1	1.4	5.2	i		0	į
В	4568.1	S	523083	5390339	5.7	3.9	136.0	21.7	15.2	44.2	1.7	31	j o	j
C	4578.0	S	523227	5390594	8.1	10.5	116.2	196.8	3.6	36.1	0.9	6	0	j
D	4599.9	S	523563	5391194	4.9	5.2	86.8	47.2	6.0	29.8	0.9	24	0	j
E	4615.4	S?	523805	5391629	2.8	4.8	15.9	47.1	2.3	7.5	j		0	į
F	4631.5	B?	524038	5392050	5.0	9.3	5.8	63.1	1.4	3.8	0.5	14	0	į
G	4642.0	B?	524183	5392324	10.2	26.5	77.8	171.2	0.8	27.6	0.5	0	0	j
H	4649.8	S	524310	5392529	2.0	0.4	7.9	24.6	0.4	3.3	i		10	j
I	4669.5	S	524632	5393121	3.1	3.6	23.6	89.1	1.5	13.0	i		5	ĺ
J	4678.4	S	524788	5393391	7.0	13.1	118.9	226.1	0.9	37.9	0.6	0	24	ĺ
K	4710.9	S	525319	5394347	5.7	0.7	21.5	26.6	2.2	5.6	i		0	j
L	4723.8	S	525527	5394740	1.7	3.6	2.9	22.7	1.4	2.5	i		0	j
M	4736.0	S?	525739	5395114	5.5	8.4	9.7	36.6	1.8	6.2	0.7	23	0	j
N	4748.4	S?	525964	5395513	0.5	17.3	58.5	156.7	2.4	25.0	i		8	į
0	4765.5	S	526260	5396025	4.9	4.4	3.7	40.3	2.6	5.4	i		0	ĺ
P	4791.3	S	526661	5396785	0.0	1.5	1.2	14.9	1.5	2.7	i		0	j
Q	4800.0	S	526817	5397081	3.5	8.6	18.0	148.2	0.9	21.0	0.4	12	0	j
R	4828.2	S	527322	5398029	5.3	0.6	1.7	20.9	0.8	3.5	j		0	į
S	4850.0		527703	5398712	7.1	12.8	32.7	113.5	2.3	15.9	0.6	0	13	ĺ
T	4855.7	S?	527797	5398885	1.1	12.7	14.7	65.5	2.2	9.8	j		0	j
Įυ	4876.2	S	528138	5399521	2.3	3.3	88.7	34.4	3.8	22.2	j		15	j
V	4891.2	S	528421	5399975	6.2	5.4	117.2	190.2	3.4	38.2	1.3	26	0	j
LINE	10260		FLIGHT	23	 						 		 	
A	5446.2	S	523150	5390256	39.2	81.7	796.4	958.4	39.2	274.7	1.0	0	0	j
ΪВ	5434.9	S?	523363	5390641	9.4	12.4	4.5	19.9	4.0	2.6	j		0	į

CX = COAXIAL

CP = COPLANAR Note:EM values shown above are local amplitudes

EM Anomaly List

					   CX 55	00 HZ	CP 7	200 HZ	 СР	900 HZ	Vertica	 l Dike	Mag. Corr	 
Labe	el Fid	Interp	XUTM	YUTM	Real	Quad	Real	Quad	Real	Quad	COND	DEPTH*		į
İ			m	m	ppm	ppm	ppm	ppm	ppm	n ppm	siemens	m	NT	į
LINE	10260		FLIGHT	23	 						 			
C	5420.8	S	523633	5391109	9.1	12.7	138.1	117.0	13.0	47.8	0.9	2	0	į
D	5388.0	S	524201	5392167	6.4	9.8	88.3	155.2	1.2	27.8	i		13	į
E	5372.5	S	524480	5392660	5.4	5.6	21.1	102.9	2.0	14.0	j		20	į
F	5354.1	S	524792	5393218	2.6	0.0	19.2	89.8	0.7	12.9	j		j o	į
G	5347.5	S	524901	5393413	2.1	37.1	77.3	343.5	1.2	49.1	i		17	į
Н	5337.8	S	525054	5393697	1.6	6.9	2.0	31.0	1.4	4.4	i		j o	į
İΙ	5323.1	S	525274	5394118	0.0	2.0	9.4	66.1	1.7	9.6	j		j 5	į
jЈ	5316.3	S	525398	5394315	0.7	2.7	8.4	60.3	0.6	8.0	j		0	į
K	5307.6	S?	525554	5394571	1.2	4.5	2.8	12.8	0.7	2.5	i		j 0	į
L	5289.8	S	525852	5395131	3.4	0.0	32.0	100.0	1.0	14.8	i		8	į
ĺМ	5280.2	S	526031	5395423	0.6	2.1	40.0	87.2	2.2	14.6	i		j o	į
N	5263.6	S	526329	5395957	0.5	1.5	3.1	9.0	0.7	1.4	i		i o	i
ĺО	5231.9		526886	5396983	0.0	4.8	4.9	67.2	1.3	8.9	i		i o	i
ĺР	5199.7		527471	5398072	1.1	6.1	5.3	52.0	1.3	7.9	i		i o	i
ĺΩ	5178.2	S	527862	5398772	2.3	11.0	55.9	159.8	4.1	23.2	i		i o	i
R	5163.9	S	528112	5399228	1.3	8.1	47.5	127.2	1.5	20.0			i o	į
İs	5157.5	S	528217	5399425	3.6	8.9	77.6	153.5	2.6	26.8			13	i
Т	5133.2		528578	5400059	2.9		112.1		3.6	30.0			0	į
LINE	10270		 FLIGHT	23	 						 			 
A	5570.7	S	523281	5390284	19.8	20.7	306.0	354.8	10.0	89.1	1.5	4	j 0	i
В	5585.7		523503	5390666	4.4	10.4	3.0	59.6	0.7	6.2				i
İc	5604.4		523774	5391165	3.0	4.6	51.0	24.4	7.1	18.7	0.5	25	0	i
D	5625.0		524101	5391754	1.5	9.7	100.9	168.7	2.3	30.7			0	i
E	5640.1		524332	5392199	1.0	15.5	50.6	136.9	1.0	20.4			0	į
F	5653.7		524549	5392589	0.4	1.6	4.2	31.5	1.6	4.3	i		i o	i
Ġ	5689.3		525151	5393627	3.6	12.9	52.8	159.4	1.3	24.5			11	i
Н	5736.3		525943	5395013	1.7	0.6	7.2	36.5	0.7	4.8			0	į
İı	5749.2	S	526128	5395385	i 0.0	3.2	36.1	91.7	1.7	14.6			j 5	i
jЈ	5760.1	S	526289	5395730	0.1	2.4	0.2	14.2	1.6	2.4			i o	i
ĸ	5799.7		526942	5396899	1.0	2.5	1.9	30.4	1.2	4.1			5	į
L	5837.4		527563	5398000	5.2	32.0	167.1	492.1	3.1	74.6	0.2	0	12	i
M	5883.8		528358	5399442	1.1	1.8	30.1	80.1	0.8	13.0			0	i
N	5897.6		528608	5399896	7.0	24.7		128.2	4.4	19.2			0	
   T.TNF	10280		 FLIGHT	23	 I						 I		 	 ا
A	6289.8	S	523349	5390211	27.5	47.9	419.9	575.3	10.3	126.7	1.0	0	0	
l B	6275.2		523595	5390661	4.7	7.2	8.5	50.1	2.3	5.4	0.6	25	94	
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CX = COAXIAL

CP = COPLANAR

EM Anomaly List

  Labe	l Fid	Inter	o XUTM	YUTM	   CX 55   Real	00 HZ Quad	CP 7	200 HZ Quad	CP Real	900 HZ Quad	   Vertica   COND	 l Dike DEPTH*	Mag. Corr 	
			m	m	ppm	ppm	ppm	ppm	ppm	n ppm	siemens	m	NT	
LINE	10280		FLIGHT	23	 						 		 	
İc	6261.5	S	523838	5391069	3.9	7.0	107.7	78.4	5.6	26.7	0.5	25	0	i
D	6239.2	S	524213	5391748	5.5	6.4	100.7	68.2	2.4	23.7	0.9	22	0	i
E	6225.5	S	524423	5392142	2.5	8.4	31.8	131.6	2.3	19.5	i		0	i
F	6210.8	S	524651	5392548	1.6	0.8	1.8	13.6	0.8	2.2	j		17	i
G	6177.3	S	525172	5393521	6.2	22.4	91.4	295.4	0.8	43.4	0.3	0	17	j
Н	6117.5	S	526216	5395385	2.3	2.4	19.2	73.7	0.7	10.8	j		7	j
İI	6036.1	S?	527666	5397980	4.8	21.2	52.6	184.2	0.9	26.8	j		10	j
J	5991.6	S	528448	5399388	1.5	3.7	2.2	20.7	1.1	1.9	j		5	j
K	5974.5	S	528705	5399863	11.3	27.0	41.6	155.1	1.8	22.7	0.6	0	0	j
LINE	10290		FLIGHT	23	 						 		 	 
A	6481.5	S	523434	5390193	5.5	7.2	110.5	137.2	2.1	29.4	0.8	8	0	i
В	6526.1	H	524136	5391388	8.5	12.4	139.6	173.2	7.5	47.5	0.8	11	0	i
ĺС	6547.5	S	524532	5392106	3.1	2.1	4.1	26.9	2.0	4.3	j		0	j
D	6582.0	S	525192	5393312	2.3	8.4	12.1	79.9	2.7	11.2	j		0	j
E	6663.2	S	526626	5395881	0.4	3.2	1.8	12.5	2.1	1.8	j		0	j
F	6727.6	S	527777	5397961	2.9	7.3	2.8	54.2	1.1	7.2	j		0	j
G	6731.6	S	527850	5398094	0.9	3.1	2.3	46.0	0.8	6.4			0	j
H	6772.6	S	528508	5399317	2.3	5.7	2.8	33.8	8.8	5.7			0	
I	6780.3	S	528648	5399536	5.4	14.5	12.3	106.3	6.6	15.0			0	
LINE	10300		FLIGHT	24	 						 			
A	628.6	S?	523524	5390097	20.5	46.4	312.5	514.8	4.0	103.7	0.7	0	24	j
В	626.0	S	523572	5390185	13.7	40.7	312.5	519.4	4.0	103.7	0.5	0	39	j
C	610.5	S	523854	5390693	2.9	3.0	3.6	27.2	2.2	3.8			27	j
D	588.0	H	524258	5391415	5.1	10.6	107.3	162.5	5.5	35.9	0.5	14	0	
E	574.4	E	524507	5391866	9.5	19.3	17.2	199.7	2.4	8.6			0	
F	531.1	S	525314	5393326	0.6	2.8	2.7	24.7	1.3	3.4			0	
G	492.8	S?	526029	5394628	0.0	4.6	3.1	32.5	0.8	4.6			0	
H	454.0	S	526752	5395917	6.2	1.7	1.1	9.9	2.4	1.5			6	
ļΙ	427.0	L	527241	5396807	18.7	1.6	184.7	13.3	192.7	24.0			185	ļ
J	393.5	S	527853	5397911	0.6	3.5	1.7	19.7	1.0	3.3			0	
K	343.5	S	528723	5399508	0.4	5.2	8.8	71.4	1.2	10.2			0	ļ
L	331.0	S 	528902 	5399828	10.2	4.3	176.8	238.1	5.1	49.6	3.8	29 	27 	
LINE	10310		FLIGHT	24	 	<b></b>	<b></b>	<b></b>	<b></b>	<b>_</b>		<b>_</b>		
A	740.7	S	523708	5390210	17.0	30.7	268.3	474.5	5.1	89.9	0.8	5	31	j
В	780.6	H	524303	5391295	6.3	11.8	189.6	123.7	9.4	39.1	0.6	18	14	j

CX = COAXIAL

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EM Anomaly List

					   CX 55	00 HZ	CP 7	 200 HZ	 CP	900 HZ	Vertica	 l Dike	Mag. Corr	
Labe	l Fid	Interp	MTUX	YUTM	Real	Quad	Real	Quad	Real	Quad	!	DEPTH*		[
			m	m	ppm	ppm	ppm	ppm	ppm	mqq ı	siemens	m	NT	
LINE	10310		FLIGHT	24	 						 			
C	883.4	S	526092	5394576	0.0	5.5	1.2	24.3	2.4	3.7	i		0	İ
D	1032.5	S	528852	5399487	5.0	4.3	7.1	36.5	0.9	5.7			0	j
E	1040.9	S	529007	5399772	7.6	10.3	103.7	112.6	3.3	27.0			0	
LINE	10321		FLIGHT	24	 						 			
A	1607.4	S	523842	5390291	27.7	40.8	297.9	418.0	7.0	80.4	1.2	5	0	
В	1639.3	S	524309	5391098	15.4	32.0	454.6	697.8	10.8	139.7	0.7	3	0	ĺ
C	1655.9	S	524583	5391584	18.7	30.7	275.3	334.0	10.6	80.7	0.9	2	54	
D	1668.1	S?	524775	5391929	3.4	6.5	36.4	93.3	1.1	14.4			0	
E	1719.6	S?	525576	5393368	0.8	10.8	19.1	86.8	1.1	12.2			14	ĺ
F	1733.1	S	525763	5393741	3.2	2.4	1.9	16.9	1.8	2.4			0	
G	1814.9	S	527103	5396144	0.5	1.5	2.1	10.3	1.1	1.3			20	
H	1832.7	L	527403	5396690	2.9	0.7	11.9	5.0	8.0	4.4			51	
I	1903.1	S	528617	5398889	1.1	3.5	12.4	15.4	10.1	1.9			0	
J	1922.3	S	528947	5399467	2.6	4.6	7.6	37.0	2.8	5.5			0	
LINE	10330		FLIGHT	24	 						 			
A	2453.4	S	523965	5390319	21.8	24.7	255.2	341.2	5.6	74.2	1.5	4	27	
В	2437.6	S	524264	5390780	3.4	20.0	116.0	409.6	5.5	62.8	0.2	0	144	
C	2428.6	S	524407	5391069	27.3	56.8	520.2	873.5	15.2	172.9	0.9	4	156	
D	2410.2	S	524700	5391642	2.6	7.2	55.5	31.7	9.7	19.3			0	
E	2351.9	S	525669	5393362	1.3	7.5	17.4	65.9	0.8	9.8			0	
F	2264.2	S	527131	5396009	1.5	3.0	1.9	39.5	1.5	5.9			30	
G	2198.6	S	528223	5397979	3.7	0.9	5.6	31.3	1.1	4.4			7	
H	2167.7	S	528731	5398858	3.1	3.7	8.3	41.1	1.2	5.5			0	
ΙI	2145.7	S	529023	5399436	0.3	3.4	9.1	52.8	0.3	7.9			26	
LINE	10340		FLIGHT	24	 						 			
A	2569.1	S?	523845	5389842	7.4	7.5	4.3	7.0	2.3	2.2	j		0	į
В	2588.6	S?	524105	5390301	26.7	46.5	292.0	527.2	0.0	106.9	1.0	4	106	j
C	2615.7	S	524473	5390983	13.5	17.0	268.1	286.6	13.7	65.8	1.1	23	0	i
D	2637.5	S	524804	5391570	19.6	35.1	290.9	408.6	11.9	89.4	0.9	8	0	į
E	2652.2	S	524988	5391940	28.3	66.9	351.0	669.7	5.8	123.7	0.8	1	0	į
F	2707.1	S	525880	5393521	0.0	6.1	100.0	109.9	5.7	27.3	j		0	į
G	2784.7	S	527019	5395589	1.3	4.4	4.1	27.2	1.1	5.0	j		0	į
Н	2847.7	S	527957	5397267	7.9	3.2	10.7	26.1	2.4	5.2	j		0	į
İI	2873.5	S	528335	5397929	3.2	8.0	36.3	58.0	1.8	11.1	i		0	į
jЈ	2899.8	S	528703	5398657	4.2	5.9	11.4	19.3	1.2	2.3	j		0	j

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

  Labe	l Fid	Inte	rp XUTM	YUTM m	CX 55   Real   ppm	00 HZ Quad ppm	CP 7 Real ppm	200 HZ Quad ppm	CP Real ppm	900 HZ Quad ppm	Vertical   COND I   siemens	l Dike DEPTH* m	Mag. Corr     NT	
	10350		FLIGHT	24	 I						 I		 I	
A	3396.4	S?	524109	5390123	10.0	8.1	15.3	23.1	0.5	6.5	l   1.6	22	0	
lB	3390.4	s: S	524223	5390123	9.0	7.5	163.0	180.0	4.6	44.7	1.5	16	0	
IC	3356.9	S	524930	5391606	8.3	9.9	223.9	273.7	8.3	66.4	1.0	27	0	
l D	3341.7	S	525251	5392190	4.7	6.2	69.1	74.8	2.8	18.1	0.8	36	0	
E	3306.1	S	525955	5393441	4.7	10.9	221.9	215.9	7.4	56.8	0.4	14	0	l
F	3193.4	S	528007	5397154	3.0	8.8	53.1	120.8	1.2	18.0	0.3	16	8	l
Ġ	3159.7	S	528554	5398180	2.5	1.6	17.9	15.6	1.3	3.3	l		0	l
H	3136.1	S	528924	5398836	4.4	11.2	18.0	68.3	2.2	10.5	 		0	i
I	3123.2	S	529137	5399202	2.0	4.1		110.9	1.6	15.6			61	İ
LINE	19010		FLIGHT	24	 						 		 	
A	5115.6	S	529012	5399495	2.9	9.0	15.3	60.3	1.2	8.4	i		0	į
В	5086.5	S	528208	5400050	8.3	14.0	244.9	290.0	10.1	67.0	0.7	8	0	į
C	5071.5	S	527790	5400335	26.6	61.6	241.6	472.0	22.6	74.1	0.8	0	213	į
D	5057.4	L	527432	5400563	19.3	10.4	40.4	13.6	47.2	3.4	3.4	23	0	ĺ
E	5042.4	L	527110	5400817	14.7	3.0	76.9	81.0	15.2	19.5			0	ĺ
F	5005.6	L	526339	5401384	21.3	2.1	21.6	31.6	18.7	32.6			0	į
LINE	19020		FLIGHT	24	 						 		 	
A	4047.2	S	521642	5390005	2.9	4.2	9.3	38.1	1.0	3.8			0	į
В	4062.6	S	521080	5389999	14.3	26.3	223.1	550.0	3.5	89.7	0.8	9	0	ĺ
C	4081.1	S	520362	5389985	5.6	10.7	186.7	108.8	17.5	56.8	0.5	17	j 7	İ

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Note:EM values shown above are local amplitudes

Area A - 19 -

\*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

    Labe	l Fid	Interp	MTUX e	YUTM	   CX 55   Real	00 HZ Quad	CP 7	200 HZ Quad	CP Real	900 HZ Quad	   Vertica   COND	 l Dike DEPTH*	   Mag. Corr 	
İ			m	m	ppm	ppm	ppm	ppm	ppm	ı ppm	siemens	m	NT	j
LINE	20010		FLIGHT	2	 						 		 	
A	722.3	L	526779	5401340	7.3	5.5	5.5	12.6	24.8	42.3			0	
В	744.4	L	527273	5401089	0.0	5.8	36.5	50.4	11.5	11.5			0	
C	760.0	S	527609	5400890	5.4	0.9	21.2	26.6	7.2	7.0			0	
D	768.5	S	527803	5400797	1.8	3.5	13.6	6.1	2.9	6.2			0	
E	785.5	L	528216	5400584	26.4	6.0	7.1	10.3	1.6	5.3	12.7	6	372	
F	796.6	S	528498	5400426	5.3	0.2	7.7	45.3	2.4	7.1			0	
G	812.2	S	528894	5400244	11.8	19.4	149.2	228.0	5.4	41.4	0.8	0	0	
H	828.2	S	529314	5400025	4.8	3.2	119.1	160.2	3.6	29.1	1.6	44	0	
I	847.9	S	529817	5399742	1.3	10.4	76.1	212.4	5.1	32.5			93	
J	879.0	S	530689	5399302	7.4	15.6	46.0	84.7	1.2	19.8	0.6	6	0	
K	910.3	S	531542	5398851	6.5	26.4	55.1	291.0	2.1	40.2			27	
L	920.9	S	531817	5398713	1.0	3.7	2.0	20.6	3.4	2.5			48	
M	932.6	S	532120	5398537	8.4	15.7	84.1	206.6	3.3	31.8			5	
N	939.9	S	532337	5398414	9.1	13.9	140.2	279.7	24.3	45.0	0.8	9	17	ĺ
0	965.9	S	533066	5398049	2.6	3.6	7.7	49.0	5.1	5.9			0	ĺ
P	972.4	S	533234	5397949	2.1	3.7	2.8	21.0	1.7	3.1			0	
Q	993.0	S	533773	5397685	0.5	1.4	3.4	8.7	3.2	1.2			0	ĺ
R	1034.0	S	534936	5397053	9.9	19.6	102.1	195.9	3.8	33.4			0	
LINE	20020		FLIGHT	3	 						 		 	
A	600.8	L	526277	5401389	12.8	0.0	2.6	0.0	104.9	156.6	i		51	Ì
В	556.2	L	527530	5400804	3.6	3.4	20.1	13.9	2.6	4.5	i		j o	į
C	526.7	L	528193	5400382	14.9	6.4	17.6	22.0	10.5	9.2	i		112	į
D	509.3	S	528673	5400131	7.7	38.6	197.6	379.1	4.1	66.4	0.3	0	j o	į
E	498.8	S	528978	5399967	3.6	10.6	140.7	74.5	10.0	33.7	0.3	2	j o	į
F	474.8	S	529674	5399601	2.8	12.5	12.5	88.3	4.9	12.2	i		j o	į
Ġ	450.2	S	530367	5399243	3.9	33.1	122.2	318.9	2.1	49.1	0.1	0	j o	į
Н	439.0	S	530707	5399058	3.0	11.1	45.9	182.6	1.6	26.4	i		j o	į
İI	416.7	S	531352	5398722	7.0	32.4	16.2	164.8	1.2	21.0			50	j
jЈ	411.6	S	531498	5398641	2.2	8.9	3.2	47.3	1.4	5.9			26	į
ĸ	395.8	S	531939	5398412	14.4		178.4	412.8	1.8	67.5	1.1	11	82	j
L	369.5	S	532687	5398016	3.9	13.3	5.3	89.4	3.4	12.2			44	j
М	363.6	S	532859	5397926	0.0	14.4	4.8	82.1	5.7	11.1			0	j
N	348.3	S	533297	5397691	1.1	5.3	2.8	13.1	2.8	2.1			0	j
ю	331.5	S	533765	5397449	1.4	8.9	7.5	70.3	0.4	9.0			0	j
P	322.2	S	534027	5397313	1.9	2.4	5.3	35.3	6.1	4.5			i o	j
Q	297.0	S?	534685	5396959	12.9	35.5		249.6	6.3	38.6	0.5	2	0	j
													· 	

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EM Anomaly List

i	l Fid	Interp	MTUX e	YUTM	CA 55   Real	00 HZ Quad	CP 7 Real	200 HZ Quad	CP Real	900 HZ Quad	Vertica   COND	I DIKE DEPTH*	Mag. Corr 	
			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	İ
LINE	20030		FLIGHT	3	 						 		 	
A	680.7	S	526105	5401262	1.1	4.4	61.0	78.4	48.9	18.3			0	
В	705.3	L	526780	5400854	0.1	3.9	28.6	18.7	7.4	10.6			0	
C	740.0	S	527775	5400347	5.8	12.6	60.9	105.2	3.5	18.4			0	
D	757.4	S	528262	5400127	9.0	23.6	114.3	269.7	0.8	44.4			0	
E	763.5	S	528431	5400042	7.2	4.8	168.5	251.9	3.6	49.9	1.9	34	0	
F	779.8	S	528890	5399788	6.9	12.9	120.8	191.5	3.0	35.0			20	
G	791.3	S	529231	5399610	0.2	0.0	9.1	61.3	2.8	8.9			0	ĺ
H	826.1	S	530253	5399070	6.1	20.1	13.0	79.4	2.0	11.8			0	ĺ
I	834.1	S	530496	5398945	5.3	16.8	59.2	253.2	0.0	36.1			0	ĺ
J	850.7	S	530981	5398692	4.0	18.5	19.2	154.3	2.0	20.8			0	ĺ
K	858.9	S	531218	5398561	5.7	25.0	11.9	100.4	1.6	13.7	i		10	İ
L	864.9	S	531393	5398470	3.3	10.4	5.5	62.4	0.8	7.4			9	ĺ
M	877.0	S	531748	5398284	17.4	59.8	139.9	546.7	2.2	78.3	0.5	0	0	į
N	886.2	S	532014	5398149	9.0	27.0	27.1	77.1	19.2	10.9			0	ĺ
0	904.6	S	532528	5397875	2.5	6.8	10.4	84.5	3.1	11.5			0	ĺ
P	948.9	S	533662	5397279	1.4	6.2	4.6	79.0	0.8	10.9	i		0	İ
Q	980.6	S	534505	5396834	9.1	12.7	30.5	102.9	2.0	14.3			j o	İ
LINE	20040		FLIGHT	3	 						 		 	
A	1330.0	E	527340	5400397	23.3	18.9	217.4	245.9	6.6	61.2	2.2	0	0	ĺ
В	1326.1	S	527427	5400339	9.0	16.5	217.0	178.7	10.5	57.8	0.7	5	0	ĺ
C	1298.7	S	528164	5399944	6.7	18.7	216.0	246.8	14.6	67.2	0.4	0	0	ĺ
D	1267.8	S	529019	5399497	2.8	8.9	9.2	67.9	0.8	9.4			0	ĺ
E	1256.2	S	529330	5399331	3.9	11.3	15.4	60.8	1.4	8.6			0	ĺ
F	1223.2	S	530192	5398875	5.8	17.0	78.7	120.3	2.2	21.8	0.4	0	23	ĺ
G	1205.0	S	530674	5398621	2.9	0.7	9.1	61.3	1.2	8.5			0	
H	1182.7	S	531256	5398327	3.8	19.8	23.2	143.2	1.2	20.2			24	ĺ
I	1167.6	S	531649	5398107	7.0	13.8	16.1	67.6	8.8	9.0			0	ĺ
J	1158.1	S?	531913	5397971	23.8	50.8	296.9	506.6	8.6	91.5	0.8	0	93	ĺ
K	1070.3	S	534283	5396725	7.2	28.4	232.3	274.5	8.2	63.4	0.3	0	0	İ
LINE	20050		FLIGHT	3	 						 		 	
A	1626.8	S	526201	5400750	7.9	4.4	22.6	76.5	14.7	11.3	2.5	37	0	j
В	1644.0	L	526713	5400502	7.4	2.5	15.2	8.1	15.2	6.9			1526	j
C	1655.4	S	527034	5400320	3.6	11.2	48.3	130.1	5.6	20.2	0.3	0	0	į
D	1671.4	S	527499	5400068	8.2	10.9	149.2	171.0	11.1	30.1	0.9	15	0	į
E	1686.0	S?	527921	5399850	28.2	31.0	26.3	225.5	12.8	8.4	1.6	7	j o	į

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EM Anomaly List

						   CX 55	00 HZ	CP 7	200 HZ	 CP	900 HZ	Vertica	 l Dike		 
LINE 20050	Labe	el Fid	Intern	XUTM	YUTM	Real	Ouad	Real	Ouad			COND	DEPTH*		i
F   1691.7   S   528091   5399765   13.3   13.0   243.3   229.7   13.5   68.7   1.5   10   0   0   1731.3   2   S   528696   5399318   0.0   10.4   12.6   64.7   4.6   8.7     147   147   147   1731.2   S   528922   5399319   2.9   7.1   7.0   20.4   5.4   2.7     0   1   1731.5   S   529220   5399163   2.3   7.8   61.0   167.7   4.7   24.7     0   1   1749.2   S   529754   5398899   1.1   11.1   42.1   103.0   2.0   15.6     0   1   1749.2   S   530186   5398606   8.0   13.3   96.6   204.8   2.5   33.6   0.7   7   13   1   1775.8   S   530530   5398255   5.2   7.0   50.7   228.7   0.7   31.8   0.7   25   27   0   1   1775.8   S   530530   5398255   5.2   7.0   50.7   228.7   0.7   31.8   0.7   25   27   0   1   1775.8   3.5   331626   5397356   0.0   6.8   27.5   118.6   2.4   17.6       0   1   1   1   1   1   1   1   1   1	İ		-	m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	j
C	LINE	20050		FLIGHT	3	 						 		 	 
C	F	1691.7	S	528091	5399766	i 13.3	13.0	243.3	229.7	13.5	68.7	1.5	10	i o	i
H 1721.2   S7   528922   5399319   2.9   7.1   7.0   20.4   5.4   2.7       0   1   1731.5   S   529220   53993163   2.3   7.8   61.0   167.7   4.7   24.7       0   0   1749.2   S   529274   539889   1.1   11.1   42.1   103.0   2.0   15.6       0   0   1   1749.2   S   529574   539889   1.1   11.1   42.1   103.0   2.0   15.6       0   0   1   1758.8   S   530186   5398660   8.0   13.3   96.6   204.8   2.5   33.6   0.7   7   7   13   1   175.8   S   530180   5398265   1.8   10.9   84.7   236.8   0.2   35.8       0   1   175.8   S   530530   5398255   5.2   7.0   50.7   228.7   0.7   31.8   0.7   25   27   1   1   1   1   1   1   1   1   1	İG					1								147	i
I	н		S?	528922			7.1		20.4					j o	i
J	İı	1731.5	S	529220		2.3	7.8	61.0	167.7	4.7				0	į
K	jЈ	1749.2	S	529754	5398889		11.1	42.1	103.0	2.0	15.6			0	į
L	K	1764.0	S	530186		8.0	13.3	96.6	204.8	2.5	33.6	0.7	7	13	į
N	L	1775.8	S	530530		1.8	10.9	84.7	236.8	0.2	35.8			0	į
O	M	1792.3	S	531010	5398225	5.2	7.0	50.7	228.7	0.7	31.8	0.7	25	27	į
P	N	1813.7	S	531626	5397899	11.1	20.1	129.6	239.5	2.7	40.1	0.7	5	0	į
Q	0	1851.0	S	532658	5397356	0.0	6.8	27.5	118.6	2.4	17.6			0	j
R	P	1879.9	S	533386	5396967	0.0	2.6	1.6	10.5	1.3	1.1			0	į
S	İQ	1903.4	S	534012	5396637	7.9	4.7	56.0	119.3	4.2	24.8	2.2	17	j o	į
LINE 20060   FLIGHT 3	R	1909.6	S?	534188	5396546	15.1	12.7	42.1	99.1	4.0	16.5	1.8	10	0	į
A 2299.8   S 526106   5400580   8.2   8.6   32.5   38.3   30.6   4.7       199	S	1919.4	S?	534443	5396417	5.6	17.3	10.0	49.6	2.7	6.6	0.4	2	0	j
A 2299.8   S 526106   5400580   8.2   8.6   32.5   38.3   30.6   4.7       199	LINE	20060		FLIGHT	3	 						 			 
C   2277.9   L?   526608   5400321   20.6   16.3   160.5   128.6   60.7   51.4   2.1   2   0     D   2264.9   H   526954   5400137   7.5   6.6   46.2   40.1   9.7   21.8   1.3   28   0     E   2224.0   S   528058   5399547   6.6   18.4   247.8   102.9   11.8   69.4   0.4   0   0     F   2214.2   S   528329   5399405   7.7   21.1   72.5   210.4   2.5   31.9   0.5   0   0     G   2185.5   S   529108   5398995   1.4   6.7   13.8   58.8   1.4   8.0       0     H   2168.5   S   529571   5398745   7.0   15.1   93.9   161.9   2.5   27.9   0.5   4   0     I   2152.2   S   529994   5398528   3.7   10.2   71.0   114.3   1.7   22.4   0.4   0   22     J   2136.3   S   530408   5398321   7.6   2.0   141.2   178.4   2.4   40.7       80     K   2123.0   S   530771   5398120   4.1   11.6   12.8   79.3   0.7   11.3   0.4   4   0     L   2112.4   S   531044   5397973   0.0   11.5   2.7   12.7   0.6   1.9       9     M   2102.9   S   531293   5397840   3.8   13.1   148.0   320.7   4.6   53.5   0.3   0   0     N   2091.8   S   531597   5397683   6.7   12.7   164.2   341.6   2.6   56.1   0.6   8   0     O   2075.8   S?   532631   5397452   2.9   29.8   31.5   177.0   4.2   23.9       0     P   2061.9   S   532432   5397245   7.2   8.2   35.0   122.9   1.9   17.4   1.0   15   0     Q   2015.8   S?   533685   5396584   4.4   7.8   18.3   63.7   6.0   9.4   0.5   23   0     R   1996.6   S   534210   5396317   2.2   10.3   214.6   341.7   5.0   63.1       16      LINE   20070   FLIGHT   3			S			8.2	8.6	32.5	38.3	30.6	4.7			199	i
C   2277.9   L?   526608   5400321   20.6   16.3   160.5   128.6   60.7   51.4   2.1   2   0     D   2264.9   H   526954   5400137   7.5   6.6   46.2   40.1   9.7   21.8   1.3   28   0     E   2224.0   S   528058   5399547   6.6   18.4   247.8   102.9   11.8   69.4   0.4   0   0     F   2214.2   S   528329   5399405   7.7   21.1   72.5   210.4   2.5   31.9   0.5   0   0     G   2185.5   S   529108   5398995   1.4   6.7   13.8   58.8   1.4   8.0       0     H   2168.5   S   529571   5398745   7.0   15.1   93.9   161.9   2.5   27.9   0.5   4   0     I   2152.2   S   529994   5398528   3.7   10.2   71.0   114.3   1.7   22.4   0.4   0   22     J   2136.3   S   530408   5398321   7.6   2.0   141.2   178.4   2.4   40.7       80     K   2123.0   S   530771   5398120   4.1   11.6   12.8   79.3   0.7   11.3   0.4   4   0     L   2112.4   S   531044   5397973   0.0   11.5   2.7   12.7   0.6   1.9       9     M   2102.9   S   531293   5397840   3.8   13.1   148.0   320.7   4.6   53.5   0.3   0   0     N   2091.8   S   531597   5397683   6.7   12.7   164.2   341.6   2.6   56.1   0.6   8   0     O   2075.8   S?   532631   5397452   2.9   29.8   31.5   177.0   4.2   23.9       0     P   2061.9   S   532432   5397245   7.2   8.2   35.0   122.9   1.9   17.4   1.0   15   0     Q   2015.8   S?   533685   5396584   4.4   7.8   18.3   63.7   6.0   9.4   0.5   23   0     R   1996.6   S   534210   5396317   2.2   10.3   214.6   341.7   5.0   63.1       16      LINE   20070   FLIGHT   3	В	2291.4	S	526307	5400471	2.6	7.1	26.6	17.9	33.7	2.9			j o	i
D	İc	2277.9	L?	526608	5400321		16.3	160.5	128.6	60.7	51.4	2.1	2	0	į
F   2214.2   S   528329   5399405   7.7   21.1   72.5   210.4   2.5   31.9   0.5   0   0   0   0   0   0   0   0   0	D				5400137							1.3	28	0	į
G 2185.5 S 529108 5398995   1.4 6.7 13.8 58.8 1.4 8.0	E	2224.0	S	528058	5399547	6.6	18.4	247.8	102.9	11.8	69.4	0.4	0	0	į
H	F	2214.2	S	528329	5399405	7.7		72.5		2.5		0.5	0	0	į
I	Ġ	2185.5	S	529108	5398995	1.4	6.7	13.8	58.8	1.4	8.0	i		j o	į
J 2136.3 S 530408 5398321   7.6 2.0 141.2 178.4 2.4 40.7   80	Н	2168.5	S	529571	5398745	7.0	15.1	93.9	161.9	2.5	27.9	0.5	4	0	į
K   2123.0   S   530771   5398120	Ī	2152.2	S	529994	5398528	3.7	10.2	71.0	114.3	1.7	22.4	0.4	0	22	į
L 2112.4 S 531044 5397973   0.0 11.5 2.7 12.7 0.6 1.9     9    M 2102.9 S 531293 5397840   3.8 13.1 148.0 320.7 4.6 53.5   0.3 0   0    N 2091.8 S 531597 5397683   6.7 12.7 164.2 341.6 2.6 56.1   0.6 8   0    O 2075.8 S? 532031 5397452   2.9 29.8 31.5 177.0 4.2 23.9     0    P 2061.9 S 532432 5397245   7.2 8.2 35.0 122.9 1.9 17.4   1.0 15   0    Q 2015.8 S? 533685 5396584   4.4 7.8 18.3 63.7 6.0 9.4   0.5 23   0    R 1996.6 S 534210 5396317   2.2 10.3 214.6 341.7 5.0 63.1     16     LINE 20070 FLIGHT 3    A 2419.5 S 525944 5400434   7.0 5.7 222.8 280.8 21.3 58.7   1.4 23   809	J	2136.3	S	530408	5398321	7.6	2.0	141.2	178.4	2.4	40.7			80	ĺ
M   2102.9   S   531293   5397840   3.8   13.1   148.0   320.7   4.6   53.5   0.3   0   0   0   0   0   0   0   0   0	K	2123.0	S	530771	5398120	4.1	11.6	12.8	79.3	0.7	11.3	0.4	4	0	į
N	L	2112.4	S	531044	5397973	0.0	11.5	2.7	12.7	0.6	1.9			9	ĺ
O 2075.8 S? 532031 5397452   2.9 29.8 31.5 177.0 4.2 23.9     O     P 2061.9 S 532432 5397245   7.2 8.2 35.0 122.9 1.9 17.4   1.0 15   O     Q 2015.8 S? 533685 5396584   4.4 7.8 18.3 63.7 6.0 9.4   0.5 23   O     R 1996.6 S 534210 5396317   2.2 10.3 214.6 341.7 5.0 63.1     16     LINE 20070 FLIGHT 3	M	2102.9	S	531293	5397840	3.8	13.1	148.0	320.7	4.6	53.5	0.3	0	0	į
P 2061.9 S 532432 5397245   7.2 8.2 35.0 122.9 1.9 17.4   1.0 15   0     Q 2015.8 S? 533685 5396584   4.4 7.8 18.3 63.7 6.0 9.4   0.5 23   0     R 1996.6 S 534210 5396317   2.2 10.3 214.6 341.7 5.0 63.1     16	N	2091.8	S	531597	5397683	6.7	12.7	164.2	341.6	2.6	56.1	0.6	8	0	į
Q 2015.8 S? 533685 5396584   4.4 7.8 18.3 63.7 6.0 9.4   0.5 23   0   R 1996.6 S 534210 5396317   2.2 10.3 214.6 341.7 5.0 63.1     16     LINE 20070 FLIGHT 3	0	2075.8	S?	532031	5397452		29.8	31.5	177.0	4.2	23.9			0	į
R 1996.6 S 534210 5396317   2.2 10.3 214.6 341.7 5.0 63.1     16	P	2061.9	S	532432	5397245	7.2	8.2	35.0	122.9	1.9	17.4	1.0	15	0	į
LINE 20070	Q	2015.8	S?	533685	5396584				63.7	6.0	9.4	0.5	23	0	į
A 2419.5 S 525944 5400434 7.0 5.7 222.8 280.8 21.3 58.7 1.4 23 809	R	1996.6	S	534210	5396317	2.2	10.3	214.6	341.7	5.0	63.1			16	j
A 2419.5 S 525944 5400434 7.0 5.7 222.8 280.8 21.3 58.7 1.4 23 809	LINE	20070		FLIGHT	3	 						 			 
			S			7.0	5.7	222.8	280.8	21.3	58.7	1.4	23	809	j
	!											l .		I .	İ

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					   CX 55		CP 7	200 HZ	CP	900 HZ	Vertical	 l Dike	Mag. Corr	
Labe:	l Fid	Interp	MTUX	YUTM	Real	Quad	Real	Quad	Real	Quad	COND I	DEPTH*		
			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	
LINE	20070		FLIGHT	3	 						 			
C	2449.7	Н	526844	5399958	4.5	2.4	20.5	34.2	7.2	10.5			0	ĺ
D	2481.8	S	527785	5399473	14.2	20.0	69.7	135.8	2.1	21.5	1.0	0	0	ĺ
E	2489.6	S	528017	5399352	5.7	10.7	218.2	253.5	5.7	59.9	0.6	13	0	ĺ
F	2508.7	S	528532	5399073	6.5	7.6	4.8	31.6	5.8	4.5			0	
G	2521.7	S	528885	5398886	4.5	0.3	20.1	54.1	3.9	8.9			0	
H	2539.8	S	529421	5398604	6.5	16.9	150.7	247.0	2.8	48.0	0.4	0	0	
I	2550.7	S	529748	5398438	6.7	17.6	90.8	214.6	1.7	37.0	0.4	0	0	
J	2572.9	S	530361	5398122	3.6	8.0	148.0	197.0	3.0	41.5	0.4	14	23	
K	2592.0	S	530887	5397832	2.4	9.8	30.8	127.5	1.0	17.7			0	
L	2600.9	S	531147	5397691	3.8	18.9	235.2	293.7	6.2	72.1	0.2	0	20	
M	2616.9	S	531600	5397456	7.6	15.7	114.3	341.3	5.7	52.3	0.6	6	0	
N	2623.7	S	531800	5397356	11.1	11.5	142.5	278.7	1.4	47.1	1.3	17	15	ĺ
0	2634.1	S	532096	5397203	0.5	11.3	182.2	349.1	3.3	59.6			0	ĺ
P	2647.5	S	532455	5397011	6.9	29.9	75.0	205.1	3.1	30.4	0.3	0	29	
Q	2663.7	S	532865	5396788	2.1	4.8	6.1	15.5	1.2	1.1			0	
R	2685.5	S?	533450	5396488	8.0	17.3	131.8	215.9	2.2	41.1	0.6	0	0	
S	2699.8	S	533859	5396269	13.8	15.0	86.5	194.4	1.5	31.8	1.3	1	7	ĺ
T	2712.5	H	534236	5396063	9.6	9.6	110.7	54.7	8.1	27.7	1.3	23	110	
LINE	20080		FLIGHT	3	 						 			
A	3274.1	S	525017	5400694	4.3	2.9	10.0	24.0	11.1	5.1			225	
В	3247.3	S	525699	5400353	13.5	12.1	139.8	244.4	5.2	41.1	1.6	7	470	ĺ
C	3232.0	L	526057	5400170	25.9	25.8	98.2	212.9	5.6	41.9	1.8	0	0	ĺ
D	3209.3	H	526687	5399833	5.1	3.9	25.2	42.4	12.2	12.0	1.4	45	0	
E	3183.0	S	527414	5399428	7.9	1.6	82.9	114.6	48.7	18.7			0	
F	3174.0	S	527635	5399309	14.8	16.6	229.3	286.1	7.6	64.0	1.3	6	0	
G	3162.1	S	527958	5399145	0.7	6.2	9.0	37.9	1.7	6.3			0	
H	3130.8	S	528789	5398708	4.4	7.0	22.7	54.2	1.7	8.7	0.6	16	0	
Ι	3112.5		529294	5398451	5.9	15.6	187.1	227.1	5.4	51.6	0.4	2	0	
J	3101.8	S	529602	5398287	12.5	14.4	104.1	212.3	2.4	37.2	1.2	4	15	
K	3083.4		530086	5398018	1.9	3.5	25.3	62.2	1.4	8.7			0	
L	3069.1		530437	5397844	10.7	24.1	62.1	236.6	2.4	34.2	0.6	1	7	
M	3049.7		530974	5397564	8.9	17.7	217.6	275.1	3.0	64.5	0.6	3	24	
N	3023.8		531658	5397201	7.8	16.8	176.3	377.6	5.3	62.0	0.6	2	0	
0	3003.3		532236	5396896	3.3	4.5	53.6	113.8	3.5	19.6	0.6	37	8	
P	2967.2	D	533223	5396379	15.3		131.9		11.6	38.8	2.7	6	0	
Q	2932.1	S	534174	5395875	12.7	20.2	145.1	128.0	8.7	46.5	0.9	2	0	

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<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

Labe	l Fid	Inter	MTUX o	YUTM m	   CX 55   Real	00 HZ Quad ppm	Real	200 HZ Quad	CP Real		Vertica   COND   siemens	l Dike DEPTH*	   Mag. Corr     NT	   
<u> </u>			 		ppm		ppm	pm	mqq 					
LINE	20090		FLIGHT	3									1	1
A	3358.3	S	524959	5400505	0.9	2.2	13.4	43.6	9.0	5.8	i		0	į
В	3377.8	S	525524	5400200	8.5	8.7	198.8	203.3	3.5	49.2	1.2	28	0	į
ĺС	3415.6	H	526578	5399648	9.5	2.7	80.6	52.8	20.2	32.1	j		0	į
D	3442.5	S?	527292	5399272	4.7	10.2	14.2	15.5	4.6	2.7	0.5	6	0	į
E	3455.6	S	527668	5399074	0.1	2.9	120.8	215.8	3.1	36.1			0	ĺ
F	3507.0	S	529089	5398326	6.0	9.7	55.3	94.6	1.9	16.9	0.7	18	0	į
G	3541.4	S	530107	5397807	4.4	5.8	6.8	12.5	0.0	1.7	0.7	30	0	į
H	3556.9	S	530570	5397550	3.6	5.0	25.0	95.2	0.8	12.6	0.6	29	8	ĺ
I	3570.1	S	530952	5397345	11.7	15.6	128.0	75.2	0.8	46.8	1.0	7	37	ĺ
J	3610.0	S	532012	5396785	8.4	12.9	306.3	300.1	7.1	80.8	0.8	11	81	ĺ
K	3639.7	S	532834	5396360	0.8	11.9	31.7	140.1	3.4	20.5			0	ĺ
L	3645.7	D	533011	5396265	23.6	25.1	101.4	297.2	10.2	41.2	1.6	2	24	ĺ
M	3678.8	H	533940	5395775	6.6	16.3	31.2	148.6	0.1	12.3	0.5	2	0	ĺ
LINE	20100		FLIGHT	3										
A	4101.1	S	524521	5400501	8.3	10.1	5.3	43.9	3.6	5.9			0	
В	4063.4	H	525486	5400004	7.7	7.4	70.4	117.4	3.4	21.0	1.2	28	0	
C	4040.0	H	526148	5399650	0.7	2.1	46.0	33.6	2.3	13.0			0	
D	4012.4	S	526954	5399229	5.4	9.5	3.4	29.3	1.2	3.6			0	
E	4004.1	S?	527188	5399113	3.8	9.4	9.2	12.8	3.7	0.9			0	
F	3997.4	S	527381	5399005	14.2	6.0	22.1	84.1	0.0	12.0	4.3	32	59	
G	3993.0	В	527509	5398930	2.6	3.6	7.9	9.7	9.1	1.2			0	
H	3981.8	S	527835	5398752	3.2	10.2		122.7	1.6	18.8			5	
I	3944.0	S	528822	5398254	0.7	4.7		142.4	3.9	35.8			0	ļ
J	3924.3	S	529360	5397959	7.0		130.8		2.8	39.7	0.6	0	47	
K	3911.9	S	529702	5397779	10.1	11.3		121.9	1.5	23.2	1.1	0	0	
L	3893.6	S	530165	5397535	14.2	27.9		101.7	2.0	14.1	0.7	0	16	ļ
M	3883.5	S	530437	5397393	3.8	23.1		176.0	0.8	25.2	0.2	0	0	
N	3869.1	S	530845	5397172	9.3	24.4		197.5	3.8	30.4	0.5	0	0	ļ
0	3860.1	S	531099	5397040	4.3	3.9	8.6	50.2	3.8	7.2			0	
P	3828.2	S	531912	5396611	24.9	50.8	233.1	413.7	10.3	73.3	0.9	0	97	ļ
Q	3801.0	S	532659	5396220	7.8	10.8		153.4	3.9	23.8	0.8	9	0	ļ
R	3796.1	D	532796		16.2	26.0		177.2	16.9	25.5	0.9	0	17	ļ
S	3764.2	H	533652	5395702	3.7	1.9	96.1	10.2	16.4	37.0			0	
	20110			2							 I		 I	
	20110	С	FLIGHT 524225	3 5400440	0.0	7 0	21 7	20 1	22.9	E 0	 		l I 0	
A	4313.8	S 	JZ4ZZJ 	54UU44U 	U.U	7.0	21.7	32.1	 	5.0			U	 

CX = COAXIAL

CP = COPLANAR

Note:EM values shown above are local amplitudes

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

Labe	l Fid	Interp	XUTM	YUTM m	   CX 55   Real   ppm	00 HZ Quad ppm	CP 7 Real	200 HZ Quad ppm	CP Real ppm	~	Vertica   COND   siemens	l Dike DEPTH*	Mag. Corr       NT	
					PP!!! 									
LINE	20110		FLIGHT	3										
В	4339.1	В	525009	5400020	13.4	16.8	222.2	154.0	27.7	60.3	1.1	12	0	
C	4361.3	H	525717	5399651	3.9	7.9	38.6	45.5	11.3	28.2	0.5	22	0	
D	4375.3	S	526156	5399427	7.5	10.0		156.1	2.6	29.4	0.9	13	5	
E	4384.3	S?	526417	5399291	9.0	11.2	6.3	43.1	0.4	4.4	1.0	21	0	
F	4402.4	S	526950	5399006	4.9	15.7	122.2	240.4	2.3	41.2	0.3	0	17	
G	4412.1		527252	5398842	7.7	15.6	208.6	207.4	4.5	53.8	0.6	4	148	
H	4420.0		527488	5398719	0.8	0.0	21.7	0.0	16.0	0.0			0	
Ι	4424.8		527629	5398647	2.1	7.1		131.2	6.3	21.5			26	
J	4461.2		528660	5398097	1.7		166.3		3.7	47.3			94	
K	4493.0	S	529608	5397601	12.7	9.5	196.9	231.0	3.3	53.4	1.9	14	0	
L	4502.0	S	529862	5397470	5.4	13.4	21.3	15.4	1.2	2.9	0.4	0	0	
M	4523.8	S	530503	5397132	15.9	41.8	159.9	378.7	3.7	61.6	0.6	0	6	
N	4531.3	S?	530724	5397010	11.7	38.9	38.3	178.8	0.0	25.4	0.4	0	0	
0	4570.5	S?	531794	5396459	10.8	29.0	53.7	200.3	5.0	28.8	0.5	0	81	
P	4593.5	S	532445	5396107	0.9	4.4	19.7	83.1	4.3	12.4			0	
Q	4598.0	D	532582	5396031	13.4	12.1	28.8	70.8	20.1	11.0	1.6	21	9	1
R	4627.0	H	533424	5395599	17.4	10.1	99.9	78.6	9.3	34.4	3.0	15	0	
LT TATE	20120		FLIGHT		 I						 I			
:	20120 5046.8	C	524210	5400225	2.2	7.7	3.5	43.7	6.2	5.5			149	- !
A					4.7		111.2	46.9			0.5	22	149	-
В  С	5014.0		525021 525664	5399794	15.5		154.0		7.5	25.4	0.5 3.9	30	0	-
	4991.4		526594	5399457	1	5.7			19.4	50.1	3.9 	30 	0	-
D	4959.2			5398961	2.5			120.0	1.8	22.6			1	-
E	4951.4 4942.3		526820	5398846	2.9	32.3 5.6	37.2	170.2	1.6	28.1	0.7	0	28	-
F			527099	5398697				84.0	1.6	13.2			1	-
G	4931.1		527452	5398513	4.5	5.2	30.3	18.4	18.0	12.6	0.8	26 14	90	- !
H	4888.7		528611 529259	5397903	13.1	13.7	98.5	122.3	6.2	22.1	1.3	14 9	0 0	- !
I	4865.2			5397568	4.4				5.4	45.9	0.6		U   7	- !
J V	4854.6		529557	5397409	2.3	3.4		106.1	3.0	16.6	1.3	36 	17	ļ
K	4845.6		529802	5397275		9.7	14.1	52.9	0.2	8.5	l		•	ļ
L	4825.2		530370	5396976	6.2	8.5	44.7	89.1	1.2	14.3	0.8	14	0	
M	4777.3		531672	5396286	5.4	10.7	28.7		3.4	17.2	0.5	3	0	
N	4753.5		532344	5395936	3.6	0.0	10.0	28.5	2.2	5.1			0	ļ
0	4726.9		533059	5395561	1 8.6	4.1	169.4	11/.8	7.3		3.0	37	0	
P	4707.2	S	533618	5395256	8.0	10.5	185.4	219.3	6.1	51.5	0.9	13	υ	 
LINE	20130	<b>_</b>	FLIGHT	3		<b></b>	<b></b>	·	<b>_</b>			·		1
A	5154.9	H	524962	5399594	1.1	4.3	70.6	15.5	5.1	20.4			0	i
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CX = COAXIAL

CP = COPLANAR

EM Anomaly List

    Labe	l Fid	Interr	XUTM	YUTM	   CX 55   Real	OO HZ Quad	CP 7	200 HZ Quad	CP Real		   Vertica   COND	 l Dike DEPTH*	   Mag. Corr 	   
			m	m	ppm	ppm	ppm	ppm	ppm		siemens	m	NT	
LINE	20130		FLIGHT	3	 						 			 
В	5173.2	H	525530	5399303	4.8	7.1	9.4	16.4	5.4	14.3	0.7	28	41	1
C	5197.1	S?	526184	5398957	1.6	7.2	5.3	20.3	1.6	3.0			0	1
D	5213.9	S	526683	5398686	7.6	10.1	97.3	168.4	1.1	30.9	0.9	7	14	1
E	5220.9	S?	526892	5398574	5.0	9.9	0.0	26.1	1.1	1.5	0.5	9	0	1
F	5227.9	В	527099	5398467	4.5	1.5	28.1	26.5	8.0	10.5			81	1
G	5230.9	S?	527188	5398421	3.8	9.9	0.3	18.9	0.3	3.7	0.4	11	0	I
H	5248.0	S	527672	5398171	1.5	11.8	4.5	65.4	1.3	9.7			0	į
I	5268.8	S	528287	5397858	8.8	18.0	78.6	200.9	2.5	31.6	0.6	0	0	į
J	5277.5	S	528550	5397715	20.6	14.1	124.2	231.7	4.6	40.9	2.6	11	0	į
K	5297.6	S	529157	5397388	13.5	37.4	53.6	218.8	2.3	30.4	0.5	0	25	į
L	5309.5	S?	529519	5397203	2.9	6.4	2.5	26.4	0.7	3.1			0	ĺ
M	5316.0	S	529719	5397100	3.5	14.4	4.3	44.4	0.4	6.0	0.3	0	13	į
N	5329.5	S	530133	5396878	18.2	34.9	184.7	255.4	4.4	48.7	0.8	0	29	į
ĺО	5339.6	S	530444		1.5	18.1	198.1	339.2	4.9	64.4	j		13	į
P	5376.9	S	531517	5396144	8.2	11.5	36.7	136.6	4.6	19.4	0.8	4	0	į
ĺΩ	5400.0	S	532219	5395777	7.9	7.6	87.3	174.1	6.7	30.9	1.2	15	12	į
R	5420.4		532812	5395462	24.7	16.1	202.4		8.2	61.9	2.9	11	28	į
S	5441.5	S	533409	5395156	4.8	20.3	268.3			79.5	0.3	0	27	į
LINE	20140		FLIGHT								 			 
A	6474.0	H	525310	5399199	3.4	7.3	42.0	93.5	7.3	25.3	0.4	25	0	į
В	6455.0	D	525866	5398911	3.8	7.9	9.2	39.0	1.3	5.1	0.4	7	0	į
C	6450.4	D	525988	5398839	4.5	14.3	25.0	44.9	0.7	7.2	0.3	2	5	į
D	6438.9	S	526285	5398682	33.4	87.7	252.2	591.1	2.7	95.8	0.8	0	33	į
E	6427.3	S?	526608	5398516	6.8	16.8	17.2	59.5	1.2	9.0	0.5	0	12	İ
F	6417.3	S	526874		2.7	1.8	6.5	31.9	1.5	3.5			0	ĺ
G	6389.8	S	527588	5397996	11.0	22.2	193.1	519.6	2.0	79.7	0.7	5	18	İ
H	6365.5	S	528218	5397666	2.5	5.9	34.2	135.7	0.5	19.9			13	İ
I	6358.8	S	528405	5397570	5.7	15.9	81.7	194.3	3.2	30.3	0.4	0	0	İ
J	6342.0	S	528884	5397311	1.0	7.7	1.6	40.0	0.7	5.8			0	İ
K	6329.7	S	529207	5397143	1.5	13.5	68.7	234.6	2.2	36.0	i		0	į
ļь	6325.8	S	529314	5397087	3.5	20.4	58.2	207.8	1.8	31.3	0.2	0	0	į
M	6315.0	S	529609	5396925	3.0	8.6	2.4	26.1	0.0	4.0	j		0	į
N	6302.6	S	529937	5396752	9.6		172.0		3.8	46.3	0.6	0	17	į
o	6288.6	S	530330	5396554	25.9	67.1	501.6	626.5	15.0	154.4	0.7	0	39	į
P	6251.8	S?	531314		12.2	37.3	80.0	257.3	3.5	37.3	0.5	0	6	į
ĺQ	6231.4	S	531864	5395746	3.1	9.9	80.2	180.3	4.5	29.1	0.3	3	0	į
R	6227.3	D	531982	5395684	8.6	1.5		23.3	12.5	16.1	i		72	į
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CX = COAXIAL

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EM Anomaly List

  Labe	l Fid	Interp	XUTM m	YUTM m	CX 55   Real   ppm	00 HZ Quad ppm	CP 7 Real	200 HZ Quad ppm	CP Real ppm	~	Vertica   COND   siemens	l Dike DEPTH* m	Mag. Corr       NT	     
LITNE	20140		FLIGHT		 I						 I		 	 I
s	6220.7	S	532168	5395578	2.4	6 3	121.1	147 9	10.7	34.2			0	i
T	6203.7		532627	5395337	10.7			153.1	7.3	47.5	0.7	0	0	ł
ĺΰ	6179.7		533283	5395001	10.4		167.2	84.6	11.4	44.7	1.3	21	0	i
V	6174.8		533416	5394933	22.4		150.1		8.7	41.6	1.7	10	0	
LITNE	20150		FLIGHT	8	 I						 I			 
A	5763.7	S	523585	5399878	3.0	5.1	22.5	73.8	8.0	11.2	i		0	i
В	5810.3		524957	5399153	2.2	2.0	3.5	9.8	2.4	4.5			0	ļ
C	5838.5		525771	5398727	1.1	5.6	7.5	16.6	1.0	3.3	i		0	i
D	5853.5		526206	5398496	0.7	14.0	35.2	88.6	2.2	14.8	i		0	į
ĖΕ	5859.0		526366	5398411	0.5	7.4	3.7	7.9	0.6	1.1	i		j o	į
F	5875.0	В	526859	5398148	4.8	15.1	291.9	369.5	6.6	85.0	0.3	0	j 39	i
Ġ	5900.0		527580	5397775	2.2	6.2	1.3	23.3	1.8	3.2	i		0	į
Н	5924.3		528313	5397384	10.1		169.2	400.7	1.0	64.5	0.4	0	0	į
İI	5951.2	S	529135	5396954	18.3	31.1	160.1	253.4	3.3	47.9	0.9	0	15	į
jл	5956.2	S	529295	5396874	9.6	21.7	74.8	161.2	2.5	26.3	0.6	0	24	į
ĺк	5967.1		529630	5396693	7.4	24.9	44.5	213.7	0.0	29.2	0.4	0	j o	i
İъ	5979.7	S	530004	5396499	8.0	23.6	50.1	241.1	1.5	34.0	0.4	0	j o	i
М	5987.8		530247	5396372	0.0	15.5	169.4	290.2	3.7	54.3	i		0	i
N	6018.8		531167	5395881	7.2	19.3	175.6	345.6	5.5	59.1	0.5	0	0	i
İo	6037.7	D?	531785	5395563	11.9	1.9	54.2	58.6	9.2	22.6	i		123	i
P	6039.7	S	531847	5395531	0.0	8.1	54.2	34.2	9.2	22.6	i		129	i
ĺQ	6060.4	S	532476	5395198	4.1	10.0		246.0	6.5	65.9	0.4	5	0	i
R	6076.9	S	532981	5394920	9.4		208.3		18.6	67.1	1.3	26	0	İ
LINE	20160		FLIGHT	8	 						 		 	 
A	5644.2	S	523399	5399756	21.7	20.0	277.4	353.1	19.7	76.3	1.8	4	0	į
В	5599.2		524735	5399037	1.3	1.3	3.4	17.2	4.9	3.3			0	į
C	5565.8		525736	5398522	5.0	20.1	11.7	74.6	1.3	10.1	i		0	j
D	5557.7		525964	5398402	3.5	10.2	8.0	18.0	1.5	3.4	i		0	i
E	5546.9		526270	5398236	6.1	15.0	11.1	36.9	1.4	6.2	0.5	9	14	i
F	5528.2		526793	5397966	9.4	20.4	161.3	297.4	3.5	52.4	0.6	0	0	i
G	5476.4		528147	5397256	3.0	9.7	88.3	177.0	2.2	29.1	0.3	0	0	i
H	5463.5		528536	5397046	4.2	7.7	18.8	58.4	1.2	8.8	0.5	18	0	i
İI	5441.6		529102	5396742	29.1	43.5	236.1	398.4	5.0	73.0	1.2	0	28	j
јJ	5428.1		529469	5396549	0.0	3.9	92.7	220.3	4.1	35.6	i		j o	j
K	5415.6		529802	5396371	7.2	37.4	48.8	237.7	4.5	33.0	0.3	0	0	i
L	5401.1	S	530190	5396169	9.3	16.1		157.6	3.2	25.7	0.7	3	0	j

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					   CX 55	00 HZ	CP 7	200 HZ	CP	900 HZ	   Vertica	 l Dike	   Mag. Corr	 
Labe	l Fid	Interp	MTUX e	YUTM	Real	Quad	Real	Quad	Real	Quad	COND	DEPTH*	İ	į
İ			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	ĺ
LINE	20160		FLIGHT	8	 						 			
M	5373.9	S	530944	5395775	6.9	14.9	28.1	135.9	3.5	18.1	0.5	0	0	
N	5354.8	S	531454	5395502	18.6	28.3	232.8	477.7	6.2	82.6	1.0	2	0	
0	5350.1	D	531592	5395429	14.1	14.5	92.6	53.8	8.2	26.7	1.4	10	0	
P	5344.1	S	531773	5395335	7.5	15.1	131.9	138.1	7.4	35.7	0.6	0	0	
Q	5324.0	S	532329	5395044	28.5	35.8	338.4	436.8	17.2	100.0	1.4	1	276	
R	5305.7	H	532820	5394779	5.7	4.8	114.1		7.2	30.4	1.3	37	0	
S	5285.6	S	533347	5394520	5.0	7.6	89.9	157.1	3.7	29.2	0.7	26	24	
LINE	20170		FLIGHT		 						 		 	 
A	4763.7	S	523219	5399611	10.9	22.5	238.8	323.1	35.0	63.3	0.6	0	0	ĺ
В	4802.0	H	524391	5398988	1.9	1.3	14.2	50.3	3.8	12.5			0	į
C	4847.0	S?	525717	5398307	11.9	16.2	51.5	83.3	2.8	14.5	1.0	1	0	ĺ
D	4854.8	S	525953	5398182	7.5	8.3	45.1	106.4	1.3	16.7	1.0	20	0	ĺ
E	4874.3	S	526542	5397867	7.4	11.2	122.5	150.6	3.6	31.5	0.7	11	0	
F	4921.4	S	527978	5397108	6.6	10.4	57.4	167.7	0.7	25.4	0.7	12	0	
G	4935.9	S	528431	5396882	10.3	11.8	68.0	174.0	3.3	27.1	1.1	24	62	
H	4956.1	S	529049	5396553	11.0	13.7		151.2	2.3	25.3	1.0	5	21	
I	4967.1	S	529364	5396373	24.7	33.0	146.9	166.3	8.5	33.7	1.3	0	0	
J	4974.0	S?	529561	5396263	12.2	42.0	48.7	186.0	5.2	24.7	0.4	0	0	
K	4994.4	S	530157	5395964	3.4	14.3	117.9	278.1	5.9	43.7	0.2	0	0	
L	5015.7	S?	530761	5395641	5.3	9.5	11.2	21.4	3.4	3.5			0	
M	5042.1	S	531581	5395213	16.5	25.8	104.1	212.4	4.1	36.5	0.9	3	0	
N	5061.7	S	532168	5394905	17.9	19.5	318.0	359.7	9.6	87.7	1.4	8	0	
0	5078.2	S	532640	5394650	6.8	12.3		156.5	1.9	24.6	0.6	13	0	
P	5086.8	S	532893	5394515	5.6	10.1	5.7	42.5	0.9	4.2	0.6	6	87	
Q	5098.9	S	533269	5394321	10.7	22.1	345.7	353.5	7.2	99.7	0.6	2	0	
LINE	20180		FLIGHT	8	 						<b></b> 		 	
ļΑ	4658.6	S	522689	5399662	2.8	6.7	55.9	152.8	1.5	22.3			0	j
В	4643.3	S	523129	5399429	2.2	9.0	34.3	100.6	3.5	14.8	i		0	j
C	4599.8	H	524516	5398712	1.0	3.0	11.5	23.9	3.2	5.5			10	j
D	4561.3	S	525667	5398113	7.0	18.4	221.0	419.7	2.5	73.0	0.5	3	25	j
E	4537.6	S	526300	5397774	19.2	28.4	258.0	390.4	4.0	81.2	1.1	5	12	j
F	4532.9	S?	526436	5397694	0.0	4.0	86.1	219.2	1.9	35.8	i		0	j
G	4481.4	S	527875	5396940	2.3	5.4	8.3	49.3	1.9	6.8			0	j
H	4464.3	S	528356	5396682	4.8	16.3	46.8	204.4	3.7	27.9	0.3	0	0	j
İΙ	4453.7	S	528651	5396530	14.6	25.7	63.2	199.2	1.8	29.9	0.8	0	0	j
jЈ	4439.9	S	529068	5396310	3.6	7.8	111.7		6.9	28.4	0.4	19	0	j
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CX = COAXIAL

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EM Anomaly List

    Labe]	l Fid	Interp	MTUX c	YUTM	   CX 55   Real	00 HZ Quad	CP 7	200 HZ Quad	CP Real	900 HZ Quad	   Vertica   COND	 l Dike DEPTH*	Mag. Corr 	
İ			m	m	ppm	ppm	ppm	ppm	ppm	n ppm	siemens	m	NT	İ
LINE	20180		FLIGHT	8	 						 			
K	4426.7	S	529432	5396112	14.1	33.8	237.5	395.9	3.8	74.5	0.6	0	0	į
ļь	4415.6	S?	529763	5395940	5.1	20.9	10.8	67.5	2.2	9.1	j		0	į
M	4407.4	S	530001	5395824	11.6	30.0	159.8	363.9	5.0	59.4	0.5	0	0	į
N	4383.2	S?	530657	5395469	8.1	23.8	38.7	162.8	2.1	23.1	0.4	0	66	
0	4366.0	H	531140	5395218	9.1	12.3	71.3	25.9	6.5	31.7	0.9	20	0	ĺ
P	4339.6	S	531905	5394813	18.3	4.9	249.5	6.1	14.5	62.3	8.8	23	119	ĺ
Q	4324.8	S	532343	5394585	6.7	12.7	98.4	171.9	3.4	30.5	0.6	7	0	
R	4319.6	S?	532495	5394510	11.3	18.8	60.7	129.1	0.3	22.7	0.8	2	0	
S	4308.7	S	532779	5394353	4.6	7.1	20.1	68.8	1.7	10.4	0.6	28	8	
T	4300.8	S	532982	5394246	14.0	25.5	98.2	195.4	3.9	32.2	0.8	0	0	İ
LINE	20190		FLIGHT	8	 						 			
A	3863.7	S	522185	5399708	0.0	3.5	0.3	17.8	0.0	3.0	i		212	į
В	3874.6	S	522508	5399540	0.1	4.2	2.4	19.8	0.0	2.7	j		70	į
ĺС	3927.5	H	524112	5398695	2.3	5.8	20.6	56.0	4.7	12.9	j		0	į
D	3966.3	S	525316	5398068	3.6	8.6	24.6	69.5	0.5	11.6	0.4	5	9	į
E	3978.9	S	525732	5397844	21.3	28.7	105.0	219.3	1.5	39.1	1.2	4	10	į
F	3991.7	S	526111	5397639	19.2	32.7	170.8	281.9	3.4	52.5	0.9	0	8	į
G	4055.6	S	528191	5396552	1.1	2.4	9.9	29.9	2.7	3.7	j		0	į
H	4067.3	S	528575	5396349	16.8	51.2	142.7	328.7	2.2	54.2	0.5	0	0	
I	4076.0	S	528858	5396190	5.7	11.1	139.6	121.6	10.1	34.6	0.5	0	0	
J	4089.9	S	529297	5395961	7.3	25.3	344.3	488.1	6.0	104.0	0.4	0	10	
K	4104.8	S?	529727	5395740	8.5	23.2	15.6	107.7	1.2	14.8	0.5	0	0	
L	4112.7	S	529973	5395601	16.9	27.1	348.7	634.1	7.9	112.3	0.9	8	0	
M	4131.5	S	530555	5395311	5.1	24.9	72.2	207.0	2.0	31.3	0.3	0	0	
N	4150.6	S	531179	5394980	14.7	32.0	432.8	400.0	28.4	144.7	0.7	3	173	Ì
0	4171.2	S	531807	5394640	9.4	8.6	226.9	109.4	19.8	57.5	1.4	22	0	
P	4187.5	S	532317	5394377	3.4	10.6	241.4	376.1	4.9	74.1	0.3	3	0	
Q	4199.5	S	532687	5394173	6.4	16.1	213.8	323.0	3.9	62.7	0.5	1	0	İ
LINE	20200		FLIGHT	8	 						 		 	ا ا
A	3474.2	H	523917	5398575	2.2	3.7	9.4	18.8	0.8	0.8	i		0	į
В	3431.8	S	525292	5397839	9.3	9.3	76.3	93.2	3.1	19.4	1.3	22	20	į
c	3419.4	S	525645	5397662	6.7	8.5	180.0	199.1	6.0	55.3	0.9	21	0	į
D	3403.0	B?	526069	5397439	2.9	11.5	30.9	98.4	1.4	14.4	i		0	į
E	3383.8	S	526549	5397179	1.9	4.6	15.3	100.9	0.2	14.6	i		0	į
F	3358.0	L	527248	5396818	3.0	0.7	18.3	0.4	17.6	1.9	i		29	į
G	3312.4	S	528477	5396169	14.6	40.3		552.2	7.7	91.8	0.6	0	0	į
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CX = COAXIAL

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EM Anomaly List

    Labe	l Fid	Inter	XUTM	YUTM	   CX 55   Real	00 HZ Quad	CP 7	200 HZ Quad	CP Real	900 HZ Quad	!	l Dike DEPTH*	   Mag. Corr 	 
			m	m	ppm	ppm	ppm	ppm	ppm	~	siemens	m	NT	İ
LINE	20200		FLIGHT	8	 						 			 
H	3304.0	S	528718	5396043	0.0	2.6	17.3	23.9	8.3	16.1			0	1
I	3289.1	S	529145	5395818	7.5	16.6	114.8	238.7	3.2	29.0	0.5	0	9	
J	3278.1	S?	529453	5395657	0.9	8.7	9.1	68.7	1.2	10.1			5	
K	3267.5	S	529746	5395494	2.2	25.1	234.3	429.7	8.1	77.2			0	
L	3244.1	S	530416	5395149		7.3	160.3	273.9	4.2	50.0			0	
M	3225.2	H	530992	5394846	18.8	33.1	458.0	382.0	34.0	149.2	0.9	2	0	
N	3213.2	S	531369	5394644	3.3	6.3	1.7	46.3	2.1	5.0	0.5	9	0	ĺ
0	3200.8	S	531728		3.5	5.9	189.8	191.7	6.1	49.7	0.5	23	63	ĺ
P	3185.5	S	532166	5394226	13.4	23.4	256.8	274.0	6.4	68.5	0.8	2	55	ĺ
Q	3174.2	D	532493	5394059	24.2	32.8	160.2	265.0	6.1	48.8	1.2	0	35	j
LINE	20210		FLIGHT	8	 						 			 
A	2738.6	S	522299	5399195	2.8	3.5	5.6	46.8	1.6	5.7	j		0	į
В	2742.9	S	522423	5399128	0.6	1.7	10.0	20.7	10.3	2.6	j		0	į
ĺС	2795.3	H	524064	5398274	1.5	1.5	11.7	23.9	3.0	5.0	j		0	į
D	2830.2	S	525156	5397699	9.0	13.6	16.8	55.0	0.4	7.6	0.8	8	0	į
E	2837.4	S	525376	5397579	11.0	12.4	86.2	214.6	1.5	33.0	1.2	16	22	į
F	2845.1	S	525619	5397455	14.2	12.1	98.5	172.5	2.9	35.7	1.8	18	9	į
Ġ	2860.8	S	526063	5397217	1.9	1.2	21.1	78.8	0.6	11.7	j		8	į
Н	2878.3	S	526597	5396934	4.5	20.7	20.7	113.8	0.7	15.4	0.2	0	6	į
İı	2941.0	S	528488	5395937	13.5	22.6	143.1	165.1	3.7	43.8	0.8	0	0	į
jЈ	2973.3	S	529447	5395427	1.0	11.2		122.3	1.6	16.8	i		j 7	į
ĸ	2978.2	S	529611	5395335	7.8	17.9	20.7	144.5	3.5	19.6	0.5	5	0	į
L	3009.3	S	530558	5394849	14.5	22.6	248.6	316.3	21.7	98.1	0.9	11	0	į
М	3037.8	S	531369	5394425	5.0	7.8	32.8	74.5	5.0	11.8	0.6	26	0	į
N	3044.1	S	531552	5394321	5.0	13.1	52.7	162.4	2.8	24.1	0.4	0	52	į
ĺО	3055.6	S	531896	5394140	16.0	19.2	225.8	272.9	8.7	57.7	1.2	10	0	į
P	3068.0	S?	532261	5393952	12.9	17.2	314.9	440.5	9.4	94.4	1.0	9	j o	j
LINE	20220		FLIGHT	8	 						 		 	ا
A	2633.9	S	521535	5399376	1.7	1.4	8.4	28.6	9.6	3.9	j		0	j
В	2567.9	H	523647	5398257	1.7	3.7	22.9	49.5	1.1	11.1	j		0	į
ĺС	2521.5	S?	525031	5397537	17.0	33.5		159.4	1.2	23.8	0.8	0	18	į
D	2509.8	S	525289	5397400	12.2	25.5	125.6	309.3	0.7	48.7	0.7	3	27	į
E	2502.5	S	525461	5397305	15.1	14.8	41.6	110.9	0.9	16.8	1.5	12	22	į
F	2491.6	S	525712	5397165	17.5	36.0		188.2	3.5	27.2	0.8	0	7	į
Ġ	2479.5	S?	526021	5397004	13.4	28.4		120.2	0.9	14.9	0.7	0	21	į
Н	2462.8	S	526470	5396781	0.0	6.8		69.6	2.6	9.5			0	į
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EM Anomaly List

					CX 55			200 HZ	CP	900 HZ		al Dike	   Mag. Corr	 !
Labe	l Fid	Interp		YUTM	Real	Quad	Real	Quad	Real	~		DEPTH*	NITT.	
<u> </u>			m	m	ppm	ppm	ppm	ppm	mqq	n ppm	siemens	m 	NT	
LINE	20220		FLIGHT	8	 						 			
Ι	2392.1	S	528276	5395826	8.6	15.1	131.7		4.8	47.4	0.7	10	0	
J	2347.7	S	529471	5395185	3.2	9.3	31.3	126.2	1.5	18.0	0.3	1	0	
K	2316.0	S	530362	5394719	13.2		176.2	179.6	12.2	59.4	2.9	26	0	
L	2300.4		530797	5394502	20.4	38.7		462.5	2.6	83.2	0.8	0	46	
M	2289.9	S?	531086	5394345	8.8	20.7	52.1	130.8	1.1	19.7	0.5	0	8	
N	2264.1	S	531702	5394021	15.8			313.0	4.8	63.5	1.0	4	0	
0	2251.9	S 	532003	5393863	13.3		349.8	358.0	8.0	99.5	0.6	0	29	
LINE	20230		FLIGHT		 						 			
A	1568.6	S?	521436	5399207	1.1	0.4	36.1	215.9	6.8	30.7			332	į
В	1586.6	S?	521887	5398966	1.5	17.8	43.4	190.6	0.6	27.2			0	į
C	1640.7	H	523342	5398204	1.9	2.5	10.3	21.8	3.9	4.9			0	İ
D	1683.4	S	524651	5397505	7.5	12.2	54.8	110.7	1.1	19.7	0.7	10	25	İ
E	1691.3	S	524881	5397385	9.3	17.2	8.3	41.7	1.5	4.0	0.7	0	0	
F	1701.7	S?	525172	5397244	21.0	42.7	144.2	323.9	1.7	52.9	0.8	0	20	
G	1720.1	S	525702	5396958	3.8	2.1	215.2	257.9	14.3	60.6			19	
H	1736.9		526178	5396708	3.7	14.7	53.5	218.9	1.1	31.3	0.3	0	0	
Ι	1772.7	S	527184	5396168	3.2	3.0	4.1	23.2	3.3	3.2			41	
J	1804.0	S	528138	5395665	7.5	6.7	37.9	36.5	4.3	13.3	1.3	31	0	
K	1845.6	S	529410	5394997	0.2		163.9	262.8	5.0	49.2			0	
L	1874.8	H	530296	5394534	17.1	21.2	341.4	487.7	10.8	103.2	1.2	10	0	
M	1886.9		530630	5394355	37.2	62.9		419.4	1.1	70.5	1.1	0	36	
N	1899.0		530934	5394200	6.6	8.7	20.7	80.8	2.2	11.1			15	
0	1919.7	S	531491	5393896	37.7	61.0	255.5	391.9	6.4	76.7	1.2	0	400	
P	1930.5	S?	531779	5393745	14.5	26.4	331.5	386.3	6.3	94.3	0.8	4	0	
LINE	20240		FLIGHT	8	 						 			
A	1475.9	S	521088	5399131	1.8	7.5	3.8	39.5	4.4	4.6	i		0	į
В	1452.4	S	521760	5398824	1.7	2.7	2.7	24.0	1.4	3.4	j		0	j
C	1398.7	H	523336	5397975	1.7	4.3	15.5	39.1	5.0	9.0	i		0	į
D	1360.4	S?	524409	5397408	6.0	19.2	44.1	83.2	2.0	13.0	i		8	į
E	1355.3	S	524536	5397345	19.0	35.7	87.9	220.4	1.3	29.8	0.8	0	34	į
F	1345.6	S	524774	5397216	19.8	41.7	27.9	181.6	0.3	23.8	0.8	0	17	į
G	1333.2	S	525059	5397071	16.7	43.4		330.7	2.8	49.4	0.6	0	13	į
Н	1318.7	S?	525398	5396890	38.5	10.6	178.2	312.1	8.2	59.7	10.8	13	16	į
İΙ	1306.3	S	525722	5396721	15.2	27.0	303.7	322.1		103.2	0.8	5	36	į
J	1288.6	S	526172	5396479	4.9	22.6	31.2	172.4	0.8	23.5			0	j
K	1250.1	S	527117	5395982	4.5	5.1	2.3	21.5	1.9	3.7			39	j
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CX = COAXIAL

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EM Anomaly List

    Labe	el Fid	Inter	XUTM	YUTM	   CX 55   Real	00 HZ Quad	CP 7	200 HZ Quad	CP Real	 900 HZ Quad	   Vertica   COND	 l Dike DEPTH*	   Mag. Corr 	 
			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	j
LINE	20240		FLIGHT	8	 						 			
L	1225.5	S	527669	5395689	5.0	15.3	42.8	90.2	5.2	14.4			0	
M	1204.9	S	528215	5395399	8.4	20.7	193.1	162.8	4.5	63.2	0.5	0	0	
N	1189.6	S	528627	5395188	4.3	3.9	22.4	93.8	1.5	11.3			7	
0	1172.9	S	529052	5394959	9.2		151.3	246.2	3.1	45.7	0.8	4	23	
P	1166.0	S	529232	5394866	6.6	15.6	148.5	239.0	2.7	47.4	0.5	2	0	
Q	1145.5	S	529742	5394599	8.7	21.4	244.7	317.6	5.1	68.1	0.5	0	0	
LINE	20250		FLIGHT	8	 						 		 	
A	749.2	S	520915	5399023	3.4	17.8	33.2	207.8	7.4	28.9	i		0	į
В	758.6	S	521176	5398889	0.5	2.3	0.0	10.6	3.5	1.5			201	İ
C	803.7	H	522355	5398259	1.8	3.1	28.0	48.3	8.4	17.1	i		0	į
D	842.6	H	523429	5397697	1.6	1.0	30.7	36.0	2.9	8.1			0	İ
E	874.0	S?	524385	5397194	17.4	38.0	74.1	188.6	0.3	31.8	0.7	0	0	
F	886.0	S	524714	5397020	13.6	35.1	151.5	389.4	1.7	60.6	0.6	0	26	
G	898.7	S	525086	5396829	17.8	7.2	110.6	217.5	3.2	38.1	4.9	26	0	
H	906.4	S	525322	5396707	1.4	2.9	95.0	17.7	7.3	23.8			0	
I	932.5	S	526054	5396317	5.6	16.7	12.1	96.1	1.1	12.5			0	
J	970.3	S	527071	5395778	3.3	6.7	7.3	30.0	3.8	4.2			0	
K	999.5	S	527937	5395323	12.5	7.0	145.2	155.6	5.0	40.6	2.8	21	0	
L	1009.7	S	528224	5395170	13.0	17.8	78.5	215.8	0.6	33.0	1.0	2	9	
M	1024.7	S	528631	5394964	9.0	10.0	122.0	233.3	2.5	40.9	1.1	12	0	
N	1034.7	S	528908	5394816	0.0	20.1	264.4	393.9	6.5	81.4			63	
0	1042.1	S	529112	5394703	10.5	23.8		472.4	2.6	78.3	0.6	2	0	
P	1059.4	S	529569	5394465	24.6	33.6	319.4	438.1	9.2	95.0	1.2	0	51	
LINE	20260		FLIGHT	7	 						 		 	
A	6365.7	S	520683	5398896	2.5	5.2	11.3	70.1	6.6	9.4			0	j
В	6424.3	H	522182	5398109	2.7	4.1	41.3	46.6	16.2	24.8			0	
C	6456.6	H	523188	5397592	1.6	3.6	35.2	52.2	2.0	11.2			0	
D	6487.8	S	524205	5397053	8.0	24.5	48.2	175.9	0.3	24.5	0.4	0	0	
E	6502.9	S?	524671	5396816	9.2	17.8	50.6	117.4	0.3	19.0	0.6	0	25	
F	6524.0	H	525394	5396428	34.3	27.3	218.3	208.3	15.1	70.7	2.5	13	8	j
G	6540.1	S	525907	5396171	1.5	5.6	1.5	22.7	2.0	3.4			0	j
H	6551.5	S	526275	5395986	0.8	2.3	3.6	43.1	1.9	4.6			0	j
İΙ	6574.4	S	526999	5395594	0.8	7.7	4.9	37.3	3.8	5.1			0	j
J	6597.5	S	527808	5395152	5.7	6.5	71.9	59.1	3.2	18.5	0.9	14	0	j
ļκ	6607.2	S	528156	5394985	6.4	11.2	4.9	29.1	1.7	2.6	0.6	12	0	j
ļъ	6617.7	S	528531	5394816	0.0	3.5	79.5	62.3	2.7	21.0	j		0	j

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EM Anomaly List

  Labe	l Fid	Inte	rp XUTM m	YUTM m	   CX 55   Real   ppm	 00 HZ Quad ppm	CP 7 Real	200 HZ Quad ppm	CP Real	~	Vertica COND	l Dike DEPTH* m	Mag. Corr       NT	
	20260	_	FLIGHT											
M	6629.9	S	528921	5394576	7.4		131.4		5.2	39.8	2.1	26	0	-
N	6646.0	S	529443	5394296	15.5	44.1	314.3	476.3	11.6	105.2	0.6	0	15	ļ
LINE	20270		FLIGHT	7	 						 		 	
A	6148.7	S	523772	5397081	3.7	4.8	57.8	98.9	2.2	20.8	0.7	18	12	i
ΪВ	6132.8	S?	524191	5396846	12.8	18.3	26.7	99.8	1.2	13.5	1.0	0	15	i
İc	6122.3	S?	524472	5396679	5.4	16.3	10.8	40.8	0.3	4.7	0.4	0	i o	i
D	6115.7	S?	524662	5396579	3.6	10.0	8.7	16.2	1.3	3.0	0.3	16	i o	i
E	6098.2	S	525141	5396345	39.0	36.2	305.2	353.8	11.7	88.8	2.2	7	20	i
F	6087.3	S	525501	5396158	0.0	12.0	149.8		2.1	54.2	j		j 0	į
Ġ	6075.5	S	525886	5395956	3.3	3.2	29.9	111.9	0.4	15.7	j		j o	į
н	6029.9	S	527165	5395280	1.3	1.6	1.5	9.4	4.0	1.8	i		j o	i
İΙ	6016.5	S	527535	5395083	5.9	9.2	92.5	192.8	2.1	33.0	0.7	22	14	į
jЈ	6006.0	S	527832	5394917	9.8	10.0	108.2	158.5	2.3	32.6	1.2	4	j 0	į
K	5996.6	S?	528105	5394775	3.5	16.2	83.7	162.9	3.0	25.3	0.2	0	6	į
İъ	5986.4	S	528406	5394612	3.2	2.6	26.4	86.3	2.1	13.7	j		12	į
М	5976.5	S	528706		1.7	11.2	137.2	215.4	3.4	41.2	i		15	i
N	5950.3	H	529424	5394087			414.3		19.3	100.6	2.3	31	0	İ
	20271		FLIGHT								!			
A	581.3	S	520757	5398652	0.7	0.9	0.3	7.0	0.0	1.3			154	ļ
В	598.4	S	521225	5398416	6.2	1.1	5.1	25.2	2.5	3.5			0	ļ
C	625.7	H	522011	5398004	3.4	4.1	36.5	48.2	14.1	22.5	0.7	42	0	
D	647.8	H		5397633	3.3	5.3	64.0	85.9	8.9	19.2	0.5	31	15	
E	669.1	S	523397	5397236	4.8	9.4	187.2	230.3	7.1	54.7	0.5	18	7	
LT.TNE	20280		FLIGHT	 7	 I						 		 	
A	5549.0	S?	520340	5398628	0.2	9.8	9.1	72.9	4.6	9.5			0	<u> </u>
lв	5571.8	S?	520809	5398360	1.0	3.1	16.6	92.2	2.9	13.5	i		0	<u> </u>
C	5614.1	н	521956	5397806	3.1	8.2	41.7	52.4	14.0	18.1	0.3	16	12	<u> </u>
D D	5656.0	S?	523129	5397188	21.2	28.6	110.2		1.3	37.1	1.2	0	15	
E	5660.9	S.	523265	5397112	28.3	43.4	170.7		3.8	58.0	1.2	5	16	
F	5676.4	B?	523689	5396897	11.3	12.5	33.5	67.7	3.2	12.6	1.2	0	10	
G	5693.5	S?	524156	5396646	8.5	14.8		149.9	3.5	23.7	0.7	0	14	
H	5701.9	S?	524414	5396505	3.9	12.6	13.9	27.9	1.4	5.2	0.7	0	1 0	
I	5720.1	s: S	525042	5396174	4.8		174.6		5.1	53.0	0.3	0	1 12	
l⊥ IJ	5735.5	S	525526	5395174	14.0		104.3		1.9	34.8	0.3	0	18	
K	5743.0	S	525743	5395802	0.0	20.5	20.8	48.1	1.6	6.4	0.7		l 0	
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CP = COPLANAR

EM Anomaly List

LINE 20280	  Labe	l Fid	Inter	XUTM m	YUTM m	CX 55   Real   ppm	00 HZ Quad ppm	CP 7 Real	200 HZ Quad ppm	CP Real ppm	~	!	al Dike DEPTH* m	Mag. Corr       NT	     
LINE	LT TNE	20280			7	 I						 I			 I
M   5792, 8   S   527425   53946903   15.1   15.2   158.8   247.2   7.5   48.9   1.5   4   82   N   5807.6   S   527975   5394622   9.0   23.7   256.7   497.6   3.5   87.4   0.5   0   11   0   0   5818.7   B?   528346   5394440   9.5   19.7   8.7   51.0   2.1   5.8   0.6   4   11   11   0   5825.6   D   528573   5394308   7.6   21.4   1.1   0.9   1.5   1.0   0.4   0   0   0   0   0   0   0   0   0			C 2			l   0.5	10 1	10 0	QΛ /	1 0	10 5	l I		10	-
N	!											I	4	1	-
D												1			-
P	!					1						1	-	1	
Q												!	_	1	1
No.   No.						•						!	0	!	i
LINE 20290   FLIGHT 7	1				5393974	35.8						!	-	!	İ
A 5215.7   S 520197   S398500   2.9   11.7   54.1   208.1   17.9   29.3       0	LINE	20290		FLIGHT		 						 			 
B			S	520197	5398500	2.9	11.7	54.1	208.1	17.9	29.3	i		0	j
D	В	5198.1	S	520784	5398189	2.0	0.4	1.7	11.8	0.4	1.7	j		0	į
E 5146.9	C	5182.0	S	521289	5397917	0.0	0.0	11.2	18.5	9.1	2.1	j		0	į
F   5130.2   S   523169   5396932   4.4   12.5   65.8   141.3   2.4   18.9   0.4   9   0   0   0   0   0   0   0   0   0	D	5167.4	H	521829	5397641	2.6	1.4	38.4	0.0	12.1	20.5	j		0	į
G   5105.8   S   523965   5396518   0.8   2.5   9.2   35.9   0.6   6.0       7     H   5098.3   S?   524190   5396405   8.1   10.9   22.7   21.2   0.6   3.2   0.9   1   17     I   5078.8   S   524748   5396092   2.3   4.1   4.7   21.4   1.0   2.8       0     J   5071.3   S   524962   5395995   4.3   9.6   24.5   70.4   1.4   10.3   0.4   0   16     K   5063.7   S?   525184   5395871   4.5   7.5   1.7   14.8   0.9   0.3   0.6   10   11     L   5057.4   S?   525374   5395764   10.4   16.1   45.3   134.4   2.2   19.7   0.8   0   31     M   5041.5   S   525854   5395515   0.9   6.5   41.2   105.5   1.5   16.3       12     N   5035.8   S   526014   5395419   3.2   1.9   25.5   17.0   1.2   4.3       0     O   4998.9   S   526975   5394919   2.3   1.6   9.5   23.5   1.4   3.4       0     P   4978.7   S   527541   5394635   9.9   13.8   131.7   224.0   4.8   39.2   0.9   17   0     Q   4970.8   S   527773   5394232   9.9   13.8   131.7   224.0   4.8   39.2   0.9   17   0     R   4959.9   S   528051   5394366   9.5   15.2   47.7   144.2   0.2   21.8   0.8   2   14     S   4950.7   S   528277   5394232   9.3   34.6   201.5   460.2   1.1   75.0   0.4   0   0     T   4934.4   S   528679   5394021   11.8   11.1   331.0   467.7   10.6   90.5   1.5   23   0     U   4912.2   H   529148   5393768   12.2   22.6   135.3   206.7   16.3   55.8   0.7   8   0      LINE   20300   FLIGHT   7	E	5146.9	H	522578	5397233	1.1	0.2	16.2	2.4	3.2	5.1	j		0	į
H   5098.3   S?   524190   5396405   8.1   10.9   22.7   21.2   0.6   3.2   0.9   1   17   1   5078.8   S   524748   5396092   2.3   4.1   4.7   21.4   1.0   2.8       0   1   5071.3   S   524962   5395995   4.3   9.6   24.5   70.4   1.4   10.3   0.4   0   16   K   5063.7   S?   525184   5395871   4.5   7.5   1.7   14.8   0.9   0.3   0.6   10   11   11   11   11   12   15   15   16.3   134.4   2.2   19.7   0.8   0   31   14   15   15   15   16.3   15   16   16	F	5130.2	S	523169	5396932	4.4	12.5	65.8	141.3	2.4	18.9	0.4	9	0	ĺ
T	G	5105.8	S	523965	5396518	0.8	2.5	9.2	35.9	0.6	6.0			7	ĺ
J	H	5098.3	S?	524190	5396405	8.1	10.9	22.7	21.2	0.6	3.2	0.9	1	17	ĺ
K   5063.7   S?   525184   5395871   4.5   7.5   1.7   14.8   0.9   0.3   0.6   10   11   1   1   5057.4   S?   525374   5395764   10.4   16.1   45.3   134.4   2.2   19.7   0.8   0   31   1   1   1   1   1   1   1   1	I	5078.8	S	524748	5396092	2.3	4.1	4.7	21.4	1.0	2.8			0	ĺ
L	J	5071.3	S	524962	5395995	4.3	9.6	24.5	70.4	1.4	10.3	0.4	0	16	
M   5041.5   S   525854   5395515   0.9   6.5   41.2   105.5   1.5   16.3       12   N   5035.8   S   526014   5395419   3.2   1.9   25.5   17.0   1.2   4.3       0   0   4998.9   S   526975   5394919   2.3   1.6   9.5   23.5   1.4   3.4       0   0   0   0   0   0   0	K	5063.7	S?	525184	5395871	4.5	7.5	1.7	14.8	0.9	0.3	0.6	10	11	
N	L	5057.4	S?	525374	5395764	1	16.1	45.3	134.4	2.2	19.7	0.8	0		
O 4998.9	M	5041.5	S	525854	5395515	0.9	6.5	41.2	105.5	1.5	16.3			12	
P	N	5035.8	S	526014	5395419	3.2	1.9	25.5	17.0	1.2	4.3			0	
Q	0	4998.9	S	526975	5394919	2.3	1.6	9.5	23.5	1.4	3.4			0	
R	P	4978.7	S	527541	5394635	9.9	13.8	131.7	224.0	4.8	39.2	0.9	17	0	
S 4950.7 S 528277 5394232   9.3 34.6 201.5 460.2 1.1 75.0   0.4 0   0    T 4934.4 S 528679 5394021   11.8 11.1 331.0 467.7 10.6 90.5   1.5 23   0    U 4912.2 H 529148 5393768   12.2 22.6 135.3 206.7 16.3 55.8   0.7 8   0     LINE 20300 FLIGHT 7	Q	4970.8	S	527773	5394524	18.4	14.3	161.8	193.4	3.5	49.7	2.1	15	0	
T 4934.4 S 528679 5394021   11.8 11.1 331.0 467.7 10.6 90.5   1.5 23   0   U 4912.2 H 529148 5393768   12.2 22.6 135.3 206.7 16.3 55.8   0.7 8   0   U 10	R	4959.9	S		5394366					0.2	21.8	0.8	2	14	
U 4912.2 H 529148 5393768   12.2 22.6 135.3 206.7 16.3 55.8   0.7 8   0	S	4950.7	S				34.6	201.5	460.2	1.1	75.0	0.4	0	0	
LINE 20300	T	4934.4	S	528679	5394021					10.6	90.5	1.5	23	0	
A 4487.0 S 520005 5398385   0.0 4.7 6.1 69.6 8.8 9.1     0	U	4912.2	H	529148	5393768	12.2	22.6	135.3	206.7	16.3	55.8	0.7	8	0	
	LINE		<b>_</b>												
B 4518.8 S 520700 5398002   0.6 3.0 2.5 8.4 2.4 1.9     0	A		S	520005		1	4.7			8.8	9.1			0	
	В	4518.8	S	520700	5398002	0.6	3.0	2.5	8.4	2.4	1.9			1	
C 4535.3 D 521054 5397818   4.3 12.2 1.2 24.4 0.0 4.4     3957	C	4535.3	D		5397818	1		1.2		0.0	4.4			3957	
D 4553.9 H 521588 5397541   6.1 4.2 32.2 69.4 9.9 28.1   1.7 48   0	D	4553.9	H	521588	5397541	I	4.2		69.4	9.9	28.1	1.7	48	0	
E 4584.1 H 522426 5397086   3.5 4.2 50.7 33.0 4.4 15.6   0.7 39   0	E	4584.1	H				4.2					0.7	39	0	
F 4608.0 S? 523113 5396747   8.8 26.4 80.5 160.3 1.1 30.8   0.4 0   0	F	4608.0	S?	523113	5396747	8.8	26.4	80.5	160.3	1.1	30.8	0.4	0	0	

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

    Labe	 l Fid	Interp	XUTM	YUTM	   CX 55   Real	00 HZ Quad	CP 7	'200 HZ Ouad	CP Real	 900 HZ Quad	   Vertica   COND	 l Dike DEPTH*	   Mag. Corr 	 
		111001	m	m	ppm	ppm	ppm	ppm	ppm	~	siemens	m	NT	
LINE	20300		FLIGHT	7	 						 			
G	4624.3	S	523480	5396537	6.3	12.8	210.9	170.3	6.9	58.7	0.5	8	43	
H	4650.4	S	524190	5396169	2.9	5.5	23.3	46.2	1.2	7.3			0	
I	4661.9	S	524524	5395982	4.2	7.3	34.8	94.6	1.0	14.2	0.5	3	0	
J	4671.5	S	524813	5395844	0.7	8.9	9.7	49.1	1.6	6.7			0	
K	4678.0	S	524999	5395749	2.3	10.9	4.3	35.0	1.0	5.2			9	
L	4687.3	S?	525270	5395613	8.3	21.9	35.2	126.5	0.4	17.9	0.5	0	23	
M	4696.3	S	525520	5395488	1.1	5.6	2.9	5.2	0.5	1.9			5	ĺ
N	4711.3	S?	525946	5395238	0.3	0.1	25.9	94.0	0.9	13.3			5	ĺ
0	4742.9	S	526883	5394741	2.5	7.4	7.4	41.8	4.9	5.3			0	ĺ
P	4750.0	S?	527128	5394630	14.5	23.8	125.4	173.0	5.6	34.2	0.9	0	265	į
İQ	4767.3	S	527734	5394301	6.4	14.5	120.7	207.8	2.2	45.9	0.5	10	299	į
R	4788.5	S	528500	5393901	2.1	6.5	97.4	68.6	6.7	18.6			j 0	į
S	4800.9	H	528963	5393664	15.1		197.9	44.0	16.7	52.9	5.3	30	0	İ
LINE	20310		FLIGHT		 						 			
A	4390.3	B?	520335	5397953	0.1	17.1	18.4	126.4	2.7	17.7			0	ĺ
В	4381.6	S	520589	5397833	0.0	5.3	4.5	23.1	4.9	3.6			0	į
ĺС	4369.0	S?	520913	5397659	1.8	3.5	3.7	10.5	2.7	2.1			1020	į
D	4345.6	Н	521561	5397320	0.0	0.0	18.1	0.0	13.1	11.8			0	į
E	4316.4	S	522301	5396947	5.2	10.8	21.2	73.4	1.2	10.2	0.5	0	0	į
F	4288.3	S	522924	5396618	7.6	7.4	184.6	200.1	7.2	52.0	1.2	27	11	į
Ġ	4266.4	S	523435	5396349	22.5	19.6	231.4	282.8	6.4	67.8	2.0	10	68	į
Н	4252.7	S	523825	5396136	2.7	5.3	6.0	21.9	1.4	2.4			8	į
İı	4241.2		524151	5395970	9.0	12.1	28.2	96.4	1.4	14.6	0.9	0	16	į
jЈ	4206.1	S	525143	5395441	10.3	21.1	75.1	164.9	0.4	25.9	0.6	0	30	į
K	4196.0	S	525430	5395289	1.6	11.4	16.9	94.8	0.3	13.2			6	į
Ĺ	4178.8	S	525895	5395053	3.7	13.4	42.1	204.4	1.5	28.5	0.3	0	6	į
M	4114.7	Н	527470	5394219	3.0	7.7	121.8	100.4	0.9	33.2			385	į
N	4085.1	Н	528261	5393806	7.9	14.1	197.3	224.8	23.4	63.9	0.6	16	0	į
0	4058.1	H	528925	5393474	9.4		173.8		9.4	54.7	1.4	24	0	İ
LINE	20320		FLIGHT	7	 						 			
A	3528.4	S	519926	5397962	0.8	5.3	8.6	33.5	11.3	4.6			195	į
В	3539.4	S	520177	5397829	0.0	1.7	1.8	9.9	1.7	1.9			0	İ
С	3553.9	S?	520519	5397663	1.8	10.0	16.0	64.2	6.5	9.1			0	j
D	3583.2	Н	521223	5397263	4.1	7.4	40.2	83.5	8.8	19.3	0.5	23	45	į
E	3597.6	S?	521634	5397061	1.0		119.1	258.2	5.4	43.7			0	
F	3621.4	S	522203	5396751	0.6	1.9	10.2	40.8	3.7	5.4			0	
											' 			

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					   CX 55			200 HZ	CP	 900 нz	   Vertica	 l Dike	Mag. Corr	 I
Labe	l Fid	Inter	D XUTM	YUTM	Real	Ouad	Real	Ouad	Real		!	DEPTH*	Mag. Corr	
	1 114	THOOTI	m	m	ppm	ppm	mqq	ppm	ppm	~	siemens	m	NT	
LINE	20320		FLIGHT	7										1
İG	3649.3	S	522996	5396340	13.6	19.7	311.1	353.1	12.6	92.0	1.0	7	j 26	į
Н	3665.2	S	523387	5396143	10.9	8.2		114.5	0.4	17.2	1.9	14	40	į
İI	3694.2	S	524178	5395723	11.5	18.3		137.9	1.4	21.9	0.8	0	9	į
jЈ	3712.1	S?	524691	5395459	10.2	27.8	125.0	210.4	6.2	37.9	0.5	0	i o	į
ĺк	3725.3	S	525066	5395261	4.0	6.8	42.9	96.6	2.4	14.3	0.5	5	14	į
ļь	3734.5	S	525341	5395125	11.0		123.3	256.6	2.8	41.4	0.5	0	12	į
ĺм	3761.6	S	526114	5394699	0.5	1.8	1.0	9.8	0.2	1.0			i o	į
N	3774.3	S	526499	5394485	1.1	3.1	2.0	21.6	1.5	2.6			i o	i
ĺО	3789.6	H	526992	5394231	7.3	5.4	98.1	27.6	15.5	34.1	1.7	31	34	į
P	3812.5	H	527750	5393832	8.8	7.4	113.9		5.3	35.8	1.5	28	15	İ
LITNE	20330		 FLIGHT	7	 I						 I		 	 I
A	3434.2	S	519749	5397831	0.1	7.0	15.3	67.6	18.2	9.2	 		310	ŀ
lB	3388.3	H	521156	5397091	5.1	3.8	46.1	76.5	16.2	39.3	1.4	45	0	ł
İc	3378.5	S?	521476	5396919	5.5	9.9	48.0	77.2	3.3	14.8	0.6	0	0	i
D	3355.3	s. S	522135	5396571	5.0		140.3	253.4	2.9	44.4	0.4	0	0	ł
E	3325.4	S	522920	5396132	8.3	28.4		443.5	4.3	75.4	0.4	0	0	ŀ
F	3310.4	S	523291	5395973	25.8	19.0	240.7	384.6	3.5	75.3	2.5	14	34	ŀ
G	3281.4	S	524093	5395538	7.9		264.2		7.2	73.1	0.5	0	16	ŀ
H	3262.3	S	524642	5395242	3.4	13.4		100.0	0.3	14.5	0.3	0	12	ŀ
I	3250.2	S	524983	5395065	12.9	16.7	110.4	221.7	1.9	36.0	1.1	12	12	ł
J	3237.5	S	525379	5394861	1.8	4.9	28.5	78.0	1.4	11.8	<del></del>		16	ŀ
K	3226.8	S	525702	5394695	0.9	3.0	2.4	15.0		3.0	 		0	ŀ
L	3215.0	S	526040	5394516	4.3	2.4	2.4	35.7	0.1	5.1	 		0	ŀ
M	3198.5	S	526468	5394290	2.1	4.6	3.3	24.3	0.3	3.1	 			ŀ
N	3177.8	Н	527011	5394007	6.5	1.5	66.9	35.4	6.4	19.5	 		57	i
0	3161.1	H	527467	5393775	10.5	10.5	348.9	188.4		109.7	1.3	24	0	ŀ
I P	3130.7	H	528253		19.2		154.1		14.0	57.7	1.1	7	6	ŀ
Q	3107.2	S	528721	5393130	8.4		267.5		5.3		0.5	6	117	
   T.TNF	20340		 FLIGHT	7	 I						 I			I
A	2687.4	S	519816	, 5397564	1.3	3.2	2.9	12.0	0.4	2.3	l 		12	-
B	2712.6	S	520430	5397304	1.0	2.4	33.6	76.4	34.6	11.0	 		1 0	-
l C	2712.0	S	520430	5396865	1.0   6.8		124.5	92.2	9.6	36.9	l 0.8	29	1 0	
l D	2740.0	S	521771	5396553	4.8	12.7		154.8	1.2	24.3	0.4	1	0	l I
E	2776.2	B?	522124	5396354	7.5	18.0	24.3	59.4		9.6	0.5	3	1 23	l I
F	2770.2	Б; S	522336	5396240	0.0	4.2		179.5	2.0	30.4	l		0	
F   G	2799.1	S	522755	5396240	10.0	12.8		108.9	2.5	16.2	1.0	2		
19					. 10.0								I	ا 

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					   CX 55		-	200 HZ	CP		   Vertica		   Mag. Corr	<u> </u>
Labe	el Fid	Inter	NTUX	YUTM	Real	Quad	Real	Quad	Real	Quad	!	DEPTH*	ļ	ļ
			m	m	ppm	ppm	ppm	ppm	ppm	ı ppm	siemens	m	NT	
	00240													
1	20340	~	FLIGHT		100	16.4	060 0	200 1	2 5	<b>70</b> 0		7.4		
H	2810.0	S	523056	5395862	10.8		262.2		3.5	78.8	0.8	14	0	-
I	2831.8	S	523697	5395533	6.0		135.6	352.8	3.5	55.1	0.3	0 0	12	-
J	2840.5	S?	523952	5395402	18.8 12.6	21.3	104.3		2.0	22.4	1.4	-	21 15	-
K  L	2846.3 2869.9	S?	524126	5395308				162.3	2.8	28.6	0.9	0 0	15	-
!		S?	524802 524990	5394928	11.0	25.6 15.8	23.7	133.2	1.2	21.3	1	2	1 0	-
M	2876.3	S?		5394839	5.3	14.8	23.7	53.6		9.4	0.4	2	I -	-
N	2881.3 2889.2	S?	525136 525360	5394767 5394643	11.3		150.5	53.6	2.4	9.4	0.4 0.5	0	8 1 12	-
0	2889.2	S?			0.4				1.4	47.1 1.9	U.5 		12	-
P	2911.2	S	525964	5394319	51.6	3.7	1.5 653.5	15.0			1.6	6	229	-
Q D		H	526710	5393927						232.9	1.6		1	-
R	2963.1	H	527467	5393530	6.5		104.3	18.2	60.7	53.9	I		0	-
S	2988.1	H	528154	5393183	12.4		320.9			91.2	1.1   0.7	18 6	0   7	-
T	3002.3	S	528534	5392977	13.1	24.I	288.6	469.2	6.2	88.5	0.7	0	/	- 1
LINE	20350		FLIGHT	7	 						 			
A	2438.4	B?	519725	5397395	3.6	25.1	33.4	186.3	0.1	26.5			11	
В	2412.5	S	520368	5397045	6.8	5.6	26.2	36.7	22.5	4.5	i		0	ĺ
C	2399.1	S	520694	5396883	7.2	11.0	357.8	205.5	128.5	86.8	0.7	18	0	ĺ
D	2374.8	S	521419	5396507	7.3	9.0	154.7	157.6	7.0	38.0	0.9	25	0	ĺ
E	2359.0	S	521841	5396274	4.7	8.7	0.0	23.4	2.1	1.8	0.5	17	0	ĺ
F	2343.5	S	522264	5396051	8.5	10.8	107.5	93.2	4.3	23.9	0.9	18	0	- 1
G	2330.4	S	522636	5395855	4.5	14.2	143.3	279.2	2.2	46.2	0.3	0	14	ĺ
H	2314.8	S	523042	5395648	19.5	28.2	198.0	297.7	2.7	56.2	1.1	8	47	ĺ
I	2293.1	S	523579	5395350	23.2	29.3	492.2	369.8	37.2	128.9	1.3	4	14	ĺ
J	2280.2	S	523892	5395201	29.7	87.4	183.9	412.8	1.7	67.6	0.7	0	31	
K	2271.2	D	524120	5395074	7.0	20.0	10.2	23.8	1.5	2.9	0.4	9	11	
L	2266.1	S	524247	5395002	2.8	9.2	13.5	65.8	1.5	7.9			12	
M	2259.8	B?	524400	5394919	1.7	9.3	4.5	15.5	1.1	2.6	i		5	ĺ
N	2247.3	B?	524707	5394764	30.9	59.6	229.2	384.6	2.8	69.6	1.0	0	40	ĺ
0	2234.3	S	525047	5394585	1.9	10.5	9.1	62.5	1.5	7.5	i		6	j
P	2224.4	S	525308	5394450	8.0	15.4	98.9	181.2	0.7	31.7	0.6	0	17	j
ĮQ	2185.5	S	526243	5393953	2.4	5.9	14.3	82.1	3.2	11.3	j		10	j
R	2178.8	E?	526391	5393877	23.5	31.6	227.6	311.3	2.6	68.1	1.2	0	0	j
S	2160.7	H	526817	5393650	7.0	8.3	48.5	51.5	15.6	24.3	1.0	22	0	j
ĪΤ	2138.4	H	527342	5393365	7.7	6.1	53.2	27.7	29.4	33.0	1.5	34	0	j
Įυ	2092.8	S	528388	5392835	16.5	21.6	394.9	573.0	8.8	116.2	1.1	13	0	į

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CX = COAXIAL

CP = COPLANAR

Note: EM values shown above are local amplitudes

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

					   CX 55	00 HZ	CP 7	200 HZ	CP	900 HZ	   Vertica	 l Dike	Mag. Corr	 
Labe	l Fid	Interp	MTUX	YUTM	Real	Quad	Real	Quad	Real	Quad	COND :	DEPTH*		
			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	
LINE	20360		FLIGHT	 7	 						 		 	 ا
A	1615.8	S	519537	5397250	2.3	4.1	1.6	19.2	0.8	2.6	 		0	i
B	1647.2		520132	5396938	3.3	1.8	8.4	58.1	21.6	8.8	 			i
C	1654.4		520275	5396862	8.5	19.6	15.6	142.8	0.0	19.6	0.5	0	1686	i
D	1685.6		520929	5396520	10.0	11.1	7.0	41.9	0.2	4.5	1.1	18	0	i
İΕ	1697.5		521238	5396358	15.2	15.9	103.8	199.1	3.6	34.5	1.4	14	12	i
F	1723.6		521903	5396003	17.2	23.5	290.8	302.3	10.1	85.0	1.1	0	i o	i
Ġ	1738.9		522329	5395782	6.2	17.3	21.2	98.2	1.1	13.2	0.4	0	6	i
Н	1748.9		522594	5395634	9.3	25.9	28.5	111.4	1.1	15.4	0.5	0	0	i
İı	1755.1		522758	5395551	2.2	4.8	2.9	7.5	1.0	1.0			0	i
jЈ	1776.4		523306	5395266	56.1	60.1	545.0	551.9		162.4	2.1	0	0	i
ĸ	1808.7		524194	5394808	19.6	19.9	144.8	274.6	3.4	46.1	1.6	4	15	i
ĹЪ	1817.3		524437	5394690	0.4	4.8	1.7	37.3	0.5	5.4			0	i
М	1825.1		524648	5394566	12.8	15.6		106.8	2.3	19.9	1.1	0	21	i
N	1833.0		524847	5394436	9.6	31.8	43.4	142.7	1.2	20.2	0.4	0	j 0	i
lo	1851.3		525265	5394234	3.6	9.6	25.0	111.9	1.1	15.8			11	i
P	1887.1		526128	5393785	7.7	10.8	40.2	139.3	1.4	20.5	0.8	20	i o	i
ĺΩ	1930.3		527276	5393192	7.5	3.1	46.3	35.4	14.6	50.5	3.6	41	i o	i
R	1951.7		527879	5392866	4.7	2.2	88.0	81.0	1.5	12.3			0	į
LINE	20370		FLIGHT	 7	 						 			 
A	741.7	S	520410	5396574	12.0	20.1	185.9	277.9	12.8	57.8	0.8	9	j o	i
Ιв	716.6		520936	5396316	6.0		170.9	110.6	8.5	44.5	0.6	20	i 0	i
İc	682.8		521724	5395879	16.8		193.4	231.2	4.0	54.8	1.3	0	26	i
ĺЪ	669.0	S?	522047	5395705	6.6	10.2	36.6	99.9	1.0	15.5	0.7	0	8	i
İΕ	651.9	S	522439	5395506	18.7	34.2	184.5	342.7	2.2	60.8	0.8	0	89	i
F	638.5	S	522738	5395358	3.4	6.1	3.2	24.8	0.9	3.9			j o	i
G	627.9		522968	5395232	10.6	25.3	76.6	153.6	2.5	26.1	0.6	0	73	i
Н	607.2	S	523467	5394960	24.7	29.5	255.0	279.5	8.8	70.9	1.4	8	11	i
İI	600.2	S	523642	5394866	13.2	35.2	134.5	380.8	0.2	60.9	0.6	0	17	į
J	575.9	S?	524172	5394581	7.0		164.8	238.3	3.1	48.3	0.3	0	26	j
K	552.8		524604	5394361	23.0		146.2	224.0	1.8	44.0	1.1	0	29	i
L	541.3		524819	5394254	4.5	12.8	20.8	103.3	1.0	15.7			10	į
M	525.2		525197	5394056	4.2	5.5	1.7	19.8	0.2	3.3			5	i
N	501.0	S	525777	5393747	2.2	2.5	2.2	27.1	4.9	4.3			0	į
0	488.6		526062	5393594	5.9	13.1		191.6	9.6	34.0	0.5	7	0	j
P	475.2	S?	526374	5393428	48.7	44.9	357.1	391.2		117.2	2.4	0	0	i
Q	441.2	Н	527146	5393022	27.8	26.9	201.8		43.1	85.4	1.9	11	0	į
													· 	

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Note: EM values shown above

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

LINE 20370	    Labe 	l Fid	Inter	p XUTM m	YUTM m		Quad	CP 7 Real ppm	200 HZ Quad ppm	CP Real ppm	Quad	COND	l Dike DEPTH* m	Mag. Corr     NT	       
A   493.9   S   519267   5396647   1.4   3.2   3.6   16.2   1.4   3.0       0			S			9.4	21.2	117.1	172.4	3.4	40.6	0.6	3	0	
A   493.9   S   519267   5396647   1.4   3.2   3.6   16.2   1.4   3.0       0	LITNE	20380		FI <sub>I</sub> TGHT	 5	 						 		 	 I
B   542.9   S   520.90   5396410   7.2   15.2   102.8   173.8   6.1   31.3   0.5   1   0   0   0   0   0   0   0   0   0						1.4	3.2	3.6	16.2	1.4	3.0	i		0	
C												1	1	0	i
D	İc	564.4	Н	520806		6.3				6.1	43.9	0.5	1	j o	i
E	D	586.3	S	521441	5395806	4.6	19.1	156.8	361.1	3.0		0.3	0	0	İ
G   615.1	E	594.9	B?	521677								0.9	0	25	İ
G   615.1	F	603.6	S?	521930	5395549	1.9	6.0	4.0	41.2	0.8	6.0	j		j 0	İ
T 644.6	Ġ	615.1	H	522268		17.0	17.0	249.9	212.4	12.1	77.6	1.5	4	j o	į
J	н	634.5	S	522860	5395045	35.0	51.6	225.8	289.8	3.7	61.6	1.3	0	94	į
J	İı	644.6	S	523162	5394900	6.1	8.9	34.3	50.0	0.4	9.4	0.7	7	16	İ
L 681.0   S 524242   5394325   4.8   22.4   15.9   79.4   1.2   10.7       9   M 690.9   B?   524525   5394169   18.7   36.5   127.1   181.9   2.0   36.5   0.8   0   47   17.2   18.5   18.	jЈ	654.8	H	523485	5394728	15.7	22.6	391.4	354.5	30.1	133.8	1.0	8	22	į
M   690.9   B?   524525   5394169   18.7   36.5   127.1   181.9   2.0   36.5   0.8   0   47     N   714.2   S   525129   5393847   1.9   8.9   2.8   13.1   1.5   1.9       0     O   742.1   S   525913   5393430   15.6   14.3   234.4   240.1   14.4   63.5   1.6   16   12     P   780.4   H   527108   5392832   7.3   6.6   57.7   34.4   23.9   26.0   1.3   20   7     Q   796.1   H   527609   5392556   11.5   11.1   48.6   71.2   5.5   11.5   1.4   12   0     R   813.2   S   528195   5392270   7.3   11.6   77.1   228.6   3.6   32.5   0.7   17   0      LINE   20390	K	674.0	S?	524035			10.6	15.3	78.8	1.3	10.2	1.1	4	14	į
M   690.9   B?   524525   5394169   18.7   36.5   127.1   181.9   2.0   36.5   0.8   0   47     N   714.2   S   525129   5393847   1.9   8.9   2.8   13.1   1.5   1.9       0     O   742.1   S   525913   5393430   15.6   14.3   234.4   240.1   14.4   63.5   1.6   16   12     P   780.4   H   527108   5392832   7.3   6.6   57.7   34.4   23.9   26.0   1.3   20   7     Q   796.1   H   527609   5392556   11.5   11.1   48.6   71.2   5.5   11.5   1.4   12   0     R   813.2   S   528195   5392270   7.3   11.6   77.1   228.6   3.6   32.5   0.7   17   0      LINE   20390	Ĺ	681.0	S	524242	5394325	4.8	22.4	15.9	79.4	1.2	10.7	j		9	į
O 742.1   S 525913   5393430   15.6   14.3   234.4   240.1   14.4   63.5   1.6   16   12	M	690.9	B?	524525	5394169	18.7	36.5	127.1	181.9	2.0	36.5	0.8	0	47	ĺ
P 780.4	N	714.2	S	525129	5393847	1.9	8.9	2.8	13.1	1.5	1.9	j		j o	į
P 780.4	ĺΟ	742.1	S	525913	5393430	15.6	14.3	234.4	240.1	14.4	63.5	1.6	16	12	j
R	P	780.4	H	527108	5392832	7.3	6.6	57.7	34.4	23.9	26.0	1.3	20	7	į
LINE 20390	ĺΩ	796.1	H	527609				48.6	71.2	5.5	11.5	1.4	12	0	į
A   6198.5   S   519102   5396808   1.7   3.6   2.8   10.2   1.5   2.1       0     B   6184.0   S   519560   5396568   5.9   0.3   7.2   11.3   1.9   1.4       0     C   6163.8   S   520125   5396264   4.1   9.7   146.6   192.6   5.9   42.9   0.4   8   0     D   6154.2   S   520412   5396115   10.6   7.7   26.7   65.6   3.3   8.3   1.9   21   0     E   6138.6   H   520898   5395856   9.6   6.6   186.7   101.5   10.2   38.9   2.0   30   0     F   6122.2   S   521407   5395594   7.7   12.0   49.6   95.7   6.5   14.2   0.7   0   0     G   6115.5   S   521601   5395485   0.0   8.0   77.0   147.7   2.2   24.3       23     H   6100.8   S   52208   5395278   2.3   8.4   5.9   60.8   0.0   8.1       71     I   6084.9   S   522440   5395055   2.2   5.4   17.4   21.5   3.4   0.0       17     J   6058.2   S?   523123   5394684   4.6   8.3   15.9   58.8   0.8   9.8   0.5   28   0     K   6046.1   H   523445   5394516   15.9   12.4   344.5   181.9   37.7   129.5   2.0   18   39	R	813.2	S	528195	5392270	7.3	11.6	77.1	228.6	3.6	32.5	0.7	17	0	ĺ
B   6184.0   S   519560   5396568   5.9   0.3   7.2   11.3   1.9   1.4       0     C   6163.8   S   520125   5396264   4.1   9.7   146.6   192.6   5.9   42.9   0.4   8   0     D   6154.2   S   520412   5396115   10.6   7.7   26.7   65.6   3.3   8.3   1.9   21   0     E   6138.6   H   520898   5395856   9.6   6.6   186.7   101.5   10.2   38.9   2.0   30   0     F   6122.2   S   521407   5395594   7.7   12.0   49.6   95.7   6.5   14.2   0.7   0   0     G   6115.5   S   521601   5395485   0.0   8.0   77.0   147.7   2.2   24.3       23     H   6100.8   S   522008   5395278   2.3   8.4   5.9   60.8   0.0   8.1       71     I   6084.9   S   522440   5395055   2.2   5.4   17.4   21.5   3.4   0.0       17     J   6058.2   S?   523123   5394684   4.6   8.3   15.9   58.8   0.8   9.8   0.5   28   0     K   6046.1   H   523445   5394516   15.9   12.4   344.5   181.9   37.7   129.5   2.0   18   39	LINE	20390		FLIGHT	4	 						 		 	 
B   6184.0   S   519560   5396568   5.9   0.3   7.2   11.3   1.9   1.4       0     C   6163.8   S   520125   5396264   4.1   9.7   146.6   192.6   5.9   42.9   0.4   8   0     D   6154.2   S   520412   5396115   10.6   7.7   26.7   65.6   3.3   8.3   1.9   21   0     E   6138.6   H   520898   5395856   9.6   6.6   186.7   101.5   10.2   38.9   2.0   30   0     F   6122.2   S   521407   5395594   7.7   12.0   49.6   95.7   6.5   14.2   0.7   0   0     G   6115.5   S   521601   5395485   0.0   8.0   77.0   147.7   2.2   24.3       23     H   6100.8   S   522008   5395278   2.3   8.4   5.9   60.8   0.0   8.1       71     I   6084.9   S   522440   5395055   2.2   5.4   17.4   21.5   3.4   0.0       17     J   6058.2   S?   523123   5394684   4.6   8.3   15.9   58.8   0.8   9.8   0.5   28   0     K   6046.1   H   523445   5394516   15.9   12.4   344.5   181.9   37.7   129.5   2.0   18   39	A	6198.5	S	519102	5396808	1.7	3.6	2.8	10.2	1.5	2.1			0	ĺ
D   6154.2   S   520412   5396115   10.6   7.7   26.7   65.6   3.3   8.3   1.9   21   0    E   6138.6   H   520898   5395856   9.6   6.6   186.7   101.5   10.2   38.9   2.0   30   0    F   6122.2   S   521407   5395594   7.7   12.0   49.6   95.7   6.5   14.2   0.7   0   0    G   6115.5   S   521601   5395485   0.0   8.0   77.0   147.7   2.2   24.3       23    H   6100.8   S   522008   5395278   2.3   8.4   5.9   60.8   0.0   8.1     71    I   6084.9   S   522440   5395055   2.2   5.4   17.4   21.5   3.4   0.0       17    J   6058.2   S?   523123   5394684   4.6   8.3   15.9   58.8   0.8   9.8   0.5   28   0    K   6046.1   H   523445   5394516   15.9   12.4   344.5   181.9   37.7   129.5   2.0   18   39	В	6184.0	S	519560	5396568	5.9	0.3	7.2	11.3	1.9	1.4			0	
E 6138.6	C	6163.8	S	520125	5396264		9.7	146.6	192.6	5.9	42.9	0.4	8	0	
E 6138.6	D		S		5396115	10.6				3.3		1.9	21	0	ĺ
G 6115.5 S 521601 5395485   0.0 8.0 77.0 147.7 2.2 24.3     23	E	6138.6	H	520898		9.6		186.7	101.5	10.2		2.0	30	1	ĺ
H     6100.8     S     522008     5395278       2.3     8.4     5.9     60.8     0.0     8.1              71         I     6084.9     S     522440     5395055       2.2     5.4     17.4     21.5     3.4     0.0              17         J     6058.2     S?     523123     5394684       4.6     8.3     15.9     58.8     0.8     9.8       0.5     28       0         K     6046.1     H     523445     5394516       15.9     12.4     344.5     181.9     37.7     129.5       2.0     18       39	F		S		5395594	7.7				6.5			0		
I     6084.9     S     522440     5395055     2.2     5.4     17.4     21.5     3.4     0.0       17       J     6058.2     S?     523123     5394684     4.6     8.3     15.9     58.8     0.8     9.8     0.5     28     0       K     6046.1     H     523445     5394516     15.9     12.4     344.5     181.9     37.7     129.5     2.0     18     39	G		S											1	
J 6058.2 S? 523123 5394684   4.6 8.3 15.9 58.8 0.8 9.8   0.5 28   0  K 6046.1 H 523445 5394516   15.9 12.4 344.5 181.9 37.7 129.5   2.0 18   39	H	6100.8	S											1	
K 6046.1 H 523445 5394516   15.9 12.4 344.5 181.9 37.7 129.5   2.0 18   39	I		S											17	
	J	6058.2	S?	523123	5394684	4.6						0.5			
	K		H									1		1	
L 6031.4 S 523827 5394296   3.5 5.5 39.3 100.1 2.4 17.5   0.6 12   0	L	6031.4	S		5394296	3.5						0.6	12	0	
M 6019.9 S 524153 5394151   6.3 5.7 5.8 23.4 1.2 3.3   1.2 26   11	M	6019.9	S	524153	5394151	6.3				1.2	3.3	1.2	26	I .	
N 6009.7 B 524435 5393993   12.3 19.8 67.6 124.7 0.4 22.0   0.8 0   18	N	6009.7	В	524435					124.7			0.8	0	1	ĺ
0 5995.6 S 524853 5393768 0.6 3.4 4.1 7.1 0.2 1.3 0.2 1.3 0.2 0	0	5995.6	S	524853	5393768	0.6	3.4	4.1	7.1	0.2	1.3			0	

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

  Labe	l Fid	Interp		YUTM	   CX 55   Real	Quad	Real	200 HZ Quad	CP Real	~		DEPTH*	Mag. Corr	
			m	m	ppm	ppm	ppm	ppm	ppm	n ppm	siemens	m	NT	ļ
LITNE	20390		FLIGHT	4	 						 I			
P	5985.0	S?	525158	5393615	2.8	10.3	35.2	99.3	1.6	15.1	 		15	i
ĺQ	5966.1	S.	525630	5393358	2.2	2.9	23.1	68.1	5.2	9.2	i		0	i
R	5955.9	S?	525880	5393231	7.5	12.9	6.6	17.5	6.3	3.5	0.7	5	0	i
s	5946.6	S?	526120	5393107	17.7	31.6	168.1	258.2	0.2	55.7	0.9	0	0	i
T	5914.6	Н	526864	5392694	6.3	14.4	111.0	24.4	26.6	49.6	0.5	1	0	i
ן ד ע	5894.5	H	527347	5392456	3.3	11.6	46.1	64.6	4.3	16.6	0.3	3	0	i
V	5869.2	S	527900	5392179	8.8	13.4		151.4	3.3	21.4	0.8	7	0	
LINE	20400		FLIGHT	4	 						 			 
A	5281.6	S	518977	5396672	0.8	0.8	1.9	9.9	2.0	1.8	j		0	į
В	5323.6	S?	519719	5396250	6.3	8.6	5.1	13.4	0.0	2.2			3737	ĺ
C	5339.2	S	520080	5396056	8.0	7.5	196.1	252.9	10.3	58.3	1.3	27	0	ĺ
D	5343.5	S?	520184	5396003	25.0	48.5	179.8	252.9	0.4	55.3	0.9	0	0	ĺ
E	5354.9	S	520388	5395901	1.0	2.8	2.7	11.9	0.5	1.9			0	
F	5376.5	S	520875	5395628	6.1	22.3	200.5	298.7	3.1	60.9	0.3	0	0	
G	5392.2	S?	521302	5395421	5.9	7.3	6.1	24.4	6.8	3.1			0	
H	5401.7	S	521545	5395294	9.0	14.1	49.3	150.3	2.1	22.1	0.8	2	55	
I	5407.7	S?	521695	5395220	5.7	21.2	27.7	110.0	4.2	17.1	0.3	0	0	
J	5425.9	S	522167	5394969	3.9	6.1	70.9	123.4	2.9	22.1	0.6	9	0	
K	5441.8	S	522629	5394733	31.0	14.9	265.8	345.6	6.7	77.5	4.6	11	26	
L	5456.2	S?	523016	5394532	3.1	10.0	16.3	33.1	2.3	6.3			0	
M	5466.3	S	523318	5394359	26.0	24.6	330.2	300.4	14.6	100.1	1.9	6	36	
N	5473.0	S?	523526	5394255	28.2	33.7	154.7	216.8	4.4	50.2	1.5	2	7	
0	5476.9	S?	523639	5394198	9.1	26.7	7.2	0.0	1.5	0.0	0.5	0	0	
P	5482.7	S?	523800	5394117	8.5	17.7	13.0	52.3	1.1	7.3	0.6	0	8	
Q	5487.2	S	523925	5394047	7.1	24.3	20.4	59.6	0.8	8.2	0.4	0	8	
R	5502.7	В	524306	5393833	13.4	22.6	238.3	252.6	7.6	68.5	0.8	0	21	ĺ
S	5526.4	S	524833	5393560	0.0	1.4	17.5	69.7	2.1	9.2			0	ĺ
T	5539.9	S	525173	5393387	4.5	16.3	20.2	117.1	1.7	16.7			10	ĺ
U	5556.0	S	525607	5393159	1.2	7.7	9.9	59.5	2.5	7.9			0	ĺ
V	5586.5	H	526570	5392654	14.0	17.7	130.7	100.0	31.6	49.7	1.1	11	0	ĺ
W	5629.9	S	527938	5391928	1.8	10.8	84.2	72.3	3.0	21.6	j 		0	 
LINE	20410		FLIGHT		!	<b></b>	<b></b>	<b></b>	<b></b>	<b>_</b>	ļ	<b>_</b>	!	
A	5167.7	S?	519590	5396100	1.3	9.8	0.0	21.6	0.4	3.6			3153	
В	5155.9	S	519899	5395951	5.2		199.5	308.6	9.9	66.6	0.2	0	0	
C	5140.1	S	520350	5395705	2.2	1.8	6.0	23.8	1.3	4.0			48	
D	5122.8	S?	520804	5395460	32.3	50.1	235.5	442.7	2.8	77.8	1.2	0	11	

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					CX 55	00 HZ	CP 7	200 HZ	CP	900 HZ	Vertical	l Dike	Mag. Corr	
Labe]	l Fid	Interp	MTUX	YUTM	Real	Quad	Real	Quad	Real	Quad	COND I	DEPTH*		
			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	
LINE	20410		FLIGHT	4	 									
E	5106.3	S	521276	5395210	8.0	30.8	78.1	320.9	13.0	46.6	0.3	0	0	
F	5098.2	S	521496	5395096	13.6	23.9	96.2	121.5	14.0	26.2	0.8	0	0	
G	5083.2	S	521870	5394906	1.3	3.5	0.6	14.5	6.1	1.4			0	
H	5061.6	S?	522320	5394662	11.3	20.6	48.8	156.0	3.1	22.9	0.7	0	0	
I	5050.4	S?	522596	5394501	22.2	31.1	146.4	231.0	2.5	43.4	1.2	0	0	
J	5022.9	S	523292	5394146	5.4	20.2	253.0	383.8	3.3	77.1	0.3	0	12	
K	5013.6	S	523537	5394013	13.1	33.7	283.3	419.2	5.3	82.4	0.6	0	18	
L	5001.4	S	523821	5393857	9.6	27.1	115.1	240.9	0.6	41.3	0.5	0	15	
M	4984.5	S?	524200	5393678	25.8	39.1	341.5	402.6	14.6	102.0	1.1	0	24	
N	4961.2	S?	524763	5393383	1.5	23.2	137.1	264.1	2.1	44.6			25	
0	4923.7	S?	525636	5392913	2.3	13.0	9.7	110.4	8.7	15.5			21	
P	4889.5	H	526561	5392412	7.9	8.0	60.2	48.5	30.4	32.6	1.2	28	0	
Q	4837.4	Н	527775	5391806	17.8	21.0	151.5	149.5	11.7	46.6	1.3	0	0	
 LINE	20420		FLIGHT	4	 						 			
A	4272.2	S	518884	5396255	1.4	1.9	3.0	25.1	0.7	3.3			j 0	
В	4312.7	S	519829	5395738	12.6	19.0	211.3	158.9	6.8	52.6	0.9	10	j 0	
C	4330.2	S	520281	5395503	4.4	13.0	12.9	96.9	0.3	13.2	0.4	0	j 0	
D	4349.9	S?	520753	5395261	2.0	10.6	28.0	93.6	4.1	13.9			0	
E	4364.8	S	521110	5395059	12.1	20.9	80.7	248.2	4.7	38.2	0.8	0	0	
F	4377.7	S	521448	5394889	10.0	7.8	136.4	154.6	8.1	34.3	1.7	12	j 0	
G	4391.2	S	521795	5394716	1.0	11.0	11.9	54.5	7.9	7.0			237	
H	4397.6	S	521939	5394635	4.6	10.4	8.2	65.5	5.3	7.9			j 0	
I	4411.2	B?	522255	5394469	7.3	5.9	33.2	97.9	4.1	16.7	1.5	18	j 0	
J	4419.7	S	522465	5394355	8.1	14.8	12.4	72.9	1.5	8.6	0.6	0	108	
K	4427.6	S	522668	5394245	10.5	21.4	32.3	148.6	0.8	20.8	0.6	0	0	
L	4439.0	S?	522969	5394093	5.6	10.7	5.2	6.2	1.3	1.0			0	
M	4454.1	S	523369	5393881	0.8	2.3	36.6	160.4	1.3	23.7			0	
N	4459.0	S	523507	5393811	17.8	18.5	235.8	316.4	4.4	64.5	1.5	9	21	
0	4466.0		523710	5393704	37.2	33.2	409.6	337.9	12.4	119.4	2.3	4	28	
P	4482.1	B?	524118	5393485	30.8	26.3	245.8	280.1	6.7	70.3	2.3	0	j 17	
Q	4496.9	S	524449	5393313	0.4	4.6	23.4	97.6	1.5	13.8			9	
~ R	4504.1		524623	5393209	1.1	14.4	36.6	143.6	1.1	20.2			0	
S	4540.0	S?	525606	5392693	21.1	29.7	311.7	348.4	4.6	90.0	1.1	0	0	
T	4569.9		526519	5392229	10.3		129.0	61.6	33.1	57.6	3.8	34	0	
IJ	4604.0	S	527626	5391654	17.3	13.5	214.3	218.6	9.4	63.2	2.1	9	i n	

CX = COAXIAL

\*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

CP = COPLANAR

Note: EM values shown above

EM Anomaly List

ļ					CX 55			200 HZ	CP	900 HZ	Vertica		   Mag. Corr	
Labe	l Fid	Interp	XUTM	YUTM	Real	Quad	Real	Quad	Real	Quad	COND	DEPTH*		
			m	m	ppm	ppm	ppm	ppm	ppm	ı ppm	siemens	m	NT	
LINE	20430		FLIGHT	4	 						 			
ĺΑ	4015.0	S?	521614	5394574	2.1	13.3	10.8	36.4	1.1	5.2			121	i
В	3986.9		522204	5394263	8.6	14.7	45.4	142.5	1.7	21.2	0.7	0	0	i
İc	3962.3		522832	5393941	4.5	10.1	9.3	67.6	0.1	9.5			0	i
р	3953.3		523059	5393819	4.1	2.5	2.4	18.8	0.3	1.7			0	i
E	3934.4	S	523540	5393555	1.0	18.6	163.5	255.8	4.0	49.5	i		22	į
F	3925.4	S?	523777	5393425	7.3	12.4	22.5	26.8	1.3	0.0	0.7	0	6	į
G	3913.4	S	524087	5393279	21.6	24.0	314.5	285.6	11.2	90.0	1.5	0	67	į
Н	3818.6	H	526347	5392089	6.2	0.3	97.0	32.3	37.8	39.6	i		0	į
	20431		FLIGHT		 I						 I			
A	1310.5	S?	518822	, 5396075	l   6.1	10.5	9.8	80.0	5.2	11.1	l 		72	-
B	1276.3	B?	519393	5395751	33.2	16.4	287.0	77.2	53.6	24.8	4.6	0	3632	
C	1265.8	H	519633	5395629	12.2	9.6	354.4	251.9	19.4	110.8	1.8	27	0	
l D	1237.1		520253	5395314	9.4	27.0	24.6	155.4	1.7	21.6	0.5	0		
E	1213.9		520233	5395057	8.4	28.4	13.7	122.2	2.8	16.7	0.4	0	125	
F	1199.2		521027	5394879	2.4	12.1	21.2	81.2	1.3	11.3	0.1 		15	ł
G	1178.3	S	521436	5394656	16.8	41.6	347.4		16.5	99.5	0.6	0	0	
													' 	
LINE			FLIGHT		ļ									ļ
A	3158.9		519255	5395573	6.1	0.1	66.5	31.3	36.3	21.0			5930	ļ
В	3170.7	H	519521	5395455	1.8	4.6	68.2	52.8	8.0	20.1			0	
C	3191.0		520005	5395203	4.7	12.8	13.0	64.3	3.0	9.3	0.4	0	0	
D	3199.6		520241	5395080	3.8	9.7	23.0	92.0	2.9	13.7	0.4	0	0	ļ
E	3213.3		520634	5394880	10.0	15.7	161.8	140.3	4.3	38.9	0.8	3	30	ļ
F	3219.9		520817	5394773	6.1	7.4	43.7	141.6	1.0	20.6	0.9	16	0	ļ
G	3239.7		521364	5394494	11.7	26.4	71.9	153.0	2.0	24.2	0.6	0	18	ļ
H	3244.2		521490	5394426	1.0	5.4	46.3	140.2	0.1	19.8			55	ļ
I	3255.7	S?	521794	5394256	2.4	9.6	7.3	61.5	1.3	8.2			0	ļ
J	3270.8		522196	5394045	2.8	22.3	131.4	213.2	3.2	39.1			13	ļ
K	3284.1		522568	5393846	2.8	1.0	36.5	129.0	1.4	19.1			8	ļ
L	3316.6		523436	5393397	0.0	5.6	194.3	174.4	5.7	51.3			14	ļ
M	3335.1	S	523970	5393128	34.6	10.7	296.5	340.3	14.3	112.5	8.9	13	119	ļ
N	3348.7		524347	5392926	0.2	6.0	7.2	37.2	0.2	4.8			0	ļ
0	3362.4		524667	5392754	1.1	1.4	5.7	30.7	0.9	4.9			0	ļ
P	3394.2		525444	5392327	14.0	17.0	237.8	254.1	11.3	46.4	1.2	9	0	ļ
Q	3424.1		526222	5391928	4.1	0.5	38.9	0.1	26.6	24.7			0	ļ
R	3455.5	B?	527215	5391410	7.3	17.4	164.1	270.3	7.3	58.2	0.5	0	1053	

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Note:EM values shown above are local amplitudes

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

    Labe	 l Fid	Inte:	rp XUTM	YUTM	   CX 55   Real	00 HZ Quad	CP 7	200 HZ Quad	CP Real	900 HZ Quad	Vertica COND	 l Dike DEPTH*	   Mag. Corr 	
	1 1 1 4	11100	m m	m	ppm	ppm	ppm	ppm	ppm		siemens	m	NT	
LINE	20450		FLIGHT	4	 						 		 	
A	2959.2	B?	519045	5395469	13.4	7.5	32.3	29.6	56.4	9.1	2.9	15	0	
В	2944.6	H	519395	5395304	8.5	10.6	142.3	65.9	56.0	43.8	1.0	0	0	
C	2922.4	S	519889	5395044	5.1	12.8	44.9	116.3	2.9	18.3	0.4	0	0	
D	2899.7	S	520438	5394748	9.6	12.8	181.4		5.6	53.5	0.9	6	24	
E	2889.4	S	520704	5394595	0.0	5.3	16.2	57.6	2.2	9.1			0	
F	2878.2	S?	520996	5394448	5.2	19.7	24.3	113.1	1.4	15.7	0.3	0	0	
G	2865.3	S?	521312	5394276	8.4	25.2	63.3	196.0	1.1	29.0	0.4	0	21	
H	2847.5	S	521733	5394056	2.0	15.5	16.3	99.2	1.1	14.0			0	
I	2832.6	S?	522092	5393875	15.9	30.8	112.6	257.2	1.5	41.2	0.8	0	22	ĺ
jЈ	2819.4	S	522410	5393700	6.9	27.4	20.9	111.8	1.8	16.4	0.3	0	0	į
K	2812.6	S	522600	5393604	13.3	34.6	55.6	132.0	2.4	19.3	0.6	0	8	į
ļь	2796.1	S	523037	5393372	6.3	23.1	278.2	411.5	3.8	80.2	0.3	0	175	į
M	2784.7	S	523339	5393200	4.3	10.6	87.4	152.1	1.8	28.8	0.4	9	7	į
N	2767.4	S	523800	5392968	17.2	24.1	76.2	154.9	1.6	26.5	1.1	0	57	į
İo	2760.8	S	523979	5392875	22.5	25.9	107.9		2.1	34.9	1.4	0	21	į
ĺР	2742.6	S	524469	5392630	4.0	5.6	11.3	42.8	1.0	6.0	i		16	į
ĺQ	2707.6	Н	525315	5392182	9.2	7.6	296.1		11.5	74.0	1.6	25	i o	i
Ŕ	2680.3	Н	526010	5391809	14.3		107.9	30.3	20.8	44.5	5.3	28	i o	i
İs	2647.2	Н	526816		7.5		319.0		43.7	89.1	0.4	1	i o	i
T	2635.0	B?	527089		5.4		39.4	40.4	28.7	14.2	0.7	29	0	
LINE	20460		FLIGHT	4	 						 		 	
A	2184.6	S	521676	5393882	1.7	8.8	32.1	129.9	0.4	18.1	j		j o	į
В	2199.7	S	522030	5393697	8.1	14.6	20.4	90.6	2.0	12.4	0.7	0	10	į
C	2204.7	S	522153	5393635	0.0	8.3	4.9	59.0	0.5	8.4	j		j o	į
D	2219.3	S	522483	5393435	9.5	17.8	36.0	114.6	2.3	17.4	0.7	0	j o	į
E	2243.1	S?	523092	5393115	12.7	16.6	29.5	98.8	2.2	13.9	1.0	0	j o	į
F	2252.0	S?	523316	5392997	7.7	25.4	1.6	16.5	1.3	2.5	0.4	0	0	į
G	2262.2	S	523601	5392849	10.7	11.3	243.2	141.7	8.0	57.1	1.2	16	55	į
Н	2283.6	S	524181	5392552	5.5	9.3	94.1	171.1	2.4	29.4	0.6	12	28	į
İΙ	2341.0	H	525739	5391739	5.1	1.7	15.1	35.9	3.4	3.5	j		115	į
jЈ	2371.5	S	526644	5391250	29.1	16.4	292.3	331.6	2.7	76.9	3.7	11	569	į
K	2388.3	S	527142	5390987	2.7	8.6	106.2	170.6	2.8	31.4	i		0	İ
LINE	20461		FLIGHT	7	 						 		 	
A	916.3	S	518201	5395700	5.3	31.4	55.1	213.5	0.6	30.9	0.2	0	0	į
В	952.3	D	518884	5395354	15.3	10.9	52.1	30.7	0.0	12.2	2.2	3	4620	į
														<u>-</u>

CX = COAXIAL

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Note: EM values shown above

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

    Labe	el Fid	Interp	XUTM	YUTM	   CX 55   Real	OO HZ Quad	CP 7	' '200 HZ Quad	CP Real	900 HZ Quad	   Vertica   COND	 l Dike DEPTH*	   Mag. Corr 	   
İ			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	į
LINE	20461		FLIGHT	 7							 			 
İc	972.4	В	519282	5395145	21.0	32.4	231.5	273.2	25.2	65.3	1.0	0	i o	i
D	976.0	В	519358	5395106	40.7	50.9	225.9	273.2	25.2	65.3	1.6	0	0	i
İΕ	998.0	S?	519736	5394894	11.5	20.4	185.5	235.4	8.5	52.2	0.7	0	j o	i
F	1036.5	S	520495	5394488	13.0	5.8	215.5	288.3	5.8	59.8	3.8	26	106	i
Ġ	1046.4	S	520699	5394378	1.8	0.0	1.9	14.3	0.8	2.3			31	i
Н	1052.4	S	520818	5394331	2.4	7.6	4.8	54.7	1.2	7.9			0	i
İı	1058.7	B?	520946	5394268	6.9	42.1		214.5	1.7	29.6	0.2	0	28	i
jЈ	1067.1	B?	521119	5394168	0.2	10.7	4.0	37.8	1.8	5.1			0	i
K	1073.4	S	521254	5394098	4.1	12.3	5.3	54.5	1.1	8.2			5	į
LT.TNE	20470		 FLIGHT	 4	 I						 I			 ا
A	1915.3	S?	518727	5395191	12.1	8.3	43.5	40.1	30.4	8.5	2.1	10	3202	
B	1899.8	s.	519190	5394953	15.7	15.7	284.0	228.9	109.1	58.4	1.5	7	0	ł
İC	1886.1	S	519623	5394730	1.4	3.6		123.4	3.9	23.1	±.5 		0	ł
D D	1879.0	S?	519836	5394609	2.2	9.6	15.2	64.1	1.4	9.2	 		74	ł
E	1857.1	s. S	520436	5394284	8.7	13.7			8.8	51.3	0.8	9	74	ŀ
F	1839.2	S	520130	5394025	3.2	9.8	6.8	37.3	0.9	5.4	0.0 		34	ł
Ġ	1825.8	S	521324	5393817	2.0	8.6	10.0	69.5	1.5	9.8	 		0	i
H	1819.4	S	521513	5393717	1.2	23.1		147.0	1.3	19.1	 		0	i
I	1814.6	S	521658	5393643	6.7	19.4	14.7	91.7	0.6	13.7	0.4	0	23	i
J	1806.0	S?	521917	5393509	14.1	36.4	81.6	231.0	1.3	34.0	0.6	0	28	
l K	1792.0	s.	522337	5393292	7.7	15.2		100.6	3.5	15.9	0.6	0	17	ł
L	1786.0	S?	522513	5393197	3.0	7.8	10.2	17.7	2.5	3.5	0.0 		0	ł
M	1767.5	S.	523065	5392909	13.1	22.5		165.1	1.0	24.3	0.8	0	0	i
N	1757.5	S	523375	5392747	0.6	13.3	202.4		3.2	60.9	l		0	i
0	1743.4	S	523792	5392516	8.9	7.8		183.8	6.0	49.3	1.5	21	17	ŀ
l P	1722.6	S	524387	5392231	2.7	4.6	16.6	53.2	1.3	7.7	±.5		0	ł
ĺQ	1683.6	H	525428	5391651	8.5	7.2	34.0	39.3	3.2	13.1	1.5	27	0	ł
R	1649.0	S	526351	5391177	10.1	23.5	77.6	99.1	9.0	35.7	0.6	0	602	ł
s	1641.5	S	526538	5391085	2.2		155.7		10.9	49.8	0.0 		0	ł
T	1627.5	S	526856	5390910	10.8	24.4		192.8	1.0	28.4	0.6	0	0	İ
	20480		 FLIGHT	Δ	 I						 I			 I
A	953.8	S	517998	5395341	1.0	4.4	4.6	61.7	1.0	8.1	l l –––		0	ł
l B	1002.2	S	517998	5394803	7.1		144.2	97.3	15.6	35.4	0.7	1	0	ł
I C	1002.2	S S	520354	5394119	10.1		102.4		3.3	33.4	0.7   1.1	6	1 0	ļ
l D	1056.7	S S	520545	5394119	20.4		173.6		8.4	52.7	1.1	0	1 0	-
E	1093.8	S S	520545	5394007	4.8	23.6		234.1	1.3	32.4	1.3 		1 0	-
<u></u>	1093.0	ు 	 	JJJJ0034 	4.8 	∠3.0	± / . 0	∠3 <b>4.</b> ⊥		34.4 	ı 		ı	ا 

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

  Label	l Fid	Inter	MTUX c	YUTM	   CX 55   Real	OO HZ Quad	CP 7	200 HZ Quad	CP Real	900 HZ Quad	Vertica COND	 l Dike DEPTH*	Mag. Corr 	
İ			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	į
LINE	20480		FLIGHT	4	 						 			
	1108.8	S	521621	5393448	4.8	8.6	14.1	37.8	1.3	4.8	i		18	į
Ġ	1119.2	S	521894	5393280	17.3	18.3	219.9	371.2	4.0	70.0	1.5	11	21	i
Н	1131.3	S	522210	5393110	22.1	32.4	525.1	424.6	30.3	159.2	1.1	3	0	į
İI	1149.1	S	522692	5392876	7.7	4.8	69.9	27.5	7.7	17.1	2.1	34	0	į
jЈ	1175.8	S?	523376	5392522	2.1	11.4	7.1	40.0	0.3	5.6	j		64	į
ĺк	1193.1	S	523846	5392270	9.7	33.5	68.8	152.7	1.2	25.5	0.4	0	8	į
ļь	1204.4	S	524163	5392114	0.0	1.5	49.4	86.3	1.7	16.1	j		0	İ
M	1234.7	S	524989	5391655	8.0	14.1	52.7	126.3	5.5	23.0	0.7	6	35	į
N	1248.5	H	525400	5391446	9.4	19.6	121.5	184.6	5.0	43.7	0.6	7	103	j
jo	1271.7	B?	526065	5391110	4.7	6.5	5.6	53.0	0.0	7.3	0.7	26	730	j
P	1289.8	H	526625	5390797	11.5	21.4	256.0	429.7	5.7	80.5	0.7	4	0	j
LINE	20490		FLIGHT	4	 						 			
A	818.0	S?	518531	5394845	0.0	17.2	97.5	22.9	108.5	3.8	j		5345	į
В	801.0	H	519040	5394582	12.8	10.6	191.9	156.9	9.3	56.9	1.7	16	0	j
ĺС	783.8	S	519501	5394340	2.9	9.3	29.6	42.1	7.1	5.7	j		j o	j
D	778.3	S	519647	5394265	4.9	8.8	35.7	56.1	40.5	6.9	j		1598	j
E	762.0	S	520029	5394052	1.0	7.1	7.2	45.7	6.1	6.6	j		0	j
F	755.8	S	520195	5393959	3.2	7.7	13.2	31.9	2.4	4.4			0	ĺ
G	746.5	S?	520451	5393831	19.3	20.5	231.1	210.4	10.6	66.0	1.5	0	0	
H	734.2	S?	520779	5393663	10.1	20.8	43.5	114.6	0.5	17.6	0.6	0	136	
I	726.7	S?	520999	5393541	9.9	16.1	40.0	80.1	2.3	14.0	0.8	0	0	ĺ
J	717.0	B?	521274	5393405	3.0	10.9	3.9	13.1	1.0	0.1			0	
K	697.9	S	521821	5393112	10.9	22.6	217.5	143.0	12.4	62.8	0.6	0	0	
L	688.5	H	522111	5392951	8.5	8.9	135.5	84.9	51.3	84.9	1.2	17	0	
M	650.0	S?	523244	5392363	3.5	13.2	17.7	76.3	1.9	11.1	0.3	6	56	
N	643.1	S	523420	5392281	4.5	0.6	44.7	77.3	1.4	13.3			0	j
0	631.8	S	523713	5392135	9.0	8.3	203.9	215.7	5.3	56.0	1.4	15	11	
P	588.2	H	524890	5391490	3.4	4.0	28.1	27.7	1.0	8.3	0.7	39	39	
Q	555.3	B?	525771	5391040	12.5	16.4	46.6	213.0	9.4	28.4	1.0	27	306	
R	524.8	H	526526	5390643	8.0	13.0	326.3	378.6	47.1	70.9	0.7	12	0	
S	508.6	H	526913	5390460	3.4	15.9	319.5	165.8	24.9	54.6	0.2	0	0	
LINE	20500		FLIGHT	2	 						 			
A	5915.1	S	517851	5394977	0.9	7.5	11.8	61.1	1.9	7.3			0	ĺ
В	5954.6	H	518821	5394479	8.2	13.8	146.4	166.6	7.4	50.3	0.7	11	52	ĺ
C	5974.2	S?	519357	5394183	2.8	9.3	6.0	9.1	29.6	1.0	j		0	j
D	5979.3	S	519496	5394111	3.2	7.0	18.1	61.1	42.3	8.0	ļ		0	İ

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

ļ					   CX 55			'200 HZ	CP		   Vertica		   Mag. Corr	 !
Labe	el Fid	Inter	•	YUTM	Real	Quad	Real	Quad	Real	~	!	DEPTH*		ļ
			m	m	ppm	ppm	ppm	ppm	ppm	ı ppm	siemens	m	NT	
											 I			
!	E 20500	00	FLIGHT		1 4 0	7 0	0 4	02 5	4 0	4 4	 			-
E   F	6000.3 6010.9	S?	520044 520332	5393829	4.0	7.2	8.4 362.2	23.5 306.2	4.0	4.4	   1.8		0	-
i =		S?	520332	5393665	26.8	40.2		368.3		108.5	1.8	0	22	-
G	6014.8 6027.8	S	520442	5393605 5393428			177.9			119.4 51.1	1.1 		507	-
H		S			2.1						!	0	20	-
I	6048.3	S	521388	5393127		39.1		418.4		104.4	0.5   3.2		· ·	!
J	6064.9	H	521862	5392850	14.7		331.7			119.1	3.2 	27 	0	ļ
K	6090.3	S	522597	5392472	2.6	3.8	2.7			4.6	I		0	ļ
L	6110.9	S	523213	5392138	19.1		223.8			61.0	2.7	12	18	ļ
M	6123.0	S?	523567	5391977	10.5	19.1	63.4			18.8	0.7	0	9	ļ
N	6149.2	H 	524334	5391567	17.8		332.6			108.1	2.2	16	0	!
0	6170.0	H	525008	5391211	7.9		258.3	86.8	11.4	63.0	0.7	13	0	!
P	6186.8	S	525502	5390947	37.8		338.3		4.6		1.4	0	21	ļ
Q	6222.8	H	526646	5390363	17.5	20.2	230.6	201.2	44.0	98.4	1.3	12	0	
LIN	E 20510		FLIGHT	2							 			 
A	5779.0	S	518233	5394541	12.7	8.2	62.5	39.7	90.7	7.1	i		0	ĺ
В	5770.5	S	518464	5394436	16.9	13.6	251.2	262.7	66.9	59.1	2.0	10	0	į
ĺС	5761.8	S	518710	5394302	3.3	21.0	115.4	237.1	1.7	41.7	0.2	0	61	į
D	5749.4	S	519044	5394123	5.4	6.6	89.5	177.5	2.9	26.7	0.8	17	0	į
E	5730.0	S	519567	5393849	5.9	1.3	29.9	24.1	35.6	3.0	j		0	į
F	5711.9	S	519981	5393626	3.0	5.2	4.7	26.8	7.3	3.6	i		0	į
Ġ	5697.7	B?	520324	5393435	37.4	42.4	285.8	298.0	10.5	79.7	1.7	0	0	i
Н	5684.8	S	520684		16.2	17.6	209.4	186.2	5.6	52.9	1.4	7	1057	i
İΙ	5663.7	S?	521227	5392976	4.0	11.0	56.4	96.4	3.0	16.6	0.4	0	16	į
jЈ	5644.4	S	521731	5392718	9.6	21.0	282.5	286.5	10.5	80.8	0.6	0	19	į
ĺК	5616.3	S	522523	5392292	16.8	19.8	303.6	264.7	17.9	92.8	1.3	4	0	į
ļь	5606.9	S	522773	5392154	8.7	16.4		221.3	3.3	36.7	0.6	4	0	į
М	5597.0	S?	523035	5392021	3.5	14.7	12.2	55.6	0.2	8.6	0.2	0	15	į
N	5587.2	S	523288	5391882	5.2	7.0	148.5	115.9	4.7	37.0	0.8	12	0	i
lo	5567.3	B?	523774	5391622	1.6	17.2		109.4	2.0	17.7	i		0	į
P	5557.4	S?	524015	5391503	21.5	26.6	261.2	277.7	5.2	74.1	1.3	11	0	į
ĺΩ	5549.7	H	524202	5391402	14.5	14.5	270.0		15.3	80.1	1.5	11	0	j
Ŕ	5530.2	H	524688	5391140	14.1			468.8	6.1	93.6	0.8	10	0	j
s	5501.7	S	525417	5390767	23.3	31.9		303.9	6.5	84.7	1.2	4	5	j
Т	5488.8	S	525747	5390598	10.8	21.8		245.3	16.9	52.9	0.7	4	0	i
ĺυ	5467.0	H	526235	5390334	8.4		208.0		25.2	81.7	0.6	5	0	i
·													· 	

CX = COAXIAL

Note: EM values shown above are local amplitudes

\*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

CP = COPLANAR Note:EM val

EM Anomaly List

!					   CX 55			200 HZ	CP	900 HZ	Vertica		Mag. Corr	 إ
Labe	l Fid	Interp		YUTM	Real	Quad	Real	Quad	Real			DEPTH*	ļ	
			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	
LINE	20520		FLIGHT	2	 						 			 
İΑ	4806.3	S	518284	5394299	5.2	5.3	106.0	78.4	33.9	20.6	1.0	15	j o	į
В	4817.0	S	518563	5394148	1.0	2.9	18.8	71.0	2.0	10.7			0	
İc	4833.9	B?	518960	5393949	8.6	14.5	67.6	153.3	3.2	24.3	0.7	0	0	İ
D	4850.8	S?	519351	5393741	4.6	7.3	36.5	16.2	40.7	3.0	i		561	į
E	4876.8	S	520000	5393392	3.1	12.2	76.9	148.9	1.7	26.4	i		j 0	į
F	4885.5	S	520254	5393258	8.2	15.8	161.8	335.5	2.9	58.2	0.6	6	j o	į
Ġ	4906.2	B?	520787	5392987	11.5	12.1	58.7	146.2	4.2	21.8	1.3	3	0	İ
Н	4921.1	S	521158	5392799	4.7	11.2	9.9	54.3	1.1	7.1			0	İ
İI	4926.5	S?	521289	5392723	4.6	17.9	23.3	113.2	0.2	15.7			10	İ
jЈ	4961.7	Н	522235	5392221	16.2	1.6	634.7	0.0	60.6	118.4			40	İ
ĺк	4987.4	S	522978	5391831	7.5	14.3	14.7	43.8	0.5	4.7	0.6	15	20	İ
İъ	5002.6	S	523413	5391597	1.4	1.4	3.1	13.4	1.7	1.8			j o	İ
M	5023.3	Н	524021	5391279	10.2	6.0	108.5	94.5	10.2	36.4	2.4	28	j o	İ
N	5058.5		525112	5390718	17.5		193.8		8.7	52.5	2.7	23	0	
0	5087.0		526037	5390224	21.4		427.8			136.1	1.3	1	0	
LITNE	20530		FLIGHT	··	 I						 I		 	 I
A	4646.5		518116	5394166	1   8.5	12 9	140.1	150 9	47.3	30.6	0.8	4	0	 
lB	4621.6		518789	5393812	0.0	14.7		148.3	2.4	26.9	0.0 			 
l C	4605.3		519224	5393578	1.2	7.1	14.0	22.3	14.7	3.2	 		343	 
l D	4579.7		519865	5393239	5.7	7.6	41.1	131.8	1.2	19.4	0.8	17	29	
E	4564.1		520271	5393020	9.5	14.6	31.3	50.9	21.9	7.7	0.8	0	1 0	 
F	4549.1		520662	5392819	30.4	29.6	166.9	261.3	13.4	47.2	1.9	0	0	 
G	4540.7		520902	5392684	16.1	20.8	264.6	330.6	5.8	74.6	1.1	5	14	
H	4516.1		521566	5392341	0.9	5.2	5.6	39.4	1.0	5.7			0	 
II	4496.6		522077	5392081	48.7	23.4	617.8	355.4	92.8	252.8	5.4	8	46	ļ
<del> </del>   J	4486.0		522367	5391927	14.6	31.4		330.7		111.2	0.7	0	0	ļ
K	4471.3		522758	5391716	1.4	3.4		135.1	4.2	23.3	0.7 		0	ļ
L	4452.2		523217	5391468	1.6	5.5	10.2	25.6	8.6	4.2	l 		0	ļ
l M	4428.3		523839	5391152	9.2	11.8	89.3	90.9	5.3	32.1	1.0	11	0	ļ
l N	4412.4		524232	5390938	0.0	12.7	14.3	39.4	3.5	6.1	l		7	l I
0	4412.4		524480	5390938	7.4		167.5	270.5	4.6	50.1	0.5	2	161	 
l P	4375.3		525083	5390486	17.7		162.0	171.1	20.8	48.3	1.1	4	1 0	l I
IQ	4375.3		525443	5390480	24.0	53.4			44.7	83.0	0.8	0	0	l I
♥  R	4339.0		525692	5390299	3.2	22.6	95.2		4.0	36.7	0.8	0	] 0	l
11/	/	ు	JZJUJZ	<del>-</del>	. J.Z		9J.Z			JU.1	0.2 		· · · · · · · · · · · · · · · · · · ·	ا 

CX = COAXIAL

CP = COPLANAR

Note: EM values shown above are local amplitudes

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

  Labe	l Fid	Inter	O XUTM	YUTM m	   CX 55   Real   ppm	00 HZ Quad ppm	CP 7 Real ppm	200 HZ Quad ppm	CP Real ppm	900 HZ Quad ppm	Vertica   COND :   siemens	 l Dike DEPTH* m	Mag. Corr       NT	
 					PPIII 									
LINE	20540		FLIGHT	2										
A	3670.5	S?	517633	5394183	7.0	4.6	25.8	39.5	39.5	19.9			4799	ĺ
В	3679.6	S	517896	5394049	5.7	6.4	92.4	91.1	52.6	13.8	0.9	21	0	ĺ
C	3691.6	S	518260	5393869	10.0	10.0	19.7	84.0	4.2	11.2	1.3	21	0	ĺ
D	3704.5	S	518641	5393656	6.7	13.0	158.9	316.5	4.4	53.1	0.6	3	0	ĺ
E	3718.5	S	519037	5393442	2.8	4.8	31.3	14.5	26.5	2.3			0	ĺ
F	3752.4	S	519943	5392978	6.4	17.7	164.1	283.2	5.1	51.6	0.4	0	0	
G	3759.1	S	520143	5392876	4.9	22.8	93.0	154.7	27.6	23.9	0.3	0	0	ĺ
H	3778.0	H	520718	5392566	13.5	8.6	172.5	42.6	16.6	53.9	2.4	25	0	ĺ
I	3814.3	S	521720	5392042	17.4	18.1	236.7	141.5	10.2	59.7	1.5	9	0	ĺ
J	3836.3	S	522348	5391708	7.6	22.9	142.2	261.9	1.9	45.9	0.4	0	0	ĺ
K	3841.1	S?	522492	5391634	0.5	1.5	4.3	37.4	1.3	5.2			0	ĺ
L	3876.8	H	523567	5391063	6.6	8.1	137.7	82.7	5.0	42.3	0.9	21	0	ĺ
M	3900.7	S	524252	5390721	3.2	10.9	19.7	88.1	1.6	13.2			99	ĺ
N	3912.2	S	524596	5390523	12.9	21.3	228.6	344.7	5.7	61.5	0.8	4	20	ĺ
0	3929.1	S	525128	5390246	13.6	13.5	175.0	99.8	59.3	45.8	1.4	16	0	ĺ
LT.TNE	20550		FLIGHT	2	 I						 I		 I	
A	3554.0	B?	517488	5394034	9.4	4.2	10.9	32.0	7.5	12.6	3.5	39	4038	l
B	3541.9	S.	517764	5393892	3.4	8.4	49.4	80.5	28.7	10.7	0.4	7	1 0	ł
İC	3523.2	S	518244	5393650	5.4	6.8	18.8	138.4	1.4	14.1	0.8	25	1 0	-
D	3510.6	S	518573	5393472	9.8		182.9	356.5	2.9	62.1	0.4	0	1 0	
E	3467.1	S?	519604	5392919	5.1	8.1	26.9	101.6	4.9	14.6	0.6	17	0	ł
F	3455.5	s.	519911	5392763	9.9	23.7		274.5	8.7	44.9	0.5	0	1 0	ł
G	3440.8	S	520291	5392564	1.2	8.1	73.7		28.8	24.6	0.5 		i o	ł
H	3426.3	H	520693	5392348	12.6	15.2	77.9	76.7	16.1	32.5	1.1	10	9	-
lI	3396.0	S	521508	5391921	7.2	12.2	267.6	212.9	8.6	74.1	0.7	10	l 0	
<del> </del>   J	3384.5	S	521825	5391769	14.3	19.4	226.2	395.1	4.2	73.7	1.0	8	51	
K	3367.6	S	522278	5391516	5.1	5.4	19.6	63.9	0.7	9.0	1.0	32	1 0	-
L	3356.8	S	522561	5391359	2.1	2.0	22.1	76.0	0.9	10.9	I.O		0	-
M M	3335.8	S	523099	5391087	4.5	0.9	125.5	79.5	3.7	35.6	l 		0	-
N N	3325.8	S	523365	5390952	4.3	7.2	39.1	88.1	5.9	14.6	0.6	25	l 0	
10	3312.3	S?	523712	5390768	7.8	7.2	17.4	36.2	1.4	4.2	1.2	31	0	
l P	3282.9	S:	524448	5390766	4.5		237.0	262.4	10.3	60.8	1.2 		1 0	
Q	3264.9	S	524948	5390111	12.8		108.5		3.1	40.1	1.4	4	50	
   T.TNF	20560		FLIGHT	2	 I						 		 I	 I
A	2916.2	S?	517271	5393947	8.2	6.5	15.0	16.2	0.0	7.8			2437	

CX = COAXIAL

CP = COPLANAR

Note:EM values shown above are local amplitudes

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

    Labe	el Fid	Interp	XUTM	YUTM	   CX 55   Real	 00 HZ Quad	CP 7	 200 HZ Quad	CP Real	900 HZ Quad	Vertica COND	 l Dike DEPTH*	   Mag. Corr 	   
İ			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	j
LINE	20560		FLIGHT	2	 						 		 	 
В	2926.9	S	517525	5393809	6.3	3.8	37.5	74.1	26.4	10.2			j o	į
İc	2940.5	S	517883	5393601	0.8	4.7	7.1	46.2	2.8	5.7			0	į
D	2951.5	S	518185	5393448	5.3	8.1	56.5	160.6	0.5	24.0	0.7	17	15	į
E	2958.3	S	518366	5393359	5.3	4.1	40.2	102.2	0.9	16.0	1.4	31	0	j
F	2977.3	S?	518819	5393132	4.1	4.4	33.1	69.2	12.0	10.4			0	j
G	3006.0	S?	519557	5392727	1.5	4.4	3.3	11.8	1.5	2.0			70	j
Н	3013.7	S	519784	5392606	5.1	10.2	91.9	136.4	39.6	21.6	0.5	0	0	j
I	3034.5	S	520425	5392273	4.0	22.0	231.2	275.8	5.5	65.9	0.2	0	6	ĺ
J	3046.9	H	520807	5392060	17.0	19.6	237.1	171.6	17.0	77.3	1.3	10	0	ĺ
K	3066.2	S	521359	5391783	14.2	19.6	84.2	137.9	4.9	28.0	1.0	0	20	
L	3074.8	S	521632	5391652	15.9	19.3	32.5	94.9	2.5	9.2	1.2	0	58	
M	3080.0	S	521790	5391557	8.3	15.8	34.6	115.8	1.0	15.7	0.6	2	19	
N	3087.3	S	522009	5391430	13.5	35.0	41.1	61.1	1.0	8.1	0.6	0	0	
0	3095.4	S	522251	5391304	4.6	9.4	80.7	173.1	2.3	27.4	0.5	6	0	
P	3121.8	H	523059	5390874	8.5	9.6	115.5	123.6	4.1	31.2	1.1	25	63	
Q	3137.1	S	523528	5390646	1.5	0.7		25.3	0.8	4.0			45	
R	3159.4	H	524219	5390263	7.0	6.3	111.1	131.8	8.6	28.2	1.3	27	56	
IT.TNF	20570		FLIGHT	2	 						 		 	I
A	2457.3	S	517323	5393671	0.3	9.1	45.1	19.5	57.9	3.5			j 0	i
ΪВ	2426.3	S	518138	5393235	3.1	10.2		166.7	1.6	28.7	0.3	0	18	i
İc	2407.2	S?	518641	5392975	3.8	8.9	54.3	81.4	40.5	12.3			0	i
D	2374.2	S?	519515	5392520	7.6	13.6	14.6	27.6	2.1	4.0	0.6	0	0	j
E	2362.7	S	519837	5392364	1.5	15.4	46.3	157.6	0.0	23.4			2173	į
F	2345.3	S	520298	5392100	0.3	7.4	4.1	27.2	1.5	4.0			0	į
Ġ	2335.2	S?	520552	5391969	0.0	1.8	39.0	156.8	1.1	23.0			25	į
н	2327.4	S	520769	5391860	0.0	11.8	142.5		3.5	42.3			29	į
I	2321.6	S	520937	5391777	12.7	21.4		132.1	0.2	17.3	0.8	0	7	į
J	2306.8	S	521345	5391554	7.5	17.0	183.3	229.4	4.2	50.3	0.5	0	39	į
K	2289.6	S	521849	5391297	4.7		107.2		1.8	34.0	0.4	0	0	j
Ĺ	2269.4	S	522395	5390993	10.2	19.7		172.8	3.0	30.4	0.7	6	0	į
M	2242.6	H	523029	5390659	10.0	15.6	165.6	142.7	10.2	56.1	0.8	8	0	j
N	2209.4	S	523851	5390248	13.7		130.6		2.4	38.6	1.0	0	53	į
   T.TNF	20580		FLIGHT	2	 I						 		 	 I
A	1976.0	S	520185	5391949	2.3	4.7	13.8	82.7	0.9	11.5	 		6	
l B	1994.7	S	520710	5391666	2.3	9.1	3.7	42.8	0.8	4.6			0	
I C	2000.8	S	520710	5391578	0.0	15.3		104.8	1.1	16.5			39	
											ı 		ı	ا 

CX = COAXIAL

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EM Anomaly List

    Labe	l Fid	Inter	p XUTM m	YUTM m	   CX 55   Real	OO HZ Quad ppm	CP 7 Real	200 HZ Quad ppm	CP Real ppm	~	Vertica   COND   siemens	.l Dike DEPTH*	Mag. Corr       NT	
 			 										N1	
LINE	20580		FLIGHT	2										1
D	2012.4	B?	521213	5391413	0.0	0.0	80.5	119.4	1.7	23.4	i		35	į
E	2021.4	S	521470	5391262	1.6	0.3	17.3	55.5	0.7	7.9			5	į
F	2026.9	S	521635	5391167	3.5	6.7	41.3	133.6	1.5	19.1	0.5	27	0	ĺ
G	2043.6	S?	522149	5390911	22.9	10.2	110.6	200.5	2.6	35.8	4.6	4	0	
H	2049.7	S?	522352	5390811	3.9	14.6	0.0	0.0	7.4	0.0			0	
ļΙ	2066.4	Н	522904	5390507	6.4	3.6	54.0	27.3	6.5	21.0	2.2	36	0	
LINE	20581		FLIGHT	8	 						 			
A	437.3	S?	517205	5393505	0.1	0.0	216.5	169.3	183.2	28.5			0	i
В	418.7	S	517663	5393276	8.1	13.1	7.9	41.5	14.2	5.9			0	i
İc	405.8	S	517987	5393098	8.5	15.9	13.0	85.3	1.0	11.7	0.6	7	0	į
ĺЪ	383.7	S	518538	5392818	3.3	18.2	10.4	85.5	5.6	11.0			167	į
E	347.5	S?	519406	5392365	7.7	19.6	108.4	189.8	6.6	34.2	0.5	0	0	į
F	333.0	S	519753	5392208	12.8	32.6	178.9	336.9	27.1	59.0	0.6	3	0	İ
LINE	20590		FLIGHT	2	 I						 I			
A	1739.9	S	517027	5393349	2.0	7.1	53.5	53.6	41.9	8.3	! 		0	
В	1722.6	S	517506	5393137	10.2	19.4	229.2	202.4	10.6	64.2	0.7	0	0	i
C	1708.9	S	517897	5392919	6.9	10.2	16.2	66.4	2.4	10.7			0	i
D	1700.7	S	518136	5392785	0.1	11.5	14.8	57.0	3.6	8.0			0	i
ĖΕ	1681.1	S?	518708	5392498	0.0	2.9	68.7	129.0	11.5	21.6			0	į
F	1658.1	S?	519291	5392170	7.5	18.6	57.6	53.2	58.4	8.3	0.5	0	0	i
Ġ	1644.7	S	519659	5391987	3.1	10.9	243.6	231.7	59.9	53.6	0.3	0	0	i
н	1635.8	S	519919	5391865	2.1	11.1	11.0	55.9	1.5	7.9			0	į
İΙ	1626.6	S	520173	5391729	4.6	10.2	10.8	80.9	0.4	11.4	i		16	į
jЈ	1604.3	S	520785	5391400	3.0	8.4	75.9	169.5	1.0	27.6	i		0	į
K	1593.8	S	521085	5391259	0.0	11.2	95.3	160.2	2.1	27.9	i		0	į
L	1583.1	S	521383	5391086	1.0	1.4	60.6	96.7	2.7	17.1			0	ĺ
M	1538.7	H	522685	5390395	6.6	10.2	88.9	36.3	12.9	32.6	0.7	14	0	
LINE	29010		FLIGHT	8	 I						 			 
A	6997.4	S	518169	5393297	2.3	7.5	122.0	217.4	2.7	40.9	 		0	
В	6986.1	S	518345	5393626	6.2	19.8	64.7	228.1	4.5	33.9	0.4	0	0	i
C	6955.9	H	518814	5394519	5.4	3.2	124.7	102.3	8.2	42.5	1.9	45	63	i
D	6926.1	H	519310	5395444	5.0	9.4	164.0	84.0	20.8	47.1	0.5	17	1198	j
E	6876.9	S	520090	5396933	1.6	0.3	6.9	21.6	5.7	3.4			0	j
F	6843.8	S	520574	5397868	0.0	2.7	3.8	31.5	1.2	4.5			0	į
G	6828.1	S?	520820	5398329	3.6	11.3		103.0	1.3	14.3	i		0	į
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EM Anomaly List

l		Interp		YUTM	Real	00 HZ Quad	Real	200 HZ Quad	CP Real			DEPTH*	Mag. Corr 	
			m 	m	ppm	ppm	ppm	ppm	mqq	ppm	siemens	m 	NT 	 
LINE	29020		FLIGHT	8	I						l			- 1
	7155.6	S	519701	5391961	7.0	19.0	232.2	263.9	4.1	63.3	0.4	0	i o	i
1	7167.9		519910	5392312	6.5	15.5	45.9	139.7	30.5	19.5			i o	i
ic 7	7187.1	S	520219	5392884	2.0	6.0	39.4	113.9	9.9	17.3			j o	i
D 7	7193.3	S	520320	5393077	0.0	1.0	22.6	60.8	3.0	8.8			j o	j
E 7	7207.1	S	520535	5393495	10.3	27.1	309.5	416.4	11.8	90.7	0.5	0	j o	İ
F 7	7224.1	S	520784	5393952	1.3	3.5	8.1	25.4	0.6	3.7			j o	i
G 7	7237.2	S	520979	5394342	4.4	11.1	50.2	227.3	0.7	31.3			j o	į
н 7	7250.8	S	521190	5394736	0.8	16.4	10.1	90.9	0.8	13.3			j o	i
İI 7	7265.7	S	521425	5395173	5.5	22.7	56.5	194.4	20.1	28.5	0.3	0	j 21	i
jл 7	7276.5	S	521599	5395501	1.3	21.1	104.4	192.8	11.8	33.0			j o	i
к 7	7293.1	S	521870	5396032	10.0	12.5	320.6	370.2	11.4	95.0	1.0	14	j o	i
L 7	7308.9	S	522140	5396534	7.0	17.1	138.1	240.0	4.0	41.7	0.5	0	j o	i
м 7	7315.2	S?	522242	5396745	3.4	13.9	0.6	79.5	1.3	12.3			j o	i
N 7	7352.7		522884	5397954	1.4	3.1	25.9	37.3	2.9	7.2			j o	į
0 7	7412.9		523870	5399827	1.1	2.7	8.0	9.8	6.6	1.6			j o	į
P 7	7432.5	S	524204	5400432	2.6	7.3	9.6	31.4	7.9	4.5			0	į
				0	 I						 I			
LINE		<b>C</b>	FLIGHT		0 1	1 - 0	71 0	100 1	1 0	20.7	0.7	0		
I	7922.7		521559	5391121	9.1	15.9		183.1	1.8	28.7	0.7	0	0 5	
	7916.4	S	521663	5391315	0.0	0.8	11.1	43.8	0.8	7.2				
1 -	7888.0	H	522126	5392224	25.4	26.5	503.9	303.4		213.0	1.7	1	0	
	7867.4	H	522438	5392807	23.7	29.7	487.7	439.7		156.6	1.3	3	0	
I	7847.0	S	522760	5393433	6.8	23.3	8.1	77.4	0.1	11.7	0.4	0	0	- !
	7801.9	H	523460	5394740	27.6	21.5	419.4	293.4		147.8	2.4	13	0	
	7789.7	S	523650	5395120	7.4	18.0	38.7	137.5	0.3	21.1	0.5	2	17	
1	7781.3	S?	523784	5395385	39.1	53.9	134.9	425.4	3.5	64.3	1.4	0	12	
	7769.8	S	523977	5395762	3.0	11.9	6.6	50.9	0.9	6.1			5	ļ
	7762.9		524086	5395985	2.7	4.2	7.6	30.2	1.2	4.1			9	ļ
1	7755.2	S	524222	5396226	0.0	0.0	37.7	87.8	0.8	13.3			12	ļ
	7728.7	S	524676	5397049	1.6	17.1	47.2	168.6	0.8	24.1			15	ļ
1	7721.6	S	524788	5397275	5.1	20.1		120.6	1.2	17.9	0.3	0	0	ļ
	7702.0	S?	525092	5397874	12.6	7.9	94.1	189.0	2.4	33.8	2.4	29	17	ļ
1 -	7692.9	S?	525249	5398160	4.3	8.3	12.4	26.5	1.3	4.9			0	ļ
	7680.5	S	525445	5398518	2.0	6.8	4.8	25.7	1.9	3.9			0	
ı ~	7667.7	H	525636	5398865	5.9		101.6		2.4	35.7	1.8	45	0	ļ
	7642.7	H	526010	5399609	3.0		122.1	72.7	4.8	31.6			0	ļ
S 7	7632.1	S	526187	5399936	7.0	16.5	19.1	73.5	2.1	5.7	0.5	4	0	

CX = COAXIAL

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Note:EM values shown above are local amplitudes

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

  Labe	l Fid	Inter <u>r</u>	XUTM m	YUTM m	CX 55   Real   ppm	00 HZ Quad ppm	CP 7 Real ppm	200 HZ Quad ppm	CP Real ppm	~	!	l Dike DEPTH* m	Mag. Corr     NT	
LINE	29030		FLIGHT	8	I						I			
İТ	7621.0	L	526371	5400271	21.5	22.0	135.7	201.4	42.9	52.2	1.6	0	0	İ
ĺυ	7605.0	S?	526606	5400745	3.2	5.9	23.0	19.0	17.7	2.6	i		0	İ
ľV	7583.5	L	526912	5401361	67.6	32.6	7.2	3.4	12.4	7.4	6.0	0	j 0	j
LINE	29040		FLIGHT	8	 						 			 
A	8095.6		523307	5390232	20.7	37.8	323.3		9.4	96.3	0.9	0	0	
В	8110.6	S	523539	5390633	5.7	9.3	4.9	51.8	1.8	5.8	0.6	23	0	
C	8133.8	H	523930	5391335	9.1	8.1	194.6	200.6	6.6	60.2	1.4	34	0	
D	8147.0	S	524143	5391756	4.8	8.5	149.1	207.0	1.8	41.7	0.6	8	0	
E	8160.1	S	524352	5392158	0.0	4.9	45.8	137.6	1.8	21.4			7	
F	8176.9	S	524633	5392687	0.8	5.6	4.6	53.0	2.8	8.8			0	
G	8207.5	S	525139	5393644	6.7	24.2	91.1	313.5	0.3	44.9	0.3	0	10	j
H	8237.4	S	525603	5394536	0.3	2.5	2.3	19.4	1.1	2.8			0	j
I	8242.8	S	525691	5394702	1.1	0.0	2.4	18.5	1.0	3.3			0	j
jЈ	8256.5	S	525903	5395123	0.2	11.1	78.6	268.8	2.2	39.9	j		5	j
K	8264.7	S	526048	5395381	4.7	6.5	76.1	200.0	2.1	30.6	0.7	16	0	j
ļь	8282.8	S	526353	5395943	0.8	1.9	1.9	18.2	1.0	2.6	j		0	j
M	8314.6	S	526875	5396952	1.3	4.1	6.7	81.7	0.7	11.3	j		9	j
N	8345.5	S	527390	5397914	3.7	11.5	4.4	65.0	2.3	9.0	0.3	4	0	j
ĺО	8350.5	S	527476	5398073	1.6	9.0	8.6	107.2	1.5	14.7	j		0	j
P	8374.5	S	527840	5398771	3.6	14.1	80.4	248.3	5.6	36.8	0.3	0	0	ĺ
ĺQ	8390.8	S	528095	5399249	7.8	16.2	118.6		3.1	40.8	0.6	0	0	j
R	8397.6	S	528199	5399455	16.2	42.5	102.1	171.9	1.5	30.4	0.6	0	21	j
İs	8406.2		528321	5399718	8.3	12.8		198.5	0.3	31.6	0.8	14	27	j
T	8417.8	S	528505	5400062	13.5	10.6	162.9		2.6	49.6	1.9	16	51	j
LINE	29050		FLIGHT	8	 						 			 
A	8869.7	S	525571	5390163	25.9	23.8	340.8	450.7	9.9	101.9	2.0	7	0	j
В	8860.7	H	525714	5390444	20.3	23.5	450.3	354.2	17.9	134.4	1.4	6	307	j
C	8841.4	S	526035	5391047	8.9	7.0	16.9	86.9	8.6	9.7	1.7	28	635	j
D	8829.8	S	526211	5391388	5.5	6.1	101.9	249.6	0.1	40.2	1.0	29	34	j
E	8786.0	H	526919	5392740	8.0	7.4	121.0	101.7	22.4	50.9	1.3	32	0	j
F	8731.2	S	527842	5394489	10.6	17.5	91.6	95.8	6.5	24.4	0.8	10	0	j
G	8691.3	S	528465	5395695	10.3	20.6		131.8	2.1	17.9	0.6	2	22	j
н	8653.1	S	529102	5396865	5.7	7.8	114.8	160.3	2.0	30.2	0.8	25	13	j
İı	8624.2		529549	5397749	1.4		121.8		5.3	37.0	i		0	j
јЈ	8601.7	S	529923	5398427	9.1		176.0		2.0	57.0	0.7	9	20	j
K	8586.8	S	530186	5398911	3.7	6.7		147.8	1.6	28.8	0.5	21	0	İ
													' 	'

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

  Labe	l Fid	Inte	rp XUTM	YUTM	CX 55	00 HZ Quad	CP 7	7200 HZ Quad	CP Real	900 HZ Quad	1 7	l Dike DEPTH*	Mag. Corr	   
			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	
LINE	29050		FLIGHT	8							 			
ļL	8573.8	S	530361	5399334	8.6	15.5	154.6	363.6	2.0	58.3	0.7	12	8	İ
LINE	29060		FLIGHT	8							 			
A	9090.7	H	530189	5394662	5.7	7.1	98.3	108.4	6.9	31.9	0.8	23	0	ĺ
В	9178.9	S	531662	5397440	4.9	12.4	124.9	352.7	11.0	55.3	0.4	9	0	ĺ
C	9195.6	S?	531934	5397972	23.4	64.6	197.7	439.6	4.8	72.6	0.7	0	211	ĺ
D	9207.4	S	532122	5398332	2.5	16.6	166.1	318.6	8.9	55.7	ļ		224	j
LINE	29070		FLIGHT	8							 			
A	9425.2	S	532057	5393902	15.7	29.9	418.0	541.3	11.9	120.0	0.8	3	23	ĺ
В	9414.2	S	532246	5394263	25.4	32.8	283.7	359.2	6.6	77.0	1.3	4	0	ĺ
C	9377.6	H	532901	5395520	9.6	8.3	132.8	101.7	8.7	39.8	1.5	23	16	ĺ
D	9349.1	B?	533409	5396473	10.1	8.3	172.3	274.4	6.5	52.7	1.6	14	0	ĺ

CX = COAXIAL

CP = COPLANAR

Note:EM values shown above are local amplitudes

Area B

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\*Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

LINE 30010   FLIGHT 12   A 5218.3   S 525096   5397626   4.2   13.6   19.1   154.3   0.0   18.0   0.3   5   19     B 5225.6   S 525097   5397870   0.8   2.4   72.2   122.0   2.0   19.7       6     C 5258.2   H 525114   5399109   2.6   3.1   16.5   42.5   11.4   12.9       0     D 5282.6   S? 525085   5400047   0.0   3.0   100.8   106.4   14.7   27.1       676     E 5300.2   S 525110   5400707   0.6   7.1   7.7   44.9   4.6   6.5       206     F 5305.2   S? 525088   5400891   1.8   7.4   35.1   9.8   34.8   4.2       0     G 5322.7   L 525091   5401570   24.6   16.4   9.9   10.2   137.4   16.3   2.8   0   0     H 5331.0   L 525097   5401881   22.6   33.8   40.8   177.4   4.0   32.9   1.1   0   0     I 5336.6   S 525086   5402081   2.8   4.4   4.4   2.3   1.5   5.4       105     J 5352.3   S 525093   5402659   4.1   5.3   230.7   249.6   15.9   57.9   0.7   33   0      LINE 30020   FLIGHT 12	al Dike   Mag. Corr   DEPTH*     m   NT	Vertica COND		CP Real	7200 HZ Quad ppm	CP 7 Real ppm	000 HZ Quad ppm	   CX 55   Real   ppm	YUTM m	XUTM m	Interp	l Fid	  Labe
A			'						12	FLIGHT		30010	LINE
B   5225.6   S   525097   5397870   0.8   2.4   72.2   122.0   2.0   19.7       6     C   5258.2   H   525114   5399109   2.6   3.1   16.5   42.5   11.4   12.9       0     D   5282.6   S?   525085   5400047   0.0   3.0   100.8   106.4   14.7   27.1       676     E   5300.2   S   525110   5400707   0.6   7.1   7.7   44.9   4.6   6.5       206     F   5305.2   S?   525098   5400891   1.8   7.4   35.1   9.8   34.8   4.2       0     G   5322.7   L   525091   5401570   24.6   16.4   9.9   10.2   137.4   16.3   2.8   0   0     H   5331.0   L   525097   5401881   22.6   33.8   40.8   177.4   4.0   32.9   1.1   0   0     I   5336.6   S   525086   5402081   2.8   4.4   4.4   2.5   31.5   5.4       105     J   5352.3   S   525093   5402659   4.1   5.3   230.7   249.6   15.9   57.9   0.7   33   0      LINE   30020   FLIGHT   12	5   19	0.3	18.0	0.0	154.3	19.1	13.6	4.2					1
C   5258.2   H   52514   5399109   2.6   3.1   16.5   42.5   11.4   12.9       0     D   5282.6   S?   525085   5400047   0.0   3.0   100.8   106.4   14.7   27.1       676     E   5300.2   S   525110   5400707   0.6   7.1   7.7   44.9   4.6   6.5       206     F   5305.2   S?   525098   5400891   1.8   7.4   35.1   9.8   34.8   4.2       0     G   5322.7   L   525097   5401570   24.6   16.4   9.9   10.2   137.4   16.3   2.8   0   0     H   5331.0   L   525097   5401881   22.6   33.8   40.8   177.4   4.0   32.9   1.1   0   0     I   5336.6   S   525086   5402081   2.8   4.4   4.4   25.3   1.5   5.4       105     J   5352.3   S   525093   5402659   4.1   5.3   230.7   249.6   15.9   57.9   0.7   33   0      LINE   30020	- 1							1					
D   5282.6   S?   525085   540047   0.0   3.0   100.8   106.4   14.7   27.1       676   E   5300.2   S   525110   5400707   0.6   7.1   7.7   44.9   4.6   6.5       206   F   5305.2   S?   525508   5400891   1.8   7.4   35.1   9.8   34.8   4.2       0   G   5322.7   L   525091   5401570   24.6   16.4   9.9   10.2   137.4   16.3   2.8   0   0   0   H   5331.0   L   525097   5401881   22.6   33.8   40.8   177.4   4.0   32.9   1.1   0   0   0   1   5336.6   S   525086   5402081   2.8   4.4   4.4   25.3   1.5   5.4       105   J   5352.3   S   525093   5402659   4.1   5.3   230.7   249.6   15.9   57.9   0.7   33   0   0   1   1   1   1   1   1   1   1	0		12.9	11.4				1					İc
E 5300.2 S 525110 5400707	676		27.1	14.7	106.4	100.8	3.0	0.0	5400047	25085	S? 5	5282.6	D
G 5322.7	206		6.5	4.6		7.7	7.1	0.6	5400707	25110	S 5	5300.2	E
H 5331.0	0			34.8	9.8	35.1	7.4	1.8	5400891	25098	S? 5	5305.2	F
T	0   0	2.8	16.3	137.4	10.2	9.9	16.4	24.6	5401570	25091	L 5	5322.7	Ġ
J 5352.3 S 525093 5402659   4.1 5.3 230.7 249.6 15.9 57.9   0.7 33   0	0   0	1.1	32.9	4.0	177.4	40.8	33.8	22.6	5401881	25097	L 5	5331.0	н
LINE 30020   FLIGHT 12	105		5.4	1.5	25.3	4.4	4.4	2.8	5402081	25086	S 5	5336.6	İI
A 5130.2   S 525306   5397849   6.1   10.7   140.1   162.4   3.6   39.5   0.6   23   15   15   15   15   15   15   15   1	33 0	0.7	57.9	15.9	249.6	230.7	5.3	4.1	5402659	25093	S 5	5352.3	jЈ
A		 						 	12	FLIGHT		30020	LINE
B   5095.8   H   525312   5399061   3.7   8.3   33.0   49.4   11.7   15.0   0.4   14   0   0   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5   0.6   0.5	23   15	0.6	39.5	3.6	162.4	140.1	10.7	6.1					
C   5068.0   S   525295   5400040   3.7   5.5   124.1   80.3   5.3   36.5   0.6   33   495     D   5037.2   S   525306   5401062   0.8   3.3   24.6   26.1   31.1   3.7       0     E   5022.0   L   525300   5401535   8.1   18.4   9.0   12.9   13.0   6.6   0.5   0   88     F   5009.5   L   525307   5401938   12.1   7.8   22.1   57.5   0.3   10.3   2.3   22   0     G   5004.7   S   525304   5402103   6.4   15.3   74.7   160.3   3.1   26.1   0.5   0   96     H   4989.1   S   525296   5402640   6.3   23.6   295.6   381.6   10.2   88.5   0.3   0   0      LINE   30030	! !	!						1					В
D	33   495	0.6		5.3			5.5	3.7					İc
F 5009.5	0			31.1	26.1	24.6	3.3	0.8					D
F 5009.5	0   88	0.5		13.0				1					E
H	22   0	2.3	10.3	0.3	57.5	22.1	7.8	12.1	5401938	25307	L 5	5009.5	F
LINE 30030   FLIGHT 12	0   96	0.5	26.1	3.1	160.3	74.7	15.3	6.4	5402103	25304	S 5	5004.7	Ġ
A       4745.5       S       525507       5397853       9.0       11.3       162.2       242.1       5.1       48.4       1.0       24       0         B       4769.8       S       525498       5398519       8.5       5.2       8.6       39.4       1.2       5.7         0         C       4797.7       H       525506       5399362       4.2       2.3       5.8       3.7       2.2       1.9         0         D       4845.0       S       525509       5401127       7.1       4.5       28.6       15.2       32.4       1.5         542         E       4854.6       L       525511       5401497       15.8       10.6       22.7       6.7       25.6       18.3       2.4       7       126         F       4867.0       L       525509       5401962       18.2       23.7       87.5       175.3       1.7       30.0       1.2       0       130	0 0	0.3	88.5	10.2	381.6	295.6	23.6	6.3	5402640	25296	S 5	4989.1	Н
B		 	·					 	12	FLIGHT		30030	LINE
B	24   0	1.0	48.4	5.1	242.1	162.2	11.3	9.0	5397853	25507	S 5	4745.5	A
D	0		5.7	1.2	39.4	8.6		8.5	5398519	25498	S 5	4769.8	В
E     4854.6     L     525511     5401497     15.8     10.6     22.7     6.7     25.6     18.3     2.4     7     126       F     4867.0     L     525509     5401962     18.2     23.7     87.5     175.3     1.7     30.0     1.2     0     130	0		1.9	2.2	3.7	5.8	2.3	4.2					ĺС
F 4867.0 L 525509 5401962   18.2 23.7 87.5 175.3 1.7 30.0   1.2 0   130	542		1.5			28.6		:	5401127	25509	S 5	4845.0	D
	7   126	2.4	18.3	25.6	6.7	22.7	10.6	15.8	5401497	25511	L 5	4854.6	E
	0   130	1.2	30.0	1.7	175.3	87.5	23.7	18.2	5401962	25509	L 5	4867.0	F
G 4003.3 5 525455 5402034   0.0 14.5 251./ 415.2 10.0 /5.4   0.5 9   0	9   0	0.5	79.4	10.6	419.2	251.7	14.5	6.8	5402634	25495	S 5	4885.3	Ġ
LINE 30040		· 	·						12	FLIGHT		30040	LINE
A 4648.6 S 525717 5397698   5.2 12.6 190.5 186.6 8.0 54.7   0.4 13   25	13   25	0.4	54.7	8.0	186.6	190.5	12.6	5.2	5397698	25717	S 5	4648.6	A
B 4637.8 S 525728 5398086   19.1 30.7 98.6 223.9 0.8 36.4   1.0 0   28	0   28	1.0	36.4	0.8	223.9	98.6	30.7	19.1	5398086	25728	S 5	4637.8	В
C 4632.2 S? 525721 5398280   5.1 12.5 67.1 120.0 1.3 21.6   0	j 0 i		21.6	1.3	120.0	67.1	12.5	5.1	5398280	25721	S? 5	4632.2	C
D 4616.4 S? 525725 5398805   5.3 12.1 43.4 127.5 0.0 21.0   0.5 1   0	1   0	0.5	21.0	0.0	127.5	43.4	12.1	5.3	5398805	25725	S? 5	4616.4	D
E 4596.0 H 525701 5399584   3.9 0.6 0.0 0.0 7.6 8.5     0	j 0 j		8.5	7.6	0.0	0.0	0.6	3.9	5399584	25701	Н 5	4596.0	E
F 4579.9 S? 525712 5400281   20.3 34.2 313.5 614.2 21.9 107.0   0.9 7   0	7   0	0.9	107.0	21.9	614.2	313.5	34.2	20.3	5400281	25712	S? 5	4579.9	F

CX = COAXIAL

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Note:EM values shown above are local amplitudes

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

  Labe	l Fid	Interp	MTUX c	YUTM m	CX 55   Real   ppm	000 HZ Quad ppm	CP 7 Real	200 HZ Quad ppm	CP Real ppm	900 HZ Quad ppm	Vertica COND siemens	Dike DEPTH*	Mag. Corr     NT	
LINE	30040		FLIGHT	12	 						 		 	
Ġ	4550.0	L	525689	5401451	22.7	25.4	8.4	5.0	26.7	22.5	1.5	0	0	i
Н	4536.5	S	525688	5401955	6.1	10.0	92.1	162.5	1.4	28.3	0.7	0	0	į
ļΙ	4516.8	H	525693	5402585	3.7	8.7	185.1	347.0	4.4	53.6	0.4	20	j 0	İ
LINE	30050		FLIGHT	12	 						 			
A	4176.7	S	525903	5398152	9.9	19.5	70.9	194.0	1.0	29.4	0.6	1	8	į
В	4189.1	S	525891	5398560	7.1	10.2	4.4	15.9	3.4	2.4	j		0	į
C	4195.5	S?	525899	5398751	11.9	32.5	53.8	197.8	0.4	27.6	0.5	0	23	ĺ
D	4206.5	S	525885	5399073	1.3	11.9	12.5	68.9	2.4	9.5			0	ĺ
E	4227.7	S	525910	5399823	5.0	8.2	104.0	110.1	7.5	24.8	0.6	32	16	j
F	4243.8	S	525890	5400413	2.3	6.2	184.5	200.2	38.6	44.9			0	
G	4270.9	L	525910	5401461	21.2	14.8	16.0	17.8	33.2	15.3	2.5	8	90	İ
H	4278.5	S?	525903	5401756	5.9	13.2	19.6	59.4	8.7	4.5			0	İ
I	4283.0	S	525896	5401934	7.4	11.2	102.9	147.7	0.2	28.3	0.7	0	110	İ
J	4305.1	H	525906	5402764	10.6	13.7	64.5	68.6	2.6	18.6	1.0	22	0	ĺ
LINE	30060		FLIGHT	12	 						 			
A	4090.2	S	526105	5397613	18.8	39.5	294.1	493.0	4.7	93.7	0.8	0	0	ĺ
В	4076.6	S	526094	5398173	0.8	2.4	6.4	19.3	3.3	2.5			0	
C	4064.6	S	526108	5398651	10.2	14.8	95.5	225.1	0.8	36.7	0.9	7	23	
D	4059.3	S	526106	5398875	3.7	9.4	51.2	112.1	1.5	18.8	0.4	4	5	
E	4041.2	H	526117	5399603	2.8	1.7	68.0	138.5	4.8	16.7			5	İ
F	4025.0	L	526111	5400264	18.7	8.2	126.7	202.3	25.2	57.1	4.5	18	0	İ
G	4017.6	S	526103	5400559	1.1	6.4	9.7	61.8	0.0	8.9			1646	İ
H	3998.6	S	526094	5401254	3.2	16.6	29.8	113.3	117.2	15.3			0	İ
I	3993.6	L	526085	5401430	28.5	22.5	40.4	61.9	22.1	43.4	2.4	0	36	ĺ
J	3978.1	S	526095	5401973	13.3	10.5	102.7	147.6	3.6	28.0	1.9	4	145	İ
K	3952.9	S	526106	5402761	16.3	28.9	212.7	209.5	15.0	69.7	0.8	12	0	
LINE	30070		FLIGHT	12	 						 			
A	3746.8	S	526313	5397709	1.1	21.2	199.8	318.5	3.3	61.4	i		0	j
В	3762.0	S?	526302	5398226	0.5	1.8	3.7	17.6	0.1	3.0	i		0	į
c	3774.2	S	526305	5398678	16.2	29.2	155.0	332.6	0.7	53.4	0.8	0	20	į
D	3806.0	H	526296	5399805	2.9	0.0	0.0	2.0	5.2	2.3	i		0	į
E	3816.2	L	526294	5400214	34.8	13.4		185.3	28.3	48.8	6.5	12	0	į
F	3833.1	S	526318	5400806	2.9	3.7	20.2	16.3	20.3	2.1	i		0	į
Ġ	3845.5	S	526294	5401272	7.7	10.1	75.6	91.0	62.3	20.7	i		0	į
н	3849.6	L	526294	5401429	21.4	6.3	7.3	13.5	31.4	15.8	8.2	4	77	į

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

  Labe	l l Fid	Inter	p XUTM m	YUTM m		00 HZ Quad ppm	CP 7 Real ppm	200 HZ Quad ppm	CP Real ppm	~	Vertica COND siemens	 l Dike DEPTH* m	Mag. Corr       NT	
LINE	30070		FLIGHT	12										1
İı	3862.0	L	526303	5401909	15.3	12.1	124.0	216.4	5.6	40.6	1.9	6	0	i
jЈ	3865.4	S	526293	5402043	0.9	5.6	126.9	202.3	5.6	39.6			0	į
ļκ	3884.2	S	526307	5402660	36.4	74.3	381.7	435.6	65.4	145.5	1.0	0	j 0	į
LINE	30080		FLIGHT	12	 						 			
A	3663.2	S	526504	5397890	7.4		157.1		3.7	48.3	0.5	8	24	
В	3641.8	S	526520	5398750	0.0	8.2	77.1	89.0	2.9	19.8			11	
C	3630.9	S	526512	5399157	0.0	0.5	44.7	61.4	0.9	9.8			0	
D	3619.7	S	526503	5399549	16.3	26.3	367.5	360.7	30.5	115.3	0.9	5	0	
E	3610.0	H	526505	5399902	4.3	6.7	53.3	82.2	7.1	16.2	0.6	33	0	
F	3598.0	L	526503	5400304	25.5	16.5	216.1	206.7	54.3	68.4	3.0	2	0	
G	3582.4	S?	526495	5400823	1.9	5.6	28.1	16.3	25.9	3.0			0	
H	3564.9	L	526492	5401413	16.0	29.3	71.9	78.5	61.2	47.9	0.8	0	143	
Ι	3551.0	L	526490	5401893	12.6	10.2	50.6	68.4	4.3	15.3	1.8	10	0	
J	3547.2	S	526499	5402022	5.6	9.3	53.9	134.4	3.0	22.8	0.6	24	0	
K	3532.3	L	526518	5402483	55.6	46.6	283.7		42.8	106.6	2.8	2	71	
L	3522.3	Н	526530	5402776	22.4	31.1	295.7	201.8	17.7	87.9	1.2	9	6	
LINE	30090		FLIGHT	12	 						 		 	
A	3246.1	S	526730	5397952	11.6	50.2	197.6	461.1	4.6	74.1	0.4	0	0	į
В	3258.1	S	526710	5398391	6.1	12.2	5.3	50.4	0.4	5.6	0.5	0	7	ĺ
C	3268.0	S	526696	5398778	16.6	35.2	127.8	221.1	2.6	39.9	0.7	0	21	į
D	3272.5	S	526687	5398960	1.2	1.2	77.6	119.3	0.4	23.0			5	
E	3302.0	H	526699	5399890	0.9	1.3	6.1	0.1	9.1	6.5			0	
F	3313.4	L	526705	5400329	25.0	24.5	230.9	252.7	23.5	74.7	1.8	0	0	
G	3329.9	S	526716	5400840	0.1	2.6	10.5	21.2	4.7	1.9			0	ĺ
H	3342.8	L	526708	5401302	6.4	15.5	32.7	8.5	38.3	28.5			0	
Ī	3357.0	L	526716	5401863	17.0	16.7	63.2	123.6	6.3	22.3	1.6	0	0	ĺ
J	3358.5	S	526717	5401923	14.7	0.1	63.2	123.6	4.1	22.3			0	ĺ
K	3372.0	L	526706	5402427	62.2	38.2	46.4	330.4	33.8	97.1	4.3	0	0	ĺ
L	3377.6	H	526700	5402628	5.9	11.0	247.4	289.0	22.1	46.0	0.6	16	0	
LINE	30100		FLIGHT	12	 						 		 	 
A	3011.1	S	526909	5398177	24.3	35.0	304.3	451.8	5.5	90.2	1.2	3	0	j
В	2998.6	S?	526917	5398605	4.8	8.6	16.9	45.9	1.5	7.9			0	j
ĺС	2989.3	S	526902	5398959	8.5	13.9	159.7	247.3	1.6	46.7	0.7	2	71	j
D	2963.4	H	526908	5399889	3.2	0.0	4.7	0.0	22.8	17.2			0	j
E	2947.0	L	526893	5400398	21.2	29.4	25.8	332.8	0.4	48.5	1.2	4	0	į

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

Label   Fid   Interp   XIFM   YUTM   Real   Quad   Real   Quad   Real   Quad   Real   Quad   COND   DEPTH*   Remain   Depth						   CX 55	00 HZ	CP 7	200 HZ	 CP	900 HZ	Vertica	 l Dike	Mag. Corr	
LINE 30100   FLIGHT 12   F 2933.6   S 526885   5400685   6.0   11.7   85.0   143.6   16.7   29.2   0.5   4   0   0   0   0   0   0   0   0   0	Labe	l Fid	Interp	XUTM	YUTM	Real	Quad	Real	Quad	Real	Quad	COND 1	DEPTH*		į
F	İ			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	j
C   2927.0	LINE	30100		FLIGHT	12	 						 			
H   2912.7	F	2933.6	S	526885	5400685	6.0	11.7	85.0	143.6	16.7	29.2	0.5	4	j o	į
I	G	2927.0	L	526884	5400893	18.9	9.2	73.1	74.0	20.2	38.5	3.8	14	j o	į
J	Н	2912.7	L	526877	5401331	71.5	22.1	23.5	11.0	41.4	41.9	11.3	0	j o	į
X	İI	2908.5	S	526875	5401447	28.0	11.5	11.9	69.0	27.1	5.6	i		10	į
LINE   30130   FLIGHT   12	jЈ	2895.0	L	526877	5401874	23.1	19.3	150.8	244.2	8.1	46.4	2.1	0	0	į
M   2867.4   H   526913   5402655   1.3   4.0   69.2   9.3   17.4   24.2       0	K	2893.8	S	526881	5401912	4.3	10.4	150.8	244.2	8.1	46.4	0.4	0	j o	į
LINE   30110	Ĺ	2875.9	L	526907	5402408	47.9	31.1	235.5	274.0	3.2	84.9	3.7	0	j o	į
A 2652.7 S 527095 5398275	M	2867.4	H	526913	5402655	1.3	4.0	69.2	9.3	17.4	24.2			0	j
A 2652.7 S 527095 5398275	LINE	30110		FLIGHT	12	 						 			
C	A	2652.7	S	527095	5398275	4.8	5.1	10.2	59.8	0.4	8.4	0.9	32	0	į
D   2704, 8   H   527094   5399939   5.3   1.6   111.2   8.1   27.9   45.7       0	В	2658.7	B?	527093	5398460	0.5	1.6	13.1	1.1	5.8	3.9			81	į
E   2734.2   L   527117   5400882   8.9   3.1   27.4   34.9   14.4   2.0   4.7   5   0	ĺС	2668.6	S	527101	5398800	10.3	18.0	108.1	185.2	2.2	32.8	0.7	0	37	į
F 2746.6 L 527120 5401274   7.6 18.2 16.7 0.7 18.7 60.1   0.5 0   0   0   0   2755.1   S 527125 5401553   2.3 10.9 0.2 37.9 13.3 7.8   0   0   0   0   0   0   0   0	D	2704.8	H	527094	5399939	5.3	1.6	111.2	8.1	27.9	45.7	i		j o	į
G 2755.1 S 527125 5401553   2.3 10.9 0.2 37.9 13.3 7.8	E	2734.2	L	527117	5400882	8.9	3.1	27.4	34.9	14.4	2.0	4.7	5	j o	į
H	F	2746.6	L	527120	5401274	7.6	18.2	16.7	0.7	18.7	60.1	0.5	0	j o	į
T	G	2755.1	S	527125	5401553	2.3	10.9	0.2	37.9	13.3	7.8	i		j o	į
J 2784.0   L 527107 5402407   18.7 9.7 5.1 18.2 0.9 3.9   3.5 7   0     K 2795.0   H 527106 5402676   15.0 14.8 328.3 319.6 21.8 87.1   1.5 16   0     LINE 30120	н	2763.0	L	527115	5401815	17.2	25.6	58.8	164.6	2.6	28.8	1.0	0	j o	į
K   2795.0   H   527106   5402676   15.0   14.8   328.3   319.6   21.8   87.1   1.5   16   0	İΙ	2764.7	S	527112	5401873	3.5	3.9	58.8	164.6	4.2	28.8	0.8	34	0	į
LINE 30120   FLIGHT 12	jЈ	2784.0	L	527107	5402407	18.7	9.7	5.1	18.2	0.9	3.9	3.5	7	0	į
A	K	2795.0	H	527106	5402676	15.0	14.8	328.3	319.6	21.8	87.1	1.5	16	0	j
B   2529.6   S?   527300   5398502   0.5   9.0   9.2   43.9   2.4   7.6       0     C   2520.2   S   527285   5398843   8.0   16.5   220.3   257.0   8.0   60.5   0.6   3   0     D   2510.8   S   527295   5399187   0.4   1.6   6.1   18.1   7.9   2.4       0     E   2505.6   S   527298   5399357   5.6   0.6   81.9   24.4   34.6   4.5       0     F   2486.0   H   527306   5400032   7.4   8.5   128.4   37.0   16.8   46.7   1.0   34   57     G   2460.6   L   527287   5400793   0.0   8.4   123.9   174.5   33.1   42.5       0     H   2452.1   S   527298   5401052   4.3   4.8   23.1   94.0   13.0   27.9       0     I   2443.6   L   527301   5401315   0.8   46.0   12.6   5.3   4.8   40.9       268     J   2430.0   L   527299   5401803   8.1   13.4   17.5   68.9   6.8   9.9   0.7   0   0     K   2406.9   L   527312   5402514   71.9   58.9   476.7   497.4   45.2   159.0   3.1   0   0     L   2399.3   S   527296   5402709   22.8   35.1   514.4   491.6   27.6   163.5   1.1   6   0      LINE   30130   FLIGHT   12	LINE	30120		FLIGHT	12	 						 			
C   2520.2   S   527285   5398843	A	2543.1	S	527291	5398029	2.3	3.4	2.8	24.3	1.8	3.3			0	į
D   2510.8   S   527295   5399187   0.4   1.6   6.1   18.1   7.9   2.4       0    E   2505.6   S   527298   5399357   5.6   0.6   81.9   24.4   34.6   4.5       0    F   2486.0   H   527306   5400032   7.4   8.5   128.4   37.0   16.8   46.7   1.0   34   57    G   2460.6   L   527287   5400793   0.0   8.4   123.9   174.5   33.1   42.5       0    H   2452.1   S   527298   5401052   4.3   4.8   23.1   94.0   13.0   27.9       0    I   2443.6   L   527301   5401315   0.8   46.0   12.6   5.3   4.8   40.9       268    J   2430.0   L   527299   5401803   8.1   13.4   17.5   68.9   6.8   9.9   0.7   0   0    K   2406.9   L   527312   5402514   71.9   58.9   476.7   497.4   45.2   159.0   3.1   0   0    L   2399.3   S   527296   5402709   22.8   35.1   514.4   491.6   27.6   163.5   1.1   6   0     LINE   30130   FLIGHT   12	В	2529.6	S?	527300	5398502	0.5	9.0	9.2	43.9	2.4	7.6			0	į
E 2505.6 S 527298 5399357   5.6 0.6 81.9 24.4 34.6 4.5     0   F 2486.0 H 527306 5400032   7.4 8.5 128.4 37.0 16.8 46.7   1.0 34   57   G 2460.6 L 527287 5400793   0.0 8.4 123.9 174.5 33.1 42.5     0   H 2452.1 S 527298 5401052   4.3 4.8 23.1 94.0 13.0 27.9     0   I 2443.6 L 527301 5401315   0.8 46.0 12.6 5.3 4.8 40.9     268   J 2430.0 L 527299 5401803   8.1 13.4 17.5 68.9 6.8 9.9   0.7 0   0   K 2406.9 L 527312 5402514   71.9 58.9 476.7 497.4 45.2 159.0   3.1 0   0   L 2399.3 S 527296 5402709   22.8 35.1 514.4 491.6 27.6 163.5   1.1 6   0	C	2520.2	S	527285	5398843	8.0	16.5	220.3	257.0	8.0	60.5	0.6	3	0	į
F	D	2510.8	S	527295	5399187	0.4	1.6	6.1	18.1	7.9	2.4			0	j
G 2460.6 L 527287 5400793   0.0 8.4 123.9 174.5 33.1 42.5     0     H 2452.1 S 527298 5401052   4.3 4.8 23.1 94.0 13.0 27.9     0     I 2443.6 L 527301 5401315   0.8 46.0 12.6 5.3 4.8 40.9     268     J 2430.0 L 527299 5401803   8.1 13.4 17.5 68.9 6.8 9.9   0.7 0   0     K 2406.9 L 527312 5402514   71.9 58.9 476.7 497.4 45.2 159.0   3.1 0   0     L 2399.3 S 527296 5402709   22.8 35.1 514.4 491.6 27.6 163.5   1.1 6   0     LINE 30130   FLIGHT 12	E	2505.6	S	527298	5399357	5.6	0.6	81.9	24.4	34.6				0	j
H 2452.1 S 527298 5401052   4.3 4.8 23.1 94.0 13.0 27.9     0   1 2443.6 L 527301 5401315   0.8 46.0 12.6 5.3 4.8 40.9     268   J 2430.0 L 527299 5401803   8.1 13.4 17.5 68.9 6.8 9.9   0.7 0   0   K 2406.9 L 527312 5402514   71.9 58.9 476.7 497.4 45.2 159.0   3.1 0   0   L 2399.3 S 527296 5402709   22.8 35.1 514.4 491.6 27.6 163.5   1.1 6   0   L LINE 30130   FLIGHT 12	F	2486.0	H	527306	5400032	7.4	8.5	128.4	37.0	16.8	46.7	1.0	34	57	j
I 2443.6 L 527301 5401315   0.8 46.0 12.6 5.3 4.8 40.9     268   J 2430.0 L 527299 5401803   8.1 13.4 17.5 68.9 6.8 9.9   0.7 0   0   0   K 2406.9 L 527312 5402514   71.9 58.9 476.7 497.4 45.2 159.0   3.1 0   0   0   L 2399.3 S 527296 5402709   22.8 35.1 514.4 491.6 27.6 163.5   1.1 6   0   C   C   C   C   C   C   C   C   C	G	2460.6	L	527287	5400793	0.0	8.4	123.9	174.5	33.1	42.5			0	į
J       2430.0       L       527299       5401803       8.1       13.4       17.5       68.9       6.8       9.9       0.7       0       0         K       2406.9       L       527312       5402514       71.9       58.9       476.7       497.4       45.2       159.0       3.1       0       0         L       2399.3       S       527296       5402709       22.8       35.1       514.4       491.6       27.6       163.5       1.1       6       0         LINE       30130       FLIGHT       12	H	2452.1	S	527298	5401052	4.3	4.8	23.1	94.0	13.0	27.9			0	j
K 2406.9 L 527312 5402514   71.9 58.9 476.7 497.4 45.2 159.0   3.1 0   0   L 2399.3 S 527296 5402709   22.8 35.1 514.4 491.6 27.6 163.5   1.1 6   0   LINE 30130   FLIGHT 12	I	2443.6	L	527301	5401315	0.8	46.0	12.6	5.3	4.8	40.9			268	j
L 2399.3 S 527296 5402709   22.8 35.1 514.4 491.6 27.6 163.5   1.1 6   0 LINE 30130 FLIGHT 12	J	2430.0	L	527299	5401803	8.1	13.4	17.5	68.9	6.8	9.9	0.7	0	0	j
LINE 30130	K	2406.9	L	527312	5402514	71.9	58.9	476.7	497.4	45.2	159.0	3.1	0	0	j
	L	2399.3	S	527296	5402709	22.8	35.1	514.4	491.6	27.6	163.5	1.1	6	0	İ
	LINE	30130		FLIGHT	12	 						 			
A 2100.9 5 52/472 50.5/10   0.9 20.4 50.9 19/.0 2.5 20.3     8	A	2168.9	S	527492	5397926	0.9	20.4	30.9	197.0	2.5	26.3			8	į

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

  Labe	 l Fid	Inter	o XUTM	YUTM	   CX 55   Real	 00 HZ Quad	CP 7	200 HZ Quad	CP Real	900 HZ Quad	   Vertica   COND	 l Dike DEPTH*	   Mag. Corr 	   
İ			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	j
LINE	30130		FLIGHT	12	 						 		 	 
В	2173.2	S	527496	5398070	1.9	37.4	20.1	264.4	0.6	35.8	j		0	į
C	2186.0	В	527490	5398496	1.8	2.1	16.6	14.0	9.3	6.1	j		66	j
D	2190.3	В	527502	5398644	5.7	3.9	35.2	21.6	25.4	12.1	j		52	j
E	2207.2	S	527522	5399248	16.2	26.7	214.8	350.7	7.2	68.0	0.9	0	0	j
F	2226.6	H	527520	5399999	9.6	13.5	130.9	126.6	10.0	33.2	0.9	15	51	j
G	2271.3	L	527520	5401238	24.3	8.1	11.4	10.5	53.6	54.9			0	
H	2289.4	L	527498	5401774	16.5	12.6	10.4	36.6	7.1	10.5	2.1	8	0	1
I	2322.7	Н	527525	5402688	27.9	25.5	539.0	524.5	36.6	176.9	2.0	9	0	
LINE	30140		FLIGHT	12	 						 		 	 
İΑ	2066.0	S?	527691	5397994	4.1	31.5	38.6	195.9	0.8	27.1	i		6	İ
В	2044.4	B?	527704	5398702	4.9	21.8	53.1	173.5	2.1	25.7	0.3	0	22	i
ĺС	2029.6	H	527690	5399232	5.6	6.6	149.0	124.2	4.2	33.6	0.9	18	0	İ
D	2010.9	S?	527695	5399840	6.5	18.1	81.9	310.5	30.7	45.1	0.4	4	0	į
E	1999.7	S	527699	5400204	9.2	2.3	170.6	332.8	14.2	54.3	j		0	į
F	1982.0	L	527696	5400655	0.2	2.0	16.0	3.3	8.8	5.5	j		0	j
G	1976.1	L	527683	5400820	2.3	2.6	36.2	54.5	16.2	20.5	j		0	j
Н	1963.9	L	527682	5401231	19.7	12.2	35.9	59.3	84.6	28.3	2.9	0	0	j
I	1950.4	L	527692	5401713	8.5	0.0	14.2	19.8	11.0	9.0	i		0	ĺ
J	1933.0	L	527701	5402272	8.4	5.1	20.3	21.7	4.8	6.4	2.2	20	0	ĺ
K	1918.6	Н	527689	5402672	52.3	59.0	747.1	711.2	53.3	269.2	2.0	6	0	İ
LINE	30150		FLIGHT	12	 						 		 	l
A	1736.9	S	527897	5398784	4.5	7.2	39.7	148.7	3.6	21.5	i		0	i
В	1756.9	S	527903	5399500	0.2	2.2	92.4	109.1	3.5	23.8	i		0	İ
ĺС	1762.2	S	527903	5399699	6.6	5.5	51.7	65.0	4.4	13.5	1.4	33	0	į
D	1770.3	S	527902	5400001	4.3	14.0	35.9	125.3	31.9	18.2	0.3	0	0	į
E	1780.3	S	527902	5400390	5.7	13.5	55.7	239.6	38.7	30.7	0.5	8	303	į
F	1794.0	L	527902	5400861	0.3	0.0	10.1	5.1	21.7	10.1	j		59	į
G	1804.1	L	527895	5401217	2.6	1.9	17.5	14.5	20.9	21.6	j		j 0	į
Н	1837.4	L	527924	5402273	8.2	4.9	15.5	13.7	3.5	5.7	j		j o	į
Ι	1851.7	Н	527931	5402726	15.7	22.2	420.5	232.7	45.9	140.4	1.0	10	j o	İ
LINE	30160		FLIGHT	12	 						 		 	 
A	1477.1	Н	528085	5399529	5.6	8.6	98.5	23.3	7.4	26.0	0.7	19	7	
B	1461.8	S	528075	5400107	30.3	50.1	232.8	327.3	20.2	72.0	1.1	0	0	
l C	1454.2	S	528075	5400382	7.5	14.6	36.9	47.9	33.2	4.2			0	
l D	1443.1	L	528083	5400741	62.3		103.6	52.4	63.5	25.7	14.7	2	0	
											· ·		·	ا 

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

Line   Fid						   CX 55	 00 HZ	7	200 HZ	CP	900 HZ	   Vertica	 l Dike	Mag. Corr	 
LINE 30160	Labe	l Fid	Interp	XUTM	YUTM	Real	Quad	Real	Quad	Real	Quad	COND :	DEPTH*		ĺ
E 1432.4 L 528088 5401082 0.0 32.0 46.7 0.5 39.7 25.2 174 F 1426.5 L 528081 5401207 42.5 42.8 114.9 154.2 30.3 32.6 2.1 0 0 G 1425.7 L 528097 5401200 4.7 18.5 114.9 154.2 15.4 32.6 0.3 0 0 H 1415.1 L 528081 5401649 13.2 11.3 37.9 39.8 6.3 10.8 1.7 3 0 H 1399.3 L 528087 5402100 3.6 10.5 19.7 13.4 23.1 2.8 0 J 1391.3 L 528087 5402109 17.5 9.7 22.7 21.2 15.1 5.5 3.2 14 67 K 1371.2 H 528085 5402219 17.5 9.7 22.7 21.2 15.1 5.5 3.2 14 67 K 1371.2 H 528085 5402814 16.1 15.5 84.7 39.7 27.2 55.7 1.6 21 0    LINE 30170 FLIGHT 12				m	m	ppm	ppm	ppm	ppm	ppm	ı ppm	siemens	m	NT	
F   1428.5   L   528081   5401207   42.5   42.8   114.9   154.2   30.3   32.6   2.1   0   0   0   0   0   0   0   0   0	LINE	30160		FLIGHT	12	 						 			
C   1425.7   L   528079   5401300   4.7   18.5   114.9   154.2   15.4   32.6   0.3   0   0     H   1415.1   L   528081   5401649   13.2   11.3   37.9   39.8   6.3   10.8   1.7   3   0     I   1399.3   L   528089   5402299   17.5   9.7   22.7   21.2   15.1   5.5   3.2   14   67     K   1371.2   H   528085   5402289   17.5   9.7   22.7   21.2   15.1   5.5   3.2   14   67     K   1371.2   H   528085   5402814   16.1   15.5   84.7   39.7   27.2   52.7   1.6   21   0      LINE   30170	E	1432.4	L	528088	5401082	0.0	32.0	46.7	0.5	39.7	25.2			174	į
H   1415.1	F	1428.5	L	528081	5401207	42.5	42.8	114.9	154.2	30.3	32.6	2.1	0	j o	į
I	G	1425.7	L	528079	5401300	4.7	18.5	114.9	154.2	15.4	32.6	0.3	0	j o	į
J   1391   3	Н	1415.1	L	528081	5401649	13.2	11.3	37.9	39.8	6.3	10.8	1.7	3	0	į
K   1371.2   H   528085   5402814   16.1   15.5   84.7   39.7   27.2   52.7   1.6   21   0	I	1399.3	L	528087	5402100	3.6	10.5	19.7	13.4	23.1	2.8			0	İ
LINE 30170	J	1391.3	L	528089	5402299	17.5	9.7	22.7	21.2	15.1	5.5	3.2	14	67	ĺ
A   1183.6   S   528303   5397962   5.1   3.8   62.9   172.2   0.2   25.8     0     B   1223.2   S?   528312   5399432   0.9   4.2   49.5   132.6   2.1   18.8     12     C   1236.3   S   528302   53999933   4.0   4.9   161.6   133.2   5.8   41.8   0.8   29   0     D   1252.9   S   528288   5400566   2.8   7.2   3.4   29.4   0.7   12.1     488     E   1256.6   L   528286   5400704   35.8   10.1   53.1   4.0   53.1   21.4   10.2   6   0     F   1264.1   S   528283   5400991   4.6   9.8   27.1   131.4   4.2   17.9   0.5   11   24     G   1267.9   L   528285   5401136   51.3   14.4   153.3   161.3   23.1   55.0   11.6   0   133     H   1283.0   S   528297   5401678   3.7   6.3   30.1   59.1   11.8   10.8     39     I   1300.5   L   528286   5402294   14.2   4.4   11.0   8.4   3.7   5.8     0     J   1311.5   H   528321   5402687   15.9   14.3   263.8   174.0   34.0   100.3   1.7   17   7      LINE   30180   FLIGHT   12	K	1371.2	H	528085	5402814	16.1	15.5	84.7	39.7	27.2	52.7	1.6	21	0	İ
B   1223.2   S?   528312   5399432   0.9   4.2   49.5   132.6   2.1   18.8     12   12   125.6   S   528288   5400566   2.8   7.2   3.4   29.4   0.7   12.1     488   E   1256.6   L   528286   5400704   35.8   10.1   53.1   4.0   53.1   21.4   10.2   6   0   0   0   0   0   0   0   0   0	LINE	30170		FLIGHT	12	 						 			I
B   1223.2   S?   528312   5399432   0.9   4.2   49.5   132.6   2.1   18.8     12   12   125.6   S   528288   5400566   2.8   7.2   3.4   29.4   0.7   12.1     488   E   1256.6   L   528286   5400704   35.8   10.1   53.1   4.0   53.1   21.4   10.2   6   0   0   0   0   0   0   0   0   0	A	1183.6	S	528303	5397962	5.1	3.8	62.9	172.2	0.2	25.8			0	j
D	В	1223.2	S?	528312	5399432	0.9	4.2	49.5	132.6	2.1	18.8			12	į
E   1256.6   L   528286   5400704   35.8   10.1   53.1   4.0   53.1   21.4   10.2   6   0	C	1236.3	S	528302	5399933	4.0	4.9	161.6	133.2	5.8	41.8	0.8	29	j o	į
F   1264.1   S   528283   5400991	D	1252.9	S	528288	5400566	2.8	7.2	3.4	29.4	0.7	12.1	i		488	į
C	E	1256.6	L	528286	5400704	35.8	10.1	53.1	4.0	53.1	21.4	10.2	6	j o	į
H	F	1264.1	S	528283	5400991	4.6	9.8	27.1	131.4	4.2	17.9	0.5	11	24	į
I	G	1267.9	L	528285	5401136	51.3	14.4	153.3	161.3	23.1	55.0	11.6	0	133	į
J   1311.5   H   528321   5402687   15.9   14.3   263.8   174.0   34.0   100.3   1.7   17   0   1   1   1   1   1   1   1   1   1	Н	1283.0	S	528297	5401678	3.7	6.3	30.1	59.1	11.8	10.8	i		j 39	į
LINE 30180   FLIGHT 12	İI	1300.5	L	528296	5402294	14.2	4.4	11.0	8.4	3.7	5.8	i		j o	į
A	jЈ	1311.5	H	528321	5402687	15.9	14.3	263.8	174.0	34.0	100.3	1.7	17	0	j
A	LINE	30180		FLIGHT	12	 						 			
C			S	528508	5397710	1.8	7.3	90.9	152.5	7.6	26.9			j o	į
D	В		S	528497		5.1	20.5	80.6	140.6	2.3	24.2	0.3	0	j o	İ
E	C	1075.3	S	528503	5399076	1.9	1.9	0.5	18.9	1.0	2.6	i		j o	į
F	D	1061.9	S?	528487	5399599	1.2	9.8	4.5	22.6	4.7	3.8	i		j o	į
G	E	1051.3	S	528481	5400025	13.4	9.4	114.1	193.6	3.4	35.4	2.2	10	29	İ
H	F	1040.0	S	528475	5400458	3.2	6.0	13.3	25.4	19.9	10.7	i		0	į
I	G	1034.0	L	528479	5400669	43.3	28.7	107.0	192.7	44.1	35.0	3.4	3	0	ĺ
J	H	1021.9	L	528496	5401080	35.6	15.5	50.2	27.1	24.2	64.8	5.6	0	0	ĺ
K 1006.1 L 528482 5401619   0.0 0.0 100.3 77.3 26.6 34.9     0   L 991.5 S 528487 5402087   0.1 10.8 29.2 108.2 7.6 15.8     42   M 986.8 L 528487 5402229   23.4 12.0 16.5 7.1 4.3 5.9   3.9 14   0   N 975.0 H 528495 5402574   22.1 26.8 573.6 545.2 45.4 188.3   1.4 9   0   LINE 30190   FLIGHT 12	Ι	1016.3	S	528493	5401266	8.6	21.6	234.1	327.2	23.4	66.0	0.5	1	0	į
L 991.5 S 528487 5402087   0.1 10.8 29.2 108.2 7.6 15.8     42	J	1008.0	L	528484	5401556	45.0	20.2	100.3	77.3	26.6	34.9	5.8	5	0	ĺ
M 986.8 L 528487 5402229   23.4 12.0 16.5 7.1 4.3 5.9   3.9 14   0   N 975.0 H 528495 5402574   22.1 26.8 573.6 545.2 45.4 188.3   1.4 9   0   LINE 30190   FLIGHT 12	K	1006.1	L	528482	5401619	0.0	0.0	100.3	77.3	26.6	34.9			0	į
N 975.0 H 528495 5402574   22.1 26.8 573.6 545.2 45.4 188.3   1.4 9   0 	L	991.5	S	528487	5402087	0.1	10.8	29.2	108.2	7.6	15.8			42	į
LINE 30190 FLIGHT 12	M	986.8	L	528487	5402229	23.4	12.0	16.5	7.1	4.3	5.9	3.9	14	0	ĺ
	N	975.0	Н	528495	5402574	22.1	26.8	573.6	545.2	45.4	188.3	1.4	9	0	İ
	LINE	30190		FLIGHT	12	 						 			
			Н			4.9	7.7	42.0	43.7	3.8	13.8	0.6	21	27	İ

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					   CX 55	00 HZ	CP 7	200 HZ	CP	900 HZ	   Vertica	 l Dike	Mag. Corr	 
Labe	l Fid	Interp	NTUX c	YUTM	Real	Quad	Real	Quad	Real	Quad	COND	DEPTH*		į
j		-	m	m	ppm	ppm	ppm	ppm	ppm		siemens	m	NT	į
LINE	30190		FLIGHT	12	 						 		 	 
Ϊв	788.2	S	528680	5399516	1.6	12.9	10.5	133.6	12.4	18.5	i		247	i
lc	797.6	S	528672	5399870	6.8	15.5	36.4	93.4	5.7	12.9	i		0	i
D	805.6	S	528683	5400172	9.7	8.2	147.1	257.3	4.6	45.9	1.6	15	0	i
E	819.0	L	528707	5400619	34.9	20.3	131.4		44.7	55.4	3.8	0	0	i
F	831.6	L	528711	5401030	28.7	0.6	3.7	0.0	42.4	31.6			872	i
İG	839.4	S	528728	5401270	21.1		152.5	246.3	17.5	40.8	6.4	18	0	i
Н	845.8	S	528735	5401470	1.0	6.7	19.1	85.8	0.5	13.1			67	i
İı	849.3	L	528730	5401580	14.9	10.5	19.1	25.2	4.0	7.3			0	i
jл	859.7	S	528696	5401903	0.0	3.0	97.7	80.2	8.0	26.3			137	i
K	868.5	L	528653	5402182	2.5	10.5	45.0	137.1	18.6	23.0			0	i
L	883.3	Н	528657	5402712	12.5	9.6	114.4	97.9	21.5	39.9	1.9	19	0	j
LINE	30200		FLIGHT	12	 						 		 	 
A	654.0	S	528902	5398373	4.3	7.7	129.6	140.9	3.4	36.4	0.5	26	0	i
В	641.1	S	528907	5398836	2.7	12.6	32.0	136.4	3.3	19.7	j		0	į
İc	622.2	S?	528897	5399555	1.1	12.2	2.7	9.6	3.0	2.3	i		26	i
D	613.8	S	528897	5399873	5.2	13.1		244.4	5.5	55.4	0.4	0	0	i
E	604.3	S	528892	5400227	10.3	29.6	199.3	344.0	23.7	65.5	0.5	0	0	į
F	592.0	L	528869	5400634	57.9	17.7	170.1	170.4	49.4	66.7	10.6	1	j o	į
G	579.6	L	528881	5400988	14.5	3.1	36.5	48.3	31.9	24.3	11.4	5	718	į
Н	571.8	S	528891	5401260	8.1	13.0	130.2	271.3	14.6	44.2	0.7	8	j o	į
Ī	564.3	L	528883	5401540	18.1	16.3	14.3	17.5	6.8	5.1	j		j o	į
J	552.9	S	528889	5401947	4.2	10.8	171.4	245.1	7.4	47.7	0.4	0	225	į
K	544.1	L	528892	5402248	14.7	9.9	15.4	18.2	3.5	3.9	2.3	2	0	j
ļL	527.1	H	528892	5402840	7.9	8.5	55.0	48.7	14.2	18.9	1.1	18	j o	j
LINE	30210		FLIGHT	11	 						 		 	 
A	2712.1	S	529105	5397857	2.7	6.7	16.0	54.3	1.8	8.0	j		0	j
В	2728.1	S	529080	5398379	6.6	20.4	167.1	255.9	5.3	48.6	0.4	0	0	j
c	2747.7	S	529102	5399037	2.9	8.0	19.4	54.6	1.8	8.1	j		0	j
D	2761.6	S	529122	5399504	0.6	2.5	3.8	37.1	1.2	6.5	i		28	į
E	2773.8	S	529107	5399942	16.8	32.8	147.4	187.5	6.8	40.2	0.8	0	0	j
F	2781.6	S	529096	5400215	3.0	4.0	54.4	106.3	16.6	24.3	j		0	j
G	2793.3	L	529110	5400604	33.0	18.1	66.5	172.1	14.7	30.6	4.0	3	0	j
Н	2803.2	L	529095	5400922	18.6	7.9	29.5	18.5	121.8	281.0	4.6	5	180	į
İI	2813.9	S	529089	5401249	5.2	11.2		338.2	57.1	75.9	0.5	12	0	j
J	2821.7	L	529086	5401494	24.9	20.4	28.2	49.6	10.2	14.6	2.2	7	0	į
K	2832.7	S	529123	5401851	3.9	4.1	10.2	38.6	4.8	8.6	j		0	j

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					   CX 55	00 HZ	CP 7	 200 HZ	CP	900 HZ	   Vertical	 l Dike	   Mag. Corr	l
Labe	l Fid	Interp	XUTM	YUTM	Real	Quad	Real	Quad	Real	Quad	COND 1	DEPTH*		į
İ			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	j
LINE	30210		FLIGHT	11	 						 		 	
İъ	2838.0	S?	529109	5402019	3.3	6.6	24.4	43.0	7.6	9.6	0.4	8	j o	į
М	2845.7	L	529043	5402237	12.2	4.4	11.7	6.0	3.5	3.4	5.0	4	j o	į
N	2852.9	S	529067	5402454	3.5	5.5	33.1	90.6	1.8	12.1	i		j o	į
0	2863.7		529090	5402807	22.2		433.8		20.6	127.5	1.4	8	0	j
LINE	30220		FLIGHT	11	 						 		 	l
A	2618.5	S	529311	5397764	2.6	11.7	159.6	260.5	2.4	50.4	i		46	į
В	2603.9		529293	5398340	5.6	10.3	98.2	107.2	4.2	23.3	0.6	16	0	į
İc	2579.9	S	529283	5399253	1.9	4.1	33.3	91.7	4.4	13.5	i		56	į
D	2560.8	S	529278	5399944	0.9	2.6	81.8	99.1	10.1	21.8	i		j o	į
İΕ	2541.2		529303	5400593	34.3	26.2	59.8	307.7	73.1	59.3	2.7	8	j o	į
F	2536.4	L	529309	5400734	10.1	21.0	155.6	307.7	66.0	214.4	0.6	0	j o	į
Ġ	2530.2		529316	5400911	32.2	14.5	0.0	0.0	70.5	172.6	5.2	0	292	į
н	2521.4		529295	5401210	13.9	34.4	280.5	406.3	19.3	79.2	0.6	0	j o	į
İı	2514.0	L	529291	5401447	29.8	42.6	10.2	192.3	15.2	28.4	1.3	0	36	į
jЈ	2495.8	S?	529283	5402002	3.3	5.5	10.9	26.8	4.7	4.5	i		j o	į
K	2491.5		529277	5402133	7.2	11.0	23.8	54.5	6.2	8.1	0.7	8	0	į
L	2469.8	S	529311	5402789	12.9	45.6	415.0	604.4		123.6	0.4	0	12	İ
LINE	30230		FLIGHT	11	 						 		 	l
İΑ	2238.3	S	529503	5397730	6.6	8.3	97.8	162.5	0.8	28.8	i 0.9	9	j o	į
Ιв	2253.4		529517	5398194	9.7	15.7	172.0	221.8	4.3	49.3	0.8	0	26	į
İc	2266.3		529502	5398628	2.6	8.9	74.7	161.6	3.0	24.5			0	į
D	2306.3		529514	5400085	11.9	16.7	178.2	188.2	11.0	50.2	0.9	1	j o	į
İΕ	2319.4	L	529502	5400557	0.7	10.9	57.9	97.8	37.1	75.9	i		j o	i
F	2325.9	L	529505	5400764	31.7	5.8	88.9	132.8	109.6	131.1	18.6	0	38	į
Ġ	2337.0	S	529510	5401075	14.3	29.0	249.5	347.6	26.6	86.7	0.7	0	j o	į
Н	2348.0		529506	5401424	19.0	22.2	54.7	185.4	9.4	17.2	1.3	6	14	į
İI	2350.4	S	529508	5401503	9.8	24.8	84.3	140.3	5.5	27.7	0.5	0	0	i
J	2372.1	S	529502	5402255	0.0	7.9	35.9	114.4	2.8	17.0	i		68	i
K	2392.2	S	529507	5402802	12.1	28.9	259.8	314.9	4.3	73.2	0.6	0	j 0	İ
LINE	30240		FLIGHT	11	 						 		 	
A	2163.0	S	529703	5397713	2.3	10.5	176.3	246.2	6.6	50.4	i		0	i
В	2145.3		529703	5398386	10.7	14.8	51.4	166.2	1.0	24.9	0.9	6	0	i
İc	2134.7		529697	5398788	6.0	7.3	43.7	65.7	1.8	14.7	0.9	16	0	i
D	2111.4		529693	5399712	0.6	5.5	22.1	98.5	5.0	14.9			0	
E	2099.4	S	529699	5400153	2.2		153.3		35.2	49.2			0	

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

  Labe	l Fid	Interp	XUTM	YUTM	   CX 55   Real	00 HZ Quad	CP 7	200 HZ Quad	CP Real	900 HZ Quad	   Vertica   COND	 l Dike DEPTH*	   Mag. Corr 	   
İ			m	m	ppm	ppm	ppm	ppm	ppm	ı ppm	siemens	m	NT	İ
LINE	30240		FLIGHT	11	 						 		 	 
F	2088.9	L	529692	5400512	55.5	31.2	179.4	365.0	59.2	66.2	4.6	2	j o	į
Ġ	2081.6	L	529691	5400741	46.2	1.0	35.4	15.3	123.6	107.4	j		j 0	j
Н	2073.8	S	529698	5401013	22.7	17.5	300.2	367.6	40.8	84.2	2.3	17	21	j
Ī	2066.7	S	529704	5401292	4.8	3.4	36.0	66.7	11.8	14.4	1.5	43	j 0	j
J	2064.0	L	529701	5401396	12.4	18.3	36.0	66.7	11.8	8.1	0.9	5	103	ĺ
K	2060.4	S	529698	5401530	6.7	16.3	115.7	277.4	15.4	42.5	0.5	0	0	ĺ
L	2038.7	S	529700	5402274	3.9	5.2	67.9	178.1	3.7	27.3	0.7	22	179	İ
M	2022.2	S	529680	5402777	7.8	17.7	311.9	324.1	10.5	91.2	0.5	0	5	İ
LINE	30250		FLIGHT	11	 						 		 	
A	1782.3	S	529910	5397970	1.8	1.2	7.9	34.8	1.6	4.4	i		j o	į
В	1796.5	S	529908	5398461	9.0	9.9	100.4	171.4	1.9	29.9	1.1	8	12	į
ĺС	1812.2	S	529909	5399008	0.9	8.0	45.8	96.7	2.6	15.7	i		j 0	į
D	1834.6	S	529901	5399793	7.6	18.7	49.0	174.8	6.4	23.4	0.5	0	60	į
E	1845.3	S	529897	5400175	1.7	10.5	115.1	219.1	24.7	38.7	j		j 0	j
F	1860.5	L	529892	5400640	34.7	3.9	181.0	58.2	119.3	334.1	39.6	2	0	į
G	1874.4	S	529912	5401071	30.8	50.8	176.6	333.8	19.1	53.5	1.1	0	0	İ
H	1885.0	S	529906	5401414	5.0	4.0	12.0	52.0	9.3	8.8	1.3	23	0	İ
I	1894.4	S	529893	5401732	2.7	3.9	6.3	12.0	7.2	3.1	i		0	ĺ
J	1904.8	S	529910	5402113	7.5	11.0	5.8	30.0	3.6	3.8	0.8	4	0	ĺ
K	1922.5	H	529899	5402790	13.4	22.4	364.9	282.7	20.3	118.8	0.8	1	16	İ
LINE	30260		FLIGHT	11	 						 		 	l
A	1686.5	S	530108	5398108	0.3	1.4	14.7	36.8	3.1	7.3	i		j o	i
В	1675.3	S	530112	5398584	6.8	6.9	77.9	173.0	3.6	25.8	1.1	21	15	į
C	1659.3	S	530107	5399285	4.1	9.1	11.6	77.0	2.8	9.4	0.4	12	j 7	į
D	1640.7	S	530103	5400087	3.9	3.1	53.7	101.0	47.2	34.3	1.2	44	j 0	į
E	1627.9	L	530104	5400640	17.0	2.3	54.1	24.3	135.2	91.8	j		0	į
F	1619.6	S	530093	5401006	14.4	6.2	102.6	143.9	42.7	32.0	4.2	14	0	İ
G	1612.0	L?	530097	5401340	14.6	12.8	13.3	27.4	7.9	9.4	1.7	5	0	į
Н	1601.5	S?	530096	5401758	3.5	8.2	86.2	182.9	3.5	28.5	0.4	3	0	į
İΙ	1594.9	S	530093	5402006	4.3	9.5	135.5	175.5	7.1	36.8	0.4	3	0	į
jЈ	1582.1	S	530104	5402428	6.3	15.6		339.3	7.3	52.1	0.5	2	j 0	į
K	1575.7	S	530120	5402657	2.7		154.6		13.0	32.8	i		0	j
LINE	30270		FLIGHT	11	 I						 		 	l
A	1261.2	S	530289	5398284	2.5	3.6	82.4	166.3	3.4	19.9	i		66	ľ
В	1278.5	S	530309	5398896	0.9	4.2		140.3	4.0	26.1	i		0	ł
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CX = COAXIAL

CP = COPLANAR

EM Anomaly List

    Labe	l Fid	Inter	P XUTM	YUTM m	   CX 55   Real   ppm	 00 HZ Quad ppm	CP 7 Real	200 HZ Quad ppm	CP Real	~	Vertica COND siemens	l Dike DEPTH* m	   Mag. Corr     NT	     
i i i i	30270		 FLIGHT	11							 I			 
C  TIME	1289.6	S	530301	5399308	4.4	11.0	83.4	203.5	2.8	30.3	0.4	3	1 6	-
l D	1306.9	S	530301	5399963	0.0	14.1	53.4	188.7	5.6	31.9	0.4 		11	ł
E	1324.0	L	530207	5400586	0.0	0.2	38.1	16.0	152.4	115.2	 		0	ł
F	1338.4	S	530312	5401082	13.6	20.8	43.4	88.8	9.5	10.8	0.9	0	0	ł
G	1343.9	L?	530311	5401032	11.9	11.8	13.2	39.9	31.8	5.8	1.4	5	0	ł
lн	1350.7	s.	530317	5401530	2.0	7.6	1.3	16.1	3.6	2.8			0	ł
II	1366.2	S	530317	5402154	8.2	11.7	254.5	319.7	7.0	75.6	0.8	12	0	ł
l J	1381.4	S	530313	5402712	8.9	9.7	202.6		21.7	76.4	1.1	21	0	
LINE	30280		FLIGHT	11										1
A	1145.9	S	530508	5398258	4.5	7.3	72.1	42.4	3.7	20.2	0.6	10	0	į
В	1130.4	S	530502	5398904	10.0	27.8	44.0	153.8	2.8	22.0	j		0	į
C	1121.1	S	530501	5399299	5.0	7.9	71.3	151.4	3.7	25.8	j		11	į
D	1099.8	L	530495	5400119	5.4	0.0	26.7	32.6	69.4	55.8			0	İ
E	1090.4	L	530498	5400461	25.4	0.0	13.5	25.0	169.8	142.0			0	İ
F	1072.2	S	530508	5401137	3.0	30.1	102.8	232.8	10.3	32.9			0	I
G	1069.5	L	530503	5401240	21.1	25.9	3.5	35.3	5.1	5.8	1.3	0	293	[
H	1059.6	S	530492	5401596	2.6	6.4	21.7	100.0	6.0	12.5			0	[
I	1048.5	S	530484	5401968	17.3	24.1	227.6	235.5	10.2	68.6	1.1	7	36	
J	1028.0	S?	530464	5402518	55.2		198.7	534.7	0.9	91.5	2.3	4	0	
K	1018.6	S	530466	5402775	42.2	61.8	489.1	491.8	24.8	168.4	1.4	0	27	
LINE	30290		FLIGHT	11	 						 		 	
A	785.1	S	530707	5397551	23.7	55.9	8.2	111.6	0.9	15.0	i		7	i
Ιв	791.2	S	530702	5397752	10.1	32.1		141.9	2.2	20.8	i		14	i
İc	807.5	S	530708	5398300	2.4	11.2	98.5	203.2	3.7	33.2	i		0	į
D	815.8	S	530716	5398620	4.6	23.2	3.7	87.7	1.7	11.1	i		33	i
E	831.3	S	530691	5399199	5.5	11.1	38.0	128.2	3.8	15.3	i		7	į
F	851.2	S	530699	5399952	6.7	12.0	94.1	180.6	40.5	38.6	j		0	į
G	864.7	L	530708	5400455	17.4	6.7	24.6	7.5	135.3	135.5	i		0	į
н	882.4	S	530691	5401060	12.5	6.7	65.9	134.6	17.6	22.6	i		0	į
I	888.0	L	530688	5401275	14.1	17.4	8.2	5.7	9.4	6.2	1.1	3	561	į
J	901.5	S	530700	5401801	3.1	9.5	37.4	91.5	1.2	13.3	i		0	į
K	909.9	S	530702	5402148	21.5	25.1	325.9	382.0	15.0	94.1	1.4	4	0	į
Ĺ	924.8	S	530705	5402702	39.5	51.0	396.9	316.8	26.8	132.1	1.5	0	0	j
	30300		 FLIGHT	11	 I						 I			 I
A   TINE	717.8	S	530897	5397706	8.9	52 7	158.2	205 /	5.8	54.3	I I		8	-
A	111.0	ు 			0.9 	JZ./	130.7	499.4 	J.0		ı		°	ا 

CX = COAXIAL

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EM Anomaly List

					   CX 55	 00 HZ	CP 7	200 HZ	CP	900 HZ	   Vertica	 l Dike	Mag. Corr	
Labe	l Fid	Interp	XUTM	YUTM	Real	Quad	Real	Ouad	Real	Quad	COND	DEPTH*	i	i
			m	m	ppm	ppm	ppm	ppm	ppm		siemens	m	NT	į
LINE	30300		FLIGHT	11										
В	705.7	S	530906	5398157	9.5	42.9	23.9	163.8	2.2	21.6			11	
C	681.4	S	530891	5399108	2.9	12.2	10.2	83.3	2.9	14.3			0	
D	668.2	S	530896	5399605	7.2	17.5	12.1	51.7	11.7	17.2			0	
E	656.7	$\mathbf{L}$	530893	5400024	10.0	0.0	68.1	264.8	47.2	90.2			383	
F	647.6	$\mathbf{L}$	530907	5400339	20.0	11.4	29.2	45.4	129.6	122.2			0	
G	639.5	S?	530889	5400641	0.0	14.0	5.3	3.9	24.4	12.3			0	
H	628.9	S	530907	5401072	11.3	21.5	53.1	140.7	4.2	19.1			0	
I	624.4	$\mathbf{L}$	530907	5401255	20.7	25.5	21.1	6.2	4.2	1.1			187	
J	611.6	S?	530903	5401763	9.4	17.3	1.0	19.9	3.7	3.3			98	
K	602.0	S	530890	5402132	2.9	11.6	51.0	100.5	3.0	19.1			0	
L	585.8	S	530898	5402662	32.1	27.8	440.6	341.1	34.1	145.8	2.2	2	0	
LINE	30310		FLIGHT	11	 						 			
A	332.1	S	531109	5397612	29.2	65.5	229.5	217.6	5.5	50.2	0.8	0	0	ĺ
В	355.8	S	531109	5398294	0.5	0.0	7.9	54.5	3.4	8.1			0	ĺ
C	391.1	S	531111	5399480	5.7	11.3	14.8	70.9	9.9	17.2			6	ĺ
D	401.0	L	531116	5399854	16.7	16.5	9.6	0.1	43.1	35.5	1.6	6	0	ĺ
E	408.5	S	531110	5400134	26.2	79.7	131.4	323.4	33.4	90.8	0.6	0	143	ĺ
F	414.7	L	531099	5400323	53.5	0.7	22.1	0.0	161.8	151.8			101	ĺ
G	422.9	S	531118	5400553	9.0	23.8	11.4	77.8	24.0	19.4			0	ĺ
H	440.5	S	531123	5401116	11.0	25.2	19.7	88.4	7.7	17.0			0	ĺ
ÌΙ	444.8	L	531112	5401261	30.1	49.7	12.1	17.6	2.4	3.2			78	ĺ
J	451.7	S	531091	5401498	6.0	15.1	7.6	36.9	4.9	6.7			0	ĺ
K	460.5	S	531078	5401808	11.8	27.8	22.3	69.3	3.0	11.1			96	
L	471.7	S	531093	5402223	22.9	33.4	19.0	54.0	2.3	6.2			408	
M	485.4	H	531107	5402754	75.1	83.3	418.9	292.9	37.6	150.0	2.2	0	0	
LINE	30320		FLIGHT	10	 						 			
A	6523.6	S	531306	5397865	3.0	13.4	116.0	273.1	0.5	42.0	0.2	0	0	į
В	6538.7	S	531318	5398393	0.2	13.0	19.8	131.7	0.4	19.1	j		12	j
C	6546.3	S	531313	5398665	1.6	8.8	6.7	83.6	0.7	10.8	j		0	į
D	6557.9	S	531309	5399076	1.2	5.5	9.6	62.8	5.4	8.7	j		0	į
E	6569.5		531298	5399508	4.3	14.8	31.0	174.5	12.9	27.6	0.3	5	0	į
F	6576.0	L	531303	5399762	14.7	14.5	18.3	35.2	59.9	21.9	1.5	19	0	į
G	6587.7	L	531316	5400220	26.8	14.3	62.8	55.9	187.3	152.9	3.9	0	0	į
Н	6598.5	S	531331	5400581	13.2	28.0	82.1	227.1	32.2	43.4	0.7	0	0	į
I	6623.6	S	531296	5401508	15.2	48.6	252.8	689.5	9.2	104.1	0.5	0	0	į
J	6637.5	S	531298	5402030	4.4	10.4	66.7	83.3	7.2	17.5	0.4	0	0	i
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CX = COAXIAL

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EM Anomaly List

					   CX 55	 00 нz		200 HZ	CP	900 HZ	   Vertica		Mag. Corr	
Labe	l Fid	Interp		YUTM	Real	Quad	Real	Quad	Real	-	!	DEPTH*	ļ	ļ
			m	m	ppm	ppm	ppm	ppm	ppm	n ppm	siemens	m	NT	
LINE	30320		FLIGHT	10	 						 			
K	6643.9	S	531302	5402288	5.9	9.3	73.3	170.8	0.0	27.8	0.7	7	393	ĺ
Ĺ	6655.1	S	531301	5402732	23.4	19.8	418.8	284.0	39.0	151.8	2.1	5	0	İ
LINE	30331		FLIGHT	12	 						 		 	 
A	240.0	S	531499	5397606	2.2	12.5	26.6	117.3	0.5	18.0	i		j 0	į
В	249.6	S	531492	5397928	8.7	17.9	124.2	381.3	2.9	57.9	0.6	8	22	į
ĺС	270.9	S	531504	5398643	0.5	8.1	1.6	54.8	0.3	8.0	j		17	į
D	276.6	S	531496	5398840	7.8	30.8	32.8	193.2	3.2	27.0	j		6	į
E	282.9	S	531501	5399060	5.9	17.9	82.1	211.3	1.2	32.0	0.4	3	205	į
F	299.5	L	531510	5399638	20.8	16.8	19.6	111.8	10.5	31.4	2.1	16	0	į
G	315.8	L	531503	5400175	13.1	8.6	13.2	23.7	57.9	75.5	2.3	0	0	į
Н	332.4	S	531503	5400625	9.7	21.3	151.9	315.4	6.4	51.6	0.6	4	0	į
İI	346.9	S	531500	5401081	4.9	11.4	36.0	188.8	9.6	27.1	j		0	į
jЈ	362.7	S	531503	5401557	5.7	35.6	43.8	245.3	2.4	34.4	j		0	į
K	383.7	S	531507	5402221	4.4	6.9	220.7	82.3	6.5	36.9	0.6	25	0	į
Ĺ	396.8	S	531502	5402702	13.9	8.3	294.9	115.2	39.0	87.9	2.7	20	j o	į
LINE	30340		FLIGHT	10	 						 		 	 
A	6099.3	S	531707	5397881	4.3	9.3	60.9	155.1	1.0	23.5	0.5	12	0	į
В	6110.1	S	531701	5398274	1.6	7.9	37.0	186.6	2.3	23.9	j		0	į
İc	6131.4	S	531706	5399047	1.3	8.1	97.4	163.2	6.5	30.2	i		j o	į
D	6147.0	L	531702	5399583	13.8	11.3	16.4	63.4	49.2	37.1	1.8	24	j o	į
E	6161.8	L	531718	5400072	4.8	7.7	5.8	10.8	191.7	182.7	0.6	9	52	į
F	6172.9	S	531731	5400459	0.1	2.1	32.7	239.3	7.2	16.5	j		0	į
G	6193.9	S	531714	5401243	8.6	4.8	48.8	128.1	16.2	19.6	2.5	36	120	į
Н	6202.8	S	531705	5401585	4.3	14.9	74.9	242.8	14.1	35.5	0.3	0	0	į
İI	6220.0	S	531708	5402242	32.0	25.4	378.3	428.2	15.2	115.1	2.5	6	j o	į
J	6230.0	S	531699	5402648	23.3	29.5	236.9	144.0	10.2	71.7	1.3	2	j o	j
LINE	30350		FLIGHT	10	 						 			 
A	6004.8	S?	531890	5397973	17.5	38.5	169.8	303.0	5.1	53.9	0.7	0	10	į
В	5995.2	S	531895	5398356	6.5	14.5	62.7	134.5	5.2	22.9	0.5	0	0	į
c	5975.4	S	531907	5399147	4.8	16.6	80.9	310.1	10.8	46.4	0.3	0	0	į
D	5967.7	L	531903	5399438	1.0	2.2	6.2	15.9	43.7	45.4			0	į
E	5949.5	L	531899	5400090	10.4	6.4	4.8	3.1	122.0	115.1	2.3	5	0	į
F	5938.6	S	531896	5400507	1.8	7.5	40.4	132.7	7.1	20.2	i		j o	į
G	5929.7	S	531893	5400854	4.7	12.6		172.8	2.1	22.5	0.4	12	240	į
Н	5917.7	L	531897	5401297	19.3	22.3	16.1	5.7	8.8	5.0	1.4	6	0	į
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EM Anomaly List

    Labe 	l Fid	Interp	XUTM m	YUTM m		00 HZ Quad ppm	CP 7 Real ppm	200 HZ Quad ppm	CP Real ppm	~	Vertica COND	l Dike DEPTH* m	Mag. Corr       NT	
LINE	30350		FLIGHT	10	1						I		I	1
I	5906.9	S	531893	5401707	7.6	19.2	185.4	376.1	8.0	62.3	0.5	0	0	i
J	5882.1	S	531902	5402530	7.7	14.5	95.7	207.1	4.8	23.5	0.6	11	0	i
K	5872.7	L	531912	5402825	14.8	16.4	160.3	73.7	17.7	62.1	1.3	8	0	j
LINE	30360		FLIGHT	10	 						 		 	 
A	5655.0	S	532101	5397793	1.2	1.9	3.5	21.1	4.0	3.1	i		0	į
В	5660.4	S	532097	5397964	1.4	2.3	4.8	17.5	2.5	2.3	j		11	į
C	5671.5	S	532093	5398324	4.7	10.0	145.3	282.8	7.0	45.3	0.5	9	46	İ
D	5700.3	S	532116	5399267	0.9	6.1	3.4	70.1	2.0	13.9			131	İ
E	5705.0	L	532117	5399431	23.6	13.5	17.0	19.6	31.5	57.3	3.4	19	0	
F	5721.5	L	532108	5400007	29.0	15.0	26.3	2.3	108.3	103.5	4.1	0	28	
G	5736.6	S	532115	5400530	0.6	2.0	14.3	49.4	3.7	10.5			0	
H	5751.6	S	532115	5401080	1.3	4.5	14.8	67.0	2.7	11.3			29	
I	5757.1	L	532117	5401292	17.8	14.4	11.0	0.0	8.0	2.0	2.0	7	0	
J	5764.5	S	532116	5401577	8.8	28.4	55.6	255.6	7.5	34.3	0.4	0	0	İ
K	5772.5	S	532097	5401872	2.0	12.0	5.1	55.7	1.7	7.2			0	
Ĺ	5795.1	H	532090	5402699	12.4	20.2	92.9	97.4	14.5	40.8	0.8	10	0	İ
LINE	30370		FLIGHT	10	 						 		 	
A	5572.1	S	532308	5397649	2.0	6.9	3.2	56.7	3.4	8.0	j		0	į
В	5553.4	S	532305	5398326	3.2	11.0	126.1	253.9	11.1	42.2	0.3	0	j o	j
İc	5535.0	S	532304	5399022	0.1	2.3	2.6	37.7	5.2	7.9	i		0	j
D	5524.0	L	532295	5399439	8.3	6.0	6.5	8.8	22.6	28.1	1.8	24	0	j
E	5510.8	L	532302	5399924	16.1	9.3	33.8	49.1	98.3	103.7	2.9	0	132	j
F	5491.9	S	532301	5400593	0.0	4.4	6.0	33.7	11.2	8.2	j		41	į
Ġ	5474.3	S	532312	5401194	0.7	13.9	31.2	159.5	5.5	25.8	i		64	į
H	5472.1	L	532309	5401270	22.4	26.0	31.2	159.5	5.5	25.8	1.4	5	0	į
Ī	5464.1	S	532322	5401545	6.4	20.1	15.0	115.9	2.0	15.9	0.4	0	0	į
J	5453.0	S	532299	5401917	3.4	0.9	6.0	29.3	3.2	4.0	j		0	į
ĺΚ	5436.4	H	532295	5402436	10.8	13.2	318.6	298.0	19.4	83.2	1.1	13	227	İ
LINE	30380		FLIGHT	10	 						 		 	 
A	5072.7	S	532494	5397903	1.3	10.4	6.7	79.8	2.9	10.5	j		0	j
В	5092.6	S	532497	5398566	3.9	32.2	144.2	362.8	1.7	55.6	0.1	0	0	j
c	5107.0	S	532497	5399060	3.0	10.8	51.1	230.3	3.5	35.0	i		0	j
D	5120.0	L	532504	5399518	18.0	21.4	22.7	38.6	38.9	51.8	1.3	3	15	j
E	5130.5	L	532494	5399876	19.9	14.3	16.8	14.9	159.8	156.2	2.4	0	0	į
F	5138.0	S	532505	5400099	2.4	2.3	4.5	30.8	9.7	8.6			0	į
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EM Anomaly List

  Labe	l Fid	Inter	p XUTM m	YUTM m		00 HZ Quad ppm	CP 7 Real	200 HZ Quad ppm	CP Real ppm	~	Vertica COND	 l Dike DEPTH* m	Mag. Corr       NT	
LINE	30380		FLIGHT	10	 						 I		 	
G	5170.7	L	532490	5401225	14.8	9.9	9.1	51.5	3.4	9.4	2.4	11	i o	i
Н	5182.8	S	532500	5401693	3.6	10.5	18.2	78.2	4.0	10.1	0.3	0	i o	i
ļΙ	5209.1	S	532497	5402713	19.0	26.7	541.9	464.1	41.7	169.7	1.1	8	j o	İ
LINE	30390		FLIGHT	10	 						 		 	
A	4963.1	S	532696	5398005	1.7	11.2	4.0	81.0	0.6	10.6	i		30	į
В	4947.5	S	532707	5398630	0.5	10.3	165.7	341.8	7.0	56.8	j		0	į
C	4929.2	S	532686	5399286	13.3	42.8	188.0	673.6	8.8	101.2	0.5	0	0	ĺ
D	4922.0	L	532690	5399546	22.3	12.8	8.6	0.0	48.5	28.7	3.3	15	0	ĺ
E	4913.3	L	532703	5399850	26.2	8.7	54.7	52.1	68.3	153.2	7.3	1	0	
F	4879.1	L	532690	5401170	12.0	11.1	10.6	25.6	1.0	4.6	1.5	7	0	
G	4872.3	S	532683	5401407	2.7	14.8	10.8	110.7	2.7	13.4			24	
H	4864.9	S	532677	5401676	8.5	31.4	94.2	313.6	2.0	43.0	0.4	0	0	
I	4855.7	S	532686	5402006	3.9	11.8	21.5	91.7	8.7	12.6			22	
J	4846.8	S?	532710	5402322	2.8	8.9	9.9	38.1	7.5	3.4			0	
K	4836.8	S	532705	5402677	17.5	10.2	534.5	396.2	47.0	183.6	3.0	25	0	
LINE	30400		FLIGHT		 								 	
A	4620.3	S	532902	5397952	1.2	4.5	3.2	39.5	1.7	5.2			0	
B	4644.3	S	532895	5398743	5.3	14.9	137.6	317.2	4.3	50.1	0.4	2	0	
C	4666.8	S	532907	5399508	0.3	7.2	49.9	147.7	22.0	36.1			0	
D	4670.0	L	532904	5399627	0.0	0.0	28.5	23.8	33.7	25.0			0	ļ
E	4673.0	L	532897	5399738	38.0	23.3	86.3		101.3	53.5	3.6	0	0	ļ
F	4679.4	S	532889	5399975	2.9	6.6	80.8	194.8	7.8	34.6			0	ļ
G	4710.1	L	532897	5401109	6.5	11.0	11.3	15.7	5.6	3.6	0.6	1	46	
H	4721.6	S	532908	5401499	5.0	5.0	69.7	164.8	1.1	25.7	1.0	25	0	
I	4732.8	S	532911	5401899	6.7	13.3	106.7	200.6	8.5	31.1	0.6	0	14	ļ
J	4756.3	S 	532898	5402765	10.4	0.0	67.8	6.1	39.8	43.3	 		0	
LINE	30410		FLIGHT	10		<b></b>	<b></b>	<b>-</b>	· <b>-</b>	<b>_</b>		<b>_</b>		
A	4518.2	S	533105	5398082	1.1	5.6	5.3	56.8	2.1	7.9			0	
В	4498.0	S	533096	5398902	4.4	12.5	81.1	258.6	4.4	36.3	0.4	5	9	į
C	4477.8	L	533105	5399684	26.1	20.0	42.4	67.4	217.4	71.1	2.4	0	0	į
D	4473.9	S	533108	5399832	8.8	18.7	114.5	208.9	24.4	30.0	0.6	0	0	į
E	4467.2	S	533096	5400106	5.6	8.8	34.2	114.9	27.0	17.6	0.7	22	0	į
F	4443.2	L	533102	5401067	10.7	21.7	28.4	96.0	10.6	11.9	0.6	0	0	İ
G	4429.6	S	533106	5401581	4.4	4.5	54.5	107.7	0.3	16.5	1.0	25	49	į
H	4416.3	S	533095	5402083	8.0	8.5	172.9	159.5	10.9	40.4	1.1	9	217	į

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

LINE 30410	    Labe]	l Fid	Interp	XUTM	YUTM	   CX 55   Real	00 HZ Quad	CP 7	200 HZ Quad	CP Real	900 HZ Quad	Vertica COND	 l Dike DEPTH*	   Mag. Corr 	     
I	ĺ			m	m	ppm	ppm	ppm	ppm	ppm	ı ppm	siemens	m	NT	į
LINE 30420   FLIGHT 10	LINE	30410		FLIGHT	10	 						 			
A 4078.7   S 533295   5398066   S.0   4.3   4.3   38.1   1.9   5.7       0     B 4086.5   S 533295   5398337   0.9   3.0   4.3   38.1   1.9   5.7   4.5       0     C 4108.0   S 533301   5399042   14.4   22.3   303.9   436.7   4.9   88.5   0.9   6   23     D 4126.1   L 533300   5399657   18.4   8.0   12.6   17.1   127.3   76.8   4.4   0   0     E 4132.3   S 533303   5399865   18.8   28.0   185.0   309.8   21.5   71.5   0.5   0   0     F 4143.5   S 533303   5400235   3.5   4.9   0.7   53.6   2.3   8.4       0     G 4167.6   L 533302   5400235   3.5   4.9   0.7   53.6   2.3   8.4       0     H 4173.8   L 533298   5401244   9.6   20.0   52.3   85.5   3.4   14.9   0.6   7   71     I 4183.9   S 533305   5402022   10.3   8.1   188.2   225.9   23.4   38.5   1.7   15   0     K 4213.8   S 533305   5402673   36.3   46.7   424.5   685.3   6.9   134.2   1.5   3   0      LINE 30430   FLIGHT 10	İΙ	4399.4	S	533068	5402668	10.1	4.9	263.7	8.0	29.7	68.6	3.1	33	0	j
B	LINE	30420		FLIGHT	10	 						 			
C	A	4078.7	S	533296	5398086	5.0	4.3	4.3	38.1	1.9	5.7	i		0	j
D	В	4086.5	S	533295	5398337	0.9	3.0	4.3	38.1	5.7	4.5			0	ĺ
E	C	4108.0	S	533301	5399042	14.4	22.3	303.9	436.7	4.9	88.5	0.9	6	23	- 1
F	D	4126.1	L	533300	5399657	18.4	8.0	12.6	17.1	127.3	76.8	4.4	0	0	ĺ
G   4167.6   L   533302   5401046   7.2   28.8   32.2   95.5   14.4   14.0   0.3   0   0     H   4173.8   L   533298   5401274   9.6   20.0   52.3   85.5   3.4   14.9   0.6   7   71     I   4183.9   S   533305   5401643   10.2   13.5   51.4   155.7   1.9   20.7   1.0   11   12     J   4194.2   S   533301   5402002   10.3   8.1   188.2   225.9   23.4   38.5   1.7   15   0     K   4213.8   S   533305   5402673   36.3   46.7   424.5   685.3   6.9   134.2   1.5   3   0      LINE   30430	E	4132.3	S	533303	5399866	10.8	28.0	185.0	309.8	21.5	71.5	0.5	0	0	
H	F	4143.5	S	533303	5400235		4.9	0.7	53.6	2.3	8.4			0	
I	G	4167.6	L	533302	5401046	7.2	28.8	32.2	95.5	14.4	14.0	0.3	0	0	
J	H	4173.8	L	533298	5401274	9.6	20.0	52.3	85.5	3.4	14.9	0.6	7	71	
K	I	4183.9	S		5401643	1	13.5	51.4		1.9	20.7	1.0	11	I .	
LINE 30430	J	4194.2	S	533301	5402002					23.4	38.5	I	15	0	
A 3796.8   S 533485   5399212   14.7   41.4   456.2   621.6   8.9   139.7   0.6   0   20     B 3780.5   L 533499   5399596   21.3   12.9   13.0   7.0   86.7   68.1   3.0   0   0     C 3768.5   S 533497   5399595   21.2   22.7   283.3   354.6   7.7   84.6   1.5   8   0     D 3741.9   L 533496   5400955   2.6   9.5   5.0   19.7   1.8   2.8       709     E 3718.2   S 533497   5401760   5.8   19.8   107.3   235.4   1.4   41.6   0.4   0   46     F 3689.5   S 533492   5402611   13.3   31.4   256.7   456.9   3.2   83.5   0.6   0   0      LINE 30440	K	4213.8	S	533305	5402673	36.3	46.7	424.5	685.3	6.9	134.2	1.5	3	0	
B	LINE	30430		FLIGHT	10	 						 			
C   3768.5   S   533497   5399957   21.2   22.7   283.3   354.6   7.7   84.6   1.5   8   0     D   3741.9   L   533496   5400955   2.6   9.5   5.0   19.7   1.8   2.8       709     E   3718.2   S   533497   5401760   5.8   19.8   107.3   235.4   1.4   41.6   0.4   0   46     F   3689.5   S   533492   5402611   13.3   31.4   256.7   456.9   3.2   83.5   0.6   0   0      LINE   30440	A	3796.8	S	533485	5399212	14.7	41.4	456.2	621.6	8.9	139.7	0.6	0	20	j
D	В	3780.5	L	533499	5399596	21.3	12.9	13.0	7.0	86.7	68.1	3.0	0	0	j
E 3718.2	C	3768.5	S	533497	5399957	21.2	22.7	283.3	354.6	7.7	84.6	1.5	8	0	j
F	D	3741.9	L	533496	5400955	2.6	9.5	5.0	19.7	1.8	2.8			709	ĺ
LINE 30440	E	3718.2	S	533497	5401760	5.8	19.8	107.3	235.4	1.4	41.6	0.4	0	46	ĺ
A 3285.9	F	3689.5	S	533492	5402611	13.3	31.4	256.7	456.9	3.2	83.5	0.6	0	0	İ
B	LINE	30440		FLIGHT	10	 						 			
C   3337.5   S   533706   5399306   0.0   14.5   128.7   227.8   7.9   46.2       0     D   3348.1   L   533698   5399609   4.2   0.0   16.3   3.7   49.3   24.8       0     E   3362.4   S   533718   5400016   13.5   19.6   280.5   258.4   10.6   76.8   1.0   8   0     F   3374.5   S   533716   5400397   2.6   7.7   23.9   105.5   3.8   16.3       0     G   3389.0   L   533701   5400884   9.7   25.6   7.4   68.7   3.3   3.9   0.5   0   443     H   3421.2   S   533698   5402047   43.2   42.3   489.0   823.0   7.3   161.2   2.2   6   83     I   3439.3   S   533709   5402656   2.1   19.0   305.6   385.7   6.7   86.3       0      LINE   30450   FLIGHT   10	A	3285.9	S	533690	5397646	1.2	0.7	1.1	13.7	0.2	2.3	i		0	j
D	В	3316.7	S	533706	5398597	1.5	6.8	8.6	54.0	8.7	7.6			0	ĺ
E	C	3337.5	S	533706	5399306	0.0	14.5	128.7	227.8	7.9	46.2			0	ĺ
F 3374.5 S 533716 5400397   2.6 7.7 23.9 105.5 3.8 16.3     0   G 3389.0 L 533701 5400884   9.7 25.6 7.4 68.7 3.3 3.9   0.5 0 443   H 3421.2 S 533698 5402047   43.2 42.3 489.0 823.0 7.3 161.2   2.2 6 83   I 3439.3 S 533709 5402656   2.1 19.0 305.6 385.7 6.7 86.3     0   C   C   C   C   C   C   C   C   C	D	3348.1	L	533698	5399609	4.2	0.0	16.3	3.7	49.3	24.8			0	ĺ
G 3389.0 L 533701 5400884   9.7 25.6 7.4 68.7 3.3 3.9   0.5 0   443    H 3421.2 S 533698 5402047   43.2 42.3 489.0 823.0 7.3 161.2   2.2 6   83    I 3439.3 S 533709 5402656   2.1 19.0 305.6 385.7 6.7 86.3     0	E	3362.4	S	533718	5400016	13.5	19.6	280.5	258.4	10.6	76.8	1.0	8	0	į
H 3421.2 S 533698 5402047   43.2 42.3 489.0 823.0 7.3 161.2   2.2 6   83	F	3374.5	S	533716	5400397	2.6	7.7	23.9	105.5	3.8	16.3			0	j
I 3439.3 S 533709 5402656   2.1 19.0 305.6 385.7 6.7 86.3     0	G	3389.0	L	533701	5400884	9.7	25.6	7.4	68.7	3.3	3.9	0.5	0		ĺ
LINE 30450	H	3421.2	S	533698	5402047	43.2	42.3	489.0	823.0	7.3	161.2	2.2	6	83	j
A     3196.5     S     533893     5398293     2.0     10.1     3.7     62.0     1.8     7.7       0       B     3186.3     S     533901     5398676     0.7     5.1     19.2     111.5     4.3     16.1       0	I	3439.3	S	533709	5402656	2.1	19.0	305.6	385.7	6.7	86.3			0	į
B 3186.3 S 533901 5398676 0.7 5.1 19.2 111.5 4.3 16.1 0	LINE	30450		FLIGHT	10	 						 			
	A	3196.5	S	533893	5398293	2.0	10.1	3.7	62.0	1.8	7.7	i		0	į
	В	3186.3	S	533901	5398676	0.7	5.1	19.2	111.5	4.3	16.1	i		0	į
	C	3163.5	L	533886	5399469	26.8	6.5	66.5	92.8	28.6	25.5	11.4	0	0	j

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					   CX 55	00 HZ	7	200 HZ	CP	900 HZ	   Vertical	 l Dike	Mag. Corr	 
Labe:	l Fid	Interp	XUTM	YUTM	Real	Quad	Real	Quad	Real	Quad	COND 1	DEPTH*		j
1			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	
LINE	30450		FLIGHT	10	 						 			
D	3150.5	S	533886	5399985	6.1	9.4	116.2	72.6	6.7	21.7	0.7	19	0	
E	3135.6	S	533907	5400601	1.8	17.7	4.7	67.3	1.2	8.8			0	
F	3128.8		533903	5400882	19.3	34.6	68.1	161.4	2.0	25.1	0.9	0	120	
G	3114.8	S	533899	5401445	4.6	3.7	74.8	19.3	5.9	20.8	1.3	35	83	
H	3090.3	S	533909	5402347	3.1	12.4	3.5	51.7	2.8	6.6			0	
Ι	3079.4	S	533906	5402722	11.4	26.5	352.4	352.2	11.6	104.6	0.6	0	0	
LINE	30461		FLIGHT	10	 						 			
A	2882.2	S	534096	5398413	2.6	15.4	5.5	94.8	4.4	12.3	j		0	į
В	2894.4	S	534091	5398829	0.2	4.4	12.9	25.2	15.2	4.0	j		0	į
C	2914.2	L	534103	5399491	9.2	7.6	21.9	19.1	22.1	12.4			0	Ì
D	2925.3	S	534114	5399835	8.1	21.2	5.6	102.2	4.8	13.5	0.5	0	14	į
E	2932.4	S	534118	5400071	6.3	12.6	220.4	262.7	3.6	59.7	0.5	13	0	Ì
F	2948.2	S	534114	5400617	5.8	16.7	47.3	197.6	0.4	27.4	0.4	3	168	
G	2953.5	L	534106	5400800	20.0	30.3	36.5	156.5	9.4	21.2	1.0	0	0	Ì
H	2964.5	S	534096	5401181	1.0	27.0	24.6	114.6	8.0	15.2			0	
I	2981.8	S	534117	5401790	4.2	3.7	31.8	36.0	5.3	12.2	1.1	38	0	Ì
J	3006.3	L	534107	5402680	29.1	32.4	355.3	295.6	17.1	113.8	1.6	0	0	Ì
K	3008.2	S	534108	5402752	20.5	30.2	355.3	295.6	17.1	113.8	1.1	1	0	ĺ
LINE	30470		FLIGHT	10	 						 			
A	2226.4	S	534307	5399032	1.4	3.0	4.2	13.7	8.7	1.9	i		435	İ
ΪВ	2239.8	L	534306	5399458	2.9	6.5	14.0	12.6	18.1	15.2	i		32	į
ĺС	2245.5	S	534321	5399621	8.7	7.0	38.5	120.9	1.7	20.7	1.6	11	0	į
D	2262.3	S	534310	5400156	13.3	5.9	212.9	214.1	9.2	57.6	3.9	23	103	į
E	2277.9	S	534307	5400672	3.7	20.0	57.3	304.8	23.0	41.7	0.2	0	0	į
F	2297.7	S	534298	5401399	7.0	18.1	33.8	119.1	6.8	17.4	0.5	0	0	į
G	2313.2	S	534305	5401971	1.7	5.8	124.1	202.2	3.5	36.1	j		0	į
Η	2336.8	S	534297	5402865	14.3	18.9	292.1	221.5	16.1	91.5	1.1	7	0	İ
LINE	30480		FLIGHT	10	 						 			
A	2082.7	S	534496	5398680	0.2	3.1	3.7	41.9	5.0	5.8	i		0	i
В	2072.3	S	534477	5399088	2.7	10.9	7.1	66.3	4.3	9.7	i		86	i
C	2065.7		534485	5399330	9.2	6.1	1.1	0.0	46.3	20.5	2.1	0	0	i
D	2057.7		534493	5399632	5.4	3.5	99.2	149.8	14.2	34.0	1.8	31	0	i
E	2045.6		534481	5400144	7.6	10.6	193.4	175.5	8.2	43.6	0.8	9	0	i
F	2031.0		534494	5400761	1.1	0.3	12.5	71.3	7.4	8.9			0	i
G	2012.9	S	534509	5401486	3.1	8.3	8.0	61.7	4.2	8.6	i		0	į
														<u>·</u>

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

					   CX 55	00 HZ	CP 7	200 HZ	 CP	900 HZ	   Vertica	 l Dike	Mag. Corr	 
Labe	l Fid	Interp	XUTM	YUTM	Real	Quad	Real	Quad	Real	Quad	COND :	DEPTH*		j
j		-	m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	j
	30480		FLIGHT	10	 I						 I			 I
H	1999.5	S	534510	5401979	6.0	0 7	150.2	172 0	5.1	40.4	l l 0.7	5	0	
ļΙ	1974.8	S S	534510	5402807	11.2		215.4		10.7	62.5	1.1	11	41	
<del> </del>											±•±			ا 
LINE	30490		FLIGHT	10									1	
A	1805.0	L	534702	5399268	9.1	7.5	25.6	66.0	15.6	40.9	1.5	0	540	į
В	1816.0	L	534714	5399575	28.7	14.9	58.9	126.7	6.6	38.0	4.1	4	284	į
C	1825.9	S	534710	5399890	4.8	4.5	85.4	60.6	3.7	19.9	1.1	32	0	İ
D	1856.3	L	534695	5400855	14.9	25.9	20.1	48.4	16.1	8.5	0.8	3	0	
E	1866.6	S	534705	5401208	1.0	15.6	23.5	93.3	20.9	12.0			19	
F	1890.0	S	534702	5402036	0.6	4.1	100.6	152.3	3.4	29.9			0	
G	1907.5	S	534705	5402712	19.7	28.8	280.3	284.6	13.4	84.0	1.1	0	0	
LINE	30500		FLIGHT	10	 						 			 
A	1659.5	S	534889	5398432	1.5	2.9	4.4	31.6	2.6	4.3			0	İ
В	1629.5	L	534904	5399399	15.3	11.5	119.7	158.5	42.3	45.3	2.1	1	339	j
C	1624.0	L	534894	5399596	15.4	13.2	16.3	61.9	13.1	4.3	1.8	5	407	
D	1613.6	S	534884	5399990	7.8	14.3	192.2	193.4	9.9	49.5	0.6	6	59	
E	1591.6	L	534910	5400858	9.3	11.3	10.5	21.9	1.9	3.9	1.0	4	0	
F	1580.2	S	534894	5401302	0.4	2.8	0.1	17.7	2.6	2.5			59	
G	1562.1		534875	5401947	3.5	5.1	52.5	70.3	3.3	15.3	0.6	30	0	
H	1540.8	S	534886	5402588	5.2	7.9	154.3	177.9	4.6	38.7	0.7	5	0	
LINE	30510		FLIGHT	10	 						 			
A	1198.4	S	535111	5398894	1.9	8.3	11.2	77.2	2.7	10.1	i		0	į
В	1211.0	L	535121	5399270	22.0	6.9	80.8	45.6	56.5	101.2	7.4	0	19	İ
C	1217.0	S	535120	5399447	17.2	34.1	232.7	426.1	16.1	79.7	0.8	0	0	
D	1223.3	L	535118	5399638	27.1	14.5	29.0	19.6	31.7	14.8	3.8	9	0	
E	1236.1	S	535114	5400042	3.7		185.4		11.1	47.1	0.4	8	0	
F	1261.1	L	535094	5400868	13.2	12.5	15.3	23.8	11.3	4.5	1.5	11	0	
G	1295.4		535113	5402067	16.3		133.1		0.8	35.9	4.6	16	67	
H	1308.5	S 	535100	5402518	7.0	16.8	226.3	203.2	8.6	63.5	0.5	0	0	
LINE	30520		FLIGHT	10			<b></b>		<b>_</b>	<b>_</b>				
ļΑ	1105.1	S	535274	5398961	0.9	5.0	5.2	10.3	11.5	11.3	<b></b>		j 0	j
В	1093.0	L	535293	5399263	40.1	2.7	21.3	32.6	89.8	93.7	<b></b>		j 0	j
C	1080.3	L	535299	5399679	30.0	22.5	24.5	0.0	21.8	16.2	2.6	6	0	
D	1076.1	S	535284	5399826	12.1	44.4	102.5	326.9	21.3	38.5	0.4	0	0	
E	1063.3	S	535299	5400286	15.1	19.7	145.8	247.1	11.5	44.7	1.1	1	18	

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

    Labe 	l Fid	Interp	XUTM m	YUTM m	CX 55   Real   ppm	00 HZ Quad ppm	CP 7 Real ppm	200 HZ Quad ppm	CP Real ppm	900 HZ Quad ppm	Vertica COND siemens	 l Dike DEPTH* m	Mag. Corr       NT	
LINE	30520		FLIGHT	10	 						 		 	
F	1047.2	L	535298	5400872	18.2	14.5	9.8	32.6	9.3	7.2	2.0	7	j 0	į
G	1012.7	S	535291	5402040	7.5	16.0	193.3	152.1	12.3	51.7	0.6	4	j 0	j
H	1000.8	S	535299	5402405	5.7	9.4	240.3	145.6	14.3	69.4	0.6	14	12	ĺ
LINE	30530		FLIGHT	10	 						 		 	
A	768.4	S	535508	5398745	1.3	1.8	9.2	25.8	21.1	5.3	i		j 0	į
В	780.4	S	535507	5399054	5.6	4.4	25.2	24.7	25.3	10.7	i		j 0	į
C	783.9	L	535507	5399137	16.0	0.6	22.9	11.8	23.8	5.9			0	ĺ
D	797.4	S	535510	5399428	11.5	18.8	25.6	205.9	8.1	27.6			35	j
E	805.9	L	535514	5399638	33.7	32.0	89.9	167.3	28.9	58.1	2.0	1	320	İ
F	812.1	S	535513	5399797	6.7	14.2	163.5	327.8	9.3	67.7	0.5	7	0	ĺ
G	830.9	S	535503	5400310	17.9	18.2	89.6	250.6	3.8	36.1	1.5	4	0	ĺ
H	848.6	L	535510	5400827	11.9	9.0	12.6	25.8	8.0	5.9	i		0	j
I	884.6	S	535495	5402020	6.3	3.1	77.9	26.8	5.1	19.7	2.6	39	0	ĺ
J	896.7	S	535500	5402453	8.1	4.4	187.7	102.3	26.1	76.8	2.6	26	5	j
LINE	30540		FLIGHT	10	 						 		 	
A	672.1	L	535698	5399126	3.6	4.7	69.5	112.7	29.1	27.8			j o	į
В	666.0	S	535696	5399324	0.7	7.7	17.8	119.2	10.0	23.4			j o	į
ĺС	659.0	L	535686	5399579	21.9	0.0	32.5	0.0	9.6	17.5			235	İ
D	650.2	S	535678	5399898	9.8	12.0	321.3	311.2	10.3	84.8	1.0	19	12	į
E	640.0	L	535682	5400265	25.4	56.5	78.4	248.8	0.0	36.6	0.8	0	i o	į
F	638.2	S	535681	5400328	25.4	56.5	78.4	248.8	14.4	36.6	0.8	0	i o	į
Ġ	625.6	L	535680	5400765	16.7	19.7	34.7	85.7	4.5	14.8	1.3	0	j o	į
Н	617.6	S	535695	5401037	1.3	7.6	17.1	69.0	3.0	11.2			j o	į
İı	585.7	S	535671	5402049	7.7	16.6	269.7	281.6	9.2	73.7	0.6	8	i o	į
јJ	566.6	S	535688	5402600	13.4	14.4	84.4	83.6	15.4	38.5	1.3	12	j o	į
LINE	30550		FLIGHT	9	 						 		 	
A	5293.1	S	535880	5398939	4.2	0.8	15.7	36.3	27.6	6.8			j o	j
ΪВ	5285.7	L	535886	5399199	4.6	11.2	75.7	101.4	34.3	35.0	0.4	0	i o	j
İc	5277.9	L	535901	5399475	22.8	27.4	0.0	36.6	4.7	23.9	1.4	0	i o	j
D	5263.5	S	535879	5399999	8.8	10.1	103.7	97.5	13.4	28.9	1.1	16	i o	
E	5246.0	L	535882	5400690	7.1	8.7	1.2	0.0	3.5	0.0	0.9	8	i o	
F	5238.2	S	535883	5400996	0.7	16.7	107.3	151.7	2.6	31.5			136	j
Ġ	5202.8	S	535933	5402130	6.1	10.2		122.1	6.8	31.5	0.6	10	24	
H	5182.7	H	535888	5402615	4.4		110.5		17.4	40.7	0.5	13	0	

CX = COAXIAL

CP = COPLANAR

Note:EM values shown above are local amplitudes

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

ı	Fid	Interp	XUTM m	YUTM m	CX 55   Real   ppm	00 HZ Quad ppm	CP 7 Real ppm	200 HZ Quad ppm	CP Real ppm		Vertica   COND :   siemens	l Dike DEPTH* m	Mag. Corr     NT	
LINE	 30560		FLIGHT	9	 I						 		 I	
	4979.8	S	536102	5398579	1.5	3.6	3.5	36.6	2.9	5.4	l 		0	l
	4997.5	L	536115	5399178	0.0	0.0	16.1	22.2	89.5	59.4	 		0	
	5002.5	L	536129	5399350	18.4	12.1	55.5	131.2	16.6	30.3	2.6	16	0	
	5010.0	S	536129	5399628	15.6	8.7	190.7	212.1	7.0	44.9	3.0	22	0	
	5019.6	S	536110	5400010	13.5	22.7	94.7	148.6	8.3	22.8	0.8	2	0	
	5035.3	L	536111	5400651	28.8	21.3	216.4	272.7	7.6	65.0	2.6	8	0	
	5043.5	S	536115	5400986	7.8	4.6	61.6	121.1	3.4	20.8	2.2	24	102	
	5051.9	S	536106	5401321	9.2	6.3	61.1	99.7	2.3	16.3	2.0	37	0	
	5073.6	H	536100	5402215	4.9	11.1	38.0	76.4	4.9	8.6	0.5	7	0	
	5087.8	S	536111	5402801	23.9	42.9	264.5		6.4	79.1	0.9	0	0	i
					' 								' 	
!	30570		FLIGHT								ļ			ļ
	4894.6	L	536303	5399083	19.3	11.5	6.0	21.5	148.9	141.4	3.0	1	0	ļ
	4884.6	S	536302	5399485	13.9	19.0	186.7	269.8	7.3	59.8	1.0	5	388	ļ
	4872.9	S	536294	5399983	13.4	4.3	112.5	247.0	4.5	40.7	6.1	28	0	
	4870.8	L	536298	5400067	29.5	44.3	112.5	247.0	9.3	40.7	1.2	0	0	
	4855.7	L	536308	5400607	7.4	17.9	287.6	432.1	7.7	89.1	0.5	4	0	ļ
	4835.1	S	536316	5401372	11.3	28.4	338.7	559.5	22.8	105.6	0.6	0	0	ļ
!	4826.6	S?	536297	5401693	19.6	31.0	142.1	190.2	6.7	36.8	1.0	0	0	ļ
	4818.0	S	536287	5402011	0.2	5.0	239.7	302.6	7.6	64.9			23	
	4810.7	S?	536289	5402271	17.7		230.2	201.7	6.4	57.9			0	
J 4	4803.6	S	536287	5402503	10.7	12.2	112.8	116.7	7.8	39.5	1.1	17	0	
LINE	 30580		FLIGHT	 a	 I						 I		 I	
	4612.1	L	536495	5399073	2.1	11.2	38.5	42.0	21.2	29.5	i		0	ŀ
	4629.8	S	536515	5399539	12.5	10.8	189.2	192.7	10.4	54.5	1.6	19	278	
	4643.5	S	536507	5399978	6.3	5.5	43.6	21.2	3.3	3.9	1.3	30	1 0	-
	4659.0	L	536503	5400492	20.8	30.3	4.6	4.4	10.8	1.0	1.1	0	)   0	-
	4667.7	L	536500	5400402	5.0	10.6	180.1	339.9	4.3	59.7	0.5	10	0	
	4682.1	S	536501	5401352	2.3	15.8	163.8	355.8	3.6	59.0	0.5		0	
!	4692.8	S	536508	5401766	9.4	4.8		141.0	3.8	24.3	2.9	21	l 0	
	4714.1	S	536499	5402609	13.5		139.7		10.3	43.0	3.3	25	l 0	
LINE			FLIGHT											
A 4	4396.0	L	536683	5398983	16.4	13.5	28.4	76.7	37.8	76.5	1.9	7	26	
B 4	4380.7	S	536683	5399608	8.8	4.8	74.3	0.4	10.4	17.2	2.6	29	0	ĺ
C 4	4367.8	S	536685	5400143	18.2	11.3	175.6	196.7	32.7	39.1	2.8	21	0	ĺ

CP = COPLANAR

Note:EM values shown above are local amplitudes

EM Anomaly List

					   CX 55	00 HZ	CP 7	200 HZ	CP	900 HZ	Vertical	Dike	   Mag. Corr	
Labe]	l Fid	Interp	XUTM	YUTM	Real	Quad	Real	Quad	Real	Quad	COND I	EPTH*		
			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	
LINE	30590		FLIGHT	9	 						 			
D	4361.1	S	536685	5400415	52.7	41.1	267.4	502.9	6.4	86.1	3.0	4	0	j
E	4351.7	S	536701	5400785	11.3	15.6	107.4	127.1	3.5	26.9	0.9	5	0	j
F	4339.4	S	536678	5401233	8.9	6.6	42.0	153.3	10.2	17.8	1.8	28	0	ĺ
G	4325.0	S	536693	5401721	0.6	9.5	43.9	158.9	7.8	22.4			0	ĺ
H	4303.6	S	536704	5402371	12.4	11.1	191.8	200.7	5.5	51.4	1.6	12	11	
I	4292.0	S	536704	5402711	25.4	30.0	414.8	601.2	12.1	125.6	1.5	10	0	
LINE	30600		FLIGHT	9	 						 			
A	4111.6	L	536919	5399006	9.2	9.3	14.3	25.1	89.6	65.7	1.2	0	0	j
В	4133.4	S	536916	5399560	1.5	9.4	40.9	28.5	0.3	8.1			0	į
ĺС	4148.7	L	536916	5400030	13.8	32.9	18.6	0.2	8.2	0.0	0.6	0	j o	į
D	4154.1	S	536906	5400197	24.2	54.2	20.6	206.6	18.0	28.1	0.8	0	0	į
E	4159.5	S	536893	5400365	9.1	12.4	81.3	112.3	21.3	16.1	0.9	14	585	į
F	4162.0	L	536890	5400446	14.4	23.9	81.3	112.3	21.3	16.1	0.9	0	0	į
G	4168.7	S	536906	5400670	5.1	2.5	128.0	76.9	4.9	29.1	i		47	j
Н	4178.6	S	536913	5401015	8.7	14.2	89.4	211.6	2.6	34.8	0.7	5	0	j
İI	4198.1	S	536889	5401721	0.0	7.0	11.3	54.2	1.8	6.9	i		0	j
J	4204.7	S	536894	5401960	4.5	10.5	12.2	78.6	0.8	9.4	0.4	0	23	ĺ
K	4221.7	H	536894	5402604	9.6	10.8	270.1	298.0	10.5	81.1	1.1	16	0	j
LINE	30610		FLIGHT	9	 						 		 	
A	3950.7	S	537095	5399654	4.7	8.6	51.3	58.1	11.0	19.3	0.5	15	0	i
В	3935.4		537092	5400218	17.3	28.7	147.2	376.8	32.8	56.9	0.9	4	0	i
ĺС	3929.9	L	537102	5400407	17.0	20.7	0.0	0.0	14.4	0.0	1.2	0	0	į
D	3922.7	S	537109	5400654	16.3	16.2	216.6	275.7	6.2	60.5	1.5	10	0	į
E	3882.1	S	537096	5402013	7.2	13.9	75.2	177.5	1.5	30.2	0.6	3	0	į
F	3871.8	S	537102	5402328	9.0	4.5	54.0	147.7	0.5	20.8	2.9	24	j o	į
Ġ	3858.3	S	537121	5402719	1.6	20.6	111.4	204.2	2.8	35.9			0	j
LINE	30620		FLIGHT	9	 						 		 	
A	3672.7	S	537315	5399665	8.7	19.9	162.9	270.0	5.4	47.7	0.5	3	0	i
В	3692.8	S	537310	5400230	5.3	6.8	110.7	317.8	6.7	48.3	0.8	26	0	i
İc	3697.0		537310	5400356	28.8	30.9	0.0	0.0	27.6	0.0	1.7	0	843	i
D	3708.8		537306	5400703	10.5	24.7	316.7	370.8	9.0	89.5	0.6	0	44	i
E	3747.7		537305	5402062	10.6	20.5	159.5	215.5	3.4	45.5	0.7	0	0	i
F	3756.8		537305	5402398	14.8	19.1		148.8	1.0	23.3	1.1	8	0	i
G	3766.9	S	537310	5402751	6.8		107.4		4.3	34.6	0.6	0	0	i
													· 	

CP = COPLANAR

Note: EM values shown above

EM Anomaly List

LINE 30630	  Labe	l Fid	Inter <sub>l</sub>	p XUTM m	YUTM m	   CX 55   Real   ppm	00 HZ Quad ppm	CP 7 Real	200 HZ Quad ppm	CP Real	900 HZ Quad ppm	Vertica   COND	 l Dike DEPTH* m	Mag. Corr       NT	
A 3606.0						PP 									
B 3589.4 L 537499 5400358 25.5 17.6 48.6 3.0 26.2 0.0 2.7 0 671 C 3579.8 S 537489 5400660 13.8 14.1 222.2 255.1 9.4 58.6 1.4 13 119 D 3553.8 S 537495 5401470 2.9 0.0 0.2 10.6 2.5 2.2 79 E 3535.4 S 537498 540245 6.1 11.2 176.4 275.2 7.0 52.5 0.6 4 140 F 3509.6 S 537488 540245 6.1 11.2 176.4 275.2 7.0 52.5 0.6 4 140 F 3509.6 S 537488 540245 7.2 58.5 98.1 0.7 15.6 0    LINE 30640 FLIGHT 9   A 3330.3 S 537707 5399584 8.3 18.0 69.7 173.2 4.6 25.6 0.6 0 164 B 3345.7 S 537706 5400013 8.7 12.9 118.7 191.6 1.8 37.8 0.8 10 118 C 3356.6 L 537711 5400322 22.7 9.2 59.8 29.4 8.8 9.8 5.3 6 0 D 3367.6 S 537718 5400914 2.3 4.6 6.3 45.0 2.0 6.8 0    LINE 30650 FLIGHT 9   A 3243.4 S 537890 5400469 12.7 8.2 14.9 194.4 271.9 4.3 58.9 0.6 10 0   LINE 3043.4 S 537890 540047 27.8 24.5 43.5 109.2 15.4 14.3 2.1 0 0   C 3221.3 S 537896 5400497 27.8 24.5 43.5 109.2 15.4 14.3 2.1 0 0   D 3211.2 S 537890 5401345 5.9 8.9 11.5 83.4 6.7 11.6 0.7 22 0   E 3202.5 S 537893 5401345 5.4 7.7 7.5 44.9 7.9 4.3 58.9 0.6 5 0   F 3177.5 S 537897 5402177 5.8 9.1 124.3 135.6 3.7 37.9 0.7 7 0   F 3177.5 S 537897 5402177 5.8 9.1 124.3 135.6 3.7 37.9 0.7 7 0   G 3159.1 S 537893 5400366 5.9 14.0 40.9 87.9 6.8 12.6 0.5 0 0   LINE 30660 FLIGHT 9   A 2878.5 S 53811 5399788 4.0 7.1 38.1 58.3 2.1 13.1 0.5 16 0   C 2890.8 S 53890 5400356 5.9 14.0 40.9 87.9 6.8 12.6 0.5 0 0   C 2890.8 S 53890 5400356 5.9 14.0 40.9 87.9 6.8 12.6 0.5 0 0   C 2897.2 S 538096 5402463 7.3 9.4 0.0 88.5 6.5 8.8 0   F 2947.8 S 538096 5402379 5.3 10.2 36.3 63.1 1.5 10.9 0.5 0 0   LINE 30660 FLIGHT 9   A 2878.5 S 53810 5400356 5.9 14.0 40.9 87.9 6.8 12.6 0.5 0 0   C 2896.8 S 538093 5400356 5.9 14.0 40.9 87.9 6.8 12.6 0.5 0 0   D 208.4 S 538096 5402377 5.3 10.2 36.3 63.1 1.5 10.9 0.5 0 0   D 208.4 S 538096 5402377 5.3 10.2 36.3 63.1 1.5 10.9 0.5 0 0   D 208.4 S 538096 5402377 5.3 10.2 36.3 63.1 1.5 10.9 0.5 0 0   D 208.4 S 538096 5402377 5.3 10.2 36.3 63.1 1.5 10.9 0.5 0 0   D 208.4 S 538006 5402377 5.3 10.2 36.3 63.1 1.5 10.9 0.5 0 0   D 208.4 S 538006 5402377 5.3 10	LINE	30630		FLIGHT	9										
C   3579.8   S   537489   5400660   13.8   14.1   222.2   255.1   9.4   58.6   1.4   13   119   19   19   19   19   19   1	A		S			I					52.9	1	0	0	
D   3553.8   S   537495   5401470   2.9   0.0   0.2   10.6   2.5   2.2     79     E   3535.4   S   537498   5402045   6.1   11.2   176.4   275.2   7.0   52.5   0.6   4   140     F   3509.6   S   537488   5402853   1.5   7.2   58.5   98.1   0.7   15.6       0	В		L			I	17.6				0.0	2.7	0	l .	
E   3535.4   S   537498   5402045   6.1   11.2   176.4   275.2   7.0   52.5   0.6   4   140	C		S	537489	5400660	I				9.4		1.4	13	119	
F   3509.6   S   537488   5402853   1.5   7.2   58.5   98.1   0.7   15.6       0	D	3553.8	S	537495	5401470	2.9	0.0	0.2	10.6	2.5	2.2			79	
LINE 30640   FLIGHT 9	E	3535.4	S	537498	5402045	6.1	11.2	176.4	275.2	7.0	52.5	0.6	4	140	
A 3330.3 S 537707 5399584	F	3509.6	S	537488	5402853	1.5	7.2	58.5	98.1	0.7	15.6			0	
B   3345.7   S   537706   5400013   8.7   12.9   118.7   191.6   1.8   37.8   0.8   10   118   12   1356.6   L   537711   5400322   22.7   9.2   59.8   29.4   8.8   9.8   5.3   6   0   0   0   0   0   0   0   0   0	LINE	30640		FLIGHT	9	 						 		 	
B   3345.7   S   537706   5400013   8.7   12.9   118.7   191.6   1.8   37.8   0.8   10   118   12   1356.6   L   537711   5400322   22.7   9.2   59.8   29.4   8.8   9.8   5.3   6   0   0   0   0   0   0   0   0   0	ĺΑ	3330.3	S	537707	5399584	8.3	18.0	69.7	173.2	4.6	25.6	0.6	0	164	i
C   3356.6	!					I						!	10	!	i
D   3367.6   S   537718   5400646   7.1   3.8   169.2   275.7   3.2   52.0   2.4   40   74     E   3376.3   S   537712   5400914   2.3   4.6   6.3   45.0   2.0   6.8     0     F   3413.8   S   537691   5402178   5.2   8.3   130.7   98.3   6.1   35.8   0.6   10   0     LINE   30650	İc		L							8.8		5.3	6	j o	į
E 3376.3 S 537712 5400914   2.3 4.6 6.3 45.0 2.0 6.8	D		S			I						!	40	74	i
F 3413.8 S 537691 5402178   5.2 8.3 130.7 98.3 6.1 35.8   0.6 10   0	İΕ					I								i o	i
A 3243.4 S 537890 5399869   7.2 14.9 194.4 271.9 4.3 58.9   0.6 5   0     B 3231.6 L 537892 5400297   27.8 24.5 43.5 109.2 15.4 14.3   2.1 0   0     C 3221.3 S 537896 5400669   13.7 8.2 155.7 299.7 12.6 51.7   2.7 31   0     D 3211.2 S 537890 5401034   5.9 8.9 11.5 83.4 6.7 11.6   0.7 22   0     E 3202.5 S 537893 5401345   1.4 7.7 7.5 44.9 7.5 6.0     0     F 3177.5 S 537897 5402177   5.8 9.1 124.3 135.6 3.7 37.9   0.7 7   0     G 3159.1 S 537898 5402746   9.3 5.2 12.2 68.0 1.1 9.3   2.6 30   0      LINE 30660	F		S			I						0.6	10	0	İ
A 3243.4 S 537890 5399869   7.2 14.9 194.4 271.9 4.3 58.9   0.6 5   0     B 3231.6 L 537892 5400297   27.8 24.5 43.5 109.2 15.4 14.3   2.1 0   0     C 3221.3 S 537896 5400669   13.7 8.2 155.7 299.7 12.6 51.7   2.7 31   0     D 3211.2 S 537890 5401034   5.9 8.9 11.5 83.4 6.7 11.6   0.7 22   0     E 3202.5 S 537893 5401345   1.4 7.7 7.5 44.9 7.5 6.0     0     F 3177.5 S 537897 5402177   5.8 9.1 124.3 135.6 3.7 37.9   0.7 7   0     G 3159.1 S 537898 5402746   9.3 5.2 12.2 68.0 1.1 9.3   2.6 30   0      LINE 30660	LT.TNE	30650		FT.TCHT	 a	 I						 I		 I	
B   3231.6	!		g			l l 72	14 9	194 4	271 9	4 3	58 9	1 1 0 6	5	i n	ł
C 3221.3 S 537896 5400669   13.7 8.2 155.7 299.7 12.6 51.7   2.7 31   0     D 3211.2 S 537890 5401034   5.9 8.9 11.5 83.4 6.7 11.6   0.7 22   0     E 3202.5 S 537893 5401345   1.4 7.7 7.5 44.9 7.5 6.0	!					I						!		l .	ł
D 3211.2 S 537890 5401034   5.9 8.9 11.5 83.4 6.7 11.6   0.7 22   0	!		_			I						I	Ū	1	
E 3202.5 S 537893 5401345	!					!						!		0	i
F 3177.5   S 537897   5402177     5.8   9.1   124.3   135.6   3.7   37.9     0.7   7     0	!					I						!		1	i
G 3159.1 S 537898 5402746   9.3 5.2 12.2 68.0 1.1 9.3   2.6 30   0	!					I						!		1 -	i
A 2878.5	1											I		1	į
A 2878.5 S 538111 5399788   4.0 7.1 38.1 58.3 2.1 13.1   0.5 16   0	IT TNE	20660		 EI TCUT	٥	 I						 I		 I	
B	1		C			l I 40	7 1	20 1	E0 2	2 1	10 1	   0 E	16	l   0	
C	!					I						I		l .	ļ
D	!					I						I .		1	
E 2927.2 S 538096 5401379   1.1 1.6 10.4 43.9 5.6 5.8   0	1 -											!	-	1	
F 2947.8 S 538103 5402117   2.8 5.4 115.1 128.4 2.7 31.4     10   G 2957.0 S? 538091 5402463   7.3 9.4 0.0 33.5 1.5 5.4   0.9 15   0   G 2957.0 S? 538096 5402737   5.3 10.2 36.3 63.1 1.5 10.9   0.5 0   0   G 2957.0 S	!											!		1	
G 2957.0 S? 538091 5402463   7.3 9.4 0.0 33.5 1.5 5.4   0.9 15   0	!											!			-
H 2964.2 S 538096 5402737   5.3 10.2 36.3 63.1 1.5 10.9   0.5 0   0	!					!						!		1	
A 2786.9 S 538300 5400133   8.7 13.7 103.1 97.9 15.0 38.5   0.8 4   52						I						I		!	
A 2786.9 S 538300 5400133   8.7 13.7 103.1 97.9 15.0 38.5   0.8 4   52		20670				 I						 I			·
	!		a				10 5	100 1	07.0	1 - 0	20 5	1 0 0	4		ļ
B 2/84.0 L 538303 540024/	!											!		•	ļ
·	lв	2784.0	Ь	538303	5400247	18.2	8.5	177.4	112.2	15.0	52.1	4.1	4	1 0	

CP = COPLANAR

Note:EM values shown above are local amplitudes

EM Anomaly List

					   CX 55	 500 HZ	CP 7	200 HZ	CP	 900 нz	Vertical	 l Dike	Mag. Corr	
Labe	l Fid	Interp	XUTM	YUTM	Real	Quad	Real	Quad	Real	Quad	COND 1	DEPTH*		į
İ			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	İ
LINE	30670		FLIGHT	9	 						 			
C	2770.2	S	538295	5400784	8.8		182.2	223.4	7.0	55.0	1.1	16	10	
D	2749.3		538305	5401601	0.3	1.8	46.0	99.6	17.6	15.6			0	
E	2738.0	S	538286	5402011	11.4	15.0	143.5	223.7	6.6	42.4	1.0	15	0	
F	2725.2	S	538282	5402469	1.9	4.9	78.3	63.4	0.5	14.8			0	
LINE	30681		FLIGHT	10	 						 			
A	307.4	S	538503	5399893	17.1	21.6	199.6	324.3	6.8	66.7	1.2	11	0	
В	318.0	L	538511	5400203	53.9	24.6	183.7	70.5	12.5	49.5	6.0	5	0	
C	336.2	S	538500	5400747	7.2	10.4	245.0	238.4	64.6	53.7	0.8	17	0	
D	351.6	S	538486	5401218	2.6	6.5	8.9	68.5	1.7	8.3			65	
E	363.1	S	538489	5401572	8.4	15.0	99.7	163.0	11.8	27.9	0.7	10	0	
F	375.8	S	538489	5401958	4.9	8.7	220.4	210.9	14.0	56.2	0.6	17	0	
G	401.6	S	538513	5402769	20.4	32.6	153.8	382.1	8.5	56.1	1.0	0	0	
LINE	30690		FLIGHT	9	 						 			
A	2453.6	S	538704	5399997	11.4	14.1	122.9	123.4	13.4	33.4	1.1	6	0	j
В	2448.0	L	538698	5400208	29.9	17.9	122.8	140.4	11.9	5.7	3.4	0	62	j
C	2442.6	S	538697	5400418	2.7	21.1	26.1	86.0	10.0	11.5	i		0	į
D	2433.6	S	538697	5400759	2.1	7.1	38.2	58.7	6.0	8.3			0	ĺ
E	2427.8	S	538695	5400974	5.4	20.5	63.2	174.8	0.2	26.5	0.3	0	42	ĺ
F	2417.2	S?	538691	5401357	1.1	4.2	18.9	64.3	2.3	9.3			0	Ì
G	2388.4	S	538694	5402375	7.1	3.7	28.9	56.7	2.8	8.1	2.6	38	22	İ
LINE	30700		FLIGHT	9	 						 			
A	2221.5	S	538899	5399987	7.3	16.2	252.7	311.2	21.4	72.3	0.5	1	0	į
В	2227.3	L	538898	5400150	32.9	29.8	118.0	239.8	20.3	52.2	2.2	0	641	j
C	2232.1	S	538899	5400288	2.3	5.0	11.6	35.0	20.5	7.0			0	į
D	2242.4	S	538893	5400610	0.9	10.7	7.2	110.3	25.2	14.7			0	j
E	2249.1	S	538902	5400827	3.8	18.8	21.1	62.5	25.0	7.2	0.2	0	0	ĺ
F	2290.7	S	538910	5402286	7.2	13.6	81.8	164.8	4.4	22.2	0.6	1	0	
LINE	30710		FLIGHT	9	 						 			
A	2124.9	H	539103	5400006	17.4	23.1	282.6	317.2	13.7	84.8	1.1	5	0	i
В	2120.0	L	539106	5400198	21.4	27.2	35.4	290.0	2.0	46.9	1.3	0	214	i
c	2099.3	S	539103	5400980	5.1	6.1	13.8	73.8	9.8	9.4	0.8	26	0	i
D	2088.9	S	539109	5401367	3.9	14.7	47.9	218.6	5.5	29.5	0.3	0	43	i
E	2071.4		539092	5401986	10.9	16.1		112.0	2.8	28.3	0.9	7	0	i
F	2051.1	S	539097	5402625	10.1	16.4		282.6	5.4	55.4	0.8	11	11	j

CX = COAXIAL

CP = COPLANAR

EM Anomaly List

Line   Fid   Interp   XUTM   YUTM   Real   Quad   Quad   Real   Quad	
A	į
B	
B	į
D	į
E	į
F	į
G	į
LINE 30730	į
A	İ
B	
C	į
D	į
E	į
F	į
G 1603.4 S 539504 5402307   16.6 14.5 83.1 318.6 3.2 46.8   1.8 17   0     1589.1 S? 539518 5402739   15.7 12.1 197.5 234.4 1.5 54.2   2.0 12   16	į
H 1589.1 S? 539518 5402739   15.7 12.1 197.5 234.4 1.5 54.2   2.0 12   16   16   16   17   18   18   18   18   18   18   18	į
LINE 30740	į
A 1433.0 L 539686 5399617   0.0 11.1 122.2 200.8 10.1 45.0     0	į
B 1446.4 S 539697 5400023   10.4 14.9 212.2 221.7 8.2 66.0   0.9 17   319	į
	į
C 1458.0 L 539695 5400405   23.1 15.1 83.0 80.3 0.0 23.8   2.8 2   0	į
D 1477.2 S 539710 5401090   12.4 28.3 249.5 372.8 8.8 67.5   0.6 2   0	į
E 1495.4 S 539705 5401726   5.7 3.8 39.7 51.5 2.7 15.1   1.7 37   0	į
F 1513.6 S 539698 5402369   8.5 3.3 62.9 112.3 2.7 19.4   4.0 41   0	į
G 1525.4 S 539703 5402805   2.6 10.7 221.6 225.3 3.2 57.6     0	į
LINE 30750 FLIGHT 9	
A 1369.6 L 539909 5399594 23.3 9.8 15.1 25.3 8.1 4.8 5.0 9 0	į
B 1352.6 S 539904 5400210   15.8 16.8 154.2 142.3 6.7 42.1   1.4 6   0	į
C 1345.0 L 539904 5400503   22.4 20.3 4.2 142.0 5.6 4.7   1.9 0   0	į
D 1330.9 S 539894 5401043   11.1 15.9 194.6 195.0 11.8 49.8   0.9 3   0	į
E 1310.4 S 539899 5401747   3.9 7.8 39.0 84.3 2.3 15.3   0.5 12   169	į
F 1287.8 S 539900 5402471   4.0 6.4 148.7 177.5 7.2 50.1   0.6 28   0	İ
LINE 30760 FLIGHT 9	
A 1102.1 L 540111 5399578 25.5 6.8 19.6 3.7 9.1 4.3 9.8 14 0	İ

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Note:EM values shown above are local amplitudes

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

					   CX 55	00 HZ	CP 7	 200 HZ	CP	900 HZ	Vertical	Dike	   Mag. Corr	 
Labe	l Fid	Interp	MTUX e	YUTM	Real	Quad	Real	Quad	Real	Quad	COND I	DEPTH*		
			m	m	ppm	ppm	ppm	ppm	ppm	ppm	siemens	m	NT	
LINE	30760		FLIGHT	9	 						 		 	
В	1124.3	S	540103	5400249	8.3	15.1	110.4	185.3	6.6	39.2	0.6	12	0	
C	1132.0	L	540101	5400500	0.2		143.4	189.8	8.6	43.9			0	
D	1140.2	S	540096	5400789	10.1	19.1		117.9	12.3	13.8			0	
E	1149.0	S	540098	5401104	6.6	12.5	135.4	285.3	13.2	47.4	0.6	6	0	
F	1161.7	S	540100	5401542	7.3	5.5	58.1	77.9	2.1	16.8	1.6	22	70	
G	1170.7	S	540110	5401856	13.0	6.2		154.4	4.7	24.4	3.5	21	269	
H	1186.7	S	540085	5402426	4.8	4.9	108.7	161.9	5.2	39.8	1.0	34	0	
LINE	30770		FLIGHT	9	 						 		 	 
A	1028.8	L	540294	5399559	35.3	11.3	10.7	2.1	9.7	9.2	8.4	17	0	ĺ
В	1021.4	S	540304	5399809	7.7	4.6	114.3	170.6	1.6	30.3	2.2	26	191	
C	1011.3	S	540291	5400156	12.6	19.9	259.2	328.9	7.5	78.8	0.9	9	0	
D	1004.5	S	540282	5400401	8.3	17.5	174.2	199.8	9.6	40.3	0.6	0	0	
E	998.0	L	540276	5400623	18.5	14.4	11.7	98.8	7.4	4.4	2.1	0	0	
F	992.2	S	540281	5400817	10.2	23.6	62.6	142.4	7.7	23.2			0	
G	985.2	S	540268	5401056	10.2	14.8	7.6	39.6	2.5	4.5			0	
H	966.4	S	540300	5401711	0.6	15.1	147.1	165.9	4.4	37.0			311	ĺ
I	951.0	S	540300	5402228	16.8	30.4	135.7	183.2	4.9	45.5	0.8	0	0	
LINE	30780		FLIGHT	9	 						 		 	
İΑ	767.5	S	540499	5399838	11.1	10.7	152.8	142.4	5.2	44.9	1.4	10	138	į
В	779.0	S	540503	5400223	6.6	16.0	155.8	167.7	4.3	43.6	0.5	0	0	į
C	791.8	L	540490	5400656	42.7	18.6	122.4	60.0	11.5	32.3	5.9	0	0	į
D	797.8	S	540491	5400860	15.7	24.8	96.3	164.1	7.6	31.4	0.9	0	0	į
E	810.8	S	540521	5401298	1.6	6.2	9.8	46.9	6.0	6.2			0	ĺ
F	827.8	S	540513	5401903	0.0	2.8	103.0	8.0	7.6	21.5			0	ĺ
G	839.5	S	540500	5402319	21.1	19.9	71.3	129.9	2.0	25.0	1.8	2	175	İ
LINE	30790		FLIGHT	9	 						 		 	 
A	675.9	S	540701	5400047	10.5	11.1	73.6	36.9	4.0	18.7	1.2	16	0	į
В	661.6	S	540709	5400540	22.5	17.3	280.9	283.0	17.2	75.7	2.3	11	0	į
c	656.2	L	540711	5400726	51.4	19.2	157.5	130.8	20.9	50.8	7.7	0	0	į
D	648.8	S	540710	5400979	5.9	6.3	206.7	299.4	0.0	52.8	1.0	29	669	į
E	636.6	S	540692	5401419	8.4	32.4	189.1	429.8	13.3	64.9	0.4	0	0	į
F	617.1	S	540693	5402103	8.9	10.5	109.4	82.6	8.5	29.5	1.0	16	0	į
G	597.1	S?	540727	5402696	16.3	14.5	67.3	154.3	0.6	20.4	1.7	24	16	
														<del>-</del>

CP = COPLANAR

Note: EM values shown above are local amplitudes

EM Anomaly List

  Labe	l Fid	Inter	o XUTM m	YUTM m	   CX 55   Real   ppm	00 HZ Quad ppm	CP 7 Real	7200 HZ Quad ppm	CP Real ppm	900 HZ Quad ppm	Vertica COND siemens	 l Dike DEPTH* m	Mag. Corr     NT	
LINE	30800		 FLIGHT		 I						 I		 I	I
A	408.6	S	540913	5399562	   4.1	8.7	14.4	41.6	4.0	9.0	 		1 15	
B	425.4	S	540913	5399988	9.5	11.6	139.3	88.2	6.0	38.3	1.0	11	1 0	
I C	446.4	S	540906	5400591	16.6	15.0	156.3	207.0	7.0	48.2	1.7	1	) 0   0	
D	451.7	S L	540908	5400591	14.9	9.5	55.7	28.7	7.0	19.4	2.5	9	] 0	!
E	483.0	S	540908	5400749	14.9	17.4		178.7	4.7	29.7	1.2	5	0   734	!
E   F	500.4	S H	540918	5401770	5.2	1.1	92.3	9.9	9.2	28.2	1.2 		1 0	
	39010		FLIGHT										[	
A	5626.5	S	525540	5402001	4.7	14.2	58.1	142.0	1.4	21.0	0.4	0	15	ļ
В	5648.3	S	526345	5402001	0.5	1.8	54.0	82.5	4.0	20.4			48	
C	5662.7	S	526915	5401996	1.0	3.6	64.3	114.3	4.4	19.8			126	
D	5703.0	S?	528532	5402006	6.0	13.9	35.9	112.6	1.4	20.3	0.5	1	0	
E	5705.9	L	528641	5402010	23.2	22.9		185.5	11.6	43.6	1.7	2	202	
F	5711.0	S	528832	5402015	12.7	12.0	187.1	175.7	10.1	45.9	1.5	14	0	
G	5728.0	S	529480	5402002	0.3	12.4	10.5	74.3	2.8	10.4			0	
H	5750.5	S	530372	5402000	8.4	16.8	110.8	179.1	6.4	41.5	0.6	9	0	
Ι	5778.7	S	531508	5401998	2.8	7.7	131.4	195.6	6.1	36.7			0	
J	5835.1	S	533767	5402000	7.6	20.0	170.3	310.0	6.0	59.6	0.5	6	0	
K	5934.5	S	537382	5401999	8.5	25.4	125.4	277.5	2.1	48.4	0.4	0	0	
L	5983.8	S	539143	5402014	2.3	5.7	34.3	44.0	2.4	11.3			18	
M	6020.7	S	540543	5401999	0.9	3.7	36.5	34.3	1.4	10.7			0	
LINE	39020		FLIGHT	12	 I						 I		 I	
A	6622.2	S?	525033	5400012	1   7.8	4.9	108.0	54.4	19.9	29.7	2.1	38	409	
В	6607.7	S	525532	5400018	4.9	2.8	57.9	53.9	1.7	16.6			0	
İC	6562.2	Н	527053	5399997	1.1	2.0	15.3	22.0	11.7	11.3			0	
D	6527.1	S	528294	5400012	3.0	7.9	71.7	68.9	5.6	29.3	i		23	
E	6497.1	S	529429	5400006	1.9	4.2	58.5	44.0	3.4	18.2	i		0	
F	6477.8	S	530116	5400019	5.1	7.7	33.5	95.0	3.7	14.2	0.7	23	0	
G	6458.6	L	530780	5400015	6.7	10.6	53.3	79.7	20.3	9.3	0.7	11	289	
H	6424.7	L	531977	5399995	2.7	0.0	19.9	10.6	19.1	77.2			0	
li.	6419.0	L	532172	5400002	3.3	4.2	4.8	19.4	16.3	86.5	l 		0	
l ±  J	6399.0	S	532172	5399996	2.4	5.0	41.8	131.6	5.8	20.2	l 		0	
K	6375.4	S	533763	5400003	9.9	11.3	125.5	106.5	4.7	26.2	1.1	19	0	
L	6349.2	S	534759	5400003	6.2	10.2	40.8	104.4	2.2	16.1	0.6	19	21	
M	6299.5	S	536475	5399982	7.0	5.3	36.9	78.9	4.3	9.5	1.6	30	1 0	-
N N	6284.0	S	537022	5399999	7.0   9.8	23.2	32.2	79.2	2.5	12.0	1.6	0	1 0	
114					۰		JZ.Z						I	ا 

CX = COAXIAL

CP = COPLANAR

Note:EM values shown above are local amplitudes

<sup>\*</sup>Estimated Depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or magnetite/overburden effects

EM Anomaly List

  Labe	l Fid	Inter	MTUX or	YUTM	CX 55   Real	00 HZ Ouad	CP 7 Real	200 HZ Quad	CP Real	900 HZ Quad	Vertica   COND	l Dike DEPTH*	Mag. Corr	
	1 114	IIICCI	m m	m	ppm	ppm	ppm	ppm	ppm		siemens	m	   NT	İ
LINE	39020		FLIGHT	12	 						 		 	I
jo	6265.7	S	537664	5400011	13.3	16.8	198.5	399.5	1.2	67.5	1.1	10	j o	į
P	6246.7	S	538380	5400018	20.6	56.0	310.1	497.8	8.5	109.2	0.6	0	j o	į
ĺΩ	6238.4	L	538691	5399995	22.7	20.6	91.8	409.8	21.7	0.0	1.9	11	j o	į
R	6229.4	S	539032	5400000	7.7	21.0	168.0	428.4	2.3	72.1	0.5	10	0	j
S	6207.0	S	539874	5400013	5.9	11.2	103.0	237.0	4.3	46.6	0.6	20	j o	j
Т	6179.1	S	540935	5399993	4.1	0.8	122.8	87.2	6.4	34.3	i		0	İ
LINE	39030		FLIGHT	12	 						 		 	I
A	6762.8	S?	525022	5398019	7.8	10.1	87.5	111.5	2.1	32.8	0.9	16	j o	į
В	6777.2	S	525356	5398001	4.5	6.9	64.5	138.5	1.5	23.0	0.6	22	10	į
ĺС	6792.5	S	525810	5398013	1.7	1.0	42.1	72.5	0.3	14.0	i		j o	į
D	6803.9	S?	526209	5398008	5.8	13.6	32.0	64.7	1.8	11.3	0.5	6	18	į
E	6812.7	S	526540	5397996	0.3	11.9	88.9	199.9	2.8	33.0	j		j o	į
F	6819.6	S	526805	5397992	11.6	22.9	199.0	362.6	1.8	64.2	0.7	1	49	į
Ġ	6843.0	S	527627	5397996	6.6	25.2	134.2	367.8	2.9	54.6	0.3	0	13	j
H	6869.0	S	528594	5398016	7.5	13.4	100.1	190.2	7.3	33.9	0.6	15	91	ĺ
İΙ	6892.7	S	529459	5398007	17.9	26.2	211.1	376.3	4.1	66.5	1.0	1	j o	j
jЈ	6920.8	S	530470	5397997	27.9	56.7	252.1	533.8	3.1	87.4	0.9	0	14	į
K	6951.8	S	531552	5397996	3.5	9.6	59.9	155.1	2.5	21.6	0.4	12	8	į
Ĺ	6961.6	В	531906	5397997	58.4	158.5	592.3	1026.6	21.4	183.6	0.9	0	0	į
M	6981.0	S	532631	5398006	0.0	8.6	9.9	103.5	3.7	13.6	i		0	į
N	6989.9	S	532954	5397999	0.1	4.2	4.0	43.8	3.5	5.5			0	į
0	7000.7	S	533319	5398011	1.6	2.3	1.0	22.0	1.8	4.3			0	ĺ
P	7042.5	S	534784	5398006	0.0	3.0	2.2	11.7	3.5	1.9			0	ĺ

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CX = COAXIAL CP = COPLANAR

Note:EM values shown above are local amplitudes

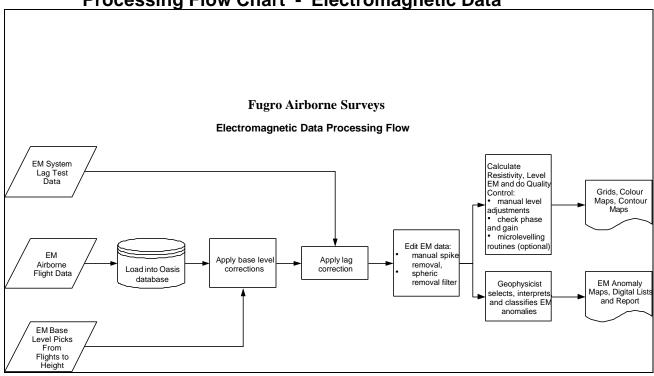
Area C

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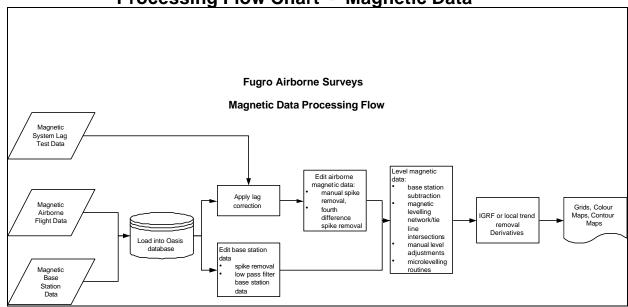
DATA PROCESSING FLOWCHARTS

# **APPENDIX E**

**Processing Flow Chart - Electromagnetic Data** 



**Processing Flow Chart - Magnetic Data** 



**APPENDIX F** 

**GLOSSARY** 

#### APPENDIX F

#### **GLOSSARY OF AIRBORNE GEOPHYSICAL TERMS**

Note: The definitions given in this glossary refer to the common terminology as used in airborne geophysics.

**altitude attenuation**: the absorption of gamma rays by the atmosphere between the earth and the detector. The number of gamma rays detected by a system decreases as the altitude increases.

**apparent-:** the **physical parameters** of the earth measured by a geophysical system are normally expressed as apparent, as in "apparent **resistivity**". This means that the measurement is limited by assumptions made about the geology in calculating the response measured by the geophysical system. Apparent resistivity calculated with **HEM**, for example, generally assumes that the earth is a **homogeneous half-space** – not layered.

**amplitude**: The strength of the total electromagnetic field. In *frequency domain* it is most often the sum of the squares of *in-phase* and *quadrature* components. In multicomponent electromagnetic surveys it is generally the sum of the squares of all three directional components.

**analytic signal**: The total amplitude of all the directions of magnetic *gradient*. Calculated as the sum of the squares.

**anisotropy**: Having different *physical parameters* in different directions. This can be caused by layering or fabric in the geology. Note that a unit can be anisotropic, but still **homogeneous**.

**anomaly**: A localized change in the geophysical data characteristic of a discrete source, such as a conductive or magnetic body: something locally different from the **background**.

**B-field**: In time-domain **electromagnetic** surveys, the magnetic field component of the (electromagnetic) **field**. This can be measured directly, although more commonly it is calculated by integrating the time rate of change of the magnetic field **dB/dt**, as measured with a receiver coil.

**background**: The "normal" response in the geophysical data – that response observed over most of the survey area. **Anomalies** are usually measured relative to the background. In airborne gamma-ray spectrometric surveys the term defines the **cosmic**, radon, and aircraft responses in the absence of a signal from the ground.

**base-level**: The measured values in a geophysical system in the absence of any outside signal. All geophysical data are measured relative to the system base level.

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**base frequency**: The frequency of the pulse repetition for a *time-domain electromagnetic* system. Measured between subsequent positive pulses.

**bird**: A common name for the pod towed beneath or behind an aircraft, carrying the geophysical sensor array.

**bucking**: The process of removing the strong **signal** from the **primary field** at the **receiver** from the data, to measure the **secondary field**. It can be done electronically or mathematically. This is done in **frequency-domain EM**, and to measure **on-time** in **time-domain EM**.

**calibration coil**: A wire coil of known size and dipole moment, which is used to generate a field of known **amplitude** and **phase** in the receiver, for system calibration. Calibration coils can be external, or internal to the system. Internal coils may be called Q-coils.

**coaxial coils**: **[CX]** Coaxial coils in an HEM system are in the vertical plane, with their axes horizontal and collinear in the flight direction. These are most sensitive to vertical conductive objects in the ground, such as thin, steeply dipping conductors perpendicular to the flight direction. Coaxial coils generally give the sharpest anomalies over localized conductors. (See also *coplanar coils*)

**coil**: A multi-turn wire loop used to transmit or detect electromagnetic fields. Time varying *electromagnetic* fields through a coil induce a voltage proportional to the strength of the field and the rate of change over time.

**compensation**: Correction of airborne geophysical data for the changing effect of the aircraft. This process is generally used to correct data in *fixed-wing time-domain electromagnetic* surveys (where the transmitter is on the aircraft and the receiver is moving), and magnetic surveys (where the sensor is on the aircraft, turning in the earth's magnetic field.

**component**: In *frequency domain electromagnetic* surveys this is one of the two **phase** measurements – *in-phase or quadrature*. In "multi-component" electromagnetic surveys it is also used to define the measurement in one geometric direction (vertical, horizontal inline and horizontal transverse – the Z, X and Y components).

**Compton scattering**: gamma ray photons will bounce off electrons as they pass through the earth and atmosphere, reducing their energy and then being detected by *radiometric* sensors at lower energy levels. See also *stripping*.

conductance: See conductivity thickness

**conductivity**: [s] The facility with which the earth or a geological formation conducts electricity. Conductivity is usually measured in milli-Siemens per metre (mS/m). It is the reciprocal of *resistivity*.

conductivity-depth imaging: see conductivity-depth transform.

**conductivity-depth transform**: A process for converting electromagnetic measurements to an approximation of the conductivity distribution vertically in the earth, assuming a *layered earth*. (Macnae and Lamontagne, 1987; Wolfgram and Karlik, 1995)

**conductivity thickness**: [st] The product of the *conductivity*, and thickness of a large, tabular body. (It is also called the "conductivity-thickness product") In electromagnetic geophysics, the response of a thin plate-like conductor is proportional to the conductivity multiplied by thickness. For example a 10 metre thickness of 20 Siemens/m mineralization will be equivalent to 5 metres of 40 S/m; both have 200 S conductivity thickness. Sometimes referred to as conductance.

**conductor**: Used to describe anything in the ground more conductive than the surrounding geology. Conductors are most often clays or graphite, or hopefully some type of mineralization, but may also be man-made objects, such as fences or pipelines.

**coplanar coils**: **[CP]** In HEM, the coplanar coils lie in the horizontal plane with their axes vertical, and parallel. These coils are most sensitive to massive conductive bodies, horizontal layers, and the *halfspace*.

**cosmic ray**: High energy sub-atomic particles from outer space that collide with the earth's atmosphere to produce a shower of gamma rays (and other particles) at high energies.

**counts** (per second): The number of *gamma-rays* detected by a gamma-ray *spectrometer*. The rate depends on the geology, but also on the size and sensitivity of the detector.

**culture**: A term commonly used to denote any man-made object that creates a geophysical anomaly. Includes, but not limited to, power lines, pipelines, fences, and buildings.

current channelling: See current gathering.

**current gathering**: The tendency of electrical currents in the ground to channel into a conductive formation. This is particularly noticeable at higher frequencies or early time channels when the formation is long and parallel to the direction of current flow. This tends to enhance anomalies relative to inductive currents (see also *induction*). Also known as current channelling.

daughter products: The radioactive natural sources of gamma-rays decay from the original "parent" element (commonly potassium, uranium, and thorium) to one or more lower-energy "daughter" elements. Some of these lower energy elements are also

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radioactive and decay further. *Gamma-ray spectrometry* surveys may measure the gamma rays given off by the original element or by the decay of the daughter products.

**dB/dt**: As the **secondary electromagnetic field** changes with time, the magnetic field [**B**] component induces a voltage in the receiving **coil**, which is proportional to the rate of change of the magnetic field over time.

decay: In *time-domain electromagnetic* theory, the weakening over time of the *eddy currents* in the ground, and hence the *secondary field* after the *primary field* electromagnetic pulse is turned off. In *gamma-ray spectrometry*, the radioactive breakdown of an element, generally potassium, uranium, thorium, or one of their *daughter* products.

decay constant: see time constant.

**decay series**: In *gamma-ray spectrometry*, a series of progressively lower energy *daughter products* produced by the radioactive breakdown of uranium or thorium.

**depth of exploration**: The maximum depth at which the geophysical system can detect the target. The depth of exploration depends very strongly on the type and size of the target, the contrast of the target with the surrounding geology, the homogeneity of the surrounding geology, and the type of geophysical system. One measure of the maximum depth of exploration for an electromagnetic system is the depth at which it can detect the strongest conductive target – generally a highly conductive horizontal layer.

**differential resistivity**: A process of transforming **apparent resistivity** to an approximation of layer resistivity at each depth. The method uses multi-frequency HEM data and approximates the effect of shallow layer **conductance** determined from higher frequencies to estimate the deeper conductivities (Huang and Fraser, 1996)

**dipole moment**: [NIA] For a transmitter, the product of the area of a *coil*, the number of turns of wire, and the current flowing in the coil. At a distance significantly larger than the size of the coil, the magnetic field from a coil will be the same if the dipole moment product is the same. For a receiver coil, this is the product of the area and the number of turns. The sensitivity to a magnetic field (assuming the source is far away) will be the same if the dipole moment is the same.

**diurnal**: The daily variation in a natural field, normally used to describe the natural fluctuations (over hours and days) of the earth's magnetic field.

**dielectric permittivity**: [e] The capacity of a material to store electrical charge, this is most often measured as the relative permittivity  $[\epsilon_r]$ , or ratio of the material dielectric to that of free space. The effect of high permittivity may be seen in HEM data at high frequencies over highly resistive geology as a reduced or negative *in-phase*, and higher *quadrature* data.

**drape**: To fly a survey following the terrain contours, maintaining a constant altitude above the local ground surface. Also applied to re-processing data collected at varying altitudes above ground to simulate a survey flown at constant altitude.

**drift**: Long-time variations in the base-level or calibration of an instrument.

**eddy currents**: The electrical currents induced in the ground, or other conductors, by a time-varying *electromagnetic field* (usually the *primary field*). Eddy currents are also induced in the aircraft's metal frame and skin; a source of *noise* in EM surveys.

**electromagnetic**: **[EM]** Comprised of a time-varying electrical and magnetic field. Radio waves are common electromagnetic fields. In geophysics, an electromagnetic system is one which transmits a time-varying *primary field* to induce *eddy currents* in the ground, and then measures the *secondary field* emitted by those eddy currents.

**energy window**: A broad spectrum of *gamma-ray* energies measured by a spectrometric survey. The energy of each gamma-ray is measured and divided up into numerous discrete energy levels, called windows.

**equivalent** (thorium or uranium): The amount of radioelement calculated to be present, based on the gamma-rays measured from a **daughter** element. This assumes that the **decay series** is in equilibrium – progressing normally.

**exposure rate**: in radiometric surveys, a calculation of the total exposure rate due to gamma rays at the ground surface. It is used as a measurement of the concentration of all the **radioelements** at the surface. See also: **natural exposure rate**.

**fiducial, or fid:** Timing mark on a survey record. Originally these were timing marks on a profile or film; now the term is generally used to describe 1-second interval timing records in digital data, and on maps or profiles.

**Figure of Merit**: **(FOM)** A sum of the 12 distinct magnetic noise variations measured by each of four flight directions, and executing three aircraft attitude variations (yaw, pitch, and roll) for each direction. The flight directions are generally parallel and perpendicular to planned survey flight directions. The FOM is used as a measure of the **manoeuvre noise** before and after **compensation**.

**fixed-wing**: Aircraft with wings, as opposed to "rotary wing" helicopters.

**footprint**: This is a measure of the area of sensitivity under the aircraft of an airborne geophysical system. The footprint of an *electromagnetic* system is dependent on the altitude of the system, the orientation of the transmitter and receiver and the separation between the receiver and transmitter, and the conductivity of the ground. The footprint of

a *gamma-ray spectrometer* depends mostly on the altitude. For all geophysical systems, the footprint also depends on the strength of the contrasting *anomaly*.

frequency domain: An *electromagnetic* system which transmits a *primary field* that oscillates smoothly over time (sinusoidal), inducing a similarly varying electrical current in the ground. These systems generally measure the changes in the *amplitude* and *phase* of the *secondary field* from the ground at different frequencies by measuring the *in-phase* and *quadrature* phase components. See also *time-domain*.

**full-stream data**: Data collected and recorded continuously at the highest possible sampling rate. Normal data are stacked (see **stacking**) over some time interval before recording.

**gamma-ray**: A very high-energy photon, emitted from the nucleus of an atom as it undergoes a change in energy levels.

**gamma-ray spectrometry**: Measurement of the number and energy of natural (and sometimes man-made) gamma-rays across a range of photon energies.

**gradient**: In magnetic surveys, the gradient is the change of the magnetic field over a distance, either vertically or horizontally in either of two directions. Gradient data is often measured, or calculated from the total magnetic field data because it changes more quickly over distance than the **total magnetic field**, and so may provide a more precise measure of the location of a source. See also **analytic signal**.

**ground effect**: The response from the earth. A common calibration procedure in many geophysical surveys is to fly to altitude high enough to be beyond any measurable response from the ground, and there establish **base levels** or **backgrounds**.

**half-space**: A mathematical model used to describe the earth – as infinite in width, length, and depth below the surface. The most common halfspace models are *homogeneous* and *layered earth*.

**heading error**: A slight change in the magnetic field measured when flying in opposite directions.

**HEM**: Helicopter ElectroMagnetic, This designation is most commonly used for helicopter-borne, *frequency-domain* electromagnetic systems. At present, the transmitter and receivers are normally mounted in a *bird* carried on a sling line beneath the helicopter.

**herringbone pattern**: A pattern created in geophysical data by an asymmetric system, where the **anomaly** may be extended to either side of the source, in the direction of flight. Appears like fish bones, or like the teeth of a comb, extending either side of centre, each tooth an alternate flight line.

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**homogeneous**: This is a geological unit that has the same *physical parameters* throughout its volume. This unit will create the same response to an HEM system anywhere, and the HEM system will measure the same apparent *resistivity* anywhere. The response may change with system direction (see *anisotropy*).

**HTEM**: Helicopter Time-domain ElectroMagnetic, This designation is used for the new generation of helicopter-borne, *time-domain* electromagnetic systems.

**in-phase**: the component of the measured **secondary field** that has the same phase as the transmitter and the **primary field**. The in-phase component is stronger than the **quadrature** phase over relatively higher **conductivity**.

**induction**: Any time-varying electromagnetic field will induce (cause) electrical currents to flow in any object with non-zero *conductivity*. (see *eddy currents*)

induction number: also called the "response parameter", this number combines many of the most significant parameters affecting the *EM* response into one parameter against which to compare responses. For a *layered earth* the response parameter is mwsh<sup>2</sup> and for a large, flat, *conductor* it is mwsth, where m is the *magnetic permeability*, w is the angular *frequency*, s is the *conductivity*, t is the thickness (for the flat conductor) and h is the height of the system above the conductor.

**inductive limit**: When the frequency of an EM system is very high, or the **conductivity** of the target is very high, the response measured will be entirely **in-phase** with no **quadrature** (**phase** angle =0). The in-phase response will remain constant with further increase in conductivity or frequency. The system can no longer detect changes in conductivity of the target.

**infinite**: In geophysical terms, an "infinite' dimension is one much greater than the **footprint** of the system, so that the system does not detect changes at the edges of the object.

**International Geomagnetic Reference Field:** [IGRF] An approximation of the smooth magnetic field of the earth, in the absence of variations due to local geology. Once the IGRF is subtracted from the measured magnetic total field data, any remaining variations are assumed to be due to local geology. The IGRF also predicts the slow changes of the field up to five years in the future.

**inversion**, or **inverse modeling**: A process of converting geophysical data to an earth model, which compares theoretical models of the response of the earth to the data measured, and refines the model until the response closely fits the measured data (Huang and Palacky, 1991)

**layered earth**: A common geophysical model which assumes that the earth is horizontally layered – the *physical parameters* are constant to *infinite* distance horizontally, but change vertically.

**magnetic permeability**: [m] This is defined as the ratio of magnetic induction to the inducing magnetic field. The relative magnetic permeability  $[\mu_r]$  is often quoted, which is the ratio of the rock permeability to the permeability of free space. In geology and geophysics, the **magnetic susceptibility** is more commonly used to describe rocks.

**magnetic susceptibility**: **[k]** A measure of the degree to which a body is magnetized. In SI units this is related to relative *magnetic permeability* by  $k=\mu_r-1$ , and is a dimensionless unit. For most geological material, susceptibility is influenced primarily by the percentage of magnetite. It is most often quoted in units of  $10^{-6}$ . In HEM data this is most often apparent as a negative *in-phase* component over high susceptibility, high *resistivity* geology such as diabase dikes.

**manoeuvre noise:** variations in the magnetic field measured caused by changes in the relative positions of the magnetic sensor and magnetic objects or electrical currents in the aircraft. This type of noise is generally corrected by magnetic **compensation**.

**model**: Geophysical theory and applications generally have to assume that the geology of the earth has a form that can be easily defined mathematically, called the model. For example steeply dipping **conductors** are generally modeled as being **infinite** in horizontal and depth extent, and very thin. The earth is generally modeled as horizontally layered, each layer infinite in extent and uniform in characteristic. These models make the mathematics to describe the response of the (normally very complex) earth practical. As theory advances, and computers become more powerful, the useful models can become more complex.

**natural exposure rate**: in radiometric surveys, a calculation of the total exposure rate due to natural-source gamma rays at the ground surface. It is used as a measurement of the concentration of all the natural **radioelements** at the surface. See also: **exposure rate**.

**noise**: That part of a geophysical measurement that the user does not want. Typically this includes electronic interference from the system, the atmosphere (*sferics*), and manmade sources. This can be a subjective judgment, as it may include the response from geology other than the target of interest. Commonly the term is used to refer to high frequency (short period) interference. See also *drift*.

**Occam's inversion**: an *inversion* process that matches the measured *electromagnetic* data to a theoretical model of many, thin layers with constant thickness and varying resistivity (Constable et al, 1987).

**off-time**: In a *time-domain electromagnetic* survey, the time after the end of the *primary field pulse*, and before the start of the next pulse.

**on-time**: In a *time-domain electromagnetic* survey, the time during the *primary field pulse*.

**overburden**: In engineering and mineral exploration terms, this most often means the soil on top of the unweathered bedrock. It may be sand, glacial till, or weathered rock.

**Phase, phase angle**: The angular difference in time between a measured sinusoidal electromagnetic field and a reference – normally the primary field. The phase is calculated from tan<sup>-1</sup>(*in-phase* / *quadrature*).

**physical parameters**: These are the characteristics of a geological unit. For electromagnetic surveys, the important parameters are **conductivity**, **magnetic permeability** (or **susceptibility**) and **dielectric permittivity**; for magnetic surveys the parameter is magnetic susceptibility, and for gamma ray spectrometric surveys it is the concentration of the major radioactive elements: potassium, uranium, and thorium.

permittivity: see dielectric permittivity.

permeability: see magnetic permeability.

**primary field**: the EM field emitted by a transmitter. This field induces **eddy currents** in (energizes) the conductors in the ground, which then create their own **secondary fields**.

**pulse**: In time-domain EM surveys, the short period of intense *primary* field transmission. Most measurements (the *off-time*) are measured after the pulse. **On-time** measurements may be made during the pulse.

**quadrature**: that component of the measured **secondary field** that is phase-shifted 90° from the **primary field**. The quadrature component tends to be stronger than the **in-phase** over relatively weaker **conductivity**.

Q-coils: see calibration coil.

**radioelements**: This normally refers to the common, naturally-occurring radioactive elements: potassium (K), uranium (U), and thorium (Th). It can also refer to man-made radioelements, most often cobalt (Co) and cesium (Cs)

radiometric: Commonly used to refer to gamma ray spectrometry.

**radon**: A radioactive daughter product of uranium and thorium, radon is a gas which can leak into the atmosphere, adding to the non-geological background of a gamma-ray spectrometric survey.

**receiver**: the **signal** detector of a geophysical system. This term is most often used in active geophysical systems – systems that transmit some kind of signal. In airborne **electromagnetic** surveys it is most often a **coil**. (see also, **transmitter**)

**resistivity**: [r] The strength with which the earth or a geological formation resists the flow of electricity, typically the flow induced by the **primary field** of the electromagnetic transmitter. Normally expressed in ohm-metres, it is the reciprocal of **conductivity**.

**resistivity-depth transforms**: similar to **conductivity depth transforms**, but the calculated **conductivity** has been converted to **resistivity**.

**resistivity section**: an approximate vertical section of the resistivity of the layers in the earth. The resistivities can be derived from the **apparent resistivity**, the **differential resistivities**, **resistivity-depth transforms**, or **inversions**.

Response parameter: another name for the induction number.

**secondary field**: The field created by conductors in the ground, as a result of electrical currents induced by the *primary field* from the *electromagnetic* transmitter. Airborne *electromagnetic* systems are designed to create and measure a secondary field.

**Sengpiel section**: a *resistivity section* derived using the *apparent resistivity* and an approximation of the depth of maximum sensitivity for each frequency.

**sferic**: Lightning, or the *electromagnetic* signal from lightning, it is an abbreviation of "atmospheric discharge". These appear to magnetic and electromagnetic sensors as sharp "spikes" in the data. Under some conditions lightning storms can be detected from hundreds of kilometres away. (see *noise*)

**signal**: That component of a measurement that the user wants to see – the response from the targets, from the earth, etc. (See also *noise*)

**skin depth**: A measure of the depth of penetration of an electromagnetic field into a material. It is defined as the depth at which the primary field decreases to 1/e of the field at the surface. It is calculated by approximately  $503 \times \sqrt{\text{(resistivity/frequency)}}$ . Note that depth of penetration is greater at higher *resistivity* and/or lower *frequency*.

**spectrometry**: Measurement across a range of energies, where *amplitude* and energy are defined for each measurement. In gamma-ray spectrometry, the number of gamma rays are measured for each energy *window*, to define the *spectrum*.

**spectrum**: In *gamma ray spectrometry*, the continuous range of energy over which gamma rays are measured. In *time-domain electromagnetic* surveys, the spectrum is the energy of the **pulse** distributed across an equivalent, continuous range of frequencies.

spheric: see sferic.

**stacking**: Summing repeat measurements over time to enhance the repeating *signal*, and minimize the random *noise*.

**stripping**: Estimation and correction for the gamma ray photons of higher and lower energy that are observed in a particular *energy window*. See also *Compton scattering*.

susceptibility: See magnetic susceptibility.

tau: [t] Often used as a name for the time constant.

TDEM: time domain electromagnetic.

**thin sheet**: A standard model for electromagnetic geophysical theory. It is usually defined as a thin, flat-lying conductive sheet, *infinite* in both horizontal directions. (see also *vertical plate*)

**tie-line**: A survey line flown across most of the *traverse lines*, generally perpendicular to them, to assist in measuring *drift* and *diurnal* variation. In the short time required to fly a tie-line it is assumed that the drift and/or diurnal will be minimal, or at least changing at a constant rate.

**time constant**: The time required for an *electromagnetic* field to decay to a value of 1/e of the original value. In *time-domain* electromagnetic data, the time constant is proportional to the size and *conductance* of a tabular conductive body. Also called the decay constant.

**Time channel**: In *time-domain electromagnetic* surveys the decaying *secondary field* is measured over a period of time, and the divided up into a series of consecutive discrete measurements over that time.

**time-domain**: **Electromagnetic** system which transmits a pulsed, or stepped **electromagnetic** field. These systems induce an electrical current (**eddy current**) in the ground that persists after the **primary field** is turned off, and measure the change over time of the **secondary field** created as the currents **decay**. See also **frequency-domain**.

**total energy envelope**: The sum of the squares of the three **components** of the **time-domain electromagnetic secondary field**. Equivalent to the **amplitude** of the secondary field.

**transient**: Time-varying. Usually used to describe a very short period pulse of *electromagnetic* field.

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**transmitter**. The source of the **signa** to be measured in a geophysical survey. In airborne **EM** it is most often a **coil** carrying a time-varying electrical current, transmitting the **primary field**. (see also **receiver**)

**traverse line**: A normal geophysical survey line. Normally parallel traverse lines are flown across the property in spacing of 50 m to 500 m, and generally perpendicular to the target geology.

**vertical plate**: A standard model for electromagnetic geophysical theory. It is usually defined as thin conductive sheet, *infinite* in horizontal dimension and depth extent. (see also *thin sheet*)

waveform: The shape of the *electromagnetic pulse* from a *time-domain* electromagnetic transmitter.

**window**: A discrete portion of a **gamma-ray spectrum** or **time-domain electromagnetic decay**. The continuous energy spectrum or **full-stream** data are grouped into windows to reduce the number of samples, and reduce **noise**.

Version 1.5, November 29, 2005 Greg Hodges, Chief Geophysicist Fugro Airborne Surveys, Toronto

# - Appendix F.13 -

## Common Symbols and Acronyms

**k** Magnetic susceptibility

e Dielectric permittivity

m, m<sub>r</sub> Magnetic permeability, relative permeability

r, r<sub>a</sub> Resistivity, apparent resistivity

s,s<sub>a</sub> Conductivity, apparent conductivity

st Conductivity thickness

t Tau, or time constant

Wm ohm-metres, units of resistivity

**AGS** Airborne gamma ray spectrometry.

CDT Conductivity-depth transform, conductivity-depth imaging (Macnae and

Lamontagne, 1987; Wolfgram and Karlik, 1995)

CPI, CPQ Coplanar in-phase, quadrature

**CPS** Counts per second

CTP Conductivity thickness product

CXI, CXQ Coaxial, in-phase, quadrature

**FOM** Figure of Merit

fT femtoteslas, normal unit for measurement of B-Field

**EM** Electromagnetic

**keV** kilo electron volts – a measure of gamma-ray energy

**MeV** mega electron volts – a measure of gamma-ray energy 1MeV = 1000keV

**NIA** dipole moment: turns x current x Area

**nT** nanotesla, a measure of the strength of a magnetic field

nG/h nanoGreys/hour – gamma ray dose rate at ground level

**ppm** parts per million – a measure of secondary field or noise relative to the primary or radioelement concentration.

pT/s picoteslas per second: Units of decay of secondary field, dB/dt

**S** siemens – a unit of conductance

**x**: the horizontal component of an EM field parallel to the direction of flight.

y: the horizontal component of an EM field perpendicular to the direction of flight.

**z**: the vertical component of an EM field.

# - Appendix F.14 -

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