## REPORT ON A HELICOPTER-BORNE

 VERSATILE TIME DOMAIN ELECTROMAGNETIC (VTEM) GEOPHYSICAL SURVEYTIMMINS WEST EXTENSION PROJECT Timmins, Ontario, Canada

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For:

## GOLDEN CHALICE RESOURCES INC.



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# REPORT ON A HELICOPTER-BORNE VERSATILE TIME DOMAIN ELECTROMAGNETIC SURVEY 

Timmins West Extension Project<br>Ontario, Canada

## Executive Summary

During August $18^{\text {th }}$ to August $22^{\text {th }}$, 2008 Geotech Ltd. carried out a helicopter-borne geophysical survey for Golden Chalice Resources Inc. over Timmins West Extension block, located about 73 km south west of Timmins in the province of Ontario, Canada.

Principal geophysical sensors included a versatile time domain electromagnetic (VTEM) system, and a caesium magnetometer. Ancillary equipment included a GPS navigation system and a radar altimeter. A total of about 742 line-kilometres were flown.

The survey operations were based in Timmins, Ontario. In-field data quality assurance and preliminary processing were carried out on a daily basis during the acquisition phase. Preliminary and final data processing, including generation of final digital data and map products were undertaken from the office of Geotech Ltd. in Aurora, Ontario.

The processed survey results are presented as electromagnetic stacked profiles for the electromagnetics and the following grid contours;

- Total magnetic intensity
- B-field time gate 1.151 ms

Digital data includes all electromagnetic and magnetic products, plus ancillary data including the waveform.

This report describes the logistics of the survey acquisition phase and final data processing phase. No formal interpretation is included in this report.

## 1. INTRODUCTION

### 1.1 General Considerations

These services are the result of the Agreement made between Geotech Ltd. and Golden Chalice Resources Inc. to perform a helicopter-borne geophysical survey over the Timmins West Extension Project property located about 73 km south west of Timmins, Ontario, Canada (Figure 1).

Mr. John Keating, President and CEO acted on behalf of Golden Chalice Resources Inc. during the data acquisition and data processing phases of this project.

The geophysical surveys consisted of helicopter borne EM using the versatile time-domain electromagnetic (VTEM) system and aeromagnetic using a caesium magnetometer. A total of about 742 line-km of geophysical data were acquired during the survey. The survey area is shown in Figure 2.

The crew was based at the town of Timmins, Ontario for the acquisition phase of the survey. Survey flying started on August $18^{\text {th }}$ and was completed on August $22^{\text {nd }}, 2008$.

In-field data quality control and quality assurance, as well as preliminary data processing were carried out daily during the acquisition phase of the project. Final data processing followed immediately after the end of the survey. Final reporting, data presentation and archiving were completed from the Aurora office of Geotech Ltd. in December, 2008.


Figure 1- Property Location

### 1.2 Survey Location and Specifications

The, Timmins West Extension, survey block is located about 73 kilometres south-west of Timmins, Ontario. The base of operations for the survey was at Timmins as shown in figure 2.

The block was flown at a 75 metre traverse line spacing wherever possible (see Figure 2.) with a flight direction of ( $\mathrm{N} 0^{\circ} \mathrm{E} / \mathrm{N} 180^{\circ} \mathrm{E}$ ), while the tie lines were flown perpendicular to the traverse lines at a spacing of 725 metres with a flight direction of ( $\mathrm{N} 90^{\circ} \mathrm{E} / \mathrm{N} 270^{\circ} \mathrm{E}$ ). For more detailed information on the flight spacing and direction see Table 1.


Figure 2 - Flight path with base of operations

### 1.3 Topographic Relief and Cultural Features

Topographically, the property exhibits moderate relief, with an elevation ranging from 327 to 460 metres above sea level (see Figure 3). There are many small rivers, lakes and wetlands that run throughout the block. The survey block is covereded by NTS (National Topographic Survey) of Canada sheets 042B01.


Figure 3-Google Earth Image with Flight Path and features

Geotech Ltd.

## 2. DATA ACQUISITION

### 2.1 Survey Area

The block (see Figure 2 and Location map in Appendix A) and general flight specifications are as follows:

Table 1 - Survey Specifications

| Surve <br> $\mathbf{y}$ <br> block | Traverse Line <br> spacing (m) | Area <br> $\left(\mathbf{K m}^{2}\right)$ | Planned <br> Line-km | Actual $^{\mathbf{1}}$ <br> Line-km | Flight direction | Line numbers |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Block <br> G | Traverse: 75 | 50 | 667 | 672 | $\mathrm{NO} 0^{\circ} \mathrm{E} / \mathrm{N} 180^{\circ} \mathrm{E}$ | $\mathrm{L} 1010-2010$ |
|  | Tie: 725 |  | 75 | 75 | $\mathrm{~N} 90^{\circ} \mathrm{E} / \mathrm{N} 270^{\circ} \mathrm{E}$ | $\mathrm{T} 3000-3090$ |
| TOTAL |  | 50 | 742 | 747 |  |  |

Survey block boundaries co-ordinates are provided in Appendix B.
Survey operations were based out of Howard Johnson hotel in the town of Timmins, Ontario from Aug $18^{\text {th }}$ to Aug $22^{\text {nd }}, 2008$. The following table shows the timing of the flying

Table 2 - Survey Operations

| Date | Flight <br> $\#$ | Flown <br> KM | Block | Crew location | Comments |
| :---: | :---: | :---: | :---: | :---: | :--- |
| 18-Aug-08 |  |  | Timmins West <br> Extension | Timmins, ON | Production aborted - rain and thunder |
| 19-Aug-08 | $1,2,3$, <br> 4 | 431 | Timmins West <br> Extension | Timmins, ON | Production |
| 20-Aug-08 | 5,6 | 198 | Timmins West <br> Extension | Timmins, ON | Production |
| 21-Aug-08 | 7 | 113 | Timmins West <br> Extension | Timmins, ON | Production |
| 22-Aug-08 |  |  | Timmins West <br> Extension | Timmins, ON | Production - Job Complete |

### 2.2 Flight Specifications

The helicopter was maintained at a mean height of 79 metres above the ground. This allowed for a nominal EM sensor terrain clearance of 44 metres and a magnetic sensor clearance of 66 metres.

[^0]The data recording rates of the data acquisition was 0.1 second for electromagnetics, magnetometer, 0.2 second for altimeter and GPS. Helicopter maintained a nominal survey speed of $80 \mathrm{~km} / \mathrm{hr}$, this translates to a geophysical reading at about every 2 metres along flight track. Navigation was assisted by a GPS receiver and data acquisition system, which reports GPS co-ordinates as latitude/longitude and directs the pilot over a pre-programmed survey grid.

The operator was responsible for monitoring of the system integrity. He also maintained a detailed flight log during the survey, tracking the times of the flight as well as any unusual geophysical or topographic feature.

On return of the aircrew to the base camp the survey data was transferred from a compact flash card (PCMCIA) to the data processing computer. The data were then uploaded via ftp to the Geotech office in Aurora for daily quality assurance and quality control by qualified personnel, operating remotely.

### 2.3 Aircraft and Equipment

### 2.3.1 Survey Aircraft

The survey was flown using a Eurocopter Aerospatiale (Astar) 350 B2 helicopter, registration C-FDEV. The helicopter was operated by Expedition Helicopters Inc. Installation of the geophysical and ancillary equipment was carried out by Geotech Ltd.

### 2.3.2 Electromagnetic System

The electromagnetic system was a Geotech Time Domain EM (VTEM) system. The configuration is as indicated in Figure 4 below.

Receiver and transmitter coils are concentric and Z-direction oriented. The loops were towed at a mean distance of 35 metres below the aircraft as shown in Figure 6. The receiver decay recording scheme is shown diagrammatically in Figure 5.


Figure 4 - VTEM Configuration


Figure 5 - VTEM Waveform \& Sample Times

The complete VTEM decay sampling scheme is shown in Table 3 below. Twenty-four time measurement gates (channels 10 to 33) were used for the final data processing in the range from $120 \mu \mathrm{~s}$ to $6578 \mu \mathrm{~s}$, as shown in Table 5.

Table 3 - Decay Sampling Scheme

| VTEM Decay Sampling scheme ${ }^{2}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Array Index | ( Microseconds) |  |  |  |
|  | Time Gate | Start | End | Width |
| 0 | 0 |  |  |  |
| 1 | 10 | 10 | 21 | 11 |
| 2 | 21 | 16 | 26 | 11 |
| 3 | 31 | 26 | 37 | 11 |
| 4 | 42 | 37 | 47 | 11 |
| 5 | 52 | 47 | 57 | 10 |
| 6 | 62 | 57 | 68 | 11 |
| 7 | 73 | 68 | 78 | 11 |
| 8 | 83 | 78 | 91 | 13 |
| 9 | 99 | 91 | 110 | 19 |
| 10 | 120 | 110 | 131 | 21 |
| 11 | 141 | 131 | 154 | 24 |
| 12 | 167 | 154 | 183 | 29 |
| 13 | 198 | 183 | 216 | 34 |
| 14 | 234 | 216 | 258 | 42 |
| 15 | 281 | 258 | 310 | 53 |
| 16 | 339 | 310 | 373 | 63 |
| 17 | 406 | 373 | 445 | 73 |
| 18 | 484 | 445 | 529 | 84 |
| 19 | 573 | 529 | 628 | 99 |
| 20 | 682 | 628 | 750 | 123 |
| 21 | 818 | 750 | 896 | 146 |
| 22 | 974 | 896 | 1063 | 167 |
| 23 | 1151 | 1063 | 1261 | 198 |
| 24 | 1370 | 1261 | 1506 | 245 |
| 25 | 1641 | 1506 | 1797 | 292 |
| 26 | 1953 | 1797 | 2130 | 333 |
| 27 | 2307 | 2130 | 2526 | 396 |
| 28 | 2745 | 2526 | 3016 | 490 |
| 29 | 3286 | 3016 | 3599 | 583 |
| 30 | 3911 | 3599 | 4266 | 667 |
| 31 | 4620 | 4266 | 5058 | 792 |
| 32 | 5495 | 5058 | 6037 | 979 |
| 33 | 6578 | 6037 | 7203 | 1167 |
| 34 | 7828 | 7203 | 8537 | 1334 |
| 35 | 9245 | 8537 | 10120 | 1584 |

[^1] Figure 5 and Appendix C

Geotech Ltd.

VTEM system parameters:

## Transmitter Section

- $\quad$ Transmitter coil diameter: 26 m
- Number of turns: 4
- Transmitter base frequency: 30 Hz
- Peak current: 176.6 Amp
- Pulse width: 7.2 ms
- Pulse width: Duty cycle: $43 \%$
- $\quad$ Peak dipole moment: 374, 880 nIA
- $\quad$ Nominal terrain clearance: 44 m


## Receiver Section

- $\quad$ Receiver coil diameter: 1.2 m
- Number of turns: 100.
- $\quad$ Effective coil area: 113.04 m $^{2}$
- Wave form shape: trapezoid
- Power Line Monitor: 60 Hz


## Magnetometer

- Nominal terrain clearance: 66 m


Figure 6 - VTEM system configuration

### 2.3.3 Airborne magnetometer

The magnetic sensor utilized for the survey was a Geometrics optically pumped caesium vapour magnetic field sensor, mounted in a separate bird, 13 metres below the helicopter, as shown in Figure 6. The sensitivity of the magnetic sensor is 0.02 nanoTesla (nT) at a sampling interval of 0.1 seconds. The magnetometer sends the measured magnetic field strength as nanoTesla to the data acquisition system via the RS-232 port.

### 2.3.4 Radar Altimeter

A Terra TRA 3000/TRI 40 radar altimeter was used to record terrain clearance. The antenna was mounted beneath the bubble of the helicopter cockpit (Figure 6).

### 2.3.5 GPS Navigation System

The navigation system used was a Geotech PC based navigation system utilizing a NovAtel's CDGPS (Canada-Wide Differential Global Positioning System Correction Service) enable OEM4-G2-3151W GPS receiver, the Geotech navigate software, a full screen display with controls in front of the pilot to direct the flight and an NovAtel GPS antenna mounted on the helicopter tail (Figure 5). As many as 11 GPS and two CDGPS satellites may be monitored at any one time. The positional accuracy or circular error probability (CEP) is 1.8 m , with CDGPS active, it is 1.0 m . The co-ordinates of the block were set-up prior to the survey and the information was fed into the airborne navigation system.

### 2.3.6 Digital Acquisition System

A Geotech data acquisition system recorded the digital survey data on an internal compact flash card. Data is displayed on an LCD screen as traces to allow the operator to monitor the integrity of the system. The data type and sampling interval as provided in Table 4.

Table 4 - Acquisition Sampling Rates

| DATA TYPE | SAMPLING |
| :---: | :---: |
| TDEM | 0.1 sec |
| Magnetometer | 0.1 sec |
| GPS Position | 0.2 sec |
| Radar Altimeter | 0.2 sec |

### 2.3.7 Base Station

A combined magnetometer/GPS base station was utilized on this project. A Geometrics Caesium vapour magnetometer was used as a magnetic sensor with a sensitivity of 0.001 nT . The base station was recording the magnetic field together with the GPS time at 1 Hz on a base station computer.

The base station magnetometer sensor was installed near the crew base in Timmins, Ontario $\left(48^{0} 28^{\prime} 48.60^{\prime \prime} \mathrm{N}, 81^{0} 23^{\prime} 44.27^{\prime \prime} \mathrm{W}\right.$ ), away from electric transmission lines and moving ferrous objects such as motor vehicles. The base station data were backed-up to the data processing computer at the end of each survey day.

## 3. PERSONNEL

The following Geotech Ltd. personnel were involved in the project.
Field:
Project Manager: Les Moschuk (Office)
Data QA/QC: Nick Venter (Office)
Crew chief: Colin Lennox

System Operator: Jonathan Howarth Bruce Rice

The survey pilot and the mechanical engineer were employed directly by the helicopter operator - Expedition Helicopters Ltd.

Pilot:
Mechanical Engineer:
Office:
Preliminary Data Processing: Nick Venter
Final Data Processing:
Final Data QC :
Mapping/Reporting: Venkata Kopalle

Data acquisition phase was carried out under the supervision of Andrei Bagrianski, P. Geo, Surveys Manager. Processing phase was carried out under the supervision of Jean Legault, P. Geo, Manager of Processing and Interpretation. The overall contract management and customer relations were by Quentin Yarie, P. Geo.

## 4. DATA PROCESSING AND PRESENTATION

Data compilation and processing were carried out by the application of Geosoft OASIS Montaj and programs proprietary to Geotech Ltd.

### 4.1 Flight Path

The flight path, recorded by the acquisition program as WGS 84 latitude/longitude, was converted into the NAD83 Datum, UTM Zone 17N in Oasis Montaj.

The flight path was drawn using linear interpolation between x , y positions from the navigation system. Positions are updated every second and expressed as UTM easting’s (x) and UTM northing’s (y).

### 4.2 Electromagnetic Data

A three stage digital filtering process was used to reject major sferic events and to reduce system noise. Local sferic activity can produce sharp, large amplitude events that cannot be removed by conventional filtering procedures. Smoothing or stacking will reduce their amplitude but leave a broader residual response that can be confused with geological phenomena. To avoid this possibility, a computer algorithm searches out and rejects the major sferic events. The filter used was a 16 point non-linear filter.

The signal to noise ratio was further improved by the application of a low pass linear digital filter. This filter has zero phase shift which prevents any lag or peak displacement from occurring, and it suppresses only variations with a wavelength less than about 1 second or 15 metres. This filter is a symmetrical 1 sec linear filter.

The results are presented as stacked profiles of EM voltages for the time gates, in linear logarithmic scale for both B-field and $\mathrm{dB} / \mathrm{dt}$ response. B-field time channel recorded at 0.573 milliseconds after the termination of the impulse is also presented as contour colour image.

Generalized modeling results of VTEM data, written by consultant Roger Barlow and Nasreddine Bournas, P. Geo., are shown in Appendix E.

Graphical representations of the VTEM transmitter input current waveform and the output voltage of the receiver coil are shown in Appendix C.

### 4.3 Magnetic Data

The processing of the magnetic data involved the correction for diurnal variations by using the digitally recorded ground base station magnetic values. The base station magnetometer data was edited and merged into the Geosoft GDB database on a daily basis. The aeromagnetic data was corrected for diurnal variations by subtracting the observed magnetic base station deviations.

Tie line levelling was carried out by adjusting intersection points along traverse lines. A micro-levelling procedure was applied to remove persistent low-amplitude components of flight-line noise remaining in the data.

The corrected magnetic data was interpolated between survey lines using a random point gridding method to yield $x-y$ grid values for a standard grid cell size of approximately 0.25 to 0.2 cm at the mapping scale. The Minimum Curvature algorithm was used to interpolate values onto a rectangular regular spaced grid.

## 5. DELIVERABLES

### 5.1 Survey Report

The survey report describes the data acquisition, processing, and final presentation of the survey results. The survey report is provided in two paper copies and digitally in PDF format.

### 5.2 Maps

Final maps were produced at scale of 1:10,000. The coordinate/projection system used was NAD 83, UTM Zone 17N. All maps show the flight path trace and topographic data; latitude and longitude are also noted on maps.

The preliminary and final results of the survey are presented as EM profiles, a late-time gate gridded EM channel, and color magnetic TMI contour maps.

The following maps are presented on paper

- VTEM B-field profiles, Time Gates $0.234-6.578 \mathrm{~ms}$ in linear - logarithmic scale with TMI colour image.
- VTEM dB/dt profiles, Time Gates $0.234-6.578 \mathrm{~ms}$ in linear - logarithmic scale.
- VTEM B-field late time, Time Gate 1.151 ms colour image.
- Total magnetic intensity (TMI) colour image and contours.


### 5.3 Digital Data

- Two copies of the data and maps on DVD were prepared to accompany the report. Each DVD-ROM contains a digital file of the line data in GDB Geosoft Montaj format as well as the maps in Geosoft Montaj Map format.
- DVD-ROMs were prepared.

There are two (2) main directories:
Data contains databases, grids and maps, as described below. Report contains a copy of the report and appendices in PDF format.

Databases in Geosoft GDB format, containing the channels listed, are presented in Table 5.

Table 5 - Geosoft GDB Data Format.

| Channel Name | Description |
| :---: | :---: |
| X: | X positional data (metres - NAD83, UTM zone 17 north) |
| Y: | Y positional data (metres - NAD83, UTM zone 17north) |
| Z: | GPS antenna elevation (metres - ASL) |
| Lon: | Longitude data (degree - NAD83 |
| Lat: | Latitude data (degree - NAD83) |
| Radar: | Helicopter terrain clearance from radar altimeter (metres - AGL) |
| RadarB: | EM Bird terrain clearance from radar altimeter (metres - AGL) |
| DEM: | Digital elevation model (metres) |
| Gtime: | GPS time (seconds of the day) |
| Mag1: | Raw Total Magnetic field data (nT) |
| Basemag: | Magnetic diurnal variation data (nT) |
| Mag2: | Diurnal corrected Total Magnetic field data (nT) |
| Mag3: | Leveled Total Magnetic field data (nT) |
| SF[10]: | $\mathrm{dB} / \mathrm{dt} 120$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[11]: | $\mathrm{dB} / \mathrm{dt} 141$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[12]: | $\mathrm{dB} / \mathrm{dt} 167$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[13]: | $\mathrm{dB} / \mathrm{dt} 198$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[14]: | $\mathrm{dB} / \mathrm{dt} 234$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[15]: | $\mathrm{dB} / \mathrm{dt} 281$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[16]: | $\mathrm{dB} / \mathrm{dt} 339$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[17]: | $\mathrm{dB} / \mathrm{dt} 406$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[18]: | $\mathrm{dB} / \mathrm{dt} 484$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[19]: | $\mathrm{dB} / \mathrm{dt} 573$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[20]: | $\mathrm{dB} / \mathrm{dt} 682$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[21]: | $\mathrm{dB} / \mathrm{dt} 818$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[22]: | $\mathrm{dB} / \mathrm{dt} 974$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[23]: | $\mathrm{dB} / \mathrm{dt} 1151$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[24]: | $\mathrm{dB} / \mathrm{dt} 1370$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| SF[25]: | $\mathrm{dB} / \mathrm{dt} 1641$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| SF[26]: | $\mathrm{dB} / \mathrm{dt} 1953$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| SF[27]: | $\mathrm{dB} / \mathrm{dt} 2307$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| SF[28]: | $\mathrm{dB} / \mathrm{dt} 2745$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| SF[29]: | $\mathrm{dB} / \mathrm{dt} 3286$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[30]: | $\mathrm{dB} / \mathrm{dt} 3911$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A} * \mathrm{~m}^{4}\right)$ |
| SF[31]: | $\mathrm{dB} / \mathrm{dt} 4620$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| SF[32]: | $\mathrm{dB} / \mathrm{dt} 5495$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| SF[33]: | $\mathrm{dB} / \mathrm{dt} 6578$ microsecond time channel $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| BF[10]: | B-field 120 microsecond time channel ( $\mathrm{pV} * \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |


| Channel Name | Description |
| :---: | :---: |
| BF[11]: | B-field 141 microsecond time channel ( $\mathrm{pV}{ }^{*} \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[12]: | B-field 167 microsecond time channel ( $\mathrm{pV}{ }^{*} \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[13]: | B-field 198 microsecond time channel ( $\mathrm{pV} * \mathrm{~ms}$ )/( $\left.\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| BF[14]: | B-field 234 microsecond time channel ( $\mathrm{pV}{ }^{*} \mathrm{~ms}$ )/( $\left.\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| BF[15]: | B-field 281 microsecond time channel ( $\mathrm{pV}{ }^{*} \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[16]: | B-field 339 microsecond time channel ( $\mathrm{pV}{ }^{*} \mathrm{~ms}$ )/( $\left.\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| BF[17]: | B-field 406 microsecond time channel ( $\mathrm{pV}{ }^{*} \mathrm{~ms}$ )/( $\left.\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| BF[18]: | B-field 484 microsecond time channel ( $\mathrm{pV} * \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[19]: | B-field 573 microsecond time channel ( $\mathrm{pV} * \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[20]: | B-field 682 microsecond time channel ( $\mathrm{pV}{ }^{*} \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[21]: | B-field 818 microsecond time channel ( $\mathrm{pV} * \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[22]: | B-field 974 microsecond time channel ( $\mathrm{pV} * \mathrm{~ms}$ )/( $\left.\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ |
| BF[23]: | B-field 1151 microsecond time channel (pV*ms)/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[24]: | B-field 1370 microsecond time channel ( $\mathrm{pV} * \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[25]: | B-field 1641 microsecond time channel ( $\mathrm{pV}^{*} \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[26]: | B-field 1953 microsecond time channel ( $\mathrm{pV}^{*} \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[27]: | B-field 2307 microsecond time channel ( $\mathrm{pV} * \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[28]: | B-field 2745 microsecond time channel ( $\mathrm{pV}^{*} \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[29]: | B-field 3286 microsecond time channel ( $\mathrm{pV}^{*} \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[30]: | B-field 3911 microsecond time channel ( $\mathrm{pV}^{*} \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[31]: | B-field 4620 microsecond time channel ( $\mathrm{pV}^{*} \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[32]: | B-field 5495 microsecond time channel ( $\mathrm{pV}^{*} \mathrm{~ms}$ )/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| BF[33]: | B-field 6578 microsecond time channel (pV*ms)/( $\mathrm{A}^{*} \mathrm{~m}^{4}$ ) |
| PLM: | Power Line monitor (60Hz) |

Electromagnetic B-field and $\mathrm{dB} /$ dt data are found in array channel format between indexes 10 - 33, as described above.

- Database of the VTEM Waveform "VTEM_waveform.gdb" in Geosoft GDB format, containing the following channels:

Time: Sampling rate interval, 10.416 microseconds
Rx_Voltage: Output voltage of the receiver coil (Volt)
Tx_Current: Output current of the transmitter (Amp)

- Grids in Geosoft GRD format, as follows:

8105_Mag: Total magnetic intensity (nT)<br>8105_BF23: B-Field Time Gate 1.151 ms

A Geosoft .GRD file has a .GI metadata file associated with it, containing grid projection information. A grid cell size of 25 metres was used.

- Maps at 1:10,000 in Geosoft MAP format, as follows:

8105_TMI: B-field profiles, Time Gates $0.234-6.578 \mathrm{~ms}$ in linear logarithmic scale, with TMI colour image.
8105_dBdt: $\quad \mathrm{dB} / \mathrm{dt}$ profiles, Time Gates $0.234-6.578 \mathrm{~ms}$ in linear logarithmic scale
8105_BF23: B-field late time Gate 1.151 ms colour image.
8105_TMI: Total magnetic intensity colour image and contours
1:50, 000 topographic vectors were taken from the NRCAN Geogratis database at; http://geogratis.gc.ca/geogratis/en/index.html.

- Google Earth files 8105_flight.kml showing the flight path of block.
- Free versions of Google Earth software from: http://earth.google.com/downloadearth.html


## 6. CONCLUSIONS AND RECOMMENDATIONS

### 6.1 Conclusions

A helicopter-borne versatile time domain electromagnetic (VTEM) survey has been completed over the Timmins West Extension, project area, approximately 73 km south-west of Timmins, in the province of Ontario, Canada.

The total area coverage is $50 \mathrm{~km}^{2}$. Total survey line coverage is 742 line kilometres. The principal sensors included a Time Domain EM system and a magnetometer. Results have been presented as stacked profiles, anomaly symbols, and contour colour images at a scale of $1: 10,000$. No formal interpretation is included in this report

### 6.2 Recommendations

Based on the geophysical results obtained, a number of potentially interesting EM and magnetic anomalies were identified on the property. We therefore recommend a more detailed interpretation of the EM and magnetic results in conjunction with the known geology including EM anomaly picks and also inversion and modelling technique to better characterize them to more accurately determine their parameters (depth, conductance, dip, etc.) prior to ground follow-up and drill testing.

Respectfully submitted ${ }^{1}$,

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January 2009

[^2]
## APPENDIX A

## SURVEY BLOCK CLAIM MAP



## APPENDIX B

## SURVEY BLOCK COORDINATES

(NAD83, UTM Zone 17N)

| X | Y |
| :---: | :---: |
| 408800 | 5336600 |
| 416300 | 5336600 |
| 416300 | 5330000 |
| 408800 | 5330000 |

## APPENDIX C

## VTEM WAVEFORM



## APPENDIX D

GEOPHYSICAL MAPS ${ }^{3}$


VTEM B-Field Profiles with TMI colour image

3 Full size geophysical maps are also available in PDF format on the final CD.


## VTEM dB/dt profiles



VTEM B-field late time Gate 1.151 ms colour image


Total magnetic intensity (TMI) colour image

## APPENDIX E <br> GENERALIZED MODELING RESULTS OF THE VTEM SYSTEM

## Introduction

The VTEM system is based on a concentric or central loop design, whereby, the receiver is positioned at the centre of a 26.1 metres diameter transmitter loop that produces a dipole moment up to 384,000 nIA at peak current. The wave form is a bi-polar, modified square wave with a turn-on and turn-off at each end. With a base frequency of 30 Hz , the duration of each pulse is approximately 7.4 milliseconds followed by an off time where no primary field is present.

During turn-on and turn-off, a time varying field is produced $(\mathrm{dB} / \mathrm{dt})$ and an electro-motive force (emf) is created as a finite impulse response. A current ring around the transmitter loop moves outward and downward as time progresses. When conductive rocks and mineralization are encountered, a secondary field is created by mutual induction and measured by the receiver at the centre of the transmitter loop.

Measurements are made during the on and off-time, when only the secondary field (representing the conductive targets encountered in the ground) is present.

Efficient modeling of the results can be carried out on regularly shaped geometries, thus yielding close approximations to the parameters of the measured targets. The following is a description of a series of common models made for the purpose of promoting a general understanding of the measured results.

## General Modeling Concepts

A set of models has been produced for the Geotech VTEM® system with explanation notes (see models C 1 to C 18 ). The reader is encouraged to review these models, so as to get a general understanding of the responses as they apply to survey results. While these models do not begin to cover all possibilities, they give a general perspective on the simple and most commonly encountered anomalies.

When producing these models, a few key points were observed and are worth noting as follows:

- For near vertical and vertical plate models, the top of the conductor is always located directly under the centre low point between the two shoulders in the classic $\mathbf{M}$ shaped response.
- As the plate is positioned at an increasing depth to the top, the shoulders of the $\mathbf{M}$ shaped response, have a greater separation distance.
- When faced with choosing between a flat lying plate and a prism model to represent the target (broad response) some ambiguity is present and caution should be exercised.
- With the concentric loop system and Z-component receiver coil, virtually all types of conductors and most geometries are most always well coupled and a response is generated (see model H). Only concentric loop systems can map this type of target.

The Maxwell ${ }^{\text {TM }}$ modeling program (Fullagar and Reid, 2001) used to generate the following responses assumes a resistive half-space.

## Variation of Plate Depth

Geometries represented by plates of different strike length, depth extent, dip, plunge and depth below surface can be varied with characteristic parameters like conductance of the target, conductance of the host and conductivity/thickness and thickness of the overburden layer.

Diagrammatic models for a vertical plate are shown in Figures C-1 \& C-2 and C-5 \& C-6 at two different depths, all other parameters remaining constant. With this transmitter-receiver geometry, the classic $\mathbf{M}$ shaped response is generated. Figures $\mathbf{C}-1$ and $\mathbf{C}-2$ show a plate where the top is near surface. Here, amplitudes of the duel peaks are higher and symmetrical with the zero centre positioned directly above the plate. Most important is the separation distance of the peaks. This distance is small when the plate is near surface and widens with a linear relationship as the plate (depth to top) increases. Figures C-5 and C-6 show a much deeper plate where the separation distance of the peaks is much wider and the amplitudes of the channels have decreased.

## Variation of Plate Dip

As the plate dips and departs from the vertical position, the peaks become asymmetrical. Figures C-3 \& C-4 and C-7 and C-8 show a near surface plate dipping $80^{\circ}$ at two different depths. Note that the direction of dip is toward the high shoulder of the response and the top of the plate remains under the centre minimum.

As the dip increases, the aspect ratio (Min/Max) decreases and this aspect ratio can be used as an empirical guide to dip angles from near $90^{\circ}$ to about $30^{\circ}$. The method is not sensitive enough where dips are less than about $30^{\circ}$. For example, for a plate dipping $45^{\circ}$, the minimum shoulder starts to vanish. In Figures C-9 \& C-10 and C-11 \& C-12, a flat lying plate is shown, relatively near surface. Note that the twin peak anomaly has been replaced by a symmetrical shape with large, bell shaped, channel amplitudes which decay relative to the conductance of the plate.

In the special case where two plates are positioned to represent a synclinal structure. Note that the main characteristic is that the centre amplitudes are higher (approximately double) compared to the high shoulder of a single plate. This model is very representative of tightly folded formations where the conductors where once flat lying.

## Variation of Prism Dip

Finally, with thicker, prism models, another algorithm is required to represent current on the plate. A plate model is considered to be infinitely thin with respect to thickness and incapable of representing the current in the thickness dimension. A prism model is constructed to deal with this problem, thereby, representing the thickness of the body more accurately.

Figures C-13 \& C-14 and C-15 \& C-16 show the same prism at the same depths with variable dips. Aside from the expected differences asymmetry prism anomalies show a characteristic change from a double-peaked anomaly to single peak signatures.

## I. THIN PLATE



Figure $\mathrm{C}-1$ : $\mathrm{dB} / \mathrm{dt}$ response of a shallow vertical thin plate. Depth $=100 \mathrm{~m}, \mathrm{CT}=20 \mathrm{~S}$. The EM response is normalized by the dipole moment and the Rx area.


Figure $\mathrm{C}-3$ : $\mathrm{dB} / \mathrm{dt}$ response of a shallow skewed thin plate. Depth $=100 \mathrm{~m}, \mathrm{CT}=20 \mathrm{~S}$. The EM response is normalized by the dipole moment and the Rx area.


Figure C-2: B-field response of a shallow vertical thin plate. Depth $=100 \mathrm{~m}, \mathrm{CT}=20 \mathrm{~S}$. The EM response is normalized by the dipole moment.


Figure C-4: B-field response of a shallow skewed thin plate. Depth $=100 \mathrm{~m}, \mathrm{CT}=20 \mathrm{~S}$. The EM response is normalized by the dipole moment.


Figure $\mathrm{C}-5$ : $\mathrm{dB} / \mathrm{dt}$ response of a deep vertical thin plate. Depth=200 m, CT=20 S. The EM response is normalized by the dipole moment and the Rx area.


Figure $\mathrm{C}-7$ : $\mathrm{dB} / \mathrm{dt}$ response of a deep skewed thin plate. Depth=200 m, CT=20 S. The EM response is normalized by the dipole moment and the Rx area.


Figure C-6: B-Field response of a deep vertical thin plate. Depth=200 m, CT=20 S. The EM response is normalized by the dipole moment.


Figure C-8: B-field response of a deep skewed thin plate. Depth=200 m, CT=20 S. The EM response is normalized by the dipole moment.


Figure C-9: dB/dt response of a shallow horizontal thin plate. Depth=100 m, CT=20 S. The EM response is normalized by the dipole moment and the Rx area.


Figure $\mathrm{C}-11$ : $\mathrm{dB} / \mathrm{dt}$ response of a deep horizontal thin plate. Depth=200 m, CT=20 S. The EM response is normalized by the dipole moment and the Rx area.


Figure C-10: B-Field response of a shallow horizontal thin plate. Depth=100 m, CT=20 S. The EM response is normalized by the dipole moment.


Figure C-12: B-Field response of a deep horizontal thin plate. Depth=200 m, CT=20 S. The EM response is normalized by the dipole moment.

## II. THICK PLATE



Figure C-13: dB/dt response of a shallow vertical thick plate. Depth=100 m, C=12 S/m, thickness $=20 \mathrm{~m}$. The EM response is normalized by the dipole moment and the Rx area.


Figure C-15: dB/dt response of a shallow skewed thick plate. Depth=100 m, C=12 S/m, thickness $=20 \mathrm{~m}$. The EM response is normalized by the dipole moment and the Rx area. by


Figure C-14: B-Field response of a shallow vertical thick plate. Depth $=100 \mathrm{~m}, \mathrm{C}=12 \mathrm{~S} / \mathrm{m}$, thickness $=20 \mathrm{~m}$. The EM response is normalized by the dipole moment.


Figure C-16: B-Field response of a shallow skewed thick plate. Depth=100 m, C=12 S/m, thickness $=20 \mathrm{~m}$. The EM response is normalized by the dipole moment.

## III. MULTIPLE THIN PLATES



Figure C-17: dB/dt response of two vertical thin plates. Depth=100 m, CT=20 S. The EM response is normalized by the dipole moment and the Rx area.


Figure C-18: B-Field response of two vertical thin plates. Depth=100 m, CT=20 S. The EM response is normalized by the dipole moment.

## General Interpretation Principals

## Magnetics

The total magnetic intensity responses reflect major changes in the magnetite and/or other magnetic minerals content in the underlying rocks and unconsolidated overburden. Precambrian rocks have often been subjected to intense heat and pressure during structural and metamorphic events in their history. Original signatures imprinted on these rocks at the time of formation have, it most cases, been modified, resulting in low magnetic susceptibility values.

The amplitude of magnetic anomalies, relative to the regional background, helps to assist in identifying specific magnetic and non-magnetic rock units (and conductors) related to, for example, mafic flows, mafic to ultramafic intrusives, felsic intrusives, felsic volcanics and/or sediments etc. Obviously, several geological sources can produce the same magnetic response. These ambiguities can be reduced considerably if basic geological information on the area is available to the geophysical interpreter.

In addition to simple amplitude variations, the shape of the response expressed in the wave length and the symmetry or asymmetry, is used to estimate the depth, geometric parameters and magnetization of the anomaly. For example, long narrow magnetic linears usually reflect mafic flows or intrusive dyke features. Large areas with complex magnetic patterns may be produced by intrusive bodies with significant magnetization, flat lying magnetic sills or sedimentary iron formation. Local isolated circular magnetic patterns often represent plug-like igneous intrusives such as kimberlites, pegmatites or volcanic vent areas.

Because the total magnetic intensity (TMI) responses may represent two or more closely spaced bodies within a response, the second derivative of the TMI response may be helpful for distinguishing these complexities. The second derivative is most useful in mapping near surface linears and other subtle magnetic structures that are partially masked by nearby higher amplitude magnetic features. The broad zones of higher magnetic amplitude, however, are severely attenuated in the vertical derivative results. These higher amplitude zones reflect rock units having strong magnetic susceptibility signatures. For this reason, both the TMI and the second derivative maps should be evaluated together.

Theoretically, the second derivative, zero contour or color delineates the contacts or limits of large sources with near vertical dip and shallow depth to the top. The vertical gradient map also aids in determining contact zones between rocks with a susceptibility contrast, however, different, more complicated rules of thumb apply.

## Concentric Loop EM Systems

Concentric systems with horizontal transmitter and receiver antennae produce much larger responses for flat lying conductors as contrasted with vertical plate-like conductors. The amount of current developing on the flat upper surface of targets having a substantial area in this dimension, are the direct result of the effective coupling angle, between the primary magnetic field and the flat surface area. One therefore, must not compare the amplitude/conductance of responses generated from flat lying bodies with those derived from near vertical plates; their ratios will be quite different for similar conductances.

Determining dip angle is very accurate for plates with dip angles greater than $30^{\circ}$. For angles less than $30^{\circ}$ to $0^{\circ}$, the sensitivity is low and dips can not be distinguished accurately in the presence of normal survey noise levels.

A plate like body that has near vertical position will display a two shoulder, classic $\mathbf{M}$ shaped response with a distinctive separation distance between peaks for a given depth to top.

It is sometimes difficult to distinguish between responses associated with the edge effects of flat lying conductors and poorly conductive bedrock conductors. Poorly conductive bedrock conductors having low dip angles will also exhibit responses that may be interpreted as surficial overburden conductors. In some situations, the conductive response has line to line continuity and some magnetic correlation providing possible evidence that the response is related to an actual bedrock source.

The EM interpretation process used, places considerable emphasis on determining an understanding of the general conductive patterns in the area of interest. Each area has different characteristics and these can effectively guide the detailed process used.

The first stage is to determine which time gates are most descriptive of the overall conductance patterns. Maps of the time gates that represent the range of responses can be very informative.

Next, stacking the relevant channels as profiles on the flight path together with the second vertical derivative of the TMI is very helpful in revealing correlations between the EM and Magnetics.

Next, key lines can be profiled as single lines to emphasize specific characteristics of a conductor or the relationship of one conductor to another on the same line. Resistivity Depth sections can be constructed to show the relationship of conductive overburden or conductive bedrock with the conductive anomaly.

## Roger Barlow

## Consultant

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## Geotech Ltd.

January 2009










[^0]:    ${ }^{1}$ Note: Actual Line-km is as deduced from the nav database file and this normally exceed the total planned line km as indicated in the survey NAV files

[^1]:    ${ }^{2}$ Measurement time delays are referenced to time zero marking the end of the transmitter current turn-off, as illustrated in

[^2]:    ${ }^{1}$ Final data processing and interpretation of the EM and magnetic data were carried out by George Lev, from the office of Geotech Ltd. in Aurora, Ontario, under the supervision of Jean Legault, P. Geo, Manager of Data Processing and Interpretation.

