# Assessment Report On A Helicopter-borne Versatile Domain Electromagnetic (VTEM Max) And Aeromagnetic Survey <br> Starburst Property <br> South Lorrain Township, Ontario <br> Larder Lake Mining Division 

FOR

## Thomas Obradovich

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## 1. INTRODUCTION

The Starburst Property ("Property") is located within South Lorrain Township, Larder Lake Mining Division, approximately 85 km north of North Bay, Ontario. The Property is covered by National Topographic System (NTS) map sheets 31M/04H and 31M/03E.

The Property is comprised of 67 mining claims, totalling approximately $1,471.6$ ha in area.

From February $10^{\text {th }}$ to $12^{\text {th }}$, 2021, Geotech Ltd. completed a helicopter-borne geophysical survey over the Property. Principal geophysical sensors included a versatile time domain electromagnetic (VTEM Max) system, as well as a caesium magnetometer. Ancillary equipment included a GPS navigation systema and a radar altimeter. A total of 135 line-kilometres of geophysical data was acquired during the survey, and forms the basis of this assessment report.

## 2. PROPERTY DESCRIPTION AND LOCATION

### 2.1 Location and Access

The Property is located within South Lorrain Township, Ontario (Figure 1). The Project is bounded by UTM NAD83 coordinates 17N 611925E to 616680E, and 5216500N to 5220660N.

Access to the Property is provided by Hwy 567, a well-maintained gravel highway, as well as secondary gravel roads. Local resources on the Property consist of mixed deciduous and coniferous trees.

A full range of services and supplies are provided in the City of Temiskaming Shores located 50 km to the north. Accommodations can be provided at several tourist lodges and motels located along Highway 567 or along Highway 11B.

### 2.2 Topography and Vegetation

The local terrain is variable from swamps to steep cliffs. Typical vegetation on the Property consists of a boreal forest with a mixture of coniferous and deciduous trees, including poplar, white birch, red pine, white pine, white spruce, black spruce, balsam, cedar, and alders. The elevation of the Property ranges from approximately 179 to 385 m above mean sea level.


Figure 1: Location of the Starburst Property, Ontario

### 2.3 Mineral Dispositions

The Property is comprised of 67 mining claims, totalling approximately $1,471.6$ ha in area (Figure 2, Table 1).


Figure 2: Land Tenure of the Starburst Property

Table 1 : Claim Details

| Tenure <br> ID | Anniversary <br> Date | Tenure <br> Status | Work <br> Required | Work <br> Applied | Available <br> Consultation <br> Reserve | Available <br> Exploration <br> Reserve | Total <br> Reserve |
| :---: | :--- | :--- | :--- | ---: | ---: | ---: | ---: |
| 549296 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549295 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549294 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549293 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549292 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549291 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549290 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549289 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549288 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549287 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549286 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549285 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549284 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549283 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549282 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549281 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549280 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549279 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549277 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549276 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549275 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549274 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549273 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549272 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549271 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549270 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549269 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549268 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549267 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549266 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549265 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549264 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549263 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549262 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549261 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549260 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549259 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
|  |  |  |  |  | 0 | 0 | 0 |


| 549258 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 549257 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549256 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549255 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549254 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549253 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549252 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549251 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549250 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549249 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549248 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549247 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549246 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549245 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549244 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549243 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549242 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549241 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549240 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549239 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549238 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549237 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549236 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549235 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549234 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549233 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549232 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549231 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549230 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |
| 549229 | $2022-05-04$ | Active | 400 | 0 | 0 | 0 | 0 |

### 3.0 HISTORY

### 3.1 Historical Mineral Exploration

Assessment files covering the Property were sourced online through ENDM's Assessment File Research Imaging (AFRI) database. Very limited documented work has been completed on the Property. A trench is shown on map M2194 east of Copper Lake, however there is no documented files in the AFRI database regarding this work.

1996: Panterra Minerals Inc. completed a fixed-wing airborne geophysical survey consisting of magnetic and spectrometer data collection.

## 4. GEOLOGICAL SETTING AND MINERALIZATION

### 4.1 Regional Geology

The Property is located within the southern part of the Cobalt Embayment which lies within the south margin of the Superior Structural Province of the Canadian Shield. The regional geology consists of early Precambrian metavolcanics and metasediments which correlate with the 2,737 Ma Chambers-Briggs Assemblage, part of the Temagami Greenstone Belt (Jackson \& Fyon, 1991). These rocks are intruded by vertical Matachewan diabase dykes dated at 2,454 Ma. In the Property area, these older rocks are unconformably overlain by Middle Precambrian Huronian sedimentary rocks deposited between 2,220 and 2,500 Ma. Nipissing Diabase sills, relatively flat lying and dated at 2,219 Ma, intrude the Huronian and older rocks (Bennett, Dressler, \& Robertson, 1991). The youngest rocks in the area are olivine diabase dykes, dated at $1,238 \mathrm{Ma}$ (Osmani, 1991).

### 4.2 Property Geology

The Property is located within the Cobalt embayment at the south margin of the Superior Province of the Canadian Shield (Figure 3). The Property geology is dominated by sedimentary rocks belonging to the Coleman Formation, part of the Huronian Supergroup. According to map M2194, the predominant rock types include quartzose siltstones and greywackes, followed by lesser amounts of conglomerate. Nipissing diabase has been intruded as a sill east of Copper Lake, which overlies the Coleman Formation rocks.

A northwestern trending olivine diabase dyke is also shown southwest of Copper Lake. All of the rock types have been block faulted along predominantly west-northwest, and northwest trending faults that are part of the Lake Temiskaming Structural Zone, which is spatially associated with kimberlite intrusions in the area.


Figure 3: Property Geology

## 5. SUMMARY OF HELICOPTER-BORNE VERSATILE DOMAIN ELECTROMAGNETIC AND AEROMAGNETIC SURVEY

From February $10^{\text {th }}$ to $12^{\text {th }}$, 2021, Geotech Ltd. completed a helicopter-borne geophysical survey over the Starburst Property. Principal geophysical sensors included a versatile time domain electromagnetic (VTEM Max) system, as well as a caesium magnetometer. Ancillary equipment included a GPS navigation systema and a radar altimeter. A total of 135 linekilometres of geophysical data was acquired during the survey, cover an area of 24 km 2 . Flight lines were spaced at 100 m intervals, oriented north-south, with perpendicular tie lines spaced at $1,000 \mathrm{~m}$ intervals.

A detailed report completed by Geotech Ltd. can be found in Appendix II, and map products can be found in Appendix III.

## 6. INTERPRETATION AND CONCLUSIONS

The helicopter-borne versatile time domain electromagnetic (VTEM Max) and magnetic geophysical survey completed by Geotech Ltd. over the Starburst Property identified a number of geophysical (both magnetic and electromagnetic) anomalies. The primary anomaly of interest is a large circular magnetic feature located to the north of the Property which may represent a buried mafic intrusion. If possible, the claims covering the anomaly should be acquired, followed by geological mapping and ground truthing over the anomaly. Diamond drilling will likely be required to explain this anomaly.

## 19. REFERENCES

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Osmani, I. 1991. Proterozoic Mafic Dike Swarms in the Superior Province of Ontario, in Geology of Ontario, Ontario Geological Survey, Special Volume 4, Part 1. p. 661-681.

Percival, J.A., Easton, R.M. 2007. Geology of the Canadian Shield in Ontario: An update; Geological Survey of Canada, Open File 5511, Ontario Geological Survey, Miscellaneous Release Data 216.

## APPENDIX I: STATEMENT OF QUALIFICATIONS

## STATEMENT OF QUALIFICATIONS

I, Joerg Martin Kleinboeck of 147 Lakeside Drive, North Bay, Ontario, do hereby certify that: I am a graduate of Laurentian University, Sudbury, Ontario with a B.Sc. Geology, 2000, and have been practising my profession as a geologist since.

I am a member with the Association of Professional Geoscientists of Ontario (\#1411).
I have an active prospector's license for the province of Ontario (\#1002600).
I am a member of the Prospectors and Developers Association of Canada.
I do not hold any interest or rights in the subject Property.


Joerg Martin Kleinboeck
February 3 ${ }^{\text {rd }}, 2022$
North Bay, Ontario

## APPENDIX II: GEOPHYSICAL REPORT

## VTEM ${ }^{\text {TM }}$ Max

REPORT ON A HELICOPTER-BORNE VERSATILE TIME DOMAIN ELECTROMAGNETIC (VTEM ${ }^{\text {™ }}$ Max) AND AEROMAGNETIC GEOPHYSICAL SURVEY

| PROJECT: | STARBURST PROJECT |
| :--- | :--- |
| LOCATION: | TEMAGAMI, ON |
| FOR: | TOM OBRADOVICH |
| SURVEY FLOWN: | FEBRUARY 2021 |
| PROJECT: | GL180320 |

JUNE 2021

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## EXECUTIVE SUMMARY

## STARBURST PROJECT <br> TEMAGAMI, ON

During February $10^{\text {th }}$ to February $12^{\text {th }}$, 2021, Geotech Ltd. carried out a helicopter-borne geophysical survey over the Starburst Project situated near Temagami, ON.

Principal geophysical sensors included a versatile time domain electromagnetic (VTEM ${ }^{m m}$ Max) system and a caesium magnetometer. Ancillary equipment included a GPS navigation system and a radar altimeter. A total of 135 line-kilometres of geophysical data were acquired during the survey.

In-field data quality assurance and preliminary processing were carried out on a daily basis during the acquisition phase. Preliminary and final data processing, including generation of final digital data and map products were undertaken from the office of Geotech Ltd. in Aurora, Ontario.

The processed survey results are presented as the following maps:

- Electromagnetic stacked profiles of the B-field Z Component,
- Electromagnetic stacked profiles of dB/dt Z Components,
- B-Field Z Component Channel grid
- dB/dt Z Component Channel grid
- Fraser Filtered dB/dt X Component Channel grid,
- Total Magnetic Intensity (TMI)
- Calculated Magnetic Vertical Derivative (CVG)
- Calculated Z component Time Constant (Tau) with Calculated Vertical Derivative contours,
- Resistivity Depth Image (RDI) cross sections and depth-slices.

Digital data includes all electromagnetic and magnetic products, plus ancillary data including the waveform.

The survey report describes the procedures for data acquisition, description of equipment, processing, final image presentation and the specifications for the digital data set.

## 1. INTRODUCTION

### 1.1 GENERAL CONSIDERATIONS

Geotech Ltd. performed a helicopter-borne geophysical survey over Starburst Project situated near Temagami, ON (Figure 1 \& Figure 2).

Tom Obradovich represented his company during the data acquisition and data processing phases of this project.

The geophysical surveys consisted of helicopter borne EM using the versatile time-domain electromagnetic (VTEM ${ }^{\text {TM }}$ ) Max system with Full-Waveform processing. Measurements consisted of Vertical (Z), In-line, and Crossline Horizontal (X \& Y) components of the EM fields using an induction coil and the aeromagnetic total field using a caesium magnetometer. A total of 135 line-km of geophysical data were acquired during the survey.

The crew was based out of Temagami, ON (Figure 2) for the acquisition phase of the survey. Survey flying started on February 10 th and was completed on February 12 ${ }^{\text {th, }} 2021$.

Data quality control and quality assurance, and preliminary data processing were carried out on a daily basis during the acquisition phase of the project. Final data processing followed immediately after the end of the survey. Final reporting, data presentation and archiving were completed from the Aurora office of Geotech Ltd. in June 2021.


Figure 1: Survey location

### 1.2 SURVEY AND SYSTEM SPECIFICATIONS

The Starburst Project survey area is located approximately 21 kilometres northeast of Temagami, ON (Figure 2).


Figure 2: Survey area location on Google Earth.

The survey area was flown in a south to north ( $\mathrm{N} 0^{\circ} \mathrm{E}$ azimuth) direction with traverse line spacing of 100 metres as depicted in Figure 3. Tie lines were flown perpendicular to the traverse lines at 1000 metre spacing. For more detailed information on the flight spacing and direction, see Table 1.

### 1.3 TOPOGRAPHIC RELIEF AND CULTURAL FEATURES

Topographically, the survey area exhibits relief with elevations ranging from 179 to 385 metres above mean sea level over an area of 24 square kilometres (Figure 3).

There are several lakes and rivers in the Starburst project area, along with signs of culture such as roads and powerlines.


Figure 3: Flight path over a Google Earth Image

## 2. DATA ACQUISITION

### 2.1 SURVEY AREA

The survey area (see Figure 3 and Appendix A) and general flight specifications are as follows:

Table 1: Survey Specifications

| Survey block | Line spacing $(\mathrm{m})$ | Area <br> $\left(\mathrm{Km}^{2}\right)$ | Planned <br> Line-km | Actual <br> Line-km | Flight direction | Line numbers |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Starburst Project | Traverse: 100 | 24 | 132 | 135 | $\mathrm{~N} 0^{\circ} \mathrm{E} / \mathrm{N} 180^{\circ} \mathrm{E}$ | $\mathrm{L} 1000-\mathrm{L} 1230$ |
|  | Tie: 1000 | $242000-\mathrm{N} 90^{\circ} \mathrm{E} / \mathrm{N} 270^{\circ} \mathrm{E}$ | $\mathrm{T} 2000-\mathrm{T} 2030$ |  |  |  |
| Total |  | 24 | 132 | 135 |  |  |

Survey area boundaries co-ordinates are provided in Appendix B.

### 2.2 SURVEY OPERATIONS

Survey operations were based out of Temagami, ON from February 10 th until February 12 th, 2021. The following table shows the timing of the flying.

Table 2: Survey schedule

| Date |  |
| :---: | :--- |
| $02 / 10 / 2021$ | Production Flight -86.60 km flown |
| $02 / 11 / 2021$ | Production Flight -86.60 km flown |
| $02 / 12 / 2021$ | Demobilization |

[^0]
### 2.3 FLIGHT SPECIFICATIONS

During the survey, the helicopter was maintained at a mean altitude of 114 metres with an average survey speed of $70 \mathrm{~km} / \mathrm{hour}$. This allowed for an actual average Transmitter-receiver loop terrain clearance of 65 metres and a magnetic sensor clearance of 104 metres.

The on-board operator was responsible for monitoring the system integrity. He also maintained a detailed flight log during the survey, tracking the times of the flight as well as any unusual geophysical or topographic features.

On return of the aircrew to the base camp the survey data was transferred from a compact flash card (PCMCIA) to the data processing computer. The data were then uploaded via ftp to the Geotech office in Aurora for daily quality assurance and quality control by qualified personnel.

### 2.4 AIRCRAFT AND EQUIPMENT

### 2.4.1 SURVEY AIRCRAFT

The survey was flown using an Aerospatiale (A-star) 350 B3 helicopter, registration C-FBZN. The helicopter is owned and operated by Geotech Aviation. Installation of the geophysical and ancillary equipment was carried out by a Geotech Ltd crew.

### 2.4.2 ELECTROMAGNETIC SYSTEM

The electromagnetic system was a Geotech Time Domain EM (VTEM ${ }^{\text {TM }}$ Max) full receiver-waveform streamed data recorded system. The "full waveform VTEM system" uses the streamed half-cycle recording of transmitter and receiver waveforms to obtain a complete system response calibration throughout the entire survey flight. VTEM with the Serial number 35 had been used for the survey. The VTEM ${ }^{T M}$ transmitter current waveform is shown diagrammatically in Figure 4.

The VTEM ${ }^{\text {TM }}$ Receiver and transmitter coils were in concentric-coplanar and Z-direction oriented configuration. The receiver system for the project also included a coincident-coaxial X-direction coil to measure the in-line $\mathrm{dB} / \mathrm{dt}$ and calculate B-Field responses. The Transmitter-receiver loop was towed at a mean distance of 49 metres below the aircraft as shown in Figure 5.

## GL180320 Waveform



Figure 4: VTEM ${ }^{\text {TM }}$ Transmitter Current Waveform
The VTEM ${ }^{\text {TM }}$ decay sampling scheme is shown in Table 3 below. Forty-three time measurement gates were used for the final data processing in the range from 0.021 to 8.083 msec . Zero time for the offtime sampling scheme is equal to the current pulse width and is defined as the time near the end of the turn-off ramp where the $\mathrm{dI} / \mathrm{dt}$ waveform falls to $1 / 2$ of its peak value.

Table 3: Off-Time Decay Sampling Scheme

| VTEM max $^{\text {TM }}$ Decay |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Index |  |  |  |  |
| Start |  |  |  |  |
| End |  |  |  |  |
| Milliseconds |  |  |  |  |
| Middle |  |  |  |  |
| 4 | 0.018 | 0.023 | 0.021 | 0.005 |
| 5 | 0.023 | 0.029 | 0.026 | 0.005 |
| 6 | 0.029 | 0.034 | 0.031 | 0.005 |
| 7 | 0.034 | 0.039 | 0.036 | 0.005 |
| 8 | 0.039 | 0.045 | 0.042 | 0.006 |
| 9 | 0.045 | 0.051 | 0.048 | 0.007 |
| 10 | 0.051 | 0.059 | 0.055 | 0.008 |
| 11 | 0.059 | 0.068 | 0.063 | 0.009 |
| 12 | 0.068 | 0.078 | 0.073 | 0.010 |
| 13 | 0.078 | 0.090 | 0.083 | 0.012 |
| 14 | 0.090 | 0.103 | 0.096 | 0.013 |
| 15 | 0.103 | 0.118 | 0.110 | 0.015 |
| 16 | 0.118 | 0.136 | 0.126 | 0.018 |
| 17 | 0.136 | 0.156 | 0.145 | 0.020 |
| 18 | 0.156 | 0.179 | 0.167 | 0.023 |
| 19 | 0.179 | 0.206 | 0.192 | 0.027 |
| 20 | 0.206 | 0.236 | 0.220 | 0.030 |
| 21 | 0.236 | 0.271 | 0.253 | 0.035 |
| 22 | 0.271 | 0.312 | 0.290 | 0.040 |


| VTEM max ${ }^{\text {TM }}$ Decay Sampling Scheme |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Index |  |  |  |  |
| Start |  |  |  |  |
| End |  |  |  |  |
| Milliseconds |  |  |  |  |
| 23 | 0.312 | 0.358 | 0.333 | 0.046 |
| 24 | 0.358 | 0.411 | 0.383 | 0.053 |
| 25 | 0.411 | 0.472 | 0.440 | 0.061 |
| 26 | 0.472 | 0.543 | 0.505 | 0.070 |
| 27 | 0.543 | 0.623 | 0.580 | 0.081 |
| 28 | 0.623 | 0.716 | 0.667 | 0.093 |
| 29 | 0.716 | 0.823 | 0.766 | 0.107 |
| 30 | 0.823 | 0.945 | 0.880 | 0.122 |
| 31 | 0.945 | 1.086 | 1.010 | 0.141 |
| 32 | 1.086 | 1.247 | 1.161 | 0.161 |
| 33 | 1.247 | 1.432 | 1.333 | 0.185 |
| 34 | 1.432 | 1.646 | 1.531 | 0.214 |
| 35 | 1.646 | 1.891 | 1.760 | 0.245 |
| 36 | 1.891 | 2.172 | 2.021 | 0.281 |
| 37 | 2.172 | 2.495 | 2.323 | 0.323 |
| 38 | 2.495 | 2.865 | 2.667 | 0.370 |
| 39 | 2.865 | 3.292 | 3.063 | 0.427 |
| 40 | 3.292 | 3.781 | 3.521 | 0.490 |
| 41 | 3.781 | 4.341 | 4.042 | 0.560 |
| 42 | 4.341 | 4.987 | 4.641 | 0.646 |
| 43 | 4.987 | 5.729 | 5.333 | 0.742 |
| 44 | 5.729 | 6.581 | 6.125 | 0.852 |
| 45 | 6.581 | 7.560 | 7.036 | 0.979 |
| 46 | 7.560 | 8.685 | 8.083 | 1.125 |
|  |  |  |  |  |

Z Component: 4-46 time gates
X Component: 20-46 time gates
Y Component: 20-46 time gates

VTEM $^{\text {TM }}$ system specifications:

| Transmitter | Receiver |
| :---: | :---: |
| - Transmitter loop diameter: 35 m <br> - Number of turns: 4 <br> - Effective Transmitter loop area: $3849 \mathrm{~m}^{2}$ <br> - Transmitter base frequency: 30 Hz <br> - Peak current: 171 A <br> - Pulse width: 7.29 ms <br> - Waveform shape: Bi-polar trapezoid <br> - Peak dipole moment: 659,625 nIA <br> - Average transmitter-receiver loop terrain clearance: 65 metres above the ground | - X Coil diameter: 0.32 m <br> - Number of turns: 245 <br> - Effective coil area: $19.69 \mathrm{~m}^{2}$ <br> - Y Coil diameter: 0.32 m <br> - Number of turns: 245 <br> - Effective coil area: $19.69 \mathrm{~m}^{2}$ <br> - Z-Coil diameter: 1.2 m <br> - Number of turns: 100 <br> - Effective coil area: $113.04 \mathrm{~m}^{2}$ |



Figure 5: VTEM ${ }^{T M}$ max System Configuration.

### 2.4.3 Airborne Magnetometer

The magnetic sensor utilized for the survey was Geometrics optically pumped caesium vapour magnetic field sensor mounted 10 metres below the helicopter, as shown in Figure 5. The sensitivity of the magnetic sensor is 0.02 nanoTesla ( nT ) at a sampling interval of 0.1 seconds.

### 2.4.4 FULL WAVEFORM VTEM ${ }^{\text {TM }}$ SENSOR CALIBRATION

The calibration is performed on the complete VTEM ${ }^{T M}$ system installed in and connected to the helicopter, using special calibration equipment. This calibration takes place on the ground at the start of the project prior to surveying.

The procedure takes half-cycle files acquired and calculates a calibration file consisting of a single stacked half-cycle waveform. The purpose of the stacking is to attenuate natural and man-made magnetic signals, leaving only the response to the calibration signal.

This calibration allows the transfer function between the EM receiver and data acquisition system and also the transfer function of the current monitor and data acquisition system to be determined. These calibration results are then used in VTEM full waveform processing.

### 2.4.5 Radar Altimeter

A Terra TRA 3000/TRI 40 radar altimeter was used to record terrain clearance. The antenna was mounted beneath the bubble of the helicopter cockpit (Figure 5).

### 2.4.6 GPS Navigation System

The navigation system used was a Geotech PC104 based navigation system utilizing a NovAtel's WAAS (Wide Area Augmentation System) enabled GPS receiver, Geotech navigate software, a full screen display with controls in front of the pilot to direct the flight and a NovAtel GPS antenna mounted on the helicopter tail (Figure 5). As many as 11 GPS and two WAAS satellites may be monitored at any one time. The positional accuracy or circular error probability (CEP) is 1.8 m , with WAAS active, it is 1.0 m . The co-ordinates of the survey area were set-up prior to the survey and the information was fed into the airborne navigation system.

### 2.4.7 Digital AcQuisition System

A Geotech data acquisition system recorded the digital survey data on an internal compact flash card. Data is displayed on an LCD screen as traces to allow the operator to monitor the integrity of the system. The data type and sampling interval as provided in Table 4.

Table 4: Acquisition Sampling Rates

| Data Type | Sampling |
| :--- | :--- |
| TDEM | 0.1 sec |
| Magnetometer | 0.1 sec |
| GPS Position | 0.2 sec |
| Radar Altimeter | 0.2 sec |
| Inclinometer | 0.1 sec |

### 2.5 BASE STATION

A combined magnetometer/GPS base station was utilized on this project. A Geometrics Caesium vapour magnetometer was used as a magnetic sensor with a sensitivity of 0.001 nT . The base station was recording the magnetic field together with the GPS time at 1 Hz on a base station computer.

The base station magnetometer sensor was installed in a secured location away from culture and electric transmission lines and moving ferrous objects such as motor vehicles. The base station data were backed-up to the data processing computer at the end of each survey day.

## 3. PERSONNEL

The following Geotech Ltd. personnel were involved in the project.
FIELD:

| Project Manager: | TaiChyi Shei (Office) |
| :--- | :--- |
| Data QC: | Marta Orta |
| Crew chief: | Paul Taylor <br> Colin Lennox |
| Operator: | Juan Carlos Florez Osorio |
|  | Juan Carlos Florez Osorio |

The survey pilot and the mechanical engineer were employed directly by the helicopter operator Geotech Aviation.

| Pilot: | Steve McGreer <br> Bill Hofstede |
| :--- | :--- |
| Mechanical Engineer: | Barry Orme |
| OFFICE: |  |
| Preliminary Data Processing: | Marta Orta |
| Final Data Processing: | Emily Data |
| Data QA/QC: | Keeme Mokubung <br> Jean M. Legault |
| Reporting/Mapping: | Moyosore Lanisa |

Processing and Interpretation phases were carried out by Emily Data under the supervision of Keeme Mokubung \& Jean M. Legault, M.Sc.A, P.Eng, and P.Geo - Chief Geophysicist. The customer relations were looked after by Jean Legault.

## 4. DATA PROCESSING AND PRESENTATION

Data compilation and processing were carried out by the application of Geosoft OASIS Montaj and programs proprietary to Geotech Ltd.

### 4.1 FLIGHT PATH

The flight path, recorded by the acquisition program as WGS 84 latitude/longitude, was converted into the WGS84 UTM Zone 17 North coordinate system in Oasis Montaj.

The flight path was drawn using linear interpolation between x , y positions from the navigation system. Positions are updated every second and expressed as UTM easting's ( x ) and UTM northing's (y).

### 4.2 ELECTROMAGNETIC DATA

The Full Waveform EM specific data processing operations included:

- Half cycle stacking (performed at time of acquisition);
- System response correction;
- Parasitic and drift removal.

A three-stage digital filtering process was used to reject major sferic events and to reduce noise levels. Local sferic activity can produce sharp, large amplitude events that cannot be removed by conventional filtering procedures. Smoothing or stacking will reduce their amplitude but leave a broader residual response that can be confused with geological phenomena. To avoid this possibility, a computer algorithm searches out and rejects the major sferic events.

The signal to noise ratio was further improved by the application of a low pass linear digital filter. This filter has zero phase shift which prevents any lag or peak displacement from occurring, and it suppresses only variations with a wavelength less than about 1 second or 15 metres. This filter is a symmetrical 1 sec linear filter.

The results are presented as stacked profiles of EM voltages for the time gates, in linear - logarithmic scale for the B-field Z component and $\mathrm{dB} / \mathrm{dt}$ responses in the Z and X components. B-field Z component time channel recorded at 1.760 milliseconds after the termination of the impulse is also presented as a colour image. Calculated Time Constant (TAU) with Calculated Vertical Derivative contours is presented in Appendix C. Resistivity Depth Image (RDI) is also presented in Appendix G.

VTEM $^{\text {TM }}$ has three receiver coil orientations. Z-axis coil is oriented parallel to the transmitter coil axis and both are horizontal to the ground. The X -axis coil is oriented parallel to the ground and along the line-of-flight. The Y-axis coil is oriented parallel to the ground and perpendicular to the line-of-flight. This combined three-coil configuration provides information on the position, depth, dip and thickness of a conductor. Generalized modeling results of VTEM data, are shown in Appendix D.

In general X-component data produce cross-over type anomalies: from "+ to - "in flight direction of flight for "thin" sub vertical targets and from "- to +" in direction of flight for "thick" targets. Z component data produce double peak type anomalies for "thin" sub vertical targets and single peak for "thick" targets.

The limits and change-over of "thin-thick" depends on dimensions of a TEM system (Appendix D, Figure D-16).

Because of X component polarity is under line-of-flight, convolution Fraser Filter (Figure 6) is applied to X component data to represent axes of conductors in the form of grid map. In this case positive FF anomalies always correspond to "plus-to-minus" X data crossovers independent of the flight direction.


Figure 6: $\mathrm{Z}, \mathrm{X}$ and Fraser filtered X (FFx) components for "thin" target.

### 4.3 MAGNETIC DATA

The processing of the magnetic data involved the correction for diurnal variations by using the digitally recorded ground base station magnetic values. The base station magnetometer data was edited and merged into the Geosoft GDB database on a daily basis. The aeromagnetic data was corrected for diurnal variations by subtracting the observed magnetic base station deviations.

Tie line levelling was carried out by adjusting intersection points along traverse lines. A microlevelling procedure was applied to remove persistent low-amplitude components of flight-line noise remaining in the data.

The corrected magnetic data was interpolated between survey lines using a random point gridding method to yield $x-y$ grid values for a standard grid cell size of approximately 25 metres at the mapping scale. The Minimum Curvature algorithm was used to interpolate values onto a rectangular regular spaced grid.

### 4.4 TAU PARAMETER AND CVG CALCULATION

The processed VTEM survey results are presented as a calculated Z-component dB/dt time constant (Tau), which is an indicator of geological unit's electrical conductance.

An explanation of the EM decay time constant calculation is provided in Appendix F . The TAU dB $\mathrm{d}_{\mathrm{Z}} / \mathrm{dt}$ map is presented in Appendix C. The map is accompanied by an overlay of the calculated vertical gradient of TMI anomaly contours for tracing possible EM-MAG anomaly correlations.

The CVG contour layer, on the top of TAU colour grid, generally is more representative of the smaller scale and shallower magnetic sources in comparison with the TMI. CVG is designed to emphasize the structures and lithological units that might not otherwise be seen on the TMI due to the nearby presence of stronger magnetic responses, showing a high resolution in terms of individual structures.

The combined TAU-CVG map will indicate how well the most highly conductive targets (with maximal TAU) are correlated with either magnetic or non-magnetic sources in the bedrock geology.

## 5. DELIVERABLES

### 5.1 SURVEY REPORT

The survey report describes the data acquisition, processing, and final presentation of the survey results. The survey report is provided in two paper copies and digitally in PDF format.

### 5.2 MAPS

Final maps were produced at scale of 1:15,000 for best representation of the survey size and line spacing. The coordinate/projection system used was WGS84 Datum, UTM Zone 17 North. All maps show the flight path trace and topographic data; latitude and longitude are also noted on maps.

The results of the survey are presented as EM profiles, a late-time gate gridded EM channel, and a colour magnetic TMI contour map.

- Maps at 1:15,000 in Geosoft MAP format, as follows:

| GL180320_**_dBdt: | dB/dt profiles Z Component, Time Gates 0.220-7.036 ms <br> in linear - logarithmic scale. |
| :--- | :--- |
| GL180320_**_BField: | B-field profiles Z Component, Time Gates 0.220-7.036 <br> ms in linear - logarithmic scale. |
| GL180320_**_BFz35: | B-field late time Z Component Channel 35, Time Gate <br> 1.760 ms colour image. |
| GL180320_**_SFxFF25: | Fraser Filtered dB/dt X Component Channel 25, Time <br> Gate 0.440 ms colour image. |
| GL180320_**_SFz30: | VTEM dB/dt Z Component Channel 30, Time Gate 0.880 <br> ms. |
| GL180320_**_TauSF: | Mid-Time dB/dt Calculated Time Constant (Tau) with <br> Calculated Vertical Derivative of TMI contours. |
| GL180320_**TMI: | Total magnetic intensity colour image and contours. <br> Calculated Vertical Derivative of Total Magnetic Intensity, <br> GL180320_*_CVG: |
|  | colour image. |

Where ** represents company and map scale, eg. GL180320_TomObradovich_15K_BFz35.map

- Maps are also presented in PDF format.
- The topographic base and inset map data were derived from 1:250,000 CANVEC data. Background shading is derived from ASTER GDEM (https://gdex.cr.usgs.gov/gdex/).
- A Google Earth file GL180320_TomObradovich.kml showing the flight path of the block is included. Free versions of Google Earth software from: http://earth.google.com/downloadearth.html


### 5.3 DIGITAL DATA

Two copies of the data and maps on DVD were prepared to accompany the report. Each DVD contains a digital file of the line data in GDB Geosoft Montaj format as well as the maps in Geosoft Montaj Map and PDF format.

- DVD structure.

Data contains databases, grids and maps, as described below.
Report contains a copy of the report and appendices in PDF format.
Databases in Geosoft GDB format, containing the channels listed in Table 5.
Table 5: Geosoft GDB Data Format

| Channel name | Units | Description |
| :---: | :---: | :---: |
| X | metres | UTM Easting NAD83 Zone 17 North |
| Y | metres | UTM Northing NAD83 Zone 17 North |
| Longitude | Decimal Degrees | WGS 84 Longitude data |
| Latitude | Decimal Degrees | WGS 84 Latitude data |
| Z | metres | GPS antenna elevation (above Geoid) |
| Zb | metres | EM bird elevation (above Geoid) |
| Radar | metres | helicopter terrain clearance from radar altimeter |
| Radarb | metres | Calculated EM transmitter-receiver loop terrain clearance from radar altimeter |
| DEM | metres | Digital Elevation Model |
| GTime | Seconds of the day | GPS time |
| Basemag | nT | Magnetic diurnal variation data |
| Mag1 | nT | Raw Total Magnetic field data |
| Mag2 | nT | Diurnal corrected Total Magnetic field data |
| Mag3 | nT | Levelled Total Magnetic field data |
| CVG | $\mathrm{nT} / \mathrm{m}$ | Calculated Magnetic Vertical Gradient |
| SFz[4] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m} 4\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.021$ millisecond time channel |
| SFz[5] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m} 4\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.026$ millisecond time channel |
| SFz[6] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.031$ millisecond time channel |
| SFz[7] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.036$ millisecond time channel |
| SFz[8] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 0.042$ millisecond time channel |
| SFz[9] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 0.048$ millisecond time channel |
| SFz[10] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.055$ millisecond time channel |
| SFz[11] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.063$ millisecond time channel |
| SFz[12] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.073$ millisecond time channel |
| SFz[13] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 0.083$ millisecond time channel |
| SFz[14] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.096$ millisecond time channel |
| SFz[15] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.110$ millisecond time channel |
| SFz[16] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 0.126$ millisecond time channel |
| SFz[17] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 0.145$ millisecond time channel |
| SFz[18] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.167$ millisecond time channel |
| SFz[19] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.192$ millisecond time channel |
| SFz[20] | $\mathrm{pV} /\left(\mathrm{A} \mathrm{m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.220$ millisecond time channel |
| SFz[21] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.253$ millisecond time channel |
| SFz[22] | $\mathrm{pV} /\left(\mathrm{A} \mathrm{m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.290$ millisecond time channel |
| SFz[23] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 0.333$ millisecond time channel |

Survey for Tom Obradovich

| Channel name | Units | Description |
| :---: | :---: | :---: |
| SFz[24] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | Z dB/dt 0.383 millisecond time channel |
| SFz[25] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.440$ millisecond time channel |
| SFz[26] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | Z dB/dt 0.505 millisecond time channel |
| SFz[27] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 0.580$ millisecond time channel |
| SFz[28] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 0.667$ millisecond time channel |
| SFz[29] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 0.766$ millisecond time channel |
| SFz[30] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 0.880$ millisecond time channel |
| SFz[31] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | Z dB/dt 1.010 millisecond time channel |
| SFz[32] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 1.161$ millisecond time channel |
| SFz[33] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 1.333$ millisecond time channel |
| SFz[34] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | Z dB/dt 1.531 millisecond time channel |
| SFz[35] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 1.760$ millisecond time channel |
| SFz[36] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 2.021$ millisecond time channel |
| SFz[37] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 2.323$ millisecond time channel |
| SFz[38] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 2.667$ millisecond time channel |
| SFz[39] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 3.063$ millisecond time channel |
| SFz[40] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 3.521$ millisecond time channel |
| SFz[41] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB} / \mathrm{dt} 4.042$ millisecond time channel |
| SFz[42] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | Z dB/dt 4.641 millisecond time channel |
| SFz[43] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 5.333$ millisecond time channel |
| SFz[44] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 6.125$ millisecond time channel |
| SFz[45] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | Z dB/dt 7.036 millisecond time channel |
| SFz[46] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Z} \mathrm{dB/dt} 8.083$ millisecond time channel |
| SFx[20] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 0.220$ millisecond time channel |
| SFx[21] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | X dB/dt 0.253 millisecond time channel |
| SFx[22] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | X dB/dt 0.290 millisecond time channel |
| SFx[23] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 0.333$ millisecond time channel |
| SFx[24] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB} / \mathrm{dt} 0.383$ millisecond time channel |
| SFx[25] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB} / \mathrm{dt} 0.440$ millisecond time channel |
| SFx[26] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 0.505$ millisecond time channel |
| SFx[27] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $X \mathrm{~dB} / \mathrm{dt} 0.580$ millisecond time channel |
| SFx[28] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 0.667$ millisecond time channel |
| SFx[29] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 0.766$ millisecond time channel |
| SFx[30] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 0.880$ millisecond time channel |
| SFx[31] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 1.010$ millisecond time channel |
| SFx[32] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{XdB} / \mathrm{dt} 1.161$ millisecond time channel |
| SFx[33] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{XdB} / \mathrm{dt} 1.333$ millisecond time channel |
| SFx[34] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 1.531$ millisecond time channel |
| SFx[35] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 1.760$ millisecond time channel |
| SFx[36] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{XdB} / \mathrm{dt} 2.021$ millisecond time channel |
| SFx[37] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 2.323$ millisecond time channel |
| SFx[38] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $X \mathrm{~dB} / \mathrm{dt} 2.667$ millisecond time channel |
| SFx[39] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 3.063$ millisecond time channel |
| SFx[40] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $X \mathrm{~dB} / \mathrm{dt} 3.521$ millisecond time channel |
| SFx[41] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB} / \mathrm{dt} 4.042$ millisecond time channel |
| SFx[42] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $X \mathrm{~dB} / \mathrm{dt} 4.641$ millisecond time channel |
| SFx[43] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 5.333$ millisecond time channel |
| SFx[44] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{XdB} / \mathrm{dt} 6.125$ millisecond time channel |
| SFx[45] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $X \mathrm{~dB} / \mathrm{dt} 7.036$ millisecond time channel |
| SFx[46] | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{X} \mathrm{dB/dt} 8.083$ millisecond time channel |


| Channel name | Units | Description |
| :---: | :---: | :---: |
| SFy | $\left(\mathrm{pV}^{*} \mathrm{~ms}\right) /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | $\mathrm{Y} \mathrm{dB} / \mathrm{dt} \mathrm{data} \mathrm{for} \mathrm{time} \mathrm{channels} \mathrm{4} \mathrm{to} \mathrm{48}$ |
| BFz | $\left(\mathrm{pV}^{*} \mathrm{~ms}\right) /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | Z B-Field data for time channels 4 to 48 |
| BFy | $\left(\mathrm{pV}^{*} \mathrm{~ms}\right) /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | Y B-Field data for time channels 4 to 48 |
| BFx | $\left(\mathrm{pV}^{*} \mathrm{~ms}\right) /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | X B-Field data for time channels 20 to 48 |
| SFxFF | $\mathrm{pV} /\left(\mathrm{A}^{*} \mathrm{~m}^{4}\right)$ | Fraser Filtered X dB/dt for time channels 20 to 48 |
| NchanBF |  | Latest time channels of TAU calculation |
| TauBF | ms | Time constant B-Field |
| NchanSF |  | Latest time channels of TAU calculation |
| TauSF | ms | Time constant dB/dt |
| PLM |  | 60 Hz power line monitor |

Electromagnetic B-field and $\mathrm{dB} / \mathrm{dt} \mathrm{Z}$ component data is found in array channel format between indexes 4-46, and X \& Y component data from 20-46, as described above.

- Database of the Resistivity Depth Images in Geosoft GDB format, containing the following channels:

Table 6: Geosoft Resistivity Depth Image GDB Data Format

| Channel name | Units | Description |
| :---: | :---: | :---: |
| Xg | metres | UTM Easting NAD83 Zone 17 North |
| Yg | metres | UTM Northing NAD83 Zone 17 North |
| Dist: | metres | Distance from the beginning of the line |
| Depth: | metres | Array channel, depth from the surface |
| Z: | metres | Array channel, depth from sea level |
| AppRes: | Ohm-m | Array channel, Apparent Resistivity |
| TR: | metres | EM system height from sea level |
| Topo: | metres | digital elevation model |
| Radarb: | metres | Calculated EM transmitter-receiver loop terrain clearance from |
| radar altimeter |  |  |

- Resistivity Depth Image:

Sections contains apparent resistivity sections along each line in .GRD and .PDF format.
Slices contains apparent resistivity slices at selected depths from 25 m to depth of investigation, at an increment of 25 m in .GRD and .PDF format.
Voxel contains 3D Voxel imaging of apparent resistivity data clipped by digital elevation and depth of investigation.

- Database of the VTEM Waveform "GL180320_Waveform.gdb" in Geosoft GDB format, containing the following channels:

Table 7: Geosoft database for the VTEM waveform

| Channel name | Units | Description |
| :---: | :---: | :---: |
| Time: | milliseconds | Sampling rate interval, 5.2083 microseconds |
| Tx_Current: | amps | Output current of the transmitter |

- Grids in Geosoft GRD and GeoTIFF format, as follows:

| GL180320_BFz35: | B-Field Z Component Channel 35 (Time Gate 1.760 ms ) |
| :--- | :--- |
| GL180320_CVG: | Calculated Vertical Gradient (nT/m) |
| GL180320_DEM: | Digital Elevation Model (metres) |
| GL180320_Mag3: | Total Magnetic Intensity (nT) |
| GL180320_PLM: | Power Line Monitor |
| GL180320_SFxFF25: | Fraser Filtered dB/dt X Component Channel 25 (Time Gate |
|  | 0.440 ms) |
| GL180320_TauBF: | B-Field Z Component, Calculated Time Constant (ms) |
| GL180320_TauSF: | dB/dt Z Component, Calculated Time Constant (ms) |
| GL180320_SFz20: | dB/dt Z Component Channel 20 (Time Gate 0.220 ms ) |
| GL18032_SFz30: | dB/dt Z Component Channel 30 (Time Gate 0.880 ms ) |
| GL180320_SFz40: | dB/dt Z Component Channel 40 (Time Gate 3.521 ms ) |

A Geosoft .GRD file has a .GI metadata file associated with it, containing grid projection information. A grid cell size of 25 metres was used.

## 6. CONCLUSIONS AND RECOMMENDATIONS

A helicopter-borne versatile time domain electromagnetic (VTEM ${ }^{m}$ Max) and magnetic geophysical survey has been completed over Starburst Project situated near Temagami, ON.

The total area coverage is $24 \mathrm{~km}^{2}$. Total survey line coverage is 135 line-kilometres. The principal sensors included a time domain VTEM ${ }^{m "}$ Max system and a caesium magnetometer. Results have been presented as stacked profiles, and contour colour images at a scale of $1: 15,000$. A formal interpretation has not been included in this report, however RDI resistivity-depth imaging has been performed in support of the VTEM data.

Geophysical anomalies have been identified on the property, most notably a prominent, moderate strength ( $>350 \mathrm{nT}$ ), intrusion-like magnetic high feature that is centred in the northern half of the block. Other, weaker dyke-like, NW-SE lineaments are also noticeable, however the main geologic strike trend appears to be NE-SW. Although the EM response is dominated by a false conductive, sinuous lineament that is attributable to a roadside powerline in the northern and east part of the block, a shallow-buried, weak to moderate EM conductive anomaly (A) is defined in the center of the survey area (Figure 7). This NE-SW trending EM conductor has a $>700 \mathrm{~m}$ strike-length and sits on the southeastern flank of the prominent magnetic high. Based on the RDI depth slices, the top depth is approx. near surface to 25 metres and extends to $\sim 250 \mathrm{~m}$ depth, with anomalous resistivities as low as $\sim 50$ ohm-m. Other weakly conductive anomalies are defined throughout the block but could be attributed to conductive overburden.


Figure 7 - VTEM RDI resistivity depth slice at 100 m depth over Starburst Project, showing anomaly of interest (A).

The geophysical results at Starburst Project are visibly affected by man-made culture, including a roadside powerline that produces false conductive lineament anomalies and added EM Noise. Although magnetic features are far less affected, care should be exercised when evaluation anomalies on the block, particularly in the EM data.

The Starburst Project is believed to be prospective for polymetallic base metal MS style mineralization (J. Kleinboeck, pers. comm., 2018) and it is likely that both EM and magnetic results will be of exploration interest. We recommend that EM anomaly picking be performed along with Maxwell EM plate modeling of major anomalies of interest prior to ground follow up and drill testing. More advanced 1D layered earth modeling of the EM data will prove useful in establishing source-depth and layering of resistivity anomalies. Magnetic CET structural analysis and 3D MVI magnetic inversions will be useful for mapping structure, alteration, and lithology in 2D-3D space across the property. We recommend that more advanced, integrated interpretation be performed on these geophysical data and these results further evaluated against the known geology for future targeting.

Respectfully submitted ${ }^{2}$,


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June 2021.

[^1]
## APPENDIX A

## SURVEY AREA LOCATION MAP



Overview of the Survey Area

## APPENDIX B

SURVEY AREA COORDINATES
(WGS84, UTM Zone 17 North)

| $X$ | $Y$ |
| :---: | :---: |
| 612004 | 5219490 |
| 613210 | 5219506 |
| 613126 | 5222205 |
| 616642 | 5222222 |
| 616752 | 5216420 |
| 612013 | 5216353 |
| 612013 | 5219498 |



VTEM B-Field Z Component Profiles, Time Gates 0.220 to 7.036 ms over Total Magnetic Intensity, Reduced to Pole
${ }^{1}$ Complete full size geophysical maps are also available in PDF format located in the final data maps folder.


VTEM dB/dt Z Component Profiles, Time Gates 0.220 to 7.036 ms


VTEM dB/dt Z Component Channel 30, Time Gate 0.880 ms


VTEM B-Field Z Component Channel 35, Time Gate 1.760 ms


Fraser Filtered dB/dt X Component Channel 25 Time Gate 0.440 ms


Total Magnetic Intensity


Calculated Vertical Gradient of Total Magnetic Intensity (TMI)

dB/dt Z Component Calculated Time Constant (TauSF) with Calculated Vertical Derivative contours

## RESISTIVITY DEPTH IMAGE (RDI)



3D View of Resistivity-Depth Image (RDI)

## APPENDIX D

## GENERALIZED MODELING RESULTS OF THE VTEM SYSTEM INTRODUCTION

The VTEM system is based on a concentric or central loop design, whereby, the receiver is positioned at the centre of a transmitter loop that produces a primary field. The wave form is a bipolar, modified square wave with a turn-on and turn-off at each end.

During turn-on and turn-off, a time varying field is produced ( $\mathrm{dB} / \mathrm{dt}$ ) and an electro-motive force (emf) is created as a finite impulse response. A current ring around the transmitter loop moves outward and downward as time progresses. When conductive rocks and mineralization are encountered, a secondary field is created by mutual induction and measured by the receiver at the centre of the transmitter loop.

Efficient modeling of the results can be carried out on regularly shaped geometries, thus yielding close approximations to the parameters of the measured targets. The following is a description of a series of common models made for the purpose of promoting a general understanding of the measured results.

A set of models has been produced for the Geotech VTEM ${ }^{\text {M }}$ system $\mathrm{dB} / \mathrm{dT} \mathrm{Z}$ and X components (see models D1 to D15). The Maxwell ${ }^{\text {TM }}$ modeling program (EMIT Technology Pty. Ltd. Midland, WA, AU ) used to generate the following responses assumes a resistive half-space. The reader is encouraged to review these models, so as to get a general understanding of the responses as they apply to survey results. While these models do not begin to cover all possibilities, they give a general perspective on the simple and most commonly encountered anomalies.

As the plate dips and departs from the vertical position, the peaks become asymmetrical.
As the dip increases, the aspect ratio (Min/Max) decreases, and this aspect ratio can be used as an empirical guide to dip angles from near 90 o to about 30 . The method is not sensitive enough where dips are less than about 30 .

Figure D-5: horizontal thick plate (linear scale of the response)
Figure D-4: horizontal thin plate

Figure D-6: horizontal thick plate (log scale of the response) $\qquad$




The same type of target but with different thickness, for example, creates different form of the response:


Figure D-17: Conductive vertical plate, depth 50 m , strike length 200 m , depth extends 150 m .

Alexander Prikhodko, PhD, P.Geo
Geotech Ltd.
September 2010

## APPENDIX E

## EM TIME CONSTANT (TAU) ANALYSIS

Estimation of time constant parameter ${ }^{1}$ in transient electromagnetic method is one of the steps toward the extraction of the information about conductances beneath the surface from TEM measurements.

The most reliable method to discriminate or rank conductors from overburden, background or one and other is by calculating the EM field decay time constant (TAU parameter), which directly depends on conductance despite their depth and accordingly amplitude of the response.

## THEORY

As established in electromagnetic theory, the magnitude of the electro-motive force (emf) induced is proportional to the time rate of change of primary magnetic field at the conductor. This emf causes eddy currents to flow in the conductor with a characteristic transient decay, whose Time Constant (Tau) is a function of the conductance of the survey target or conductivity and geometry (including dimensions) of the target. The decaying currents generate a proportional secondary magnetic field, the time rate of change of which is measured by the receiver coil as induced voltage during the Off time.

The receiver coil output voltage ( $\mathbf{e}_{\mathbf{0}}$ ) is proportional to the time rate of change of the secondary magnetic field and has the form,

$$
\mathrm{e}_{0} \alpha(1 / \tau) \mathrm{e}^{-(\mathrm{t} / \tau)}
$$

Where,
$\tau=\mathrm{L} / \mathrm{R}$ is the characteristic time constant of the target (TAU)
$\mathrm{R}=$ resistance
$\mathrm{L}=$ inductance
From the expression, conductive targets that have small value of resistance and hence large value of $\tau$ yield signals with small initial amplitude that decays relatively slowly with progress of time. Conversely, signals from poorly conducting targets that have large resistance value and small $\tau$, have high initial amplitude but decay rapidly with time ${ }^{1}$ (Fig. E1).


Figure E-1: Left - presence of good conductor, right - poor conductor.

[^2]
## EM Time Constant (Tau) Calculation

The EM Time-Constant (TAU) is a general measure of the speed of decay of the electromagnetic response and indicates the presence of eddy currents in conductive sources as well as reflecting the "conductance quality" of a source. Although TAU can be calculated using either the measured $\mathrm{dB} / \mathrm{dt}$ decay or the calculated B-field decay, $\mathrm{dB} / \mathrm{dt}$ is commonly preferred due to better stability ( $\mathrm{S} / \mathrm{N}$ ) relating to signal noise. Generally, TAU calculated on base of early time response reflects both near surface overburden and poor conductors whereas, in the late ranges of time, deep and more conductive sources, respectively. For example, early time TAU distribution in an area that indicates conductive overburden is shown in Figure 2.


Figure E-2: Map of early time TAU. Area with overburden conductive layer and local sources.


Figure E-3: Map of full time-range TAU with EM anomaly due to deep highly conductive target.
There are many advantages of TAU maps:

- TAU depends only on one parameter (conductance) in contrast to response magnitude.
- TAU is an integral parameter, which covers time range, and all conductive zones and targets are displayed independently of their depth and conductivity on a single map.
- Very good differential resolution in complex conductive places with many sources with different conductivity.
- Signs of the presence of good conductive targets are amplified and emphasized independently of their depth and level of response accordingly.

In the example shown in Figure 4 and 5, three local targets are defined, each of them with a different depth of burial, as indicated on the resistivity depth image (RDI). All are very good conductors, but the deeper target (number 2) has a relatively weak $\mathrm{dB} / \mathrm{dt}$ signal yet also features the strongest total TAU (Figure 4). This example highlights the benefit of TAU analysis in terms of an additional target discrimination tool.


Figure E-4: dB/dt profile and RDI with different depths of targets.


Figure E-5: Map of total TAU and dB/dt profile.

The EM Time Constants for $\mathrm{dB} / \mathrm{dt}$ and B-field were calculated using the "sliding Tau" in-house program developed at Geotech2. The principle of the calculation is based on using of time window ( 4 time channels) which is sliding along the curve decay and looking for latest time channels which have a response above the level of noise and decay. The EM decays are obtained from all available decay channels, starting at the latest channel. Time constants are taken from a least square fit of a straight-line (log/linear space) over the last 4 gates above a pre-set signal threshold level (Figure F6). Threshold settings are pointed in the "label" property of TAU database channels. The sliding Tau method determines that, as the amplitudes increase, the time-constant is taken at progressively later times in the EM decay. Conversely, as the amplitudes decrease, Tau is taken at progressively earlier times in the decay. If the maximum signal amplitude falls below the threshold or becomes negative for any of the 4 time gates, then Tau is not calculated and is assigned a value of "dummy" by default.


Figure E-6: Typical dB/dt decays of VTEM data

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## APPENDIX F

## TEM RESISTIVITY DEPTH IMAGING (RDI)

Resistivity depth imaging (RDI) is technique used to rapidly convert EM profile decay data into an equivalent resistivity versus depth cross-section, by deconvolving the measured TEM data.
The used RDI algorithm of Resistivity-Depth transformation is based on scheme of the apparent resistivity transform of Maxwell A.Meju (1998) ${ }^{1}$ and TEM response from conductive half-space. The program is developed by Alexander Prikhodko and depth calibrated based on forward plate modeling for VTEM system configuration (Fig. 1-10).

RDIs provide reasonable indications of conductor relative depth and vertical extent, as well as accurate 1D layered-earth apparent conductivity/resistivity structure across VTEM flight lines. Approximate depth of investigation of a TEM system, image of secondary field distribution in half space, effective resistivity, initial geometry and position of conductive targets is the information obtained on base of the RDIs.

Maxwell forward modeling with RDI sections from the synthetic responses (VTEM system).


Figure F-1: Maxwell plate model and RDI from the calculated response for conductive "thin" plate (depth 50 m , dip 65 degrees, depth extend 100 m ).

[^3]

Figure F-2: Maxwell plate model and RDI from the calculated response for "thick" plate 18 m thickness, depth 50 m , depth extend 200 m ).


Figure F-3: Maxwell plate model and RDI from the calculated response for bulk ("thick") 100 m length, 40 m depth extend, 30 m thickness.


Figure F-4: Maxwell plate model and RDI from the calculated response for "thick" vertical target (depth 100 m , depth extend 100 m ). 19-44 chan.


Figure F-5: Maxwell plate model and RDI from the calculated response for horizontal thin plate (depth 50 m , dim $50 \times 100 \mathrm{~m}$ ). 15-44 chan.


Figure F-6: Maxwell plate model and RDI from the calculated response for horizontal thick (20m) plate less conductive (on the top), more conductive (below).


Figure F-7: Maxwell plate model and RDI from the calculated response for inclined thick ( 50 m ) plate. Depth extends 150 m , depth to the target 50 m .


Figure F-8: Maxwell plate model and RDI from the calculated response for the long, wide and deep subhorizontal plate (depth 140 m , dim $25 \times 500 \times 800 \mathrm{~m}$ ) with conductive overburden.


Figure F-9: Maxwell plate models and RDIs from the calculated response for "thick" dipping plates (35, $50,75 \mathrm{~m}$ thickness), depth 50 m , conductivity $2.5 \mathrm{~S} / \mathrm{m}$.


Figure F-10: Maxwell plate models and RDIs from the calculated response for "thick" ( 35 m thickness) dipping plate on different depth ( $50,100,150 \mathrm{~m}$ ), conductivity $2.5 \mathrm{~S} / \mathrm{m}$.


Figure F-11: RDI section for the real horizontal and slightly dipping conductive layers.

## FORMS OF RDI PRESENTATION

PRESENTATION OF SERIES OF LINES


3D PRESENTATION OF RDIS


## APPARENT RESISTIVITY DEPTH SLICES PLANS:



3D VIEWS OF APPARENT RESISTIVITY DEPTH SLICES:


## REAL BASE METAL TARGETS IN COMPARISON WITH RDIS:

RDI section of the line over Caber deposit ("thin" subvertical plate target and conductive overburden.


3D RDI VOXELS WITH BASE METALS ORE BODIES (MIDDLE EAST):



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April 2011

## APPENDIX G

RESISTIVITY DEPTH IMAGES (RDI)
Please see RDI Folder on DVD for the PDF's

APPENDIX III: MAPS










[^0]:    ${ }^{1}$ Note: Actual Line kilometres represent the total line kilometres in the final database. These line-km normally exceed the Planned Line-km, as indicated in the survey NAV files.

[^1]:    ${ }^{2}$ Final data processing of the EM and magnetic data was carried out by Emily Data, from the office of Geotech Ltd. in Aurora, Ontario, under the supervision of Jean M. Legault, M.Sc.A, P.Eng, and P.Geo - Chief Geophysicist.

[^2]:    1 McNeill, JD, 1980, "Applications of Transient Electromagnetic Techniques", Technical Note TN-7 page 5, Geonics Limited, Mississauga, Ontario.

[^3]:    ${ }^{1}$ Maxwell A.Meju, 1998, Short Note: A simple method of transient electromagnetic data analysis, Geophysics, 63, 405-410.

