# REPORT ON A HELICOPTER-BORN VERSATILE TIME DOMAIN ELECTROMACNETIC (VTEM) AND AEROMAGNETIC GEOPHYSICAL SURVEY

Misehkow River Project

Pickle Lake, Ontario/

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Survey flown during September 2009

Project 8161

November, 2009

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# REPORT ON A HELICOPTER-BORNE VERSATILE TIME DOMAIN ELECTROMAGNETIC SURVEY

Misehkow River Project Pickle Lake, Ontario

# **Executive Summary**

During September 10<sup>th</sup> to 20<sup>th</sup>, 2009 Geotech Ltd. carried out a helicopter-borne geophysical survey over the Misehkow River Project situated near the town of Pickle Lake in Ontario, Canada.

Principal geophysical sensors included a versatile time domain electromagnetic (VTEM) system, and a caesium magnetometer. Ancillary equipment included a GPS navigation system and a radar altimeter. A total of 786 line-kilometres were flown.

The survey operations were based out of the town of Pickle Lake located in the province of Ontario. In-field data quality assurance and preliminary processing were carried out on a daily basis during the acquisition phase. Preliminary and final data processing, including generation of final digital data and map products were undertaken from the office of Geotech Ltd. in Aurora, Ontario.

The processed survey results are presented as electromagnetic stacked profiles of the B-field Z Component and dB/dt X and Z Components, and as colour grids of a B-Field Z Component Channel, and Total Magnetic Intensity.

Digital data includes all electromagnetic and magnetic products, plus ancillary data including the waveform.

The survey report describes the procedures for data acquisition, processing, final image presentation and the specifications for the digital data set. No Interpretation summary is included with this report.



#### 1. INTRODUCTION

#### 1.1 General Considerations

Geotech Ltd. performed a helicopter-borne geophysical survey over the Misehkow River Project located near the town of Pickle Lake in the province of Ontario, Canada (Figure 1).

Jim Parres, President and CEO, acted on behalf of Jiminex Inc. during the data acquisition and data processing phases of this project.

The geophysical surveys consisted of helicopter borne EM using the versatile time-domain electromagnetic (VTEM) system with Z and X component measurements and aeromagnetics using a caesium magnetometer. A total of 786 line-km of geophysical data were acquired during the survey. The survey area is shown in Figure 2 and 3.

The crew was based out of Pickle Lake, Ontario for the acquisition phase of the survey. Survey flying started on September 10<sup>th</sup> and was completed on September 20<sup>th</sup>, 2009.

Data quality control and quality assurance, and preliminary data processing were carried out on a daily basis during the acquisition phase of the project. Final data processing followed immediately after the end of the survey. Final reporting, data presentation and archiving were completed from the Aurora office of Geotech Ltd. in November, 2009.



Figure 1 - Property Location



# 1.2 Survey and System Specifications

The Misehkow River Project (51° 8'39.30"N, 89°37'21.14"W) is located approximately 53 kilometres south-east of the town of Pickle Lake, Ontario (Figure 2).

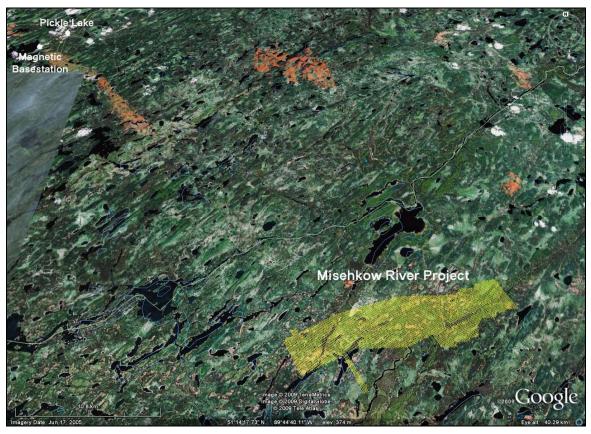
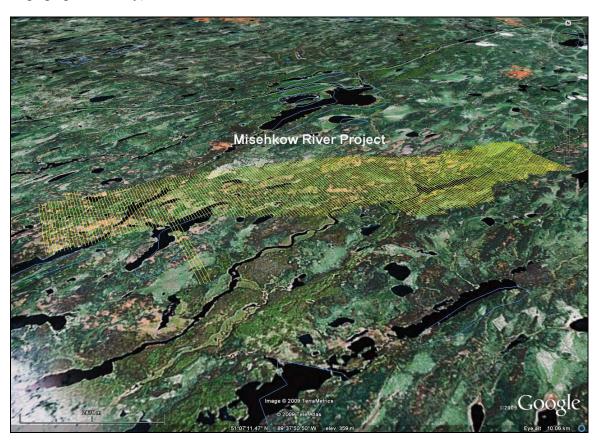


Figure 2 – Misehkow River Project, showing the magnetic base station location on Google Earth.

The Misehkow River Project was flown in a northwest to southeast (N 155° E / N 335° E) direction with a traverse line spacing of 100 metres, as depicted in Figure 3. Tie lines were flown perpendicular to the traverse lines at a spacing of 1000 metres in a southwest to northeast (N 65° E / N 225° E) direction. For more detailed information on the flight spacing and direction see Table 1.

#### 1.3 Topographic Relief and Cultural Features

Topographically, the Misehkow River Project exhibits a moderate relief, with an elevation ranging from 335 to 489 metres above sea level over an area of 41 square kilometres (see Figure 3). The survey block is covered with numerous small lakes and wetlands, with some rivers and streams connecting the various small water features. There is one notable Lake, Webb Lake, along the south-western portion of the survey block. Running directly thru the eastern portion of the block is the Misehkow River, running from the northeast to the southwest. There are no visible roads or trails running within the survey area; however special care is recommended in identifying any other potential cultural features from other sources that might be recorded in the data. The survey block covers 19 Ontario mining claims, which are shown in Appendix A. The survey block is covered by NTS (National Topographic Survey) of Canada sheets 052P03 and 052P04.



**Figure 3** – Misehkow River Project flight path over a Google Earth Image.

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# 2. DATA ACQUISITION

# 2.1 Survey Area

The survey blocks (see Figure 3 and Appendix A) and general flight specifications are as follows:

Table 1 - Survey Specifications

Survey block	Traverse Line spacing (m)	Area (Km²)	Planned <sup>1</sup> Line-km	Actual Line-km	Flight direction	Line numbers
Misehkow	Traverse: 100	71.5	712.2	718.4	N 155° E / N 335° E	L510 - L2390
River Project	Tie: 1000		73.8	74.5	N 65° E / N 225° E	T3010 - T3070
TOTAL		71.5	786	792.9		

Survey block boundaries co-ordinates are provided in Appendix B.

# 2.2 Survey Operations

Survey operations were based out of the Birchville Motel in the Town of Pickle Lake, Ontario on August 30<sup>th</sup>, 2009. The following table shows the timing of the flying.

Table 2 - Survey schedule

Date	Flight #	Flown km	Block	Crew location	Comments
09-10-2009				Pickle Lake	System Installation
09-11-2009				Pickle Lake	System Installation
09-12-2009				Pickle Lake	System Installation
09-13-2009				Pickle Lake	Test Flight
09-14-2009	1,2	185.5	Misehkow	Pickle Lake	Production
09-15-2009	3,4	184.8	Misehkow	Pickle Lake	Production
09-16-2009				Pickle Lake	No Production due to weather
09-17-2009				Pickle Lake	No Production due to weather
09-18-2009	5	145.6	Misehkow	Pickle Lake	Production
09-19-2009	6,7	252.2	Misehkow	Pickle Lake	Production
09-20-2009	8	17.6	Misehkow	Pickle Lake	Production – job complete

<sup>&</sup>lt;sup>1</sup> Note: Actual Line kilometres represent the total line kilometres in the final database. These line-km normally exceed the Planned line-km, as indicated in the survey NAV files



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#### 2.3 Flight Specifications

During the survey of the Misehkow River Project the helicopter was maintained at a mean height of 76 metres above the ground with a nominal survey speed of 80 km/hour. This allowed for a nominal EM sensor terrain clearance of 45 metres and a magnetic sensor clearance of 63 metres.

The data recording rates of the data acquisition was 0.1 second for electromagnetics, magnetometer and 0.2 second for altimeter and GPS. This translates to a geophysical reading about every 2 metres along flight track. Navigation was assisted by a CDGPS receiver and data acquisition system, which reports GPS co-ordinates as latitude/longitude and directs the pilot over a pre-programmed survey grid.

The operator was responsible for monitoring of the system integrity. He also maintained a detailed flight log during the survey, tracking the times of the flight as well as any unusual geophysical or topographic feature.

On return of the aircrew to the base camp the survey data was transferred from a compact flash card (PCMCIA) to the data processing computer. The data were then uploaded via ftp to the Geotech office in Aurora for daily quality assurance and quality control by qualified personnel, operating remotely.

#### 2.4 Aircraft and Equipment

#### 2.4.1 Survey Aircraft

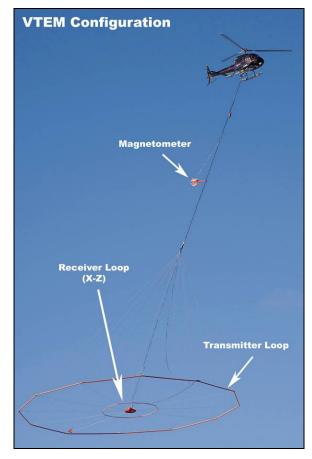
The survey was flown using a Euro copter Aerospatiale (Astar) 350 B3 helicopter, registration C-GEOY. The helicopter is owned by Geotech Ltd. and operated by Gateway Helicopters Ltd. out if North Bay, Ontario. Installation of the geophysical and ancillary equipment was carried out by Geotech Ltd.

#### 2.4.2 Electromagnetic System

The electromagnetic system was a Geotech Time Domain EM (VTEM) system. The configuration is as indicated in Figure 4 below.

The standard VTEM Receiver and transmitter coils are concentric-coplanar and Z-direction oriented. The receiver system for the project also included a coincident-coaxial X-direction sensor to measure the in-line dB/dt and calculate B-Field responses. All loops were towed at a mean distance of 35 metres below the aircraft as shown in Figures 4 and 6. The receiver decay recording scheme is shown diagrammatically in Figure 5





**Figure 4 -** VTEM Configuration, with magnetometer.

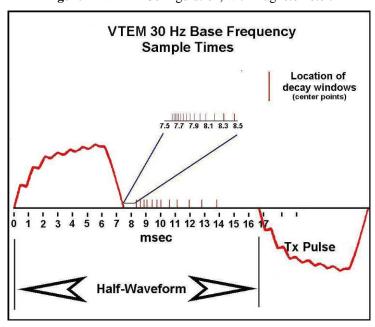


Figure 5 - VTEM Waveform & Sample Times



The VTEM decay sampling scheme is shown in Table 3 below. Twenty-four time measurement gates were used for the final data processing in the range from 120 to 6578  $\mu$  sec², as shown in Table 5.

Table 3 - Decay Sampling Scheme

VTEM Decay Sampling scheme						
Array						
Index	Time Gate	Start	End	Width		
0	5	0	10	10		
1	16	10	21	11		
2	21	16	26	10		
3	31	26	37	11		
4	42	37	47	10		
5	52	47	57	10		
6	62	57	68	11		
7	73	68	78	11		
8	83	78	91	13		
9	99	91	110	19		
10	120	110	131	21		
11	141	131	154	24		
12	167	154	183	29		
13	198	183	216	34		
14	234	216	258	42		
15	281	258	310	53		
16	339	310	373	63		
17	406	373	445	73		
18	484	445	529	84		
19	573	529	628	99		
20	682	628	750	123		
21	818	750	896	146		
22	974	896	1063	167		
23	1151	1063	1261	198		
24	1370	1261	1506	245		
25	1641	1506	1797	292		
26	1953	1797	2130	333		
27	2307	2130	2526	396		
28	2745	2526	3016	490		
29	3286	3016	3599	583		
30	3911	3599	4266	667		
31	4620	4266	5058	792		
32	5495	5058	6037	979		
33	6578	6037	7203	1167		
34	7828	7203	8537	1334		
35	9245	8537	10120	1584		

<sup>&</sup>lt;sup>2</sup> Note: Measurement times-delays are referenced to time-zero marking the end of the transmitter current turn-off, as illustrated in Figure 5 and Appendix C.



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#### VTEM system parameters:

#### **Transmitter Section**

- Transmitter coil diameter: 26 m

- Number of turns: 4

- Transmitter base frequency: 30 Hz

Peak current: 188.4 APulse width: 7.14 msDuty cycle: 43 %

Wave form shape: trapezoid
 Peak dipole moment: 400, 100 nIA
 Nominal terrain clearance: 45 metres

#### **Receiver Section**

# X-Coil

- X Coil diameter: 0.32 m - Number of turns: 245

- Effective coil area: 19.69 m<sup>2</sup>

**Z-Coil** 

Z-Coil coil diameter: 1.2 mNumber of turns: 100

- Effective coil area: 113.04 m<sup>2</sup>

#### Magnetometer

- Nominal terrain clearance: 63 metres

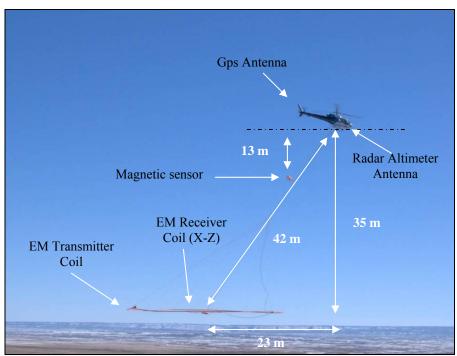


Figure 6 - VTEM System Configuration

#### 2.4.3 Airborne magnetometer

The magnetic sensor utilized for the survey was a Geometrics optically pumped caesium vapour magnetic field sensor, mounted on the EM bird, 13 metres below the helicopter, as shown in Figure 6. The sensitivity of the magnetic sensor is 0.02 nanoTesla (nT) at a sampling interval of 0.1 seconds. The magnetometer sends the measured magnetic field strength as nanoTesla to the data acquisition system via the RS-232 port.

#### 2.4.4 Radar Altimeter

A Terra TRA 3000/TRI 40 radar altimeter was used to record terrain clearance. The antenna was mounted beneath the bubble of the helicopter cockpit (Figure 6).

## 2.4.5 GPS Navigation System

The navigation system used was a Geotech PC104 based navigation system utilizing a NovAtel's CDGPS (Canada-Wide Differential Global Positioning System Correction Service) enable OEM4-G2-3151W GPS receiver, Geotech navigate software, a full screen display with controls in front of the pilot to direct the flight and an NovAtel GPS antenna mounted on the helicopter tail (Figure 6). As many as 11 GPS and two CDGPS satellites may be monitored at any one time. The positional accuracy or circular error probability (CEP) is 1.8 m, with CDGPS active, it is 1.0 m. The co-ordinates of the block were set-up prior to the survey and the information was fed into the airborne navigation system.

# 2.4.6 Digital Acquisition System

A Geotech data acquisition system recorded the digital survey data on an internal compact flash card. Data is displayed on an LCD screen as traces to allow the operator to monitor the integrity of the system. The data type and sampling interval as provided in Table 4.

Table 4 - Acquisition Sampling Rates

DATA TYPE	SAMPLING
TDEM	0.1 sec
Magnetometer	0.1 sec
GPS Position	0.2 sec
Radar Altimeter	0.2 sec



#### 2.5 Base Station

A combined magnetometer/GPS base station was utilized on this project. A Geometrics Caesium vapour magnetometer was used as a magnetic sensor with a sensitivity of 0.001 nT. The base station was recording the magnetic field together with the GPS time at 1 Hz on a base station computer.

The base station magnetometer sensor was installed 300 metres north-east of the Winston Motor Hotel (51° 27'58.7' N, 90° 11'59.1' W); away from electric transmission lines and moving ferrous objects such as motor vehicles (see Figure 2). The base station data were backed-up to the data processing computer at the end of each survey day.



#### 3. PERSONNEL

The following Geotech Ltd. personnel were involved in the project.

Field: Project Manager: Lee Harper (office) Data QA/QC: Neil Fiset (office) Crew chief: Roger LeBlanc **System Operators:** Joseph Florjancic The survey pilot and the mechanical engineer were employed directly by the helicopter operator – Gateway Helicopters Inc. / Geotech Ltd. Pilot: Stephanie Rivard Office: Preliminary Data Processing: Neil Fiset Final Data Processing: Neil Fiset Final Data QA/QC: Harish Kumar

Data acquisition phase was carried out under the supervision of Andrei Bagrianski, P. Geo, Surveys Manager. Processing phase was carried out under the supervision of Gord Smith, Manager of Data Processing. The overall contract management and customer relations were by Quentin Yarie, P.Geo.

Eric Steffler



Reporting/Mapping:

#### 4. DATA PROCESSING AND PRESENTATION

Data compilation and processing were carried out by the application of Geosoft OASIS Montaj and programs proprietary to Geotech Ltd.

## 4.1 Flight Path

The flight path, recorded by the acquisition program as WGS 84 latitude/longitude, was converted into the NAD83 Datum, UTM Zone 16 North coordinate system in Oasis Montaj.

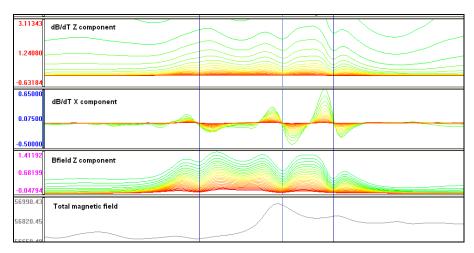
The flight path was drawn using linear interpolation between x, y positions from the navigation system. Positions are updated every second and expressed as UTM easting's (x) and UTM northing's (y).

# 4.2 Electromagnetic Data

A three stage digital filtering process was used to reject major sferic events and to reduce system noise. Local sferic activity can produce sharp, large amplitude events that cannot be removed by conventional filtering procedures. Smoothing or stacking will reduce their amplitude but leave a broader residual response that can be confused with geological phenomena. To avoid this possibility, a computer algorithm searches out and rejects the major sferic events. The filter used was a 16 point non-linear filter.

The signal to noise ratio was further improved by the application of a low pass linear digital filter. This filter has zero phase shift which prevents any lag or peak displacement from occurring, and it suppresses only variations with a wavelength less than about 1 second or 15 metres. This filter is a symmetrical 1 sec linear filter.

The results are presented as stacked profiles of EM voltages for the time gates, in linear logarithmic scale for the B-field Z component and dB/dt responses in the Z and X components. B-field Z component time channel recorded at 3.911 milliseconds after the termination of the impulse is also presented as contour color image.



**Figure 7 -** VTEM Z and X Component data.



Generalized modeling results of VTEM data, are shown in Appendix E.

Graphical representations of the VTEM transmitter input current and the output voltage of the receiver coil are shown in Appendix C.

#### **VTEM X Component Polarity**

VTEM X component data do not exhibit maxima or minima above conductors; in fact they produce cross-over type anomalies (Figure 7). The crossover polarity sign convention for VTEM X component polarity is according to the right hand rule for multi-component transient electromagnetic methods.

For the northwest to southeast lines of the Misehkow River Project the sign convention for the X in-line component crossover is positive-negative pointing northwest to southeast for tabular conductor's perpendicular to the profile (Figure 8). Similarly, for the north-south tie lines, the X Component polarity is positive to negative pointing southwest to northeast. X component data for alternating/opposite flight directions have been reversed (multiplied by negative one) in the final database to account for this polarity convention.

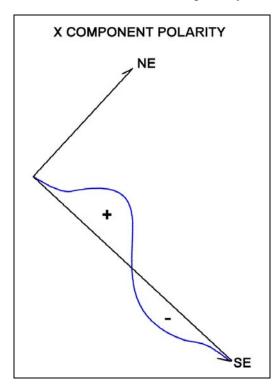


Figure 8 - VTEM X Component Polarity Convention for the Misehkow River Project.

# 4.3 Magnetic Data

The processing of the magnetic data involved the correction for diurnal variations by using the digitally recorded ground base station magnetic values. The base station magnetometer data was edited and merged into the Geosoft GDB database on a daily basis. The aeromagnetic data was corrected for diurnal variations by subtracting the observed magnetic base station deviations.

Tie line levelling was carried out by adjusting intersection points along traverse lines. A micro-levelling procedure was applied to remove persistent low-amplitude components of flight-line noise remaining in the data.

The corrected magnetic data was interpolated between survey lines using a random point gridding method to yield x-y grid values for a standard grid cell size of approximately 0.125 cm at the mapping scale. The Minimum Curvature algorithm was used to interpolate values onto a rectangular regular spaced grid.



#### 5. DELIVERABLES

# 5.1 Survey Report

The survey report describes the data acquisition, processing, and final presentation of the survey results. The survey report is provided in two paper copies and digitally in PDF format.

# 5.2 Maps

Final maps were produced at scale of 1:20,000 for best representation of the survey size and line spacing. The coordinate/projection system used was NAD 83, UTM Zone 16 North. All maps show the flight path trace and topographic data; latitude and longitude are also noted on maps. Mineral claims, provided by the Ontario Ministry of Northern Development and Mines, are also presented on each map.

The preliminary and final results of the survey are presented as EM profiles, a late-time gate gridded EM channels, and color magnetic TMI contour maps. The following maps are presented on paper;

- VTEM B-field Z Component profiles, Time Gates 0.234 6.578 ms in linear logarithmic scale over Total Magnetic Intensity color grid.
- VTEM dB/dt profiles Z Component, Time Gates 0.234 6.578 ms in linear logarithmic scale.
- VTEM dB/dt profiles X Component, Time Gates 0.234 6.578 ms in linear logarithmic scale.
- VTEM B-field late time Z Component Channel 30, Time Gate 3.911 ms color image.
- Total magnetic intensity (TMI) color image and contours.

#### 5.3 Digital Data

- Two copies of the data and maps on DVD were prepared to accompany the report. Each DVD contains a digital file of the line data in GDB Geosoft Montaj format as well as the maps in Geosoft Montaj Map and PDF format.
- DVD structure.

**Data** contains databases, grids and maps, as described below. **Report** contains a copy of the report and appendices in PDF

format.

Databases in Geosoft GDB format, containing the channels listed in Table 5.

**Table 5 -** Geosoft GDB Data Format.

Channel name	Units	Description
X:	metres	NAD83 / UTM zone 16N
Y:	metres	NAD83 / UTM zone 16N



Channel name	Units	Description
Lat:	Decimal Degrees	WGS 84 Latitude data
Lon:	Decimal Degrees	WGS 84 Longitude data
Z:	metres	GPS antenna elevation (Geoid)
Gtime:	Seconds of the day	GPS time
Radar:	metres	helicopter terrain clearance from radar altimeter
Radarb:	metres	EM bird terrain clearance from radar altimeter
DEM:	metres	Digital Elevation Model
Basemag:	nT	Magnetic diurnal variation data
Mag1:	nT	Raw Total Magnetic field data
Mag2:	nT	Diurnal corrected Total Magnetic field data
Mag3:	nT	Levelled Total Magnetic field data
BFz[10]:	$(pV*ms)/(A*m^4)$	Z B-field 120 microsecond time channel
BFz[11]:	(pV*ms)/(A*m4)	Z B-field 141 microsecond time channel
BFz[12]:	(pV*ms)/(A*m <sup>4</sup> )	Z B-field 167 microsecond time channel
BFz[13]:	$(pV*ms)/(A*m^4)$	Z B-field 198 microsecond time channel
BFz[14]:	$(pV*ms)/(A*m^4)$	Z B-field 234 microsecond time channel
BFz[15]:	$(pV*ms)/(A*m^4)$	Z B-field 281 microsecond time channel
BFz[16]:	$(pV*ms)/(A*m^4)$	Z B-field 339 microsecond time channel
BFz[17]:	(pV*ms)/(A*m4)	Z B-field 406 microsecond time channel
BFz[18]:	(pV*ms)/(A*m4)	Z B-field 484 microsecond time channel
BFz[19]:	$(pV*ms)/(A*m^4)$	Z B-field 573 microsecond time channel
BFz[20]:	$(pV*ms)/(A*m^4)$	Z B-field 682 microsecond time channel
BFz[21]:	$(pV*ms)/(A*m^4)$	Z B-field 818 microsecond time channel
BFz[22]:	$(pV*ms)/(A*m^4)$	Z B-field 974 microsecond time channel
BFz[23]:	$(pV*ms)/(A*m^4)$	Z B-field 1151 microsecond time channel
BFz[24]:	$(pV*ms)/(A*m^4)$	Z B-field 1370 microsecond time channel
BFz[25]:	$(pV*ms)/(A*m^4)$	Z B-field 1641 microsecond time channel
BFz[26]:	(pV*ms)/(A*m <sup>4</sup> )	Z B-field 1953 microsecond time channel
BFz[27]:	$(pV*ms)/(A*m^4)$	Z B-field 2307 microsecond time channel
BFz[28]:	$(pV*ms)/(A*m^4)$	Z B-field 2745 microsecond time channel
BFz[29]:	$(pV*ms)/(A*m^4)$	Z B-field 3286 microsecond time channel
BFz[30]:	$(pV*ms)/(A*m^4)$	Z B-field 3911 microsecond time channel
BFz[31]:	$(pV*ms)/(A*m^4)$	Z B-field 4620 microsecond time channel
BFz[32]:	(pV*ms)/(A*m4)	Z B-field 5495 microsecond time channel
BFz[33]:	$(pV*ms)/(A*m^4)$	Z B-field 6578 microsecond time channel
SFz[10]:	$pV/(A*m^4)$	Z dB/dt 120 microsecond time channel
SFz[11]:	$pV/(A*m^4)$	Z dB/dt 141 microsecond time channel
SFz[12]:	$pV/(A*m^4)$	Z dB/dt 167 microsecond time channel
SFz[13]:	$pV/(A*m^4)$	Z dB/dt 198 microsecond time channel
SFz[14]:	$pV/(A*m^4)$	Z dB/dt 234 microsecond time channel
SFz[15]:	$pV/(A*m^4)$	Z dB/dt 281 microsecond time channel
SFz[16]:	$pV/(A*m^4)$	Z dB/dt 339 microsecond time channel
SFz[17]:	$pV/(A*m^4)$	Z dB/dt 406 microsecond time channel
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SFz[19]:	$pV/(A*m^4)$	Z dB/dt 573 microsecond time channel
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SFz[23]:	$pV/(A*m^4)$	Z dB/dt 1151 microsecond time channel
SFz[24]:	$pV/(A*m^4)$	Z dB/dt 1370 microsecond time channel
SFz[25]:	pV/(A*m <sup>4</sup> )	Z dB/dt 1641 microsecond time channel
SFz[26]:	$pV/(A*m^4)$	Z dB/dt 1953 microsecond time channel



Channel name	Units	Description
SFz[27]:	$pV/(A*m^4)$	Z dB/dt 2307 microsecond time channel
SFz[28]:	$pV/(A*m^4)$	Z dB/dt 2745 microsecond time channel
SFz[29]:	$pV/(A*m^4)$	Z dB/dt 3286 microsecond time channel
SFz[30]:	$pV/(A*m^4)$	Z dB/dt 3911 microsecond time channel
SFz[31]:	$pV/(A*m^4)$	Z dB/dt 4620 microsecond time channel
SFz[32]:	$pV/(A*m^4)$	Z dB/dt 5495 microsecond time channel
SFz[33]:	$pV/(A*m^4)$	Z dB/dt 6578 microsecond time channel
BFx[13]:	(pV*ms)/(A*m4)	X B-field 198 microsecond time channel
BFx[14]:	(pV*ms)/(A*m4)	X B-field 234 microsecond time channel
BFx[15]:	(pV*ms)/(A*m4)	X B-field 281 microsecond time channel
BFx[16]:	$\frac{(pV*ms)/(A*m^4)}{(pV*ms)/(A*m^4)}$	X B-field 339 microsecond time channel
BFx[17]:	(pV*ms)/(A*m4)	X B-field 406 microsecond time channel
BFx[18]:	(pV*ms)/(A*m4)	X B-field 484 microsecond time channel
BFx[19]:	(pV*ms)/(A*m4)	X B-field 573 microsecond time channel
BFx[20]:	$\frac{(pV^*ms)/(A^*m^4)}{(pV^*ms)/(A^*m^4)}$	X B-field 682 microsecond time channel
BFx[21]:	$\frac{(pV^*ms)/(A^*m^4)}{(pV^*ms)/(A^*m^4)}$	X B-field 818 microsecond time channel
BFx[21]:	$\frac{(pV \text{ ms})/(A \text{ m})}{(pV*\text{ms})/(A*\text{m}^4)}$	X B-field 974 microsecond time channel
BFx[22]:	$\frac{(pV^*ms)/(A^*m^4)}{(pV^*ms)/(A^*m^4)}$	X B-field 174 inicrosecond time channel  X B-field 1151 microsecond time channel
BFx[24]:	$\frac{(pV^*ms)/(A^*m^4)}{(pV^*ms)/(A^*m^4)}$	X B-field 1370 microsecond time channel
BFx[25]:	$\frac{(pV^*ms)/(A^*m^4)}{(pV^*ms)/(A^*m^4)}$	X B-field 1641 microsecond time channel
BFx[26]:	$\frac{(pV \text{ ms})/(A \text{ m})}{(pV*\text{ms})/(A*\text{m}^4)}$	X B-field 1953 microsecond time channel
BFx[27]:	$\frac{(pV ms)/(A m)}{(pV*ms)/(A*m^4)}$	X B-field 2307 microsecond time channel
BFx[28]:	$\frac{(pV \text{ ms})/(A \text{ m})}{(pV*\text{ms})/(A*\text{m}^4)}$	X B-field 2745 microsecond time channel
BFx[29]:	$\frac{(pV^*ms)/(A^*m^4)}{(pV^*ms)/(A^*m^4)}$	X B-field 3286 microsecond time channel
BFx[30]:	$\frac{(pV \text{ ms})/(A \text{ m})}{(pV*\text{ms})/(A*\text{m}^4)}$	X B-field 3911 microsecond time channel
BFx[31]:	$\frac{(pV \text{ ms})/(A \text{ m})}{(pV*\text{ms})/(A*\text{m}^4)}$	X B-field 4620 microsecond time channel
BFx[31]. BFx[32]:	$\frac{(pV^*ms)/(A^*m^4)}{(pV^*ms)/(A^*m^4)}$	X B-field 4020 microsecond time channel  X B-field 5495 microsecond time channel
BFx[32]:	$\frac{(pV^*ms)/(A^*m^4)}{(pV^*ms)/(A^*m^4)}$	X B-field 5473 microsecond time channel  X B-field 6578 microsecond time channel
SFx[13]:	$pV/(A*m^4)$	X dB/dt 198 microsecond time channel
SFx[14]:	$\frac{pV/(A^*m^4)}{pV/(A^*m^4)}$	X dB/dt 178 microsecond time channel
SFx[14].	$pV/(A^*m^4)$	X dB/dt 281 microsecond time channel
SFx[15]. SFx[16]:	$pV/(A^*m^4)$	X dB/dt 281 microsecond time channel
SFx[10]. SFx[17]:	$pV/(A^*m^4)$	X dB/dt 406 microsecond time channel
SFx[17]. SFx[18]:	$pV/(A^*m^4)$	X dB/dt 484 microsecond time channel
SFx[19]:	$\frac{pV/(A^*m^4)}{pV/(A^*m^4)}$	X dB/dt 444 inicrosecond time channel  X dB/dt 573 microsecond time channel
SFx[19]:	$pV/(A^*m^4)$ $pV/(A^*m^4)$	X dB/dt 575 inicrosecond time channel  X dB/dt 682 microsecond time channel
SFx[20]. SFx[21]:	$pV/(A^*m^4)$	X dB/dt 818 microsecond time channel
SFx[21]. SFx[22]:	$pV/(A^*m^4)$	X dB/dt 974 microsecond time channel
SFx[22]:	$pV/(A^*m^4)$	X dB/dt 9/4 inicrosecond time channel  X dB/dt 1151 microsecond time channel
SFx[23]. SFx[24]:	$pV/(A^*m^4)$ $pV/(A^*m^4)$	X dB/dt 1331 microsecond time channel  X dB/dt 1370 microsecond time channel
SFx[24]. SFx[25]:	$pV/(A^*m^4)$	X dB/dt 1570 microsecond time channel  X dB/dt 1641 microsecond time channel
SFx[25]. SFx[26]:	$pV/(A^*m^4)$	X dB/dt 1953 microsecond time channel
SFx[20]. SFx[27]:	$pV/(A^*m^4)$	X dB/dt 1933 microsecond time channel  X dB/dt 2307 microsecond time channel
SFx[27]. SFx[28]:	$pV/(A^*m^4)$ $pV/(A^*m^4)$	X dB/dt 2345 microsecond time channel
SFx[29]:	pV/(A*m')	X dB/dt 2743 microsecond time channel  X dB/dt 3286 microsecond time channel
SFx[29]. SFx[30]:	$pV/(A^*m^4)$	X dB/dt 3280 inicrosecond time channel
SFx[30]. SFx[31]:	$pV/(A^*m^4)$	X dB/dt 4620 microsecond time channel
SFx[31]. SFx[32]:	$pV/(A^*m^4)$	X dB/dt 5495 microsecond time channel
SFx[32]. SFx[33]:	$pV/(A*m^4)$	X dB/dt 5493 microsecond time channel  X dB/dt 6578 microsecond time channel
SFx Rev	$pV/(A^*m^4)$	X dB/dt cos/8 inicrosecond time channels X dB/dt reversed data for time channels 10 to 33
BFx Rev	$\frac{\text{pV/(A^*III')}}{\text{(pV*ms)/(A*m}^4)}$	X B-field reversed data for time channels 10 to 33
PLM:	(pv ms)/(A m)	60 Hz power line monitor
LIVI.		00 11z power filie monitor



Electromagnetic B-field and dB/dt data is found in array channel format between indexes 10-33, as described above.

• Database of the VTEM Waveform "8161\_Waveform.gdb" in Geosoft GDB format, containing the following channels:

Time: Sampling rate interval, 10.416 microseconds Rx\_Volt: Output voltage of the receiver coil (Volt) Tx Current: Output current of the transmitter (Amp)

• Grids in Geosoft GRD format, as follows:

BFz30: B-Field Z Component Channel 30 (Time Gate 3.911 ms)

TMI: Total magnetic intensity (nT)

A Geosoft .GRD file has a .GI metadata file associated with it, containing grid projection information. A grid cell size of 25 metres was used.

• Maps at 1:20,000 in Geosoft MAP format, as follows:

8161 20k Misehkow Bfieldz: B-field Z Component profiles, Time Gates 0.234 –

6.578 ms in linear - logarithmic scale over Total

Magnetic Intensity color grid s.

8161\_20k\_Misehkow\_dBdtz: dB/dt profiles Z Component, Time Gates 0.234 -

6.578 ms in linear – logarithmic scale.

8161\_20k\_Misehkow\_dBdtx: dB/dt profiles X Component, Time Gates 0.234 –

6.578 ms in linear – logarithmic scale.

8161\_20k\_Misehkow\_BF3911: B-field late time Z Component Channel 30, Time

Gate 13.911 ms color image.

8161 20k Misehkow TMI: Total magnetic intensity (TMI) color image and

contours.

Maps are also presented in PDF format.

1:50,000 topographic vectors were derived from the NRC (Natural Resources Canada) NTDB (National Topographic Database) on the Geogratis webpage; <a href="http://geogratis.gc.ca/geogratis/en/index.html">http://geogratis.gc.ca/geogratis/en/index.html</a>. Ontario Mining claims were derived from the Ontario Ministry of Northern Development and Mines. <a href="http://www.claimaps.mndm.gov.on.ca">http://www.claimaps.mndm.gov.on.ca</a>

• A Google Earth file, 8161\_Misehkow\_Final.kmz, showing the flight path of the block is included. Free versions of Google Earth software from: http://earth.google.com/download-earth.html



#### 6. CONCLUSIONS AND RECOMMENDATIONS

#### 6.1 Conclusions

A helicopter-borne versatile time domain electromagnetic (VTEM) geophysical survey has been completed over the Misehkow River Project near the town of Pickle Lake, Ontario

The total area coverage is 71.5 km<sup>2</sup>. Total survey line coverage is 786 line kilometres. The principal sensors included a Time Domain EM system and a magnetometer. Results have been presented as stacked profiles, and contour color images at a scale of 1:20,000. No interpretative discussion is included in this report.

#### 6.2 Recommendations

Based on the geophysical results obtained, a number of interesting EM anomalies were identified across the property. The magnetic results may also contain worthwhile information in support of exploration targets of interest. We therefore recommend a detailed interpretation of the available geophysical data, in conjunction with the geology. It should include 2D - 3D inversion modeling analyses and magnetic derivative analysis prior to ground follow up and drill testing.

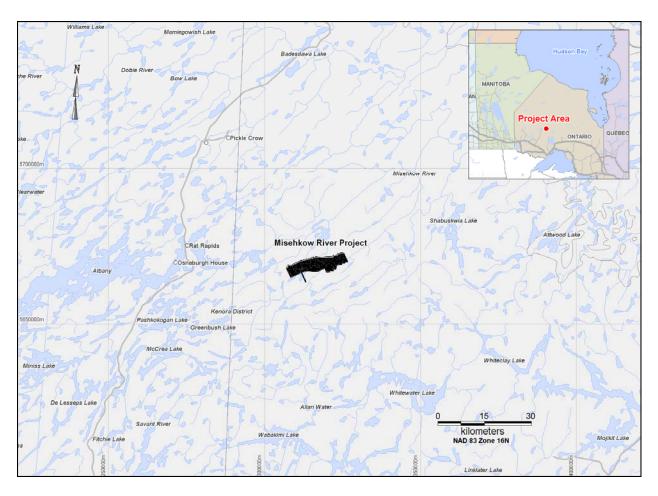
Respectfully submitted <sup>6</sup> ,	
Eric Steffler Geotech Ltd.	Jean Legault, P. Geo, P. Eng Geotech Ltd.
Will St	
Neil Fiset	Gord Smith

<sup>&</sup>lt;sup>6</sup> Final data processing of the EM and magnetic data were carried out by Neil Fiset, from the office of Geotech Ltd. in Aurora, Ontario, under the supervision of Gord Smith, Manager of Data Processing and Interpretation, and Jean Legault, P. Geo, P. Eng, Chief Geophysicists (Interpretation).

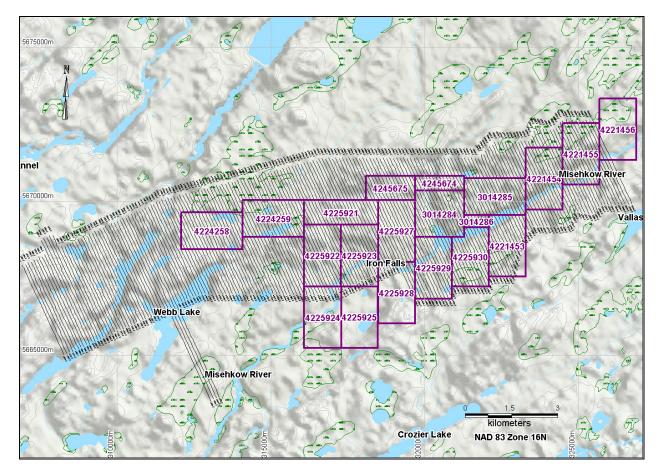


# **APPENDIX A**

# **SURVEY BLOCK LOCATION MAP**



**Survey Overview of the Misehkow River Project** 



Misehkow River Project Flight Path over Ontario Mining Claims.

# **APPENDIX B**

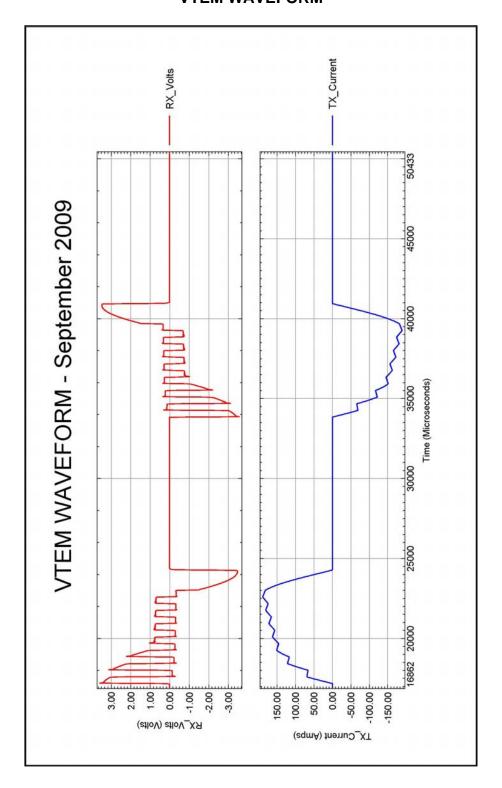
# **SURVEY BLOCK COORDINATES**

(NAD 83, UTM Zone 16 North)

Misehkow				
Х	Υ			
311500	5670050			
316700	5671400			
323286	5671400			
324486	5671742			
324486	5672542			
325600	5672542			
326800	5670000			
325586	5670000			
324486	5670502			
324486	5669742			
323286	5669742			
322800	5667562			
322086.5	5667562			
322087.5	5667242			
320887.5	5667242			
320887.5	5666842			
319650	5666842			
319100	5667950			
317000	5667000			
316000	5667000			
312725	5667000			
311950	5666700			
313400	5663700			
313000	5663500			
311600	5666500			
308250	5665000			
306900	5667900			
307699.7	5668274			
307488.4	5668727			
308032.4	5668981			
308243.6	5668528			

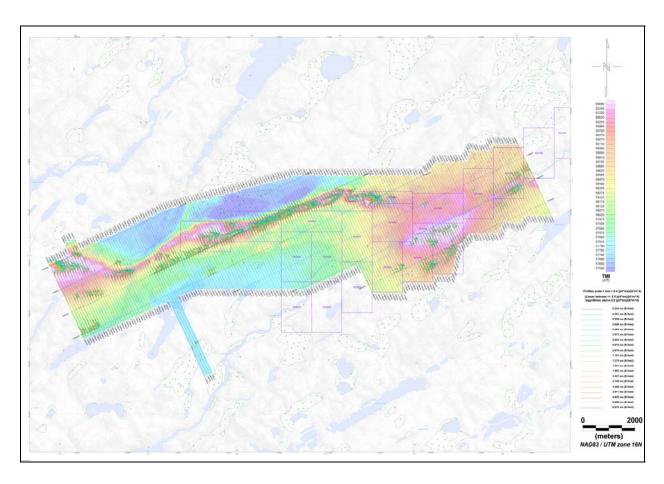


# APPENDIX C VTEM WAVEFORM



# **APPENDIX D**

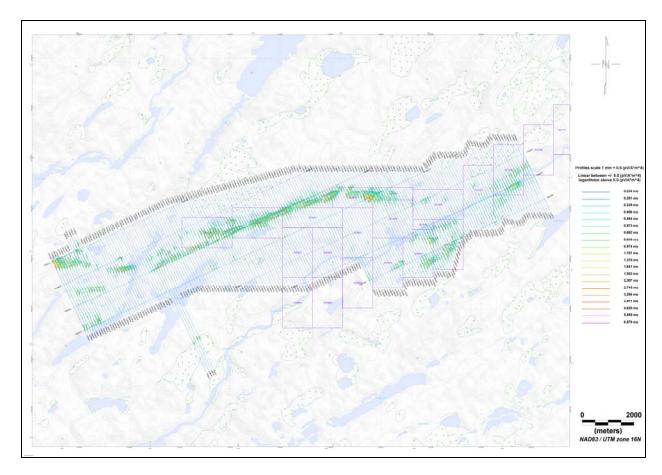
# GEOPHYSICAL MAPS<sup>1</sup>



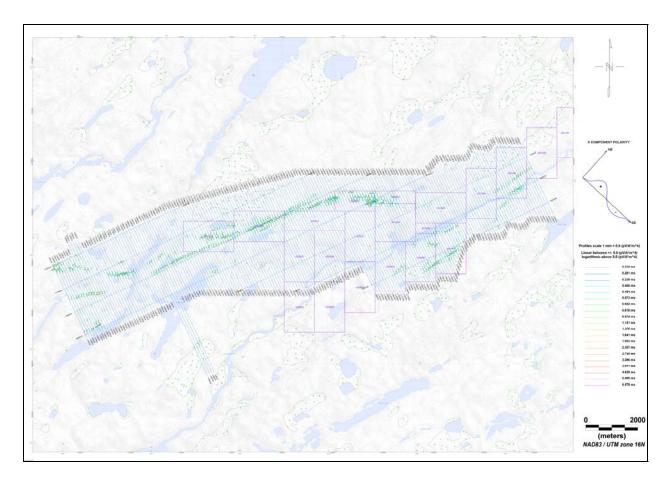
Misehkow Property - VTEM B-Field Z Component Profiles, Time Gates 0.234 to 6.578 ms.

<sup>&</sup>lt;sup>1</sup>Full size geophysical maps are also available in PDF format on the final DVD

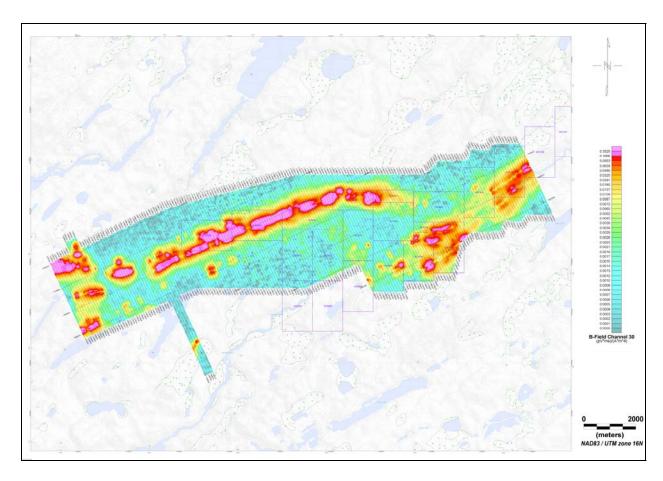




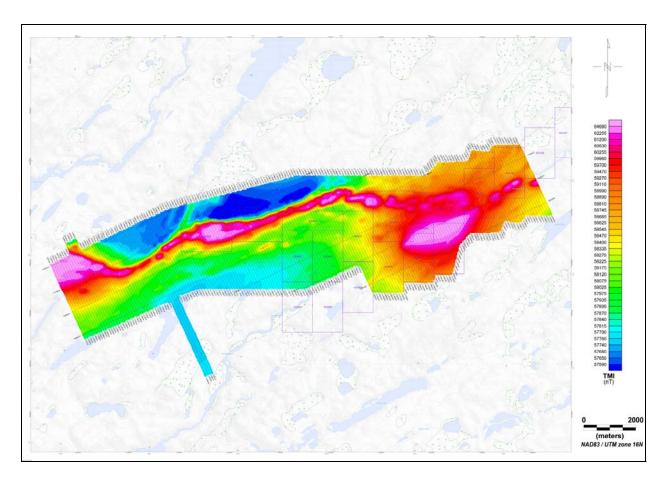
Misehkow Property - VTEM dB/dt Z Component Profiles, Time Gates 0.234 to 6.578 ms.



Misehkow Property - VTEM dB/dt X Component Profiles, Time Gates 0.234 to 6.578 ms.



Misehkow Property - VTEM B-Field Z Component Channel 30, Time Gate 3.911 ms.



Misehkow Property – Total Magnetic Intensity (TMI).

#### APPENDIX E

#### GENERALIZED MODELING RESULTS OF THE VTEM SYSTEM

#### Introduction

The VTEM system is based on a concentric or central loop design, whereby, the receiver is positioned at the centre of a 26.1 metres diameter transmitter loop that produces a dipole moment up to 400, 100 nIA at peak current. The wave form is a bi-polar, modified square wave with a turn-on and turn-off at each end. With a base frequency of 30 Hz, the duration of each pulse is approximately 7.14 milliseconds followed by an off time where no primary field is present.

During turn-on and turn-off, a time varying field is produced (dB/dt) and an electro-motive force (emf) is created as a finite impulse response. A current ring around the transmitter loop moves outward and downward as time progresses. When conductive rocks and mineralization are encountered, a secondary field is created by mutual induction and measured by the receiver at the centre of the transmitter loop.

Measurements are made during the on and off-time, when only the secondary field (representing the conductive targets encountered in the ground) is present.

Efficient modeling of the results can be carried out on regularly shaped geometries, thus yielding close approximations to the parameters of the measured targets. The following is a description of a series of common models made for the purpose of promoting a general understanding of the measured results.

# **General Modeling Concepts**

A set of models has been produced for the Geotech VTEM® system with explanation notes (see models E1 to E18). The Maxwell <sup>TM</sup> modeling program (EMIT Technology Pty. Ltd. Midland, WA, AU) used to generate the following responses assumes a resistive half-space. The reader is encouraged to review these models, so as to get a general understanding of the responses as they apply to survey results. While these models do not begin to cover all possibilities, they give a general perspective on the simple and most commonly encountered anomalies.

- When producing these models, a few key points were observed and are worth noting as follows:
  - For near vertical and vertical plate models, the top of the conductor is always located directly under the centre low point between the two shoulders in the classic **M** shaped response.
  - As the plate is positioned at an increasing depth to the top, the shoulders of the **M** shaped response, have a greater separation distance.
  - When faced with choosing between a flat lying plate and a prism model to represent the target (broad response) some ambiguity is present and caution should be exercised.



• With the concentric loop system and Z-component receiver coil, virtually all types of conductors and most geometries are most always well coupled and a response is generated (see Figures E17 & E18). Only concentric loop systems can map such wide varieties of target geometries.

#### **Variation of Plate Depth**

Geometries represented by plates of different strike length, depth extent, dip, plunge and depth below surface can be varied with characteristic parameters like conductance of the target, conductance of the host and conductivity/thickness and thickness of the overburden layer.

Diagrammatic models for a vertical plate are shown in Figures E-1 & E-2 and E-5 & E-6 at two different depths, all other parameters remaining constant. With this transmitter-receiver geometry, the classic **M** shaped response is generated. Figures E-1 and E-2 show a plate where the top is near surface. Here, amplitudes of the duel peaks are higher and symmetrical with the zero centre positioned directly above the plate. Most important is the separation distance of the peaks. This distance is small when the plate is near surface and widens with a linear relationship as the plate (depth to top) increases. Figures E-5 and E-6 show a much deeper plate where the separation distance of the peaks is much wider and the amplitudes of the channels have decreased.

#### **Variation of Plate Dip**

As the plate dips and departs from the vertical position, the peaks become asymmetrical. Figures E-3 & E-4 and E-7 and E-8 show a near surface plate dipping 80° at two different depths. Note that the direction of dip is toward the high shoulder of the response and the top of the plate remains under the centre minimum.

As the dip increases, the aspect ratio (Min/Max) decreases and this aspect ratio can be used as an empirical guide to dip angles from near 90° to about 30°. The method is not sensitive enough where dips are less than about 30°. For example, for a plate dipping 45°, the minimum shoulder starts to vanish. In Figures E-9 & E-10 and E-11 & E-12, a flat lying plate is shown, relatively near surface. Note that the twin peak anomaly has been replaced by a symmetrical shape with large, bell shaped, channel amplitudes which decay relative to the conductance of the plate.

In the special case where two plates are positioned to represent a synclinal structure. Note that the main characteristic is that the centre amplitudes are higher (approximately double) compared to the high shoulder of a single plate. This model is very representative of tightly folded formations where the conductors where once flat lying.



# **Variation of Prism Dip**

Finally, with thicker, prism models, another algorithm is required to represent current on the plate. A plate model is considered to be infinitely thin with respect to thickness and incapable of representing the current in the thickness dimension. A prism model is constructed to deal with this problem, thereby, representing the thickness of the body more accurately.

Figures E-13 & E-14 and E-15 & E-16 show the same prism at the same depths with variable dips. Aside from the expected differences asymmetry prism anomalies show a characteristic change from a double-peaked anomaly to single peak signatures.

#### I. THIN PLATE

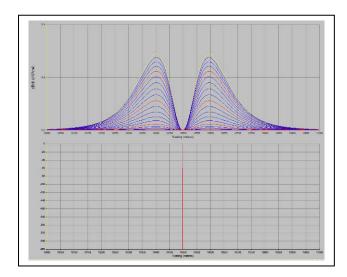


Figure E-1: dB/dt response of a shallow vertical thin plate. Depth=100 m, CT=20 S. The EM response is normalized by the dipole moment and the Rx area.

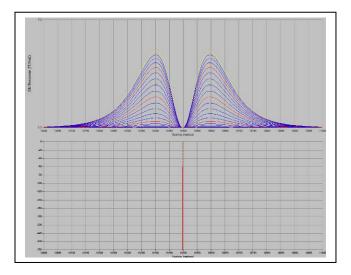


Figure E-2: B-field response of a shallow vertical thin plate. Depth=100 m, CT=20 S. The EM response is normalized by the dipole moment.

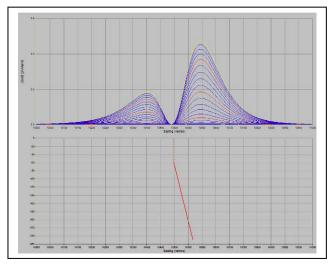


Figure E-3: dB/dt response of a shallow skewed thin plate. Depth=100 m, CT=20 S. The EM response is normalized by the dipole moment and the Rx area.

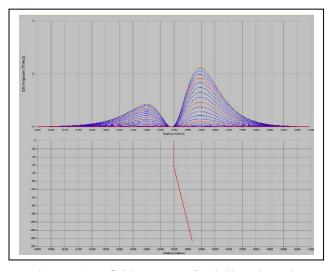
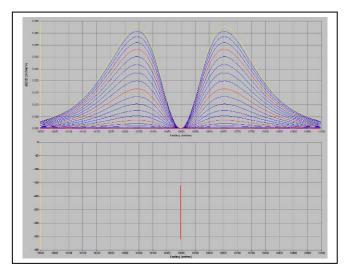


Figure E-4: B-field response of a shallow skewed thin plate. Depth=100 m, CT=20 S. The EM response is normalized by the dipole moment.



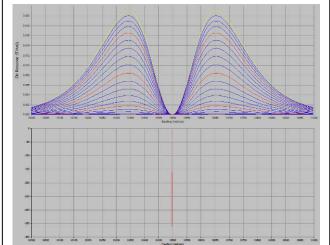


Figure E-5: dB/dt response of a deep vertical thin plate. Depth=200 m, CT=20 S. The EM response is normalized by the dipole moment and the Rx area.

Figure E-6: B-Field response of a deep vertical thin plate. Depth=200 m, CT=20 S. The EM response is normalized by the dipole moment.

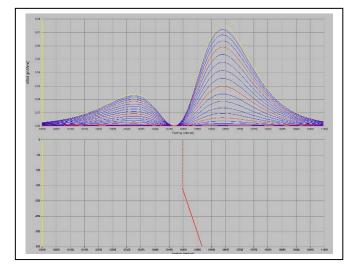


Figure E-7: dB/dt response of a deep skewed thin plate. Depth=200 m, CT=20 S. The EM response is normalized by the dipole moment and the Rx area.

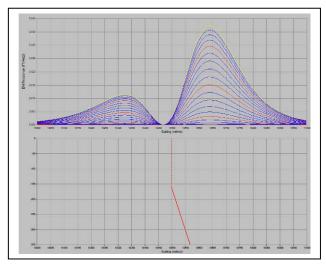


Figure E-8: B-field response of a deep skewed thin plate. Depth=200 m, CT=20 S. The EM response is normalized by the dipole moment.

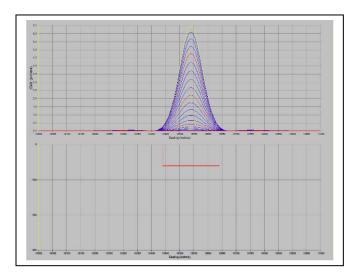


Figure E-9: dB/dt response of a shallow horizontal thin plate. Depth=100 m, CT=20 S. The EM response is normalized by the dipole moment and the Rx area.

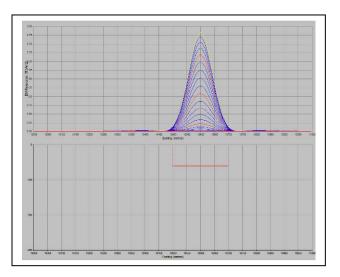


Figure E-10: B-Field response of a shallow horizontal thin plate. Depth=100 m, CT=20 S. The EM response is normalized by the dipole moment.

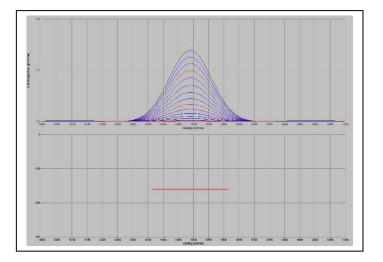


Figure E-11: dB/dt response of a deep horizontal thin plate. Depth=200 m, CT=20 S. The EM response is normalized by the dipole moment and the Rx area.

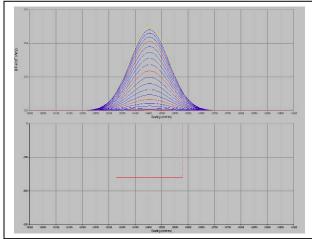


Figure E-12: B-Field response of a deep horizontal thin plate. Depth=200 m, CT=20 S. The EM response is normalized by the dipole moment.

#### II. THICK PLATE

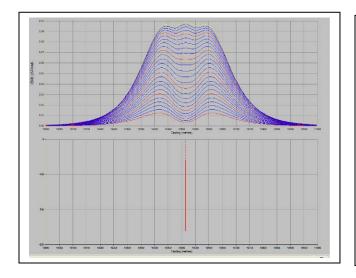


Figure E-13: dB/dt response of a shallow vertical thick plate. Depth=100 m, C=12 S/m, thickness=20 m. The EM response is normalized by the dipole moment and the Rx area.

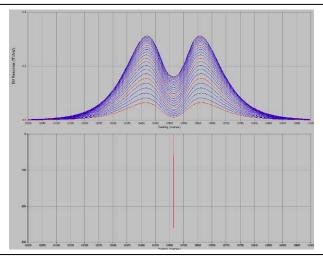


Figure E-14: B-Field response of a shallow vertical thick plate. Depth=100 m, C=12 S/m, thickness= 20 m. The EM response is normalized by the dipole moment.

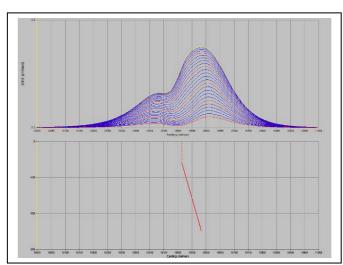


Figure E-15: dB/dt response of a shallow skewed thick plate. Depth=100 m, C=12 S/m, thickness=20 m. The EM response is normalized by the dipole moment and the Rx area.

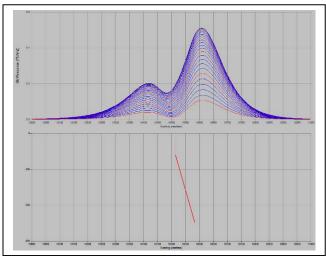


Figure E-16: B-Field response of a shallow skewed thick plate. Depth=100 m, C=12 S/m, thickness=20 m. The EM response is normalized by the dipole moment.

#### III. MULTIPLE THIN PLATES

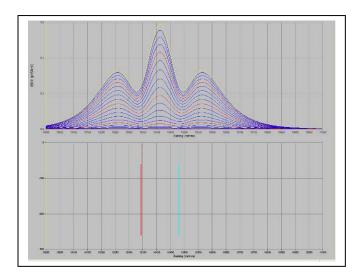


Figure E-17: dB/dt response of two vertical thin plates. Depth=100 m, CT=20 S. The EM response is normalized by the dipole moment and the Rx area.

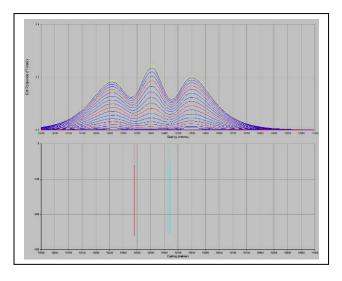


Figure E-18: B-Field response of two vertical thin plates. Depth=100 m, CT=20 S. The EM response is normalized by the dipole moment.

#### **General Interpretation Principals**

#### **Magnetics**

The total magnetic intensity responses reflect major changes in the magnetite and/or other magnetic minerals content in the underlying rocks and unconsolidated overburden. Precambrian rocks have often been subjected to intense heat and pressure during structural and metamorphic events in their history. Original signatures imprinted on these rocks at the time of formation have, it most cases, been modified, resulting in low magnetic susceptibility values.

The amplitude of magnetic anomalies, relative to the regional background, helps to assist in identifying specific magnetic and non-magnetic rock units (and conductors) related to, for example, mafic flows, mafic to ultramafic intrusives, felsic intrusives, felsic volcanics and/or sediments etc. Obviously, several geological sources can produce the same magnetic response. These ambiguities can be reduced considerably if basic geological information on the area is available to the geophysical interpreter.

In addition to simple amplitude variations, the shape of the response expressed in the wave length and the symmetry or asymmetry, is used to estimate the depth, geometric parameters and magnetization of the anomaly. For example, long narrow magnetic linears usually reflect mafic flows or intrusive dyke features. Large areas with complex magnetic patterns may be produced by intrusive bodies with significant magnetization, flat lying magnetic sills or sedimentary iron formation. Local isolated circular magnetic patterns often represent plug-like igneous intrusives such as kimberlites, pegmatites or volcanic vent areas.

Because the total magnetic intensity (TMI) responses may represent two or more closely spaced bodies within a response, the second derivative of the TMI response may be helpful for distinguishing these complexities. The second derivative is most useful in mapping near surface linears and other subtle magnetic structures that are partially masked by nearby higher amplitude magnetic features. The broad zones of higher magnetic amplitude, however, are severely attenuated in the vertical derivative results. These higher amplitude zones reflect rock units having strong magnetic susceptibility signatures. For this reason, both the TMI and the second derivative maps should be evaluated together.

Theoretically, the second derivative, zero contour or color delineates the contacts or limits of large sources with near vertical dip and shallow depth to the top. The vertical gradient map also aids in determining contact zones between rocks with a susceptibility contrast, however, different, more complicated rules of thumb apply.



#### Concentric Loop EM Systems

Concentric systems with horizontal transmitter and receiver antennae produce much larger responses for flat lying conductors as contrasted with vertical plate-like conductors. The amount of current developing on the flat upper surface of targets having a substantial area in this dimension, are the direct result of the effective coupling angle, between the primary magnetic field and the flat surface area. One therefore, must not compare the amplitude/conductance of responses generated from flat lying bodies with those derived from near vertical plates; their ratios will be quite different for similar conductances.

Determining dip angle is very accurate for plates with dip angles greater than 30°. For angles less than 30° to 0°, the sensitivity is low and dips can not be distinguished accurately in the presence of normal survey noise levels.

A plate like body that has near vertical position will display a two shoulder, classic **M** shaped response with a distinctive separation distance between peaks for a given depth to top.

It is sometimes difficult to distinguish between responses associated with the edge effects of flat lying conductors and poorly conductive bedrock conductors. Poorly conductive bedrock conductors having low dip angles will also exhibit responses that may be interpreted as surficial overburden conductors. In some situations, the conductive response has line to line continuity and some magnetic correlation providing possible evidence that the response is related to an actual bedrock source.

The EM interpretation process used, places considerable emphasis on determining an understanding of the general conductive patterns in the area of interest. Each area has different characteristics and these can effectively guide the detailed process used.



The first stage is to determine which time gates are most descriptive of the overall conductance patterns. Maps of the time gates that represent the range of responses can be very informative.

Next, stacking the relevant channels as profiles on the flight path together with the second vertical derivative of the TMI is very helpful in revealing correlations between the EM and Magnetics.

Next, key lines can be profiled as single lines to emphasize specific characteristics of a conductor or the relationship of one conductor to another on the same line. Resistivity Depth sections can be constructed to show the relationship of conductive overburden or conductive bedrock with the conductive anomaly.

