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BEAUCAGE MINES LIMITED  
GEOLOGICAL REPORT

O.E. OWENS

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North Bay, Ontario  
August 10, 1956

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INTRODUCTIONINTRODUCTION

The columbium-uranium deposits of Beaucage Mines Limited are located 6 miles west of the city of North Bay, Ontario in an area bounded by the Manitou Islands of Lake Nipissing.

There are five islands in the Manitou group arranged in a ring about 1½ miles in diameter. The total land area of these islands is 328.7 acres.

Uranium was discovered during the summer of 1952 on Newman Island. Subsequent examination of rock samples revealed that the radioactive mineral was a uranian-pyrochlore thus indicating presence of columbium.

Diamond drilling from the ice during the winter of 1953 indicated 4,037,685 tons of metamorphic alkaline rocks grading more than 0.5%  $Cb_2O_5$  and 0.04%  $U_3O_8$ .

This was followed by a detailed geological and magnetometer investigation of the other islands, and the area as a whole. Small occurrences of columbium-uranium bearing rocks were uncovered on Big Manitou and Calder Islands.

Further diamond drilling on the main Newman Zone during that winter of 1955 increased the tonnage of ore to 5,431,000 tons at a grade of 0.53%  $Cb_2O_5$  and 0.039%  $U_3O_8$ , established continuity to the zone, and indicated the presence of higher grade cores to

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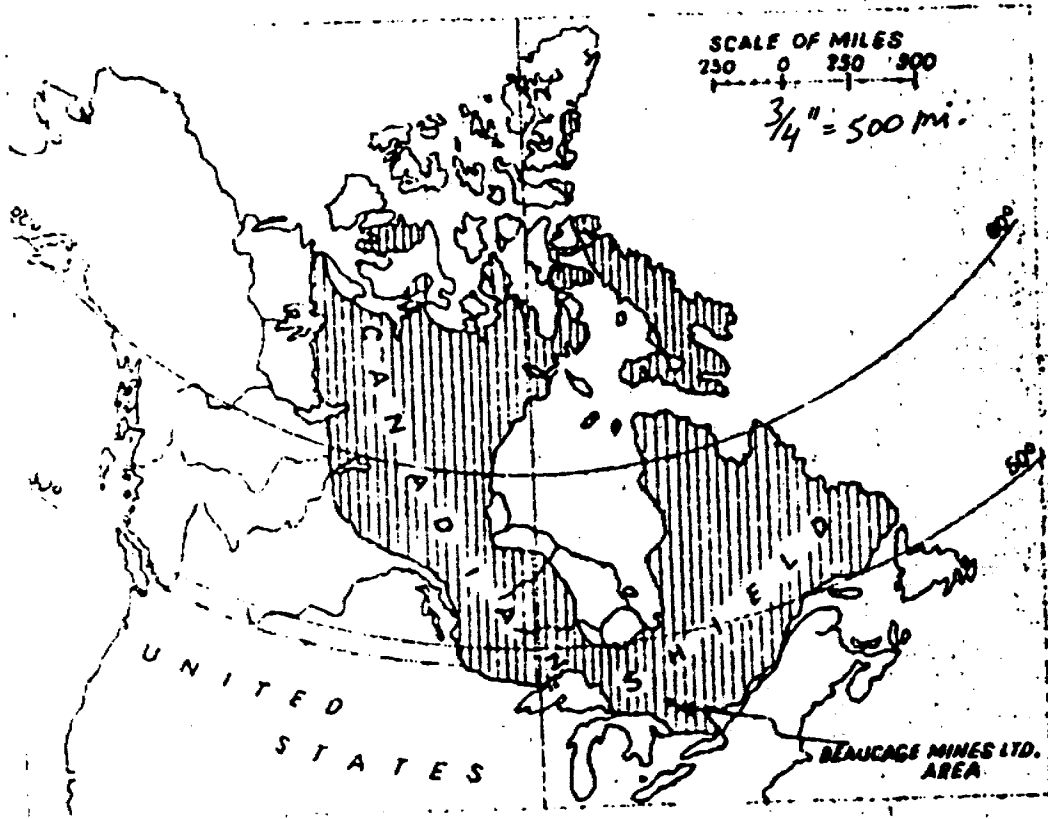
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the ore masses.

Shaft sinking commenced in September 1954. The shaft is bottomed at 427 feet with one level at 400'. To date 2500 feet of drifting and crosscutting have been completed on this level.

Underground sampling, diamond drilling and a re-evaluation of the surface drilling in the light of underground data indicates the presence of 3,384,740 tons of ore rock in the Newman Zone at a grade of 0.73%  $\text{Cb}_2\text{O}_3$  and 0.053%  $\text{U}_3\text{O}_8$ .

Property:

The property of Beaucage Mines Limited consists of 7923.72 acres held under License of Occupation No.12268, of which 328.62 acres comprise the Manitou Islands as follows:

|                       |             |
|-----------------------|-------------|
| Great Manitou Island  | 203.0 acres |
| Little Manitou Island | 69.22 acres |
| Calder Island         | 26 acres    |
| Rankin Island         | 22.75 acres |
| Newman Island         | 7.15 acres  |

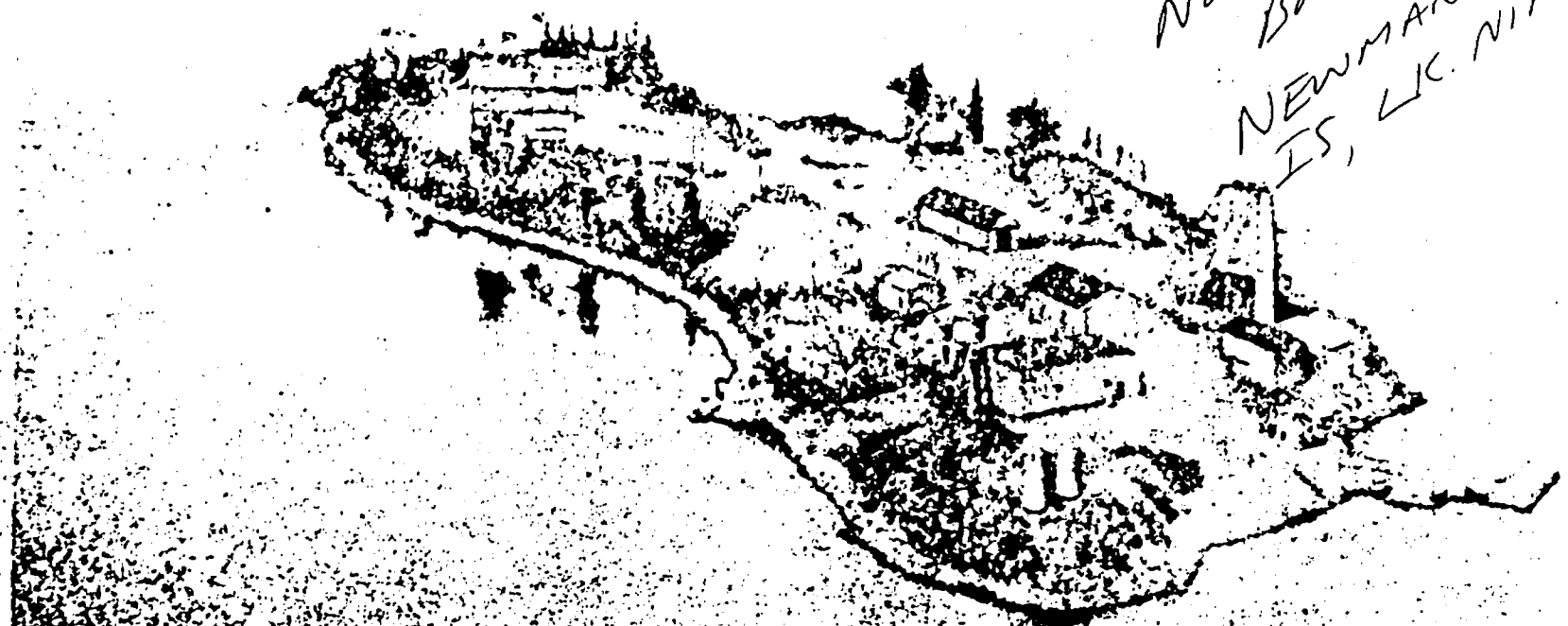
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BEAUCAGE  
MS LTD,  
NORTH  
BAY  
NEWMAN  
IS, LK. NIPISSING.



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During the winter of 1953 7510 feet of diamond drilling was carried out from the ice in the area east of Newman Island, which is now referred to as the Newman Zone. During March of the same year a magnetometer survey was made of the Newman Zone. A substantial tonnage of rock of probable economic value was indicated and Battelle Memorial Institute of Columbus, Ohio and others were engaged to conduct metallurgical studies on the ore.

Diamond drilling was continued on Calder (6,010) and Big Manitou (9,697') islands during the spring and summer. At the same time geological and scintillation surveys were made of the islands, and an aeromagnetic survey was conducted of the Manitou Island area.

Drilling was resumed in the Newman Zone in January 1954 and 7069' were drilled from the ice. Interest in aeromagnetic anomalies were surveyed with a ground magnetometer survey during the same winter.

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Underground operations commenced on September 17th, 1954 and 427' of four-compartment shaft was completed by February. Stations were cut at the 275' and 400' levels. Since this time 2423 feet of drifting and crosscutting have been completed on the 400 foot level, 12,769 tons of stope sills have been mined for pilot plant operation, and 12,944 feet of underground diamond drilling has been completed.

Construction of a 50 ton per day pilot plant commenced during June of 1955 on the mainland 10 miles west of the City of North Bay with the flotation section commencing operation in December and the chemical section in July 1956.

#### REGIONAL GEOLOGY

The rocks in the North Bay area are typical Grenville, quartz-feldspar paragneisses. Their altitude varies from place to place, but commonly they are folded into open folds with an irregular increase in metamorphic grade which results in areas of nearly massive granitic gneisses. This assemblage is intruded by dykes and larger intrusive bodies of basic composition. Some of these are slightly radioactive and contain traces of columbium.

The only geological mapping in the area is a reconnaissance map of the region south of Lake Nipissing which was done by J. Satterly of the Ontario Department of Mines in 1943. This map shows numerous islands of Grenville limestone within the quartz feldspar gneisses.

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The topography of the district is typical of that of the Canadian Shield; difference of relief is about 200-300 feet.

The area is on strike of two topographic breaks, one along the Ottawa-Mattawa river valleys and the other along the C. N. R. mainline to Ottawa. There is not sufficient geological information on the subject to indicate whether these breaks are due to faulting, however this is a likely hypothesis.

Lake Nipissing is a large shallow lake lying at the headwaters of rivers flowing to Georgian Bay and the Ottawa River. The maximum depth of the lake is about 50 feet.

The Manitou Islands rise less than 100 feet above lake level.

#### GEOLOGY MANITOU ISLANDS

The rocks exposed underground and in diamond drill cores are mainly paragneisses, crystalline limestone, alkaline intrusives and metamorphoses equivalents. It is a complex assemblage typical of the Grenville province but with local peculiarities, notably concentrations of sodium, phosphorous, fluorine, uranium and columbium; as well as a regional brecciation of the rocks.

Resting unconformably upon these rocks are scattered patches of Palaeozoic conglomerate, limestone, and dolomite.

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## BEAUCAGE MINES LTD.

## TABLE I

## TABLE OF FORMATIONS

## PALAEOZOIC

- 8 Ordovician
- 8c Lower Trenton limestone
- 8b Upper Black River dolomite
- 8a Upper Black River conglomerate
  
- 7 Oxidized Precambrian Rocks

## UNCONFORMITY

## PRECAMBRIAN

- 6 Ore
- 5 Lamprophyre Dykes
- 4 Diorite
- 4b Diabase
  
- 3 Feldspar acmite gneiss
- 3a Grey feldspar
- 3b Pink feldspar
- 3br Red feldspar
- 3b<sub>2</sub> Pegmatite
- 3aa Fine grain acidic dyke
- 3b<sub>1</sub> Distinct gneissic landing
  
- 2 Basic Silicate Rock (probably skarn)
- 2a Fine grain biotite predominant mineral
- 2b Acmite and calcite predominant minerals
- 2c Acmite and feldspar predominant minerals
- 2f Acmite and apatite predominant minerals
- 2g Basic dykes
  
- 1 Grenville type limestone
- 1a Laminated grey limestone
- 1b<sub>1</sub> Massive white carbonate
- 1b<sub>2</sub> White carbonate porphyroblasts acmite
- 1c Carbonate dykes
  
- 0 Quartz feldspar gneiss

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| PRECAMBRIAN  | <ul style="list-style-type: none"> <li>6 Ore</li> <li>5 Lamprophyre Dykes</li> <li>4 Diorite</li> <li>4b Diabase</li> <li>3 Feldspar acmite gneiss               <ul style="list-style-type: none"> <li>3a Grey feldspar</li> <li>3b Pink feldspar</li> <li>3br Red feldspar</li> <li>3b<sub>2</sub> Pegmatite</li> <li>3aa Fine grain acidic dykes</li> <li>3b<sub>1</sub> Distinct gneissic banding</li> </ul> </li> <li>2 Basic Silicate Rock (probably skarn)               <ul style="list-style-type: none"> <li>2a Fine grain biotite predominant mineral</li> <li>2b Acmite and calcite predominant minerals</li> <li>2c Acmite and feldspar predominant minerals</li> <li>2f Acmite and apatite predominant minerals</li> <li>2g Basic dykes</li> </ul> </li> <li>1 Grenville type limestone               <ul style="list-style-type: none"> <li>1a Laminated grey limestone</li> <li>1b<sub>1</sub> Massive white carbonate</li> <li>1b<sub>2</sub> White carbonate porphyroblasts acmite</li> <li>1c Carbonate dykes</li> </ul> </li> <li>0 Quartz feldspar gneiss</li> </ul> |

The Precambrian assemblage has been divided into seven main groups with subdivision as listed in Table 1. There is generally a gradation between the rock types.

Geological details and the results of a magnetometer survey suggest a circular structure to the rock units.

### Granite Gneiss

The outermost unit in the rock series is a medium grained equigranular quartz feldspar gneiss. Gneissic banding is poorly developed largely because of its fine texture and subsequent alteration which includes streaks of migmatite and 1-3 mm. wide stringers of acmite\*. This member is well exposed on the islands.

The rock is composed of 5-20% quartz, 60% pink feldspar (mainly potash type) and 30% ferromagnesian minerals (mainly acmite with lesser amounts of biotite and arfvedsonite\*\*). The grain size of the rock is between 1 and 3 millimeters although in places there are segregations of coarser(?) grained material resembling migmatite structure.

The features of the gneiss which distinguish it from other rocks in the North Bay area are finer and more even grain size, a general brecciation of the rock, the presence of fine stringers of acmite intimately cutting the rock, and the low quartz content.

\* Soda Pyroxene

\*\* Soda Amphibole

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Grenville Limestone

The Grenville limestone is exposed on Calder Island and in the drill cores from Calder, Big Manitou and Newman Island. It may be subdivided on the basis of appearance and mineral composition into three types:

- 1 (a) "Laminated" Carbonate
- 1 (b) Carbonate, Porpyroblasts of Acmite or Biotite
- 1 (c) Carbonate veins

The "Laminated" Carbonate is a crystalline calcium carbonate with a variegated appearance due to irregular streaks, layers, beds or disseminated grains of biotite, acmite, apatite, magnetite and feldspar. The carbonate, which is almost entirely calcite, is medium grained and white to light grey in colour. In appearance the rock closely resembles Grenville limestone in many parts of Ontario and Quebec. The nearest reported occurrence of Grenville limestone is in Lount Township about 36 miles south of North Bay.

The Carbonate, Porpyroblasts of Acmite or Biotite is exposed on Calder and Big Manitou Islands where it occurs as 5 to 75 feet thick bands separated by sheet like masses of syenite gneiss. It is composed of medium grained crystalline carbonate and 10-30% of porpyroblasts of acmite, biotite and magnetite. The porphyroblasts of acmite are commonly about  $\frac{1}{4}$  -  $\frac{1}{2}$  inches in diameter and are partially replaced by arfvedsonite and biotite. The calcite is white and medium to coarse grained. Apparently this rock is the re-crystallized and altered equivalent of the Laminated Carbonate.

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North of Rankin island a large area of this member has been intersected by diamond drilling. Results listed on page 24 show that this type of rock contains a major tonnage of columbium. It is believed that it should have separate metallurgical study because of its high calcite content, (see p.18) and because the pyrochlore is associated with concentration of apatite and acmite.

The carbonate veins are 1 to 6 inch wide dyke-like masses of carbonate which cut all other rocks in the area. They are composed especially of carbonate and fluorite, with small amounts of feldspar, pyrite and hematite. The carbonate varies in composition; much of it is calcite, but dolomite, siderite and very rarely rhodochrosite are present. The fluorite fraction which varies between 10 and 40% of the whole, is a deep purple variety and although it is commonly fine grained, locally it occurs as well developed grain up to 3/8" diameter.

#### Basic Silicate rock

The Basic silicate group of rock types contains most of the ore developed to date. It is medium grained and consists essentially of acmite and biotite with lesser amounts of calcite, apatite or feldspar. The rock may be subdivided into three types on the basis of the percentage of calcite, apatite or feldspar.

This rock type is restricted to the ore zone on Newman and Big Manitou Islands and will be described in the Economic Geology section.

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This rock type is restricted to the ore zone on Neaman and is described in detail and will be described in the Economic Geology section.



Syenite Gneiss

The syenite gneiss is fine to medium grained and equigranular. It usually consists of 70% potash feldspar and 30% acmite with small amounts of carbonate, apatite, pyrite, magnetite, arfvedsonite, and uranium pyrochlore.

The acmite occurs as dark gneissic bands, irregular blobs and fine stringers. Photo #2 show the gradual change from fine gneissic banding to a massive syenite. The photographs are taken of core picked in sequence across the zone from south (right) to north (left). The alteration is more intense on the north side of the Newman Zone. Generally speaking, most of the syenite gneiss from the ore zone is only faintly gneissic and shows nearly a massive texture similar to the centre pieces of core in the photograph. Apparently the various types of gneiss represent the gradual development of metasomatic alteration with the source to the north of the Newman Zone. The syenite gneiss, throughout the one zone, is shattered and cut by fine acmite stringers.

DIORITE

Diamond drill holes from Big Manitou, Little Manitou and Newman Islands have intersected a medium grained rock consisting of about 55% pearl grey potash feldspar, 40% acmite or its altered equivalent, and magnetite, Diorite is the field term for this rock since the more correct name, syenite, might be confused with the syenite gneiss.

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The Diorite apparently has the form of a ring dyke on the inner side of the islands. The grain size, and relative proportions of feldspar and dark minerals vary along and across the strike. It is common on Big Manitou Island to find phases with grain size in excess of  $\frac{1}{4}$ ". These dykes may be a gradation of the more common medium to coarse grain diorite, or parallel pegmatitic structures intruding the Syenite Gneiss and Basic Silicate Rock group.

Apparently water-rich solutions have been important in the process of emplacement of the diorite. It is believed that the diorite is an offshoot of a deeper more significant intrusive.

#### PALAEOZOIC ROCKS

There is a total of about 6 acres of Palaeozoic limestone at or near the surface on Newman, Rankin, Calder, Big Manitou and Little Manitou Islands. The greatest measureable thickness is 25'. These are buff weathering grey limestones and dolomites of Ordovician age. The uppermost unit is Lower Trenton limestone which is separated from the Black River dolomite by a thin shale stratigraphic horizon. These rocks are nearly flat lying, resting unconformably on the underlying Pre-cambrian rock.

The lower most unit of the Palaeozoic series is a conglomerate with fragments of syenite gneiss altered in a manner similar to that of the ore zone; also the gneiss fragments are slightly radioactive. The limestone is not cut by any other rock type.

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The Diorite apparently has the form of a ring dyke on the inner side of the islands. The grain size, and relative proportions of feldspar and dark minerals vary along and across the strike. It is common on Big Manitou Island to find phases with grain size in excess of  $\frac{1}{2}$ ". These dykes may be a gradation of the more common medium to coarse grain diorite, or parallel pegmatitic structures intruding the Syenite Gneiss and Basic Silicate Rock group.

Apparently water-rich solutions have been important in the process of emplacement of the diorite. It is believed that the diorite is an offshoot of a deeper more significant intrusive.

#### PALAEOZOIC ROCKS

There is a total of about 6 acres of Palaeozoic limestone at or near the surface on Newman, Rankin, Calder, Big Manitou and Little Manitou islands. The greatest measureable thickness is 25'. These are buff weathering grey limestones and dolomites of Ordovician age. The uppermost unit is Lower Trenton limestone which is separated from the Black River dolomite by a thin shale stratigraphic horizon. These rocks are nearly flat lying, resting unconformably on the underlying Pre-cambrian rock.

The lower most unit of the Palaeozoic series is a conglomerate with fragments of syenite gneiss altered in a manner similar to that of the ore zone; also the gneiss fragments are slightly radioactive. The limestone is not cut by any other rock type.

It is thus most likely that the Beaucage ore is pre-Black River in age.

### STRUCTURE

The rocks in the vicinity of the Manitou Islands are crystalline limestone, steeply dipping gneisses and various intrusives. Diamond drill intersections and surface mapping indicate that these rocks strike parallel to the circumference of the islands. The similarity of the rocks on each island and the constant sequence on each, suggests a circular structure to the bedrock pattern. Also the contours of the airborne magnetometer survey form a circular pattern about the islands with local variations following deviations in bedrock structure. The circular magnetic highs may be due to topographic features, but this does not seem likely.

Superimposed on this circular bedrock structure is a regional brecciation or shattering of the gneisses, with an intimate network of secondary acmite stringers.

In certain localities such as the area east of Newman Island this shattering is intense and apparently has produced a porous zone favourable for the deposition of columbium and uranium.

Within the Newman Zone the areas containing the highest columbium and uranium content are those with the highest

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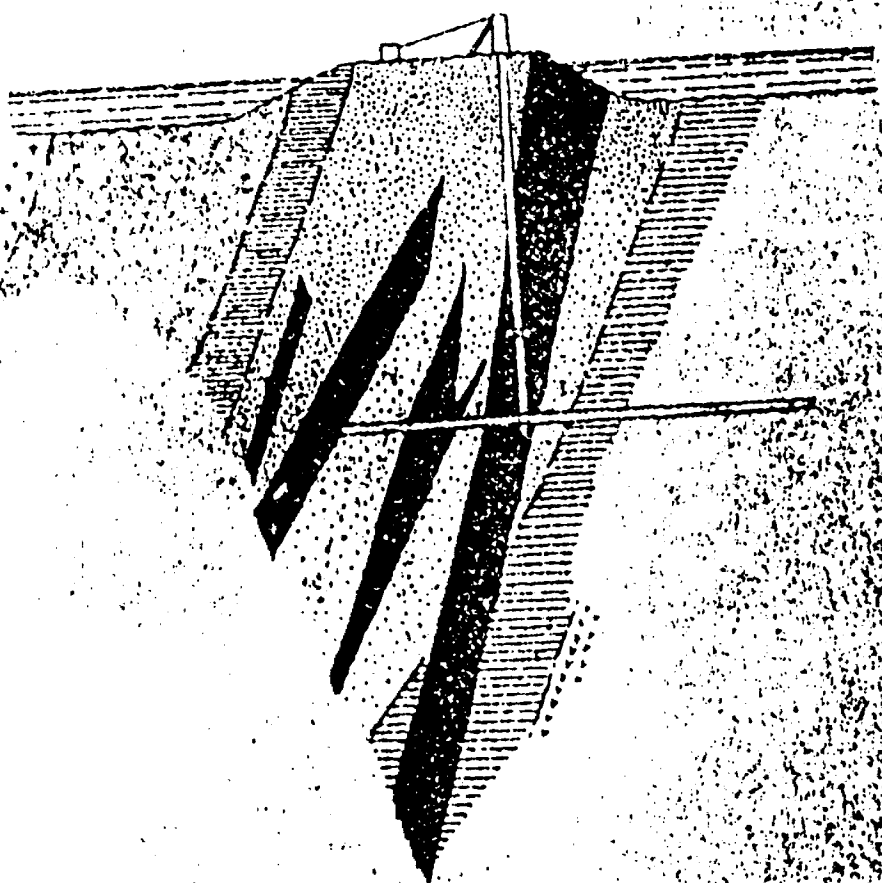
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



Within the Newman Zone the areas containing the highest columbium and uranium content are those with the highest

SOUTH

NORTH



LEGEND

-  ORE ORE
-  DIORITE DIORITE
-  BASIC SILICATE ROCKS
-  SYENITE GNEISS
-  CARBONATE ROCKS
-  GRANITE GNEISS

1"=200'

0 100 200 300  
1"=200'

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degree of brecciation, and the most intense secondary alteration.

The limestone member of the series has evidently yielded plastically to the forces which caused brecciation of the gneiss, as evidenced by the swirls and irregular flowage banding of the carbonate rocks.

#### ECONOMIC GEOLOGY

The Beaucage columbium-uranium deposit contains an unusually high percentage of sodium, phosphorus, and iron and is closely associated with masses of carbonate rocks.

The carbonate rocks resemble Grenville limestone, such as that outcropping to the south of Lake Nipissing. It seems logical to classify the carbonate rocks as recrystallized Grenville limestones, which may perhaps in many instances, have been mobilized and squeezed into new locations.

A characteristic feature of the rocks in the vicinity of the Manitou Island is a regional brecciation. This brecciation is most intense in the vicinity of the Newman deposit, and is the dominant structural feature of the ore zone.

The main tonnage of rock, outlined to date, containing more than 0.5%  $Cb_2O_5$ , occurs in a brecciated series of Acidic Silicate Rocks along the contact with Grenville Limestone.

All the uranium and columbium in the rock is contained in the mineral, uranian-pyrochlore. This mineral is associated with concentrations of acmite, apatite, red feldspar, biotite, magnetite, and pyrite.

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Newman ore zone

A group of rocks terms Basic Silicate Rocks constitute the major part of the Newman Ore zone. They are acmite-biotite-arfvedsonite-rich rocks which appear to have formed as a result of metasomatic alteration of pre-existing limestone and acidic gneisses. They may conveniently be sub-divided into two types :

Ferromagnesian - Calcite rock

Ferromagnesian - Feldspar rock

The ferromagnesian-calcite rock which constitutes about 60% of the total ore, is composed of about 50% ferromagnesian minerals, and 30% calcite and apatite, with lesser amounts of feldspar pyrrhotite, pyrite, magnetite, fluorite, and uranian-pyrochlore. The rock consists of 2-8 mm. diameter porphyroblasts of acmite and biotite in a medium grained groundmass of white calcite and pale green apatite. The acmite is a dark dull green in hand specimen and a medium green in thin section. The grains may be clear or altered to a felty mass of biotite, arfvedonite, and chlorite.

The ferromagnesian Calcite type of rock occurs as a matrix in, and as a replacement of, a brecciated area of syenite gneiss, and also as a replacement in the limestone stratigraphic horizon. The more intense the brecciation and replacement the higher the percentage of iron silicates in the rock. They appear to have formed as a result of metasomatic alteration of limestone material which has been squeezed

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Newman Ore Zone

A group of rocks termed Basic Silicate Rocks constitutes the major part of the Newman Ore Zone. They are actinolite-biotite-arfvedsonite-rich rocks which appear to have formed as a result of metasomatic alteration of pre-existing limestone and acidic gneisses. They may conveniently be sub-divided into two types.

## Ferromagnesian - Calcite Rock

## Ferromagnesian - Feldspar Rock

The Ferromagnesian - Calcite Rock which constitutes about 80% of the total ore, is composed of about 50% ferromagnesian minerals, and 30% calcite and apatite, with lesser amounts of feldspar, pyroxenite, pyrite, magnetite, fluorite, and uranian-pyroxenite. The rock consists of 2-8 mm. diameter porphyroblasts of actinolite and biotite in a medium grained groundmass of white calcite and pale green apatite. The actinolite is a dark dull green in hand specimen and a medium green in thin section. The grains may be clear or altered to a felty mass of biotite, arfvedsonite, and chlorite.

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COMPOSITION BEAUCAGE ORE

CHEMICAL ANALYSIS

|                                |      |
|--------------------------------|------|
| Cb <sup>2</sup> O <sub>5</sub> | .59  |
| Ta <sup>2</sup> O <sub>5</sub> | Nil  |
| U <sup>3</sup> O <sub>8</sub>  | .034 |
| P <sup>2</sup> O <sub>5</sub>  | 3.1  |
| ScO <sub>2</sub>               | 26.7 |
| CaO                            | 19.2 |
| Fe                             | 12.2 |
| CO <sup>2</sup>                | 11.4 |
| Al <sup>2</sup> O <sub>3</sub> | 4.6  |
| MgO                            | 5.3  |

SEMIQUANTITATIVE SPECTROGRAPHIC ANALYSIS

|                   |           |
|-------------------|-----------|
| ErO <sup>2</sup>  | .03 - .3% |
| TiO <sup>2</sup>  | .2 - 2%   |
| Na <sup>2</sup> O | .5 - 5%   |
| K <sup>2</sup> O  | 1 - 5%    |

MINERAL COMPOSITION

|              |          |
|--------------|----------|
| Pyrochlore   |          |
| Calcite      | 10 - 50% |
| Acmite       | 25 - 50% |
| Biotite      | 5 - 30%  |
| Arfredsonite |          |
| Feldspar     | 5 - 60%  |
| Apatite      | 0 - 30%  |
| Zincon       |          |
| Hematite     |          |
| Magnetite    |          |

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COMPOSITION BLAGAGE ONE

CHEMICAL ANALYSIS

|           |      |
|-----------|------|
| $Cb_2O_5$ | .59  |
| $Ta_2O_5$ | NIL  |
| $U_3O_8$  | .034 |
| $P_2O_5$  | 9.1  |
| $SO_2$    | 26.7 |
| $CaO$     | 19.2 |
| $Fe$      | 12.2 |
| $CO_2$    | 11.4 |
| $Al_2O_3$ | 4.6  |
| $MgO$     | 5.3  |

SEMIQUANTITATIVE SPECTROGRAPHIC ANALYSIS

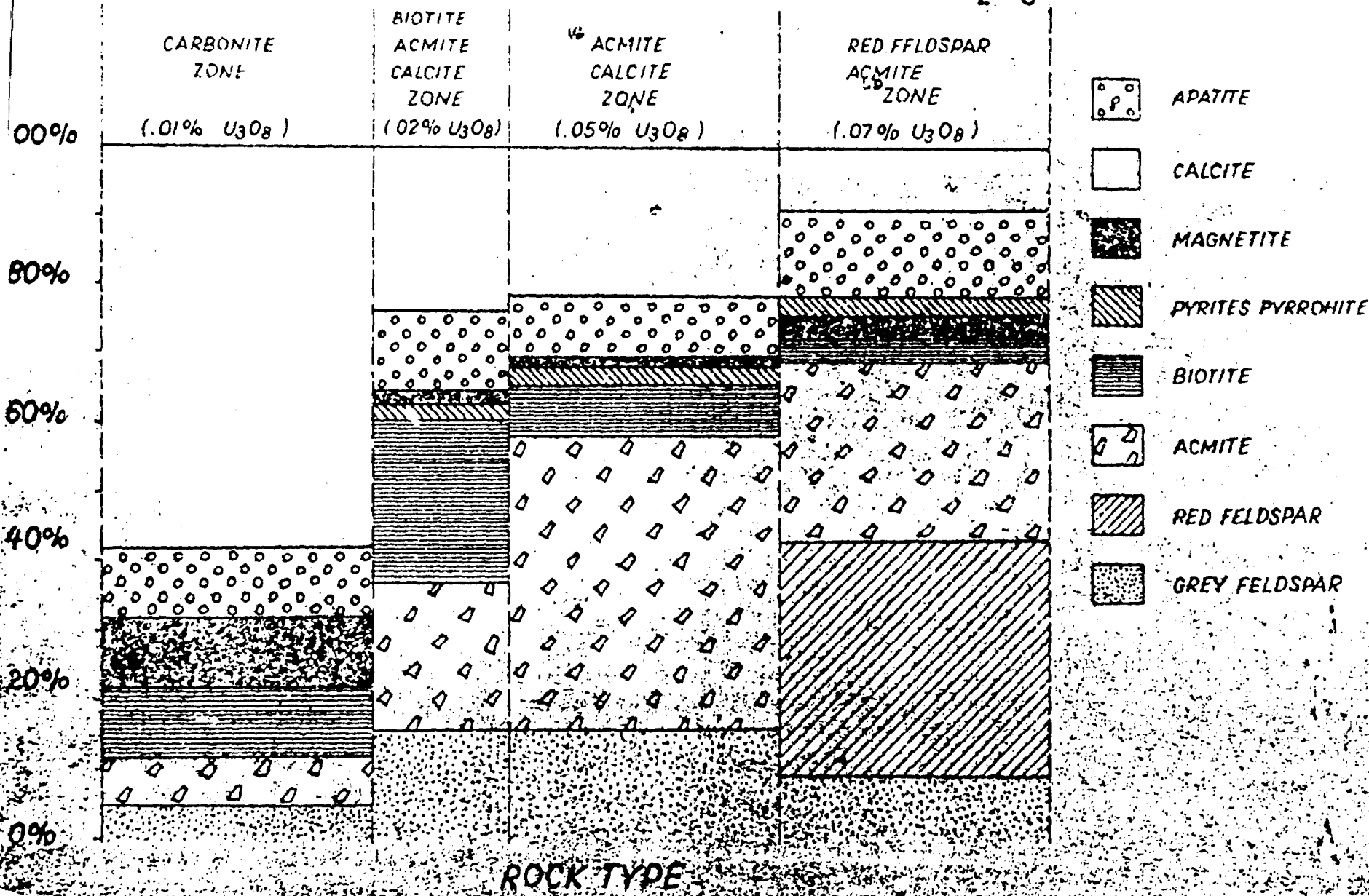
|         |           |
|---------|-----------|
| $ZrO_2$ | .03 - .3% |
| $TiO_2$ | .2 - 2%   |
| $Na_2O$ | .5 - 5%   |
| $K_2O$  | 1 - 5%    |

MINERAL COMPOSITION

|              |          |
|--------------|----------|
| Pyrochlore   |          |
| calcite      | 10 - 50% |
| Aegirite     | 25 - 50% |
| Eliotite     | 5 - 30%  |
| Arfvedsonite |          |
| Feldspar     | 5 - 60%  |
| apatite      | 0 - 30%  |
| Zircon       |          |
| Hematite     |          |
| Magnetite    |          |

TABLE 2

COMPOSITION OF ROCK AT GRADE OF 0.70%  $Cb_2O_5$



ROCK TYPE

51037

into the adjacent brecciated rhyenite. Apparently this zone is one of recurrent brecciation which provided a porous structure, in a chemically favourable zone, for replacement by solutions rich in iron, sodium, phosphorus, fluorine, columbium and uranium.

The composition of this type of ore is not constant, but varies with the degree of alteration. Table II shows the range in average composition but in practice there is a considerably greater variation than this. The acmite content varies between 20 and 60%; the calcite between 10 and 40%; the apatite between 2 and 30%; the biotite between 10 and 30%; and the magnetite, pyrite and pyrrhotite content generally increases in with grade to a combined maximum of about 20%. The feldspar content of the ore diminishes as the percentage of columbium increases. The most intensely brecciated, and most completely altered sections contain the highest percentage of columbium and the lowest amount of feldspar.

The colour and appearance of the uranian-pyrochlore varies as the columbium-uranium ratio. The high uranian-pyrochlore is dark steel grey to brown in colour with a vitreous to metallic luster and is partially opaque in thin section; while the low uranian-pyrochlore is honey yellow in colour and clear in thin section. The grains vary in size between 0.01 and 0.5 mm. Detailed thin section study, with the aid of short exposure autoradiographs, indicates that the radioactivity is restricted to the dark chocolate brown to black part of the pyrochlore grain which commonly occurs as a border to, or along cracks in, the clear pyrochlore core. Photo #12 shows two

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into the adjacent brecciated syenite. Apparently this zone is one of recurrent brecciation which provided a porous structure, in a chemically favourable zone, for replacement by solutions rich in iron, sodium, phosphorus, fluorine, columbium and uranium.

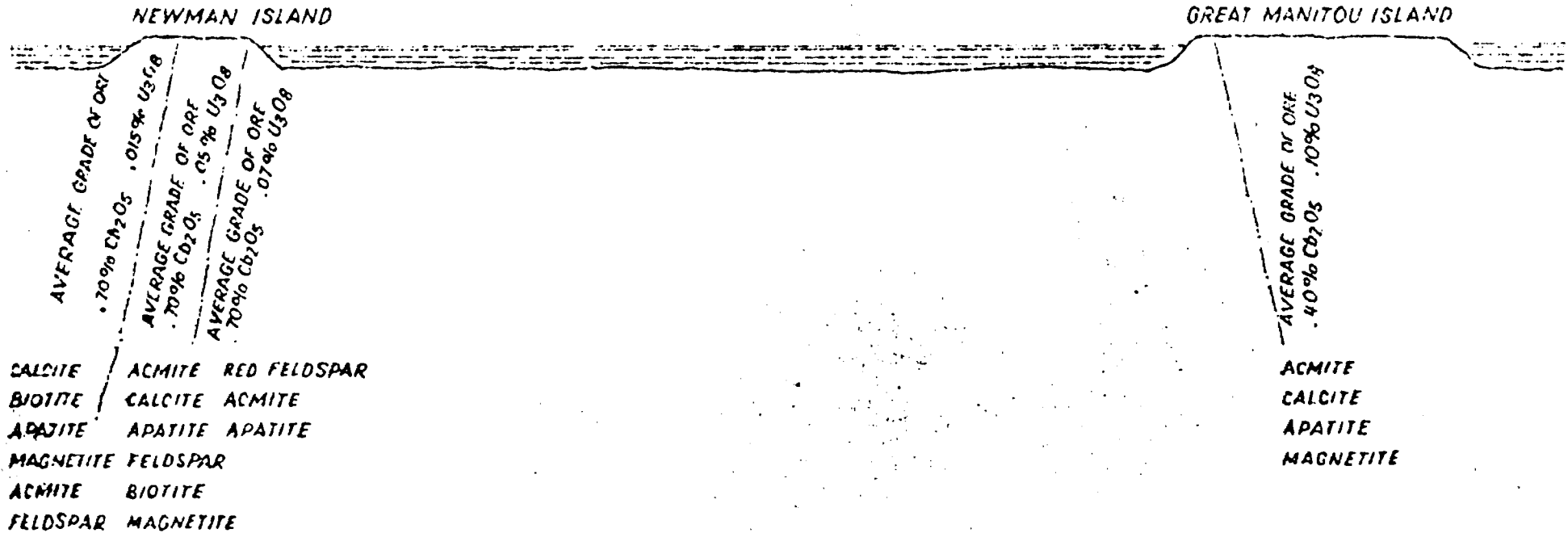
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FIGURE 1



MINERALS LISTED IN DECREASING ORDER OF ABUNDANCE  
FOR VARIOUS TYPES OF ORE

VERTICAL CROSS SECTION MANITOU ISLANDS

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pyrochlore grains with a slightly offset autoradiograph. Note how the pattern of the alpha tracks corresponds to the outline of the dark material in the pyrochlore grain. These plates were exposed for 48 hours. It seems likely that this dark material is a replacement phenomena, and is close to Ellsworthite or Betafite in composition. The higher the percentage of uranium in the rock the greater the percentage of dark grains of pyrochlore or the amount of dark material constituting the pyrochlore grains.

The composition of the pyrochlore has been determined by calculating the weight of pyrochlore in the rock with the aid of two thin sections, cut at right angles, and by assaying the enclosing rock fragments for uranium and columbium. This method indicates that the pyrochlore contains between 0.6 and 11%  $U_3O_8$  and between 20 and 50%  $Cb_2O_5$ .

Pyrochlore with a low uranium content is clear and commonly occurs in the southern part of the ore zone, in the high calcite and the high biotite type of rocks, while the darker variety occurs in the northern part of the ore zone in those rocks containing a high percentage of acmite and red feldspar (see figure I).

The average composition of the feldspar acmite type of Basic Silicate Rock is 45% potash feldspar, 25% acmite, 10% calcite, 13% apatite, 3% pyrite and pyrrhotite, 3% magnetite, and 3% biotite. The rock is commonly equigranular, medium grained with veinlets of acmite and feldspar. The majority of the feldspar contains fine disseminated red-coloured dust-like material believed to be hematite,

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which gives a red colour to the mineral and the rock. The acmite occurs either as short prismatic grains disseminated through the rock, in aggregates of crystals, or in veinlets. In places the acmite is a clear green mineral, in others it is cloudy or is partly replaced by arfvedsonite and biotite. The calcite fraction of the rock occurs either as 1"-6" wide veins, or very small clots. The apatite occurs as disseminated grains and fine clusters. The pyrochlore is always dark in colour with a sub-metallic lustre and has a uranium to columbium ratio of 1 to 10. These grains are between 0.025 and 0.5 mm. in diameter and occur disseminated through the rock, and commonly associated with the acmite.

#### Newman Ore Reserves

The Newman zone of columbium-bearing rock strikes east-west and dips steeply south. It is about 500 feet wide, and so far has been traced for a length of 1,000 feet, and to a depth of 1100 feet. Within this zone are definable lenses or lensitic pipes of ore at higher grades. To date 2,536,000 tons at a grade of 0.053%  $U_3O_8$  and .77%  $Cb_2O_5$  have been indicated by surface and underground diamond drilling. This is largely contained in lensitic pipes between 20-150 feet in width, 300 feet in length and extending to a depth of at east 1100 feet.

All the ore intersections uncovered to date are associated with higher than normal amounts of magnetite, and magnetometer anomalies have been the most favourable zones for investigation.

The underground work has shown that the ore is a clearly recognizable rock; however because it occurs as a matrix in a breccia zone, it has assay walls (allrock fragments of Syenite Gneiss are waste).

\*(Providing ore outlines 25' on either side of ore areas on section)?

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\* (PROVIDING ORE OUTLINES 25' ON EITHER SIDE OF ORE AREAS ON SKETCHES)

The ore zone has been nearly completely drilled to a depth of 700'. There is an indicated tonnage of 1,821,290 tons at a grade of .056%  $U_3O_8$  and .81%  $Cb_2O_5$  between the 300' level and an average depth of 700'. i.e. 4,560 tons per vertical foot below the 300 foot level.

Of the total tonnage developed to date 903,170 tons consists of the Basic Silicate, Ferromagnesian Feldspar type of ore. The grade of this material is .062%  $U_3O_8$  and 0.78%  $Cb_2O_5$ .

A considerable part of the wider sections of ore is above mine grade, and it is possible that substantial units of ore might be outlined at grades up to 1%  $Cb_2O_5$ . In the figures included in the appendix, 617,650 tons averages .077(?)  $U_3O_8$  and .92%  $Cb_2O_5$ .

One of the major considerations in arriving at an estimate of the columbium content of the Beaucage ore has been assaying. In the early stages of the operation, duplicate analysis sent to different assay laboratories and duplicates sent to the same laboratory, did not check. To improve this situation and reduce the cost of analysis the Geology Department of McGill University developed an X-Ray Fluorescent method of columbium analysis. Repeated checks by rerunning splits of original samples produced consistent results and the McGill results were chosen as a standard. Subsequent checks with later methods developed by the United States Geological Survey and the Canadian Geological Survey indicated that the McGill results were lower by 15-24%. With the

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advent of more interest in the columbium situation, and the setting up of more highly developed methods of analysis at commercial assay offices, McGill dropped out of the commercial assay picture and columbium analysis were performed at X-Ray Assay Laboratories, Toronto.

Up until March 9, 1956 X-Ray Assay Laboratories results were reduced by 15% to equate them with checks at McGill.

Thus the results listed on all development plans, sections, and reports to date including those listed in this report are probably low by 15%\*. A list of check analysis is included in the appendix.

All Beaucage analysis are presently conducted in our own labs, by a colorimetric method; the results are standardized on McGill plus 15%.

Uranium check analysis suggest that the Beaucage uranium assaying may be high by 5%.

The average grade of the ore exposed in the underground development completed to date, as indicated by muck samples is .04%  $U_3O_8$  0.51%  $Cb_2O_5$ , as indicated by face samples is .04%  $U_3O_8$  .63%  $Cb_2O_5$  (15% above standard of foregoing figures). The calculated grade of this material on diamond drill sections is .05%  $U_3O_8$  and 175%  $Cb_2O_5$ . It appears that the grade of the

\*Exception 1955 Beaucage Mines Limited Annual Report  
Radiometric Method.

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\* Exception 1955 Beaucage Mines Limited Annual Report

RADIOMETRIC METHOD.

ore removed to date is about 28% lower than calculated grade (though only 13% lower in absolute  $Cb_2O_5$  content). This is not due to wall rock dilution, but apparently is a result of geometric difficulties in relating diamond drill hole results, in a brecciated rock, to actual grade of rock in place; especially in narrow sections of ore which have been developed to date.

#### Big Manitou Island Ore Zone

During the summer season of 1953, some 40 diamond drill holes were drilled along a broad zone of radioactivity on the south west arm of Big Manitou Island. Most of the holes intersected at least 5 feet of material grading more than .10%  $U_3O_8$  or .40%  $Cb_2O_5$ ; however these intersections were scattered and are not part of a continuous mass of ore. An exception to this was found at the south end of the zone where some 20 short vertical holes, at 50' centres, indicated 27,000 tons of ore grading .104%  $U_3O_8$ , .38%  $Cb_2O_5$ , and 10%  $P_2O_5$ . This ore is at the surface and could be easily removed. It is interesting to note the high uranium ratio on this island.

#### Rankin Ore Zone

Three diamond drill holes, at 200' intervals have been drilled in the area just north of Rankin Island. These holes were 437', 495 and 679' in length and averaged .01%  $U_3O_8$  and .33%  $Cb_2O_5$  for their combined total lengths. As these holes were drilled at  $-55^\circ$ , and the ore on the Beaucage property is believed to dip steeply, they indicate a major tonnage of low grade material. These holes also have correlateable intersections of rock grading .01%  $U_3O_8$  and .60 - 1.00%  $Cb_2O_5$ . This is the high carbonate type of ore shown in table 2, p.18. The pyrochlore is associated with concentrations of apatite.

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This area of ore is of considerable importance, since it lies along the shortest distance from the Newman Ore Zone to Rankin Island where an ideal second opening to the underground workings could be located.

North-east of this ore, and 1500' due east of the Newman ore bodies is another important magnetic anomaly, as yet not drilled, which probably contains important columbium reserves.

#### Calder Island

Nineteen diamond drill holes were drilled on Calder Island in the spring of 1953. Carbonate, and Syenite Gneiss rocks were intersected, but with only widely scattered, low values, in columbium and uranium.

#### ORIGIN

The Beaucage columbium-uranium deposits are believed to be hydrothermal deposits connected with contact metasomatism of soda-iron rich intrusives. The metamorphic grade of the Syenite Gneiss suggests that the locus of the most intense alteration is in the vicinity of the centre of the Manitou Islands.

The "Diorite" and pegmatites are believed to be offshoots of a major basic intrusive which is not exposed underground or on surface.

Doming and shattering of the rocks in the region accompanied the main intrusion. The granitic gneisses were recrystallized and shattered. The free silica was converted to soda-iron silicates by silica-deficient solutions. The Grenville Lime-

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Doming and shattering of the rocks in the region accompanied the main intrusion. The granitic gneisses were re-crystallized and shattered. The free silica was converted to soda-iron silicates by silica-deficient solutions. The Grenville Lims-

stone was recrystallized, mobilized, and partially replaced by acmite, biotite, apatite, and magnetite.

In regions of intense repeated brecciation of the Syenite Gneiss, Basic Silicate Rock was formed by squeezing in of adjacent Limestone, and alteration of the breccia zone by solution rich in soda, iron, phosphorus, columbium, uranium, titanium, zirconium, and fluorine.

The inferred paragenesis of the ore is shown in figure II. Acmite, calcite and feldspar are the earliest minerals in the ore. The acmite has been subsequently partially altered to arfvedsonite and biotite. Biotite also replaced feldspar. Next in the sequence is apatite and honey yellow columbium pyrochlore. Apparently the first stage of pyrochlore is uranium free. This followed, perhaps in part simultaneously, by dark uranian-pyrochlore (noted dark borders and dark stringers in pyrochlore in uranium-bearing rock). This phase is closely followed by deposition of iron oxides and iron sulphides. The last stage is late calcite as blob-like replacements and narrow dykes or veins.

#### Recommendations

The Beaucage columbium-uranium deposit is one of numerous reported deposits containing exceptional quantities of columbium. Some of these are located at Oka, Province of Quebec; Nemegos, Province of Ontario; Mountain Pass, California; Magnet Cove, Arkansas; Manono, Belgium Congo; Panda Hill, Tanganyika;

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#### REFERENCES

The Beauveage columbium-uranium deposit is one of the more reported deposits containing exceptional quantities of columbium. Some of these are located at Oka, Province of Quebec; Magnet Hill, Province of Ontario; Mountain Pass, California; Magnet Hill, Arkansas; Manono, Belgium Congo; Panda Hill, Tanganyika;

FIGURE II

PARAGENESIS OF BEAUCAGE ORE

MIGMATITATION

---

BRECCIATION

---

MOBALIZATION OF LIMESTONE

---

PEGMATITES

---

ACMITE

---

BIOTITE

---

APATITE

---

COLUMBIAN PYROCHLORE

---

MAGNETITE

---

RED ALT. OF FELDSPAR

---

PYRITE & PYRRHOTITE

---

URANIAN PYROCHLORE

---

CALCITE

---

TRAP DYKES

---

HEMATITE

---



Mrima Hill, Kenya; Sukulu, Uganada; Chilwa Island, Southern Nyasaland; Tundulu, Nyasaland, Tororo Uganda; Kola Peninsula Russia, and some granites of Nigeria.

From the limited information available to date it appears that the Beaucage, Newman Island deposit is higher in grade than the fore mentioned deposits, and is the only one with any significant amount of underground development. Also indications in the Rankin island area suggest that Beaucage has a major tonnage of low grade material.

The mineralogy of the Beaucage deposit may turn out to be its most significant feature. The only ore material found in the extensive studies to date is pyrochlore. The pyrochlore is tantalum free. It contains upto 10% uranium, but no thorium, nor are any rare earths present in the deposit. Information released by other columbium properties suggests that Beaucage may be unique in having such simple mineralogy. This mono mineralistic ore, without other rare earths simplifies the metallurgical picture (relative to other potential producers), and may enable production, of a relatively pure columbium metal, to be undertaken at a considerably lower cost than other properties.

With this view in mind it is important to examine the metallurgical details of the different types of ores and studies should not be conducted only on one type of ore from one locality in the ore zone.

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From the limited information available to date it appears that the Beaucage, Newman Island deposit is higher in grade than the fore mentioned deposits, and is the only one with any significant amount of underground development. Also indications in the Rankin Island area suggest that Beaucage has a large tonnage of low grade material.

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The discrepancy between calculated grade and grade mined, in the narrow sections of the ore mined on the 400 feet level, points out the need for further underground development, at deeper levels, in the wider sections of ore, to ascertain more closely actual grade of rock which may be obtained. It seems likely thta the wider sections of ore will average closer to calculated grade.

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APPENDIX

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APIENDIX

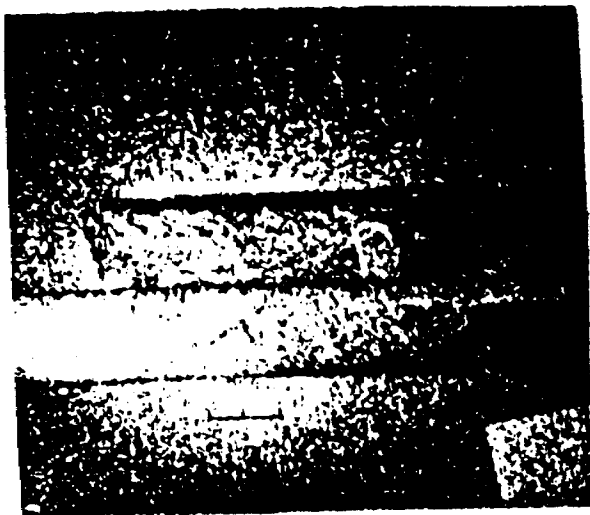


Photo #1 - Diamond Drill cores of Granite Gneiss. Note acmite stringer in large section of core, and brecciated nature of smaller core.



Photo #2 - Diamond drill core of a Syenite Gneiss series across the ore zone from south (right) to north (left).



Photo #3 - Handspecimen Laminated Carbonate

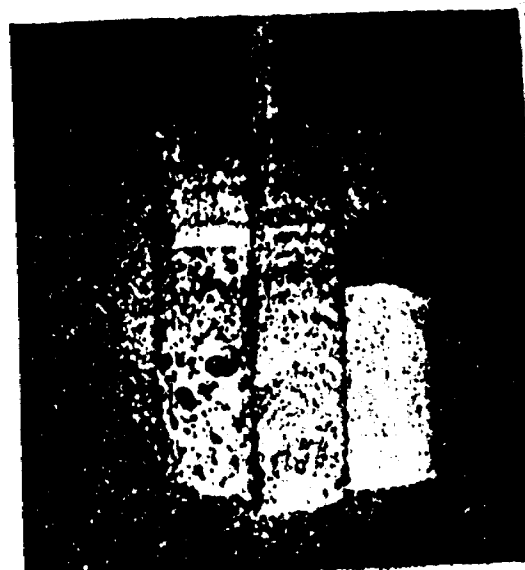


Photo #4 - Diamond Drill cores of White Carbonate (right) Laminated Carbonate (centre) Acmite & Biotite (left)



Photo #5 Hand specimen  
Basic Silicate Rock  
Ferromagnesian Calcite type.



Photo #6 - Diamond Drill  
cores Basic Silicate Rock  
Ferromagnesian Calcite type  
(top) Ferromagnesian Feldspar  
type (bottom)

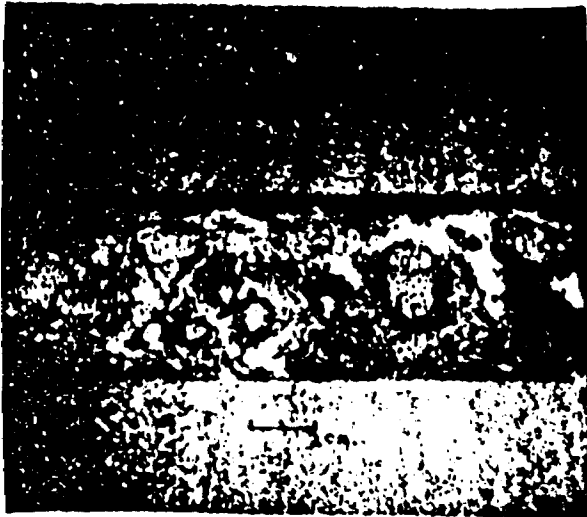
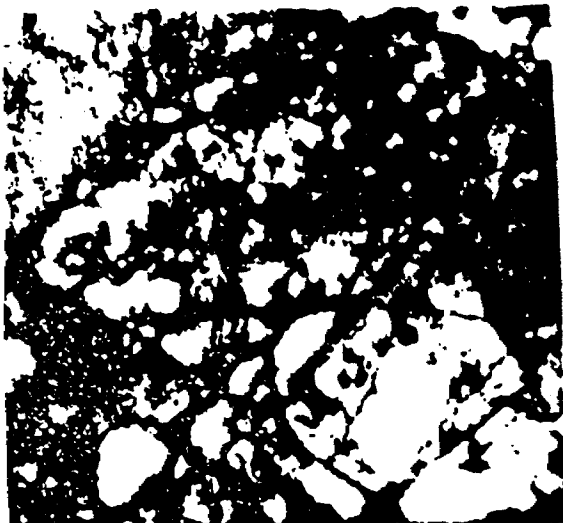


Photo #7 Diamond Drill core.  
Basic Silicate Rock. Ferromagnesian  
Calcite type with breccia fragments  
of pink Syenite Gneiss.

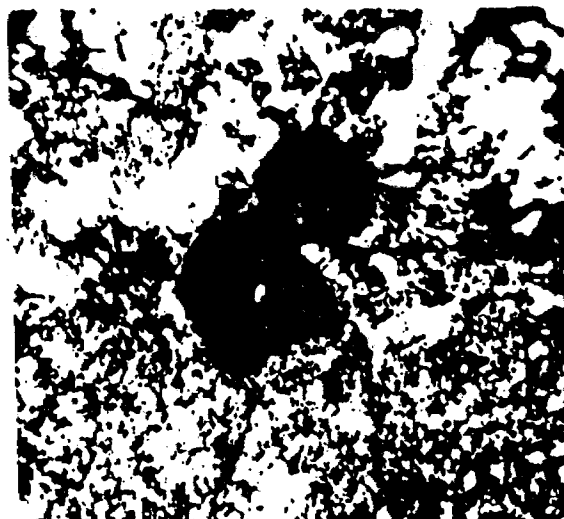


Photomicrograph #8  
Basic Silicate Rock  
Ferromagnesian Calcite  
Type, x 65, ordinary light  
Acmite (a) Apatite (ap)  
Calcite (c) Pyrochlore (p)

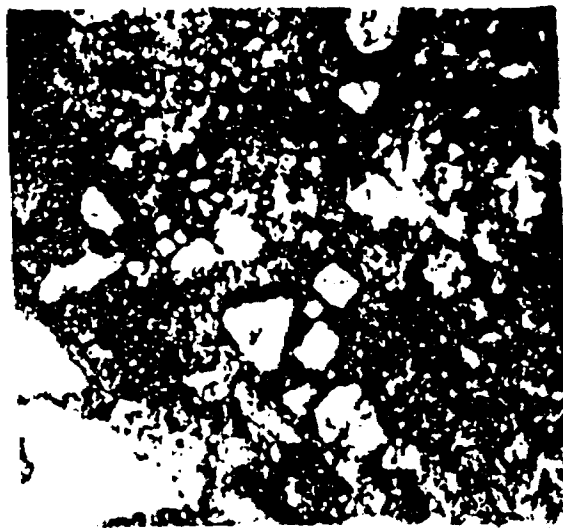




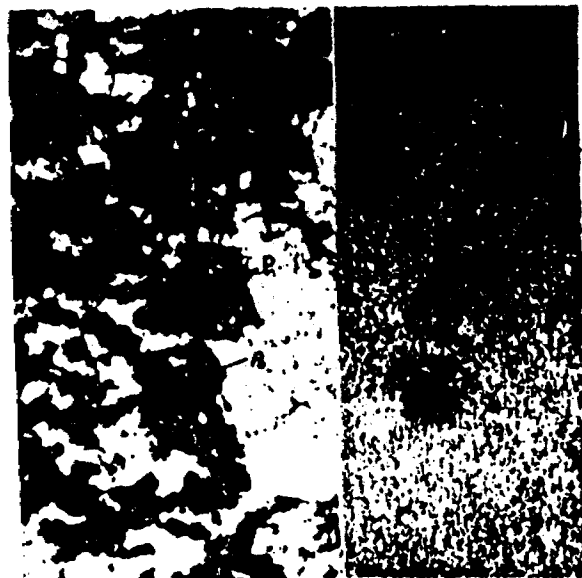
Photomicrograph #9  
 Pyrochlore grain, x 65  
 Ordinary light. Note dark  
 stringers cutting clear pyrochlore.



Photomicrograph #10  
 Two dark pyrochlore  
 grains in Basic Silicate  
 matrix. x 65, ordinary light.



Photomicrograph #11  
 Clear pyrochlore grains (p)  
 in Basic Silicate matrix  
 x 50, ordinary light



Photomicrograph #12  
 Pyrochlore grains with offset  
 nuclear track plate showing  
 alpha track pattern corres-  
 ponding to dark section of  
 pyrochlore grains

## TOTAL TONNAGE NEWMAN ZONE

| <u>SECTION</u> | <u>AREA</u> | <u>TONS</u> | <u>%U<sub>2</sub>O</u> | <u>%Cb<sub>2</sub>O</u> | <u>TONS x %U<sub>2</sub>O</u> | <u>TONS x %Cb<sub>2</sub>O</u> |           |
|----------------|-------------|-------------|------------------------|-------------------------|-------------------------------|--------------------------------|-----------|
| 5190E          | A           | 17,770      | .014                   | .66                     | 248.78                        | 11,728.20                      |           |
|                | B           | 22,220      | .014                   | .85                     | 311.09                        | 17,887.00                      |           |
| 5240E          | A           | 8,300       | .011                   | .81                     | 91.30                         | 6,723.00                       |           |
|                | D           | 6,250       | .013                   | .56                     | 81.25                         | 3,500.00                       |           |
|                | E           | 48,800      | .025                   | .87                     | 1,220.00                      | 42,456.00                      |           |
|                | F           | 3,680       | .023                   | .68                     | 84.64                         | 2,502.40                       |           |
|                | G           | 12,000      | .062                   | .76                     | 744.00                        | 9,120.00                       |           |
|                | H           | 28,500      | .03                    | .58                     | 855.00                        | 16,530.00                      |           |
|                | 5290E       | A           | 14,000                 | .038                    | .99                           | 532.00                         | 13,860.00 |
|                |             | B           | 33,800                 | .077                    | .94                           | 2,602.60                       | 31,772.00 |
| C              |             | 22,500      | .057                   | .60                     | 1,282.50                      | 13,500.00                      |           |
| D              |             | 15,750      | .074                   | .75                     | 1,165.40                      | 11,812.50                      |           |
| F              |             | 70,800      | .06                    | .70                     | 4,248.00                      | 49,560.00                      |           |
| 5240E          |             | A           | 25,200                 | .06                     | .61                           | 1,512.00                       | 15,372.00 |
|                | B           | 20,000      | .07                    | .66                     | 1,400.00                      | 13,200.00                      |           |
|                | C           | 102,000     | .041                   | .69                     | 4,182.00                      | 70,380.00                      |           |
|                | D           | 22,020      | .046                   | .66                     | 1,012.92                      | 14,533.20                      |           |
|                | E           | 10,800      | .05                    | .64                     | 540.00                        | 6,912.00                       |           |
|                | F           | 16,600      | .035                   | .69                     | 581.00                        | 11,454.00                      |           |
|                | G           | 32,600      | .055                   | .82                     | 1,793.00                      | 26,732.00                      |           |
|                | H           | 8,000       | .038                   | .58                     | 304.00                        | 4,640.00                       |           |
|                | I           | 8,000       | .035                   | .55                     | 280.00                        | 4,400.00                       |           |
|                | J           | 36,000      | .075                   | .81                     | 2,700.00                      | 29,160.00                      |           |
|                | K           | 222,000     | .063                   | .81                     | 13,986.00                     | 179,820.00                     |           |
|                | L           | 30,600      | .066                   | .64                     | 2,019.60                      | 19,584.00                      |           |
|                | 5390E       | A           | 23,400                 | .073                    | .68                           | 1,708.20                       | 15,912.00 |
| B              |             | 14,000      | .057                   | .80                     | 798.00                        | 11,200.00                      |           |
| C              |             | 137,500     | .097                   | 1.15                    | 13,337.50                     | 158,125.00                     |           |
| 5440E          | A           | 50,400      | .075                   | .64                     | 3,780.00                      | 34,776.00                      |           |
|                | B           | 10,000      | .056                   | .69                     | 560.00                        | 6,900.00                       |           |
|                | D           | 42,700      | .08                    | .72                     | 3,416.00                      | 30,744.00                      |           |
|                | E           | 33,200      | .055                   | .56                     | 1,826.00                      | 18,592.00                      |           |
|                | F           | 53,300      | .086                   | 1.04                    | 4,583.80                      | 55,432.00                      |           |
|                | I           | 39,100      | .066                   | .92                     | 2,580.60                      | 35,972.00                      |           |
|                | 5490E       | A           | 14,000                 | .01                     | .63                           | 140.00                         | 8,820.00  |
| B              |             | 19,000      | .012                   | .82                     | 228.00                        | 15,580.00                      |           |
| C              |             | 44,000      | .034                   | .73                     | 1,496.00                      | 32,120.00                      |           |
| D              |             | 31,000      | .11                    | 1.07                    | 3,410.00                      | 33,170.00                      |           |
| E              |             | 9,000       | .071                   | .77                     | 639.00                        | 6,930.00                       |           |
| 5540E          | A           | 24,300      | .061                   | .76                     | 1,482.30                      | 20,403.00                      |           |
|                | B           | 13,850      | .14                    | 1.21                    | 1,939.00                      | 16,758.50                      |           |
|                | C           | 14,400      | .107                   | 1.11                    | 1,540.80                      | 15,984.00                      |           |

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TOTAL TONNAGE NEWMAN ZONE

| <u>SECTION</u> | <u>AREA</u> | <u>TONS</u> | <u>%U<sub>3</sub>O<sub>8</sub></u> | <u>%Cb<sub>2</sub>O<sub>5</sub></u> | <u>Tons x %U<sub>3</sub>O<sub>8</sub></u> | <u>Tons x %Cb<sub>2</sub>O<sub>5</sub></u> |
|----------------|-------------|-------------|------------------------------------|-------------------------------------|---|--|
| 5190E          | A           | 17,770      | .014                               | .66                                 | 248.78                                    | 11,728.20                                  |
|                | B           | 22,220      | .014                               | .85                                 | 311.09                                    | 18,887.00                                  |
| 5240E          | A           | 8,300       | .011                               | .81                                 | 91.30                                     | 6,723.00                                   |
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|                | C           | 22,500      | .057                               | .60                                 | 1,282.50                                  | 13,500.00                                  |
|                | D           | 15,750      | .074                               | .75                                 | 1,165.50                                  | 11,812.50                                  |
|                | F           | 70,800      | .06                                | .70                                 | 4,248.00                                  | 49,560.00                                  |
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|                | B           | 20,000      | .07                                | .66                                 | 1,400.00                                  | 13,200.00                                  |
|                | C           | 102,000     | .041                               | .69                                 | 4,182.00                                  | 70,380.00                                  |
|                | D           | 22,020      | .046                               | .66                                 | 1,012.92                                  | 14,533.20                                  |
|                | E           | 10,800      | .05                                | .64                                 | 540.00                                    | 6,912.00                                   |
|                | F           | 16,600      | .035                               | .69                                 | 581.00                                    | 11,454.00                                  |
|                | G           | 32,600      | .055                               | .82                                 | 1,793.00                                  | 26,732.00                                  |
|                | H           | 8,000       | .038                               | .58                                 | 304.00                                    | 4,640.00                                   |
|                | I           | 8,000       | .035                               | .55                                 | 280.00                                    | 4,400.00                                   |
|                | J           | 36,000      | .075                               | .81                                 | 2,700.00                                  | 29,160.00                                  |
|                | K           | 222,000     | .063                               | .81                                 | 13,986.00                                 | 179,820.00                                 |
|                | L           | 30,600      | .066                               | .64                                 | 2,019.60                                  | 19,584.00                                  |
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| B              |             | 14,000      | .057                               | .80                                 | 798.00                                    | 11,200.00                                  |
| C              |             | 137,500     | .097                               | 1.15                                | 13,337.50                                 | 158,125.00                                 |
| 5440E          | A           | 50,400      | .075                               | .64                                 | 3,780.00                                  | 34,776.00                                  |
|                | B           | 10,000      | .056                               | .69                                 | 560.00                                    | 6,900.00                                   |
|                | D           | 42,700      | .08                                | .72                                 | 3,416.00                                  | 30,744.00                                  |
|                | E           | 33,200      | .055                               | .56                                 | 1,826.00                                  | 18,592.00                                  |
|                | F           | 53,300      | .086                               | 1.04                                | 4,583.80                                  | 55,432.00                                  |
|                | I           | 39,100      | .066                               | .92                                 | 2,580.60                                  | 35,972.00                                  |
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|                | E           | 9,000       | .071                               | .77                                 | 639.00                                    | 6,930.00                                   |
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|                | B           | 13,850      | .14                                | 1.21                                | 1,939.00                                  | 16,758.50                                  |
|                | C           | 14,400      | .107                               | 1.11                                | 1,540.80                                  | 15,984.00                                  |

Cont'd

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| <u>SECTION</u> | <u>AREA</u> | <u>TONS</u> | <u>%U<sub>2</sub>O<sub>8</sub></u> | <u>%Cb<sub>2</sub>O<sub>5</sub></u> | <u>TONS x %U<sub>2</sub>O<sub>8</sub></u> | <u>TONS x %Cb<sub>2</sub>O<sub>5</sub></u> |
|----------------|-------------|-------------|------------------------------------|-------------------------------------|---|--|
| 5590E          | A           | 23,000      | .054                               | .52                                 | 1,242.00                                  | 11,960.00                                  |
| 5640E          | A           | 10,200      | .085                               | .41                                 | 867.00                                    | 4,182.00                                   |
|                | B           | 7,150       | .058                               | 1.29                                | 414.70                                    | 9,223.50                                   |
|                | C           | 15,600      | .045                               | 1.22                                | 702.00                                    | 19,032.00                                  |
| 5690E          | A           | 17,000      | .045                               | .60                                 | 765.00                                    | 10,200.00                                  |
|                | B           | 9,500       | .05                                | .51                                 | 475.00                                    | 4,845.00                                   |
| 5740E          | A           | 36,000      | .01                                | 1.31                                | 360.00                                    | 47,160.00                                  |
|                | B           | 90,000      | .01                                | .54                                 | 900.00                                    | 48,600.00                                  |
|                | C           | 58,800      | .037                               | .91                                 | 2,175.60                                  | 53,508.00                                  |
|                | D           | 68,000      | .05                                | .71                                 | 3,400.00                                  | 48,280.00                                  |
|                | E           | 142,000     | .066                               | .62                                 | 9,372.00                                  | 88,040.00                                  |
|                | F           | 120,200     | .063                               | .78                                 | 7,572.60                                  | 93,756.00                                  |
|                | G           | 144,000     | .055                               | .71                                 | 7,920.00                                  | 102,240.00                                 |
|                | H           | 35,070      | .04                                | .60                                 | 1,402.80                                  | 21,042.00                                  |
| 5790E          | A           | 12,500      | .054                               | .80                                 | 675.00                                    | 10,000.00                                  |
| 5840E          | A           | 16,500      | .031                               | .89                                 | 511.50                                    | 14,685.00                                  |
|                | B           | 19,600      | .077                               | 1.16                                | 1,509.20                                  | 22,736.00                                  |
| 5890E          | A           | 35,000      | .052                               | 1.00                                | 1,820.00                                  | 35,000.00                                  |
| 5940E          | A           | 52,000      | .015                               | .75                                 | 780.00                                    | 39,000.00                                  |
|                | B           | 79,600      | .044                               | .61                                 | 3,502.40                                  | 48,556.00                                  |
|                | C           | 17,250      | .04                                | .70                                 | 690.00                                    | 12,075.00                                  |
|                | D           | 22,800      | .007                               | .56                                 | 159.60                                    | 12,768.00                                  |
| 6140E          | A           | 57,000      | .01                                | .93                                 | 570.00                                    | 53,010.00                                  |
|                | B           | 36,000      | .02                                | .86                                 | 720.00                                    | 30,960.00                                  |
| TOTAL          |             | 2,536,110   | .053                               | .77                                 | 135,748.78                                | 1,986,415.30                               |

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| <u>SECTION</u> | <u>AREA</u> | <u>TONS</u> | <u>%U<sub>3</sub>O<sub>8</sub></u> | <u>%Cb<sub>2</sub>O<sub>5</sub></u> | <u>Tons x %U<sub>3</sub>O<sub>8</sub></u> | <u>Tons x %Cb<sub>2</sub>O<sub>5</sub></u> |
|----------------|-------------|-------------|------------------------------------|-------------------------------------|---|--|
| 5590E          | A           | 23,000      | .054                               | .52                                 | 1,242.00                                  | 11,960.00                                  |
| 5640E          | A           | 10,200      | .085                               | .41                                 | 867.00                                    | 4,182.00                                   |
|                | B           | 7,150       | .058                               | 1.29                                | 414.70                                    | 9,223.50                                   |
|                | C           | 15,600      | .045                               | 1.22                                | 702.00                                    | 19,032.00                                  |
| 5690E          | A           | 17,000      | .045                               | .60                                 | 765.00                                    | 10,200.00                                  |
|                | B           | 9,500       | .05                                | .51                                 | 475.00                                    | 4,845.00                                   |
| 5740E          | A           | 36,000      | .01                                | 1.31                                | 360.00                                    | 47,160.00                                  |
|                | B           | 90,000      | .01                                | .54                                 | 900.00                                    | 48,600.00                                  |
|                | C           | 58,800      | .037                               | .91                                 | 2,175.60                                  | 53,508.00                                  |
|                | D           | 68,000      | .05                                | .71                                 | 3,400.00                                  | 48,280.00                                  |
|                | E           | 142,000     | .066                               | .62                                 | 9,372.00                                  | 88,040.00                                  |
|                | F           | 120,200     | .063                               | .78                                 | 7,572.60                                  | 93,756.00                                  |
|                | G           | 144,000     | .055                               | .71                                 | 7,920.00                                  | 102,240.00                                 |
|                | H           | 35,070      | .04                                | .60                                 | 1,402.80                                  | 21,042.00                                  |
| 5790E          | A           | 12,500      | .054                               | .80                                 | 675.00                                    | 10,000.00                                  |
| 5840E          | A           | 16,500      | .031                               | .89                                 | 511.50                                    | 14,685.00                                  |
|                | B           | 19,600      | .077                               | 1.16                                | 1,509.20                                  | 22,736.00                                  |
| 5890E          | A           | 35,000      | .052                               | 1.00                                | 1,820.00                                  | 35,000.00                                  |
| 5940E          | A           | 52,000      | .015                               | .75                                 | 780.00                                    | 39,000.00                                  |
|                | B           | 79,600      | .044                               | .61                                 | 3,502.40                                  | 48,556.00                                  |
|                | C           | 17,250      | .04                                | .70                                 | 690.00                                    | 12,075.00                                  |
|                | D           | 22,800      | .007                               | .56                                 | 159.60                                    | 12,768.00                                  |
| 6140E          | A           | 57,000      | .01                                | .93                                 | 570.00                                    | 53,010.00                                  |
|                | B           | 36,000      | .02                                | .86                                 | 720.00                                    | 30,960.00                                  |
| TOTAL          |             | 2,536,110   | .053                               | .77                                 | 135,748.78                                | 1,986,415.30                               |

TONNAGE BETWEEN 300' - 700' LEVEL  
NEWMAN ZONE

| <u>SECTION</u> | <u>AREA</u> | <u>TONS</u> | <u>%U<sub>3</sub>O<sub>8</sub></u> | <u>%Cb<sub>2</sub>O<sub>5</sub></u> | <u>Tons x %U<sub>3</sub>O<sub>8</sub></u> | <u>Tons x %Cb<sub>2</sub>O<sub>5</sub></u> |            |
|----------------|-------------|-------------|------------------------------------|-------------------------------------|---|--|------------|
| 5190E          | A           | 17,770      | .014                               | .66                                 | 248.78                                    | 11,728.20                                  |            |
|                | B           | 22,220      | .014                               | .85                                 | 311.09                                    | 18,887.00                                  |            |
| 5240E          | A           | 8,300       | .011                               | .81                                 | 91.30                                     | 6,723.00                                   |            |
|                | D           | 6,250       | .013                               | .56                                 | 81.25                                     | 3,500.00                                   |            |
|                | E           | 48,800      | .025                               | .87                                 | 1,220.00                                  | 42,456.00                                  |            |
|                | F           | 3,680       | .023                               | .68                                 | 84.64                                     | 2,502.40                                   |            |
|                | G           | 12,000      | .062                               | .76                                 | 744.00                                    | 9,120.00                                   |            |
|                | H           | 28,500      | .03                                | .58                                 | 855.00                                    | 16,530.00                                  |            |
| 5290E          | A           | 14,000      | .038                               | .99                                 | 532.00                                    | 13,860.00                                  |            |
|                | B           | 33,800      | .077                               | .94                                 | 2,602.60                                  | 31,772.00                                  |            |
|                | C           | 22,500      | .057                               | .60                                 | 1,282.50                                  | 13,500.00                                  |            |
|                | D           | 15,750      | .074                               | .75                                 | 1,165.50                                  | 11,812.50                                  |            |
|                | F           | 70,800      | .06                                | .70                                 | 4,248.00                                  | 49,560.00                                  |            |
|                | 5340E       | A           | 25,200                             | .06                                 | .61                                       | 1,512.00                                   | 15,372.00  |
| E              |             | 10,800      | .05                                | .64                                 | 540.00                                    | 6,912.00                                   |            |
| F              |             | 16,600      | .035                               | .69                                 | 581.00                                    | 11,454.00                                  |            |
| G              |             | 32,600      | .055                               | .82                                 | 1,793.00                                  | 26,732.00                                  |            |
| H              |             | 8,000       | .038                               | .58                                 | 304.00                                    | 4,640.00                                   |            |
| I              |             | 8,000       | .035                               | .55                                 | 280.00                                    | 4,400.00                                   |            |
| J              |             | 36,000      | .075                               | .81                                 | 2,700.00                                  | 29,160.00                                  |            |
| K              |             | 222,000     | .063                               | .81                                 | 13,986.00                                 | 179,820.00                                 |            |
| L              |             | 30,600      | .066                               | .64                                 | 2,019.60                                  | 19,584.00                                  |            |
| 5390E          |             | A           | 23,400                             | .073                                | .68                                       | 1,708.20                                   | 15,912.00  |
|                |             | B           | 14,000                             | .057                                | .80                                       | 798.00                                     | 11,200.00  |
|                |             | C           | 137,500                            | .097                                | 1.15                                      | 13,337.50                                  | 158,125.00 |
| 5440E          | F           | 53,300      | .086                               | 1.04                                | 4,583.80                                  | 55,432.00                                  |            |
|                | I           | 39,100      | .066                               | .92                                 | 2,580.60                                  | 35,972.00                                  |            |
| 5490E          | A           | 14,000      | .01                                | .63                                 | 140.00                                    | 8,820.00                                   |            |
|                | B           | 19,000      | .012                               | .82                                 | 228.00                                    | 15,580.00                                  |            |
|                | C           | 44,000      | .034                               | .73                                 | 1,496.00                                  | 32,120.00                                  |            |
|                | D           | 31,000      | .11                                | 1.07                                | 3,410.00                                  | 33,170.00                                  |            |
|                | E           | 9,000       | .07                                | .77                                 | 639.00                                    | 6,930.00                                   |            |
| 5540E          | C           | 14,400      | .107                               | 1.11                                | 1,540.30                                  | 15,984.00                                  |            |
| 5390E          | A           | 23,000      | .054                               | .52                                 | 1,242.00                                  | 11,960.00                                  |            |
| 5640E          | C           | 15,600      | .045                               | 1.22                                | 702.00                                    | 19,032.00                                  |            |

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TONNAGE BETWEEN 300' - 700' LEVEL  
NEWMAN ZONE

| SECTION | AREA  | TONS    | %U <sub>3</sub> O <sub>8</sub> | %Cb <sub>2</sub> O <sub>5</sub> | TONS x %U <sub>3</sub> O <sub>8</sub> | TONS x %Cb <sub>2</sub> O <sub>5</sub> |           |
|---------|-------|---------|--------------------------------|---------------------------------|---------------------------------------|--|-----------|
| 5190E   | A     | 17,770  | .014                           | .66                             | 248.78                                | 11,728.20                              |           |
|         | B     | 22,220  | .014                           | .85                             | 311.09                                | 18,887.00                              |           |
| 521,0E  | A     | 8,300   | .011                           | .81                             | 91.30                                 | 6,723.00                               |           |
|         | D     | 6,250   | .013                           | .56                             | 81.25                                 | 3,500.00                               |           |
|         | E     | 48,800  | .025                           | .87                             | 1,220.00                              | 42,456.00                              |           |
|         | F     | 3,680   | .023                           | .68                             | 84.64                                 | 2,502.40                               |           |
|         | G     | 12,000  | .062                           | .76                             | 744.00                                | 9,120.00                               |           |
|         | H     | 28,500  | .03                            | .58                             | 855.00                                | 16,530.00                              |           |
| 5290E   | A     | 14,000  | .038                           | .99                             | 532.00                                | 13,860.00                              |           |
|         | B     | 33,800  | .077                           | .94                             | 2,602.60                              | 31,772.00                              |           |
|         | C     | 22,500  | .057                           | .60                             | 1,282.50                              | 13,500.00                              |           |
|         | D     | 15,750  | .074                           | .77                             | 1,165.50                              | 11,812.50                              |           |
|         | F     | 70,800  | .06                            | .71                             | 4,248.00                              | 49,560.00                              |           |
| 5340E   | A     | 25,200  | .06                            | .61                             | 1,512.00                              | 15,372.00                              |           |
|         | E     | 10,800  | .05                            | .64                             | 540.00                                | 6,912.00                               |           |
|         | F     | 16,600  | .035                           | .69                             | 581.00                                | 11,454.00                              |           |
|         | G     | 32,600  | .055                           | .82                             | 1,793.00                              | 26,732.00                              |           |
|         | H     | 8,000   | .038                           | .58                             | 304.00                                | 4,640.00                               |           |
|         | I     | 8,000   | .035                           | .55                             | 280.00                                | 4,400.00                               |           |
|         | J     | 36,000  | .075                           | .81                             | 2,700.00                              | 29,160.00                              |           |
|         | K     | 222,000 | .063                           | .81                             | 13,986.00                             | 179,820.00                             |           |
|         | L     | 30,600  | .066                           | .64                             | 2,019.60                              | 19,584.00                              |           |
|         | 5390E | A       | 23,400                         | .073                            | .68                                   | 1,708.20                               | 15,912.00 |
|         |       | H       | 14,000                         | .057                            | .80                                   | 798.00                                 | 11,200.00 |
| C       |       | 137,500 | .097                           | 1.15                            | 13,337.50                             | 158,125.00                             |           |
| 5440E   | F     | 53,300  | .086                           | 1.04                            | 4,583.80                              | 55,432.00                              |           |
|         | I     | 39,100  | .066                           | .92                             | 2,580.60                              | 35,972.00                              |           |
| 5490E   | A     | 14,000  | .01                            | .63                             | 140.00                                | 8,820.00                               |           |
|         | B     | 19,000  | .012                           | .82                             | 228.00                                | 15,580.00                              |           |
|         | C     | 44,000  | .034                           | .73                             | 1,496.00                              | 32,120.00                              |           |
|         | D     | 31,000  | .11                            | 1.07                            | 3,410.00                              | 33,170.00                              |           |
|         | E     | 9,000   | .07                            | .77                             | 639.00                                | 6,930.00                               |           |
| 5540E   | C     | 14,400  | .107                           | 1.11                            | 1,540.80                              | 15,984.00                              |           |
| 5590E   | A     | 23,000  | .054                           | .52                             | 1,242.00                              | 11,960.00                              |           |
| 5640E   | C     | 15,600  | .045                           | 1.22                            | 702.00                                | 19,032.00                              |           |

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| <u>SECTION</u> | <u>AREA</u> | <u>TONS</u> | <u>%U<sub>3</sub>O<sub>8</sub></u> | <u>%Cb<sub>2</sub>O<sub>5</sub></u> | <u>Tons x %U<sub>3</sub>O<sub>8</sub></u> | <u>Tons x %Cb<sub>2</sub>O<sub>5</sub></u> |
|----------------|-------------|-------------|------------------------------------|-------------------------------------|---|--|
| 5690E          | A           | 17,000      | .045                               | .60                                 | 765.00                                    | 10,200.00                                  |
|                | B           | 9,500       | .05                                | .51                                 | 475.00                                    | 4,845.00                                   |
| 5740E          | A           | 36,000      | .01                                | 1.31                                | 360.00                                    | 47,160.00                                  |
|                | B           | 90,000      | .01                                | .54                                 | 900.00                                    | 48,600.00                                  |
|                | D           | 68,000      | .05                                | .71                                 | 3,400.00                                  | 48,280.00                                  |
|                | F           | 120,200     | .063                               | .78                                 | 7,572.60                                  | 93,756.00                                  |
|                | G           | 144,000     | .055                               | .71                                 | 7,920.00                                  | 102,240.00                                 |
|                | H           | 35,070      | .04                                | .60                                 | 1,402.80                                  | 21,042.00                                  |
| 5790E          | A           | 12,500      | .054                               | .80                                 | 675.00                                    | 10,000.00                                  |
| 5840E          | A           | 16,500      | .031                               | .89                                 | 511.50                                    | 14,685.00                                  |
|                | B           | 19,600      | .077                               | 1.16                                | 1,509.20                                  | 22,736.00                                  |
| 5890E          | A           | 35,000      | .052                               | 1.00                                | 1,820.00                                  | 35,000.00                                  |
| 5940E          | C           | 17,250      | .04                                | .70                                 | 690.00                                    | 12,075.00                                  |
| 6140E          | B           | 36,000      | .02                                | .86                                 | 720.00                                    | 30,960.00                                  |
| TOTAL          |             | 1,821,290   | .055                               | .81                                 | 100,026.06                                | 1,470,432.10                               |

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| <u>SECTION</u> | <u>AREA</u> | <u>TONS</u> | <u>%U<sub>3</sub>O<sub>8</sub></u> | <u>%Cb<sub>2</sub>O<sub>5</sub></u> | <u>Tons x %U<sub>3</sub>O<sub>8</sub></u> | <u>Tons x %Cb<sub>2</sub>O<sub>5</sub></u> |
|----------------|-------------|-------------|------------------------------------|-------------------------------------|---|--|
| 5690E          | A           | 17,000      | .045                               | .60                                 | 765.00                                    | 10,200.00                                  |
|                | B           | 9,500       | .05                                | .51                                 | 475.00                                    | 4,845.00                                   |
| 5740E          | A           | 36,000      | .01                                | 1.31                                | 360.00                                    | 47,160.00                                  |
|                | B           | 90,000      | .01                                | .54                                 | 900.00                                    | 48,600.00                                  |
|                | D           | 68,000      | .05                                | .71                                 | 3,400.00                                  | 48,280.00                                  |
|                | F           | 120,200     | .063                               | .78                                 | 7,572.60                                  | 93,756.00                                  |
|                | G           | 144,000     | .055                               | .71                                 | 7,920.00                                  | 102,240.00                                 |
|                | H           | 35,070      | .04                                | .60                                 | 1,402.80                                  | 21,042.00                                  |
| 5790E          | A           | 12,500      | .054                               | .80                                 | 675.00                                    | 10,000.00                                  |
| 5840E          | A           | 16,500      | .031                               | .89                                 | 511.50                                    | 14,685.00                                  |
|                | B           | 19,600      | .077                               | 1.16                                | 1,509.20                                  | 22,736.00                                  |
| 5890E          | A           | 35,000      | .052                               | 1.00                                | 1,820.00                                  | 35,000.00                                  |
| 5940E          | C           | 17,250      | .04                                | .70                                 | 690.00                                    | 12,075.00                                  |
| 6140E          | B           | 36,000      | .02                                | .86                                 | 720.00                                    | 30,960.00                                  |
| TOTAL          |             | 1,821,290   | .055                               | .81                                 | 100,026.06                                | 1,470,432.10                               |

TONS BASIC SILICATE ROCK FERROMAGNESIAN FELDSPAR TYPE

| <u>SECTION</u> | <u>AREA</u> | <u>TONS</u> | <u>%U<sub>3</sub>O<sub>8</sub></u> | <u>%Cb<sub>2</sub>O<sub>3</sub></u> | <u>Tons x %U<sub>3</sub>O<sub>8</sub></u> | <u>Tons x %Cb<sub>2</sub>O<sub>3</sub></u> |
|----------------|-------------|-------------|------------------------------------|-------------------------------------|---|--|
| 5240E          | G           | 12,000      | .062                               | .76                                 | 744.00                                    | 9,120.00                                   |
|                | H           | 28,500      | .03                                | .58                                 | 855.00                                    | 16,530.00                                  |
| 5290E          | B           | 33,800      | .077                               | .94                                 | 2,602.60                                  | 31,772.00                                  |
|                | C           | 22,500      | .057                               | .60                                 | 1,282.50                                  | 13,500.00                                  |
|                | D           | 15,750      | .074                               | .75                                 | 1,165.50                                  | 11,812.50                                  |
|                | F           | 70,800      | .06                                | .70                                 | 4,248.00                                  | 49,560.00                                  |
| 5340E          | G           | 32,600      | .055                               | .82                                 | 1,793.00                                  | 26,732.00                                  |
|                | H           | 8,000       | .038                               | .58                                 | 304.00                                    | 4,640.00                                   |
|                | I           | 8,000       | .035                               | .55                                 | 280.00                                    | 4,400.00                                   |
|                | J           | 36,000      | .075                               | .81                                 | 2,700.00                                  | 29,160.00                                  |
|                | K           | 222,000     | .063                               | .81                                 | 13,986.00                                 | 179,820.00                                 |
|                | L           | 30,600      | .066                               | .64                                 | 2,019.60                                  | 19,584.00                                  |
| 5390E          | C           | 68,700      | .097                               | 1.15                                | 6,664.20                                  | 79,062.00                                  |
| 5440E          | I           | 39,100      | .066                               | .92                                 | 2,580.60                                  | 35,972.00                                  |
| 5490E          | E           | 9,000       | .071                               | .77                                 | 639.00                                    | 6,930.00                                   |
| 5600E          | B           | 9,500       | .05                                | .51                                 | 475.00                                    | 4,845.00                                   |
| 5740E          | G           | 144,000     | .055                               | .71                                 | 7,920.00                                  | 102,240.00                                 |
|                | F           | 60,000      | .063                               | .78                                 | 3,780.00                                  | 46,800.00                                  |
|                | H           | 35,070      | .04                                | .60                                 | 1,402.80                                  | 21,042.00                                  |
| 5940E          | G           | 17,250      | .04                                | .70                                 | 690.00                                    | 12,075.00                                  |
| TOTAL          |             | 903,170     | .062                               | .78                                 | 55,131.80                                 | 705,596.50                                 |

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TONS BASIC SILICATE ROCK FERROMAGNESIAN FELDSPAR TYPE

| <u>SECTION</u> | <u>AREA</u> | <u>TONS</u> | <u>%U308</u> | <u>%CU205</u> | <u>Tons x %U308</u> | <u>Tons x %Cu205</u> |
|----------------|-------------|-------------|--------------|---------------|---------------------|----------------------|
| 5240E          | G           | 12,000      | .062         | .76           | 744.00              | 9,120.00             |
|                | H           | 28,500      | .03          | .58           | 855.00              | 16,530.00            |
| 5290E          | B           | 33,800      | .077         | .94           | 2,602.60            | 31,772.00            |
|                | C           | 22,500      | .057         | .60           | 1,282.50            | 13,500.00            |
|                | D           | 15,750      | .074         | .75           | 1,165.50            | 11,812.50            |
|                | F           | 70,800      | .06          | .70           | 4,248.00            | 49,560.00            |
| 5340E          | G           | 32,600      | .055         | .82           | 1,793.00            | 26,732.00            |
|                | H           | 8,000       | .038         | .58           | 304.00              | 4,640.00             |
|                | I           | 8,000       | .035         | .55           | 280.00              | 4,400.00             |
|                | J           | 36,000      | .075         | .81           | 2,700.00            | 29,160.00            |
|                | K           | 222,000     | .063         | .81           | 13,986.00           | 179,820.00           |
|                | L           | 30,600      | .066         | .64           | 2,019.60            | 19,584.00            |
| 5390E          | C           | 68,700      | .097         | 1.15          | 6,664.20            | 79,062.00            |
| 5440E          | I           | 39,100      | .066         | .92           | 2,580.60            | 35,972.00            |
| 5490E          | E           | 9,000       | .071         | .77           | 639.00              | 6,930.00             |
| 5690E          | B           | 9,500       | .05          | .51           | 475.00              | 4,845.00             |
| 5740E          | G           | 144,000     | .055         | .71           | 7,920.00            | 102,240.00           |
|                | F           | 60,000      | .063         | .78           | 3,780.00            | 46,800.00            |
|                | h           | 35,070      | .04          | .60           | 1,402.80            | 21,042.00            |
| 5940E          | C           | 17,250      | .04          | .70           | 690.00              | 12,075.00            |
| TOTAL          |             | 903,170     | .062         | .78           | 56,131.80           | 705,596.50           |

TONNAGE "HIGH GRADE" SECTION NEWMAN ZONE

| <u>SECTION</u> | <u>AREA</u> | <u>TONS</u> | <u>%U<sub>3</sub>O<sub>8</sub></u> | <u>%Cb<sub>2</sub>O<sub>5</sub></u> | <u>Tons x %U<sub>3</sub>O<sub>8</sub></u> | <u>Tons x %Cb<sub>2</sub>O<sub>5</sub></u> |
|----------------|-------------|-------------|------------------------------------|-------------------------------------|---|--|
| 5290E          | B           | 33,800      | .077                               | .94                                 | 2,602.60                                  | 31,772.00                                  |
|                | D           | 15,750      | .074                               | .75                                 | 1,165.50                                  | 11,812.00                                  |
|                | F           | 70,800      | .06                                | .70                                 | 4,248.00                                  | 49,560.00                                  |
| 5340E          | K           | 222,000     | .063                               | .81                                 | 13,986.00                                 | 179,820.00                                 |
| 5390E          | C           | 137,500     | .097                               | 1.15                                | 13,337.50                                 | 158,125.00                                 |
| 5440E          | F           | 53,300      | .086                               | 1.04                                | 4,583.80                                  | 55,432.00                                  |
|                | I           | 39,100      | .066                               | .92                                 | 2,580.60                                  | 35,972.00                                  |
| 5490E          | D           | 31,000      | .11                                | 1.07                                | 3,410.00                                  | 33,170.00                                  |
| 5540E          | C           | 14,400      | .107                               | 1.11                                | 1,540.80                                  | 15,984.00                                  |
| 5640E          | C           | 15,600      | .045                               | 1.22                                | 702.00                                    | 19,032.00                                  |
| 5840E          | A           | 16,500      | .031                               | .89                                 | 511.50                                    | 14,685.00                                  |
|                | B           | 19,600      | .077                               | 1.16                                | 1,509.20                                  | 22,736.00                                  |
| 5890E          | A           | 35,000      | .052                               | 1.00                                | 1,820.00                                  | 35,000.00                                  |
| 6140E          | B           | 36,000      | .0                                 | .86                                 | 720.00                                    | 30,960.00                                  |
| TOTAL          |             | 740,350     | .071                               | .94                                 | 52,717.50                                 | 694,060.00                                 |

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TOURNAJE "HIGH GRADE" SECTION NEWMAN ZONE

| <u>SECTION</u> | <u>AREA</u> | <u>TONS</u> | <u>%U<sub>3</sub>O<sub>8</sub></u> | <u>%Cb<sub>2</sub>O<sub>5</sub></u> | <u>TONS x %U<sub>3</sub>O<sub>8</sub>N</u> | <u>TONS x %Cb<sub>2</sub>O<sub>5</sub></u> |
|----------------|-------------|-------------|------------------------------------|-------------------------------------|--|--|
| 5290E          | B           | 33,800      | .077                               | .94                                 | 2,602.60                                   | 31,772.00                                  |
|                | D           | 15,750      | .074                               | .75                                 | 1,165.50                                   | 11,812.00                                  |
|                | F           | 70,800      | .06                                | .70                                 | 4,248.00                                   | 49,560.00                                  |
| 5340E          | K           | 222,000     | .063                               | .81                                 | 13,986.00                                  | 179,820.00                                 |
| 5390E          | C           | 137,500     | .097                               | 1.15                                | 13,337.50                                  | 158,125.00                                 |
| 5440E          | F           | 53,300      | .086                               | 1.04                                | 4,583.80                                   | 55,432.00                                  |
|                | I           | 39,100      | .066                               | .92                                 | 2,580.60                                   | 35,972.00                                  |
| 5490E          | D           | 31,000      | .11                                | 1.07                                | 3,410.00                                   | 33,170.00                                  |
| 5540E          | C           | 14,400      | .107                               | 1.11                                | 1,540.80                                   | 15,984.00                                  |
| 5640E          | C           | 15,600      | .045                               | 1.22                                | 702.00                                     | 19,032.00                                  |
| 5840E          | A           | 16,500      | .031                               | .89                                 | 511.50                                     | 14,685.00                                  |
|                | B           | 19,600      | .077                               | 1.16                                | 1,509.20                                   | 22,736.00                                  |
| 5890E          | A           | 35,000      | .052                               | 1.00                                | 1,820.00                                   | 35,000.00                                  |
| 6140E          | B           | 36,000      | .0                                 | .86                                 | 720.00                                     | 30,960.00                                  |
| TOTAL          |             | 740,350     | .071                               | .94                                 | 52,717.50                                  | 694,060.00                                 |

Section 5190ED.D.Hs. U16, U20

|        |                |   |
|--------|----------------|---|
| Area A | average grade  | .014% U <sup>3</sup> O <sub>8</sub> and Cb <sup>2</sup> O <sub>5</sub>      |
|        | true width     | 27'   |
|        | assumed depth  | 131'  |
|        | assumed length | 50'   |
|        | Tons 17,770 @  | .014% U <sup>3</sup> O <sub>8</sub> and .66% Cb <sup>2</sup> O <sub>5</sub> |
| Area B | average grade  | .014% U <sup>3</sup> O <sub>8</sub> and .85% Cb <sup>2</sup> O <sub>5</sub> |
|        | true width     | 34'   |
|        | assumed depth  | 131'  |
|        | assumed length | 50'   |
|        | Tons 22,200 @  | .014%                      and .85%   |

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TABLE 1

D. S. H.'s U19, U20

Area A      average grade  
              true width  
              assumed depth  
              assumed length  
  
              Tons 17,770 @

.014%  $U_3O_8$  & .66%  $Cb_2O_5$   
 27'  
 131'  
 50'

Area B      average grade  
              true width  
              assumed depth  
              assumed length  
  
              Tons 22,200 @

.014%  $U_3O_8$  & .66%  $Cb_2O_5$   
 34'  
 131'  
 50'  
  
 .014                      & .85

SECTION 5240ED.D.H's U2, U3, U8, U12, U14, U23

|        |                |  |   |   |
|--------|----------------|--|---|---|
| Area A | average grade  | .011% U <sub>3</sub> O <sub>8</sub>                            | & | .81% Cb <sub>2</sub> O <sub>5</sub>                           |
|        | true width     | 20'  |   |   |
|        | assumed depth  | 83'  |   |   |
|        | assumed length | 50'  |   |   |
|        | Tons 8,300 @   | .011   | & | .81   |
| Area D | average grade  | .013% U <sub>3</sub> O <sub>8</sub>                            | & | .56% Cb <sub>2</sub> O <sub>5</sub>                           |
|        | true width     | 25'  |   |   |
|        | assumed depth  | 50'  |   |   |
|        | assumed length | 50'  |   |   |
|        | Tons 6,250 @   | .013   | & | .56   |
| Area E | average grade  | $\frac{.012 + .038}{2} = .025\%$ U <sub>3</sub> O <sub>8</sub> |   | $\frac{.56 + 1.18}{2} = .87\%$ Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | $\frac{58 + 65}{2} = 61'$                                      |   |   |
|        | assumed depth  | 160'   |   |   |
|        | assumed length | 50'  |   |   |
|        | Tons 48,800 @  | .025   | & | .87   |
| Area F | average grade  | .023% U <sub>3</sub> O <sub>8</sub>                            | & | .68% Cb <sub>2</sub> O <sub>5</sub>                           |
|        | true width     | 21'  |   |   |
|        | assumed depth  | 35'  |   |   |
|        | assumed length | 50'  |   |   |
|        | Tons 3,680 @   | .023   | & | .68   |
| Area H | average grade  | .03% U <sub>3</sub> O <sub>8</sub>                             | & | .58% Cb <sub>2</sub> O <sub>5</sub>                           |
|        | true width     | 38'  |   |   |
|        | assumed depth  | 150'   |   |   |
|        | assumed length | 50'  |   |   |
|        | Tons 28,500 @  | .03  | & | .58   |
| Area G | average grade  | .062% U <sub>3</sub> O <sub>8</sub>                            | & | .76% Cb <sub>2</sub> O <sub>5</sub>                           |
|        | true width     | 24'  |   |   |
|        | assumed depth  | 100'   |   |   |
|        | assumed length | 50'  |   |   |
|        | Tons 12,000 @  | .062   | & | .76   |

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SECTION 527.0ED.D.H.'s U2, U3, U8, U12, U14, U23

|        |                |  |
|--------|----------------|--|
| Area A | average grade  | .011% U <sub>3</sub> O <sub>8</sub> & .81% Cb <sub>2</sub> O <sub>5</sub>                  |
|        | true width     | 20'  |
|        | assumed depth  | 83'  |
|        | assumed length | 50'  |
|        | Tons 8,300 @   | .011 & .81   |
| Area D | average grade  | .013% U <sub>3</sub> O <sub>8</sub> & .56% Cb <sub>2</sub> O <sub>5</sub>                  |
|        | true width     | 25'  |
|        | assumed depth  | 50'  |
|        | assumed length | 50'  |
|        | Tons 6,250 @   | .013 & .56   |
| Area E | average grade  | $\frac{.012 + .038}{2} = .025\%$ U <sub>3</sub> O <sub>8</sub> $\frac{.56 + 1.18}{2} = .8$ |
|        | true width     | $\frac{58 + 65}{2} = 61'$  |
|        | assumed depth  | 160'   |
|        | assumed length | 50'  |
|        | Tons 48,800 @  | .025 & .87   |
| Area F | average grade  | .023% U <sub>3</sub> O <sub>8</sub> & .68% Cb <sub>2</sub> O <sub>5</sub>                  |
|        | true width     | 21'  |
|        | assumed depth  | 35'  |
|        | assumed length | 50'  |
|        | Tons 3,680 @   | .023 & .68   |
| Area H | average grade  | .03% U <sub>3</sub> O <sub>8</sub> & .58% Cb <sub>2</sub> O <sub>5</sub>                   |
|        | true width     | 33'  |
|        | assumed depth  | 150'   |
|        | assumed length | 50'  |
|        | Tons 28,500 @  | .03 & .58  |
| Area C | average grade  | .062% U <sub>3</sub> O <sub>8</sub> & .76% Cb <sub>2</sub> O <sub>5</sub>                  |
|        | true width     | 24'  |
|        | assumed depth  | 100'   |
|        | assumed length | 50'  |
|        | Tons 12,000 @  | .062 & .76   |

SECTION 5290ED.D.H.'s U15, U17, U19, U46

|        |                |                                     |   |                                     |
|--------|----------------|-------------------------------------|---|-------------------------------------|
| Area A | average grade  | .038% U <sub>3</sub> O <sub>8</sub> | & | .99% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 14'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 14,000 @  | .038                                | & | .99                                 |
| Area B | average grade  | .077% U <sub>3</sub> O <sub>8</sub> | & | .94% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 54'                                 |   |                                     |
|        | assumed depth  | 125'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 33,800 @  | .077                                | & | .94                                 |
| Area C | average grade  | .057% U <sub>3</sub> O <sub>8</sub> | & | 60% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 45'                                 |   |                                     |
|        | assumed depth  | 100'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 22,500 @  | .057                                | & | .60                                 |
| Area D | average grade  | .074% U <sub>3</sub> O <sub>8</sub> | & | .75% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 45'                                 |   |                                     |
|        | assumed depth  | 70'                                 |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 15,750 @  | .074                                | & | .75                                 |
| Area F | average grade  | .06% U <sub>3</sub> O <sub>8</sub>  | & | .70% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 86'                                 |   |                                     |
|        | assumed depth  | 16'                                 |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 70,800 @  | .06                                 | & | .70                                 |

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SECTION 5290E

D.D.H.'s U15, U17, U19, U46

|        |  |   |
|--------|--|---|
| Area A | average grade<br>true width<br>assumed depth<br>assumed length | .038% U <sub>3</sub> O <sub>8</sub> & .99% Cb <sub>2</sub> O <sub>5</sub><br>14'<br>200'<br>50' |
|        | Tons 14,000 @  | .038 & .99  |
| Area B | average grade<br>true width<br>assumed depth<br>assumed length | .077% U <sub>3</sub> O <sub>8</sub> & .94% Cb <sub>2</sub> O <sub>5</sub><br>54'<br>125'<br>50' |
|        | Tons 33,800 @  | .077 & .94  |
| Area C | average grade<br>true width<br>assumed depth<br>assumed length | .057% U <sub>3</sub> O <sub>8</sub> & .60% Cb <sub>2</sub> O <sub>5</sub><br>45'<br>100'<br>50' |
|        | Tons 22,500 @  | .057 & .60  |
| Area D | average grade<br>true width<br>assumed depth<br>assumed length | .074% U <sub>3</sub> O <sub>8</sub> & .75% Cb <sub>2</sub> O <sub>5</sub><br>45'<br>70'<br>50'  |
|        | Tons 15,750 @  | .074 & .75  |
| Area F | average grade<br>true width<br>assumed depth<br>assumed length | .06% U <sub>3</sub> O <sub>8</sub> & .70% Cb <sub>2</sub> O <sub>5</sub><br>86'<br>165'<br>50'  |
|        | Tons 70,800 @  | .06 & .70   |

SECTION 5342ED.D.H.'s 9, 30, 34, U5, U7, U13, U18, U34, NX3.

|        |                |                                     |   |                                     |
|--------|----------------|-------------------------------------|---|-------------------------------------|
| Area A | average grade  | .06% U <sub>3</sub> O <sub>8</sub>  | & | .61% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 28'                                 |   |                                     |
|        | assumed depth  | 180'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 25,200 @  | .06                                 | & | .61                                 |
| Area B | average grade  | .07% U <sub>3</sub> O <sub>8</sub>  | & | .66% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 20'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 20,000 @  | .07                                 | & | .66                                 |
| Area C | average grade  | .041% U <sub>3</sub> O <sub>8</sub> | & | .69% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 102'                                |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 102,000 @ | .041                                | & | .69                                 |
| Area D | average grade  | .046% U <sub>3</sub> O <sub>8</sub> | & | .66% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 42'                                 |   |                                     |
|        | assumed depth  | 105'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 22,020 @  | .046                                | & | .66                                 |
| Area E | average grade  | .05% U <sub>3</sub> O <sub>8</sub>  | & | .64% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 54'                                 |   |                                     |
|        | assumed depth  | 40'                                 |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 10,800 @  | .05                                 | & | .64                                 |
| Area F | average grade  | 1035% U <sub>3</sub> O <sub>8</sub> | & | .69% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 19'                                 |   |                                     |
|        | assumed depth  | 175'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 16,600 @  | .035                                | & | .69                                 |
| Area G | average grade  | .055% U <sub>3</sub> O <sub>8</sub> | & | .82% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 31'                                 |   |                                     |
|        | assumed depth  | 210'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 32,600 @  | .055                                | & | .82                                 |
| Area H | average grade  | .038% U <sub>3</sub> O <sub>8</sub> | & | .58% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 8'                                  |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 8,000 @   | .038                                | & | .58                                 |

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SECTION 5342E

D.D.H.'s 9, 30, 34, U5, U7, U13, U18, U34, MX3.

|        |  |  |   |                                     |
|--------|--|--|---|-------------------------------------|
| Area A | average grade<br>true width<br>assumed depth<br>assumed length | .06% U <sub>3</sub> O <sub>8</sub><br>28'<br>180'<br>50'   | & | .61% Cb <sub>2</sub> O <sub>5</sub> |
|        | Tons 25,200 @  | .06  | & | .61                                 |
| Area B | average grade<br>true width<br>assumed depth<br>assumed length | .07% U <sub>3</sub> O <sub>8</sub><br>20'<br>200'<br>50'   | & | .66% Cb <sub>2</sub> O <sub>5</sub> |
|        | Tons 20,000 @  | .07  | & | .66                                 |
| Area C | average grade<br>true width<br>assumed depth<br>assumed length | .041% U <sub>3</sub> O <sub>8</sub><br>102'<br>200'<br>50' | & | .69% Cb <sub>2</sub> O <sub>5</sub> |
|        | Tons 102,000 @   | .041   | & | .69                                 |
| Area D | average grade<br>true width<br>assumed depth<br>assumed length | .046% U <sub>3</sub> O <sub>8</sub><br>42'<br>105'<br>50'  | & | .66% Cb <sub>2</sub> O <sub>5</sub> |
|        | Tons 22,020 @  | .046   | & | .66                                 |
| Area E | average grade<br>true width<br>assumed depth<br>assumed length | .05% U <sub>3</sub> O <sub>8</sub><br>54'<br>40'<br>50'    | & | .64% Cb <sub>2</sub> O <sub>5</sub> |
|        | Tons 10,800 @  | .05  | & | .64                                 |
| Area F | average grade<br>true width<br>assumed depth<br>assumed length | .035% U <sub>3</sub> O <sub>8</sub><br>19'<br>175'<br>50'  | & | .69% Cb <sub>2</sub> O <sub>5</sub> |
|        | Tons 16,600 @  | .035   | & | .69                                 |
| Area G | average grade<br>true width<br>assumed depth<br>assumed length | .055% U <sub>3</sub> O <sub>8</sub><br>31'<br>210'<br>50'  | & | .82% Cb <sub>2</sub> O <sub>5</sub> |
|        | Tons 32,600 @  | .055   | & | .82                                 |
| Area H | average grade<br>true width<br>assumed depth<br>assumed length | .038 U <sub>3</sub> O <sub>8</sub><br>8'<br>200'<br>50'    | & | .58% Cb <sub>2</sub> O <sub>5</sub> |
|        | Tons 8,000 @   | .038   | & | .58                                 |

SECTION 5340E Cont'dD.D.H.'s 9,30,34,U5,U7,U13,U18,U34,NX3.

|        |                |  |   |                                     |
|--------|----------------|--|---|-------------------------------------|
| Area I | average grade  | .035% U <sub>3</sub> O <sub>8</sub>                      | & | .55% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 8'   |   |                                     |
|        | assumed depth  | 200'   |   |                                     |
|        | assumed length | 50'  |   |                                     |
|        | Tons 8,000 @   | .035   | & | .55                                 |
| Area J | average grade  | .075% U <sub>3</sub> O <sub>8</sub>                      | & | .81% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 24'  |   |                                     |
|        | assumed depth  | 300'   |   |                                     |
|        | assumed length | 50'  |   |                                     |
|        | Tons 36,000 @  | .075   | & | .81                                 |
| Area K | average grade  | $.08/3 + .056/3 + .053/3 = .063\% \text{ U}_3\text{O}_8$ |   |                                     |
|        | true width     | $.91/3 + .85/3 + .65/3 = .81\% \text{ Cb}_2\text{O}_5$   |   |                                     |
|        | assumed depth  | 120'   |   |                                     |
|        | assumed length | 370'   |   |                                     |
|        | Tons 222,000 @ | .063   | & | .81                                 |
| Area L | average grade  | .066% U <sub>3</sub> O <sub>8</sub>                      | & | .64% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 18'  |   |                                     |
|        | assumed depth  | 340'   |   |                                     |
|        | assumed length | 50'  |   |                                     |
|        | Tons 30,600 @  | .066   | & | .64                                 |

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SECTION 534PE Cont'd

D.D.H.'s 9, 30, 34, U5, U7, U13, U18, U34, NX3.

|        |                |  |   |                                     |
|--------|----------------|--|---|-------------------------------------|
| Area I | average grade  | .035% U <sub>3</sub> O <sub>8</sub>                              | & | .55% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 8'   |   |                                     |
|        | assumed depth  | 200'   |   |                                     |
|        | assumed length | 50'  |   |                                     |
|        | Tons 8,000 @   | .035   | & | .55                                 |
| Area J | average grade  | .075% U <sub>3</sub> O <sub>8</sub>                              | & | .81% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 24'  |   |                                     |
|        | assumed depth  | 300'   |   |                                     |
|        | assumed length | 50'  |   |                                     |
|        | Tons 36,000 @  | .075   | & | .81                                 |
| Area K | average grade  | $.08/3 + .056/3 + .053/3 = .063\%$ U <sub>3</sub> O <sub>8</sub> |   |                                     |
|        | true width     | $.91/3 + .85/3 + .65/3 = .81\%$ Cb <sub>2</sub> O <sub>5</sub>   |   |                                     |
|        | assumed depth  | 120'   |   |                                     |
|        | assumed length | 370'   |   |                                     |
|        | Tons 222,000 @ | .063   | & | .81                                 |
| Area L | average grade  | .066% U <sub>3</sub> O <sub>8</sub>                              | & | .64% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 18'  |   |                                     |
|        | assumed depth  | 340'   |   |                                     |
|        | assumed length | 50'  |   |                                     |
|        | Tons 30,600 @  | .066   | & | .64                                 |

SECTION 5390ED.D.H.'s U10, U11, U51

|        |                |                                     |   |                                      |
|--------|----------------|-------------------------------------|---|--------------------------------------|
| Area A | average grade  | .073% U <sub>3</sub> O <sub>8</sub> | & | .68% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 39'                                 |   |                                      |
|        | assumed depth  | 120'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 23,400 @  | .073                                | & | .68                                  |
| Area B | average grade  | .057% U <sub>3</sub> O <sub>8</sub> | & | .80% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 14'                                 |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 14,000 @  | .057                                | & | .80                                  |
| Area C | average grade  | .097% U <sub>3</sub> O <sub>8</sub> | & | 1.15% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 157'                                |   |                                      |
|        | assumed depth  | 175'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 137,500 @ | .097                                | & | 1.15                                 |

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SECTION 5390ED.D.H.'s U10, U11, U51

|        |                |                                     |   |                                      |
|--------|----------------|-------------------------------------|---|--------------------------------------|
| Area A | average grade  | .073% U <sub>3</sub> O <sub>8</sub> | & | .68% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 39'                                 |   |                                      |
|        | assumed depth  | 120'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 23,400 @  | .073                                | & | .68                                  |
| Area B | average grade  | .057% U <sub>3</sub> O <sub>8</sub> | & | .80% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 14'                                 |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 14,000 @  | .057                                | & | .80                                  |
| Area C | average grade  | .097% U <sub>3</sub> O <sub>8</sub> | & | 1.15% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 157'                                |   |                                      |
|        | assumed depth  | 175'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 137,500 @ | .097                                | & | 1.15                                 |

SECTION 5440ED.D.H.'s 37, U21, U22, U31, U40

|        |                |                                     |   |                                     |
|--------|----------------|-------------------------------------|---|-------------------------------------|
| Area A | average grade  | .075% U <sub>3</sub> O <sub>8</sub> | & | .64% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 56'                                 |   |                                     |
|        | assumed depth  | 180'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 50,400 @  | .075                                | & | .64                                 |
| Area B | average grade  | .056% U <sub>3</sub> O <sub>8</sub> | & | .69% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 10'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 10,000 @  | .056                                | & | .69                                 |
| Area D | average grade  | .08% U <sub>3</sub> O <sub>8</sub>  | & | .72% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 45'                                 |   |                                     |
|        | assumed width  | 190'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 42,700 @  | .08                                 | & | .72                                 |
| Area E | average grade  | .055% U <sub>3</sub> O <sub>8</sub> | & | .56% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 51'                                 |   |                                     |
|        | assumed depth  | 130'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 33,200 @  | .055                                | & | .56                                 |
| Area F | average grade  | .086% U <sub>3</sub> O <sub>8</sub> | & | 1.04 Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 82'                                 |   |                                     |
|        | assumed depth  | 130'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 53,300 @  | .086                                | & | 1.04                                |
| Area H | average grade  | .066% U <sub>3</sub> O <sub>8</sub> | & | .92% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 46'                                 |   |                                     |
|        | assumed depth  | 170'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 39,100 @  | .066                                | & | .92                                 |

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SECTION 5440ED.D.H.'s 37, U21, U22, U31, U40

|        |                |                                     |   |                                     |
|--------|----------------|-------------------------------------|---|-------------------------------------|
| Area A | average grade  | .075% U <sub>3</sub> O <sub>8</sub> | & | .64% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 56'                                 |   |                                     |
|        | assumed depth  | 180'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 50,400 @  | .075                                | & | .64                                 |
| Area B | average grade  | .056% U <sub>3</sub> O <sub>8</sub> | & | .69% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 10'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 10,000 @  | .056                                | & | .69                                 |
| Area D | average grade  | .08% U <sub>3</sub> O <sub>8</sub>  | & | .72% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 45'                                 |   |                                     |
|        | assumed width  | 190'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 42,700 @  | .08                                 | & | .72                                 |
| Area E | average grade  | .055% U <sub>3</sub> O <sub>8</sub> | & | .56% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 51'                                 |   |                                     |
|        | assumed depth  | 130'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 33,200 @  | .055                                | & | .56                                 |
| Area F | average grade  | .086% U <sub>3</sub> O <sub>8</sub> | & | 1.04 Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 82'                                 |   |                                     |
|        | assumed depth  | 130'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 53,300 @  | .086                                | & | 1.04                                |
| Area H | average grade  | .066% U <sub>3</sub> O <sub>8</sub> | & | .92% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 46'                                 |   |                                     |
|        | assumed depth  | 170'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 39,100 @  | .066                                | & | .92                                 |

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SECTION 5440ED.D.H.'s 37, U21, U22, U31, U40.

|        |                |                                     |   |                                      |
|--------|----------------|-------------------------------------|---|--------------------------------------|
| Area A | average grade  | .075% U <sub>3</sub> O <sub>8</sub> | & | .64% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 56'                                 |   |                                      |
|        | assumed depth  | 180'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 50,400 @  | .075                                | & | .64                                  |
| Area B | average grade  | .056% U <sub>3</sub> O <sub>8</sub> | & | .69% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 10'                                 |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 10,000 @  | .056                                | & | .69                                  |
| Area D | average grade  | .08% U <sub>3</sub> O <sub>8</sub>  | & | .72% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 45'                                 |   |                                      |
|        | assumed depth  | 190'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 42,700 @  | .08                                 | & | .72                                  |
| Area E | average grade  | .055% U <sub>3</sub> O <sub>8</sub> | & | .56% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 51'                                 |   |                                      |
|        | assumed depth  | 130'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 33,200 @  | .055                                | & | .56                                  |
| Area F | average grade  | .086% U <sub>3</sub> O <sub>8</sub> | & | 1.04% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 82'                                 |   |                                      |
|        | assumed depth  | 130'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 53,300 @  | .086                                | & | 1.04                                 |
| Area H | average grade  | .066% U <sub>3</sub> O <sub>8</sub> | & | .92% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 46'                                 |   |                                      |
|        | assumed depth  | 170'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 39,100 @  | .066                                | & | .92                                  |

SECTION 5490ED.D.H.'s U24, U25, U47

|        |                |                                     |   |                                      |
|--------|----------------|-------------------------------------|---|--------------------------------------|
| Area A | average grade  | .10% U <sub>3</sub> O <sub>8</sub>  | & | .63% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 14'                                 |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 14,000 @  | .01                                 | & | .63                                  |
| Area B | average grade  | .012% U <sub>3</sub> O <sub>8</sub> | & | .82% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 19'                                 |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 19,000 @  | .012                                | & | .82                                  |
| Area C | average grade  | .034% U <sub>3</sub> O <sub>8</sub> | & | .73% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 44'                                 |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 44,000 @  | .034                                | & | .73                                  |
| Area D | average grade  | .11% U <sub>3</sub> O <sub>8</sub>  | & | 1.07% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 31'                                 |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 31,000 @  | .11                                 | & | 1.07                                 |
| Area E | average grade  | .071% U <sub>3</sub> O <sub>8</sub> | & | .77% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 9'                                  |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 9,000 @   | .071                                | & | .77                                  |

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SECTION 5490ED.D.H.'s U24, U25, U47.

|        |                |                                     |   |                                      |
|--------|----------------|-------------------------------------|---|--------------------------------------|
| Area A | average grade  | .01% U <sub>3</sub> O <sub>8</sub>  | & | .63% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 14'                                 |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 14,000 @  | .01                                 | & | .63                                  |
| Area B | average grade  | .012% U <sub>3</sub> O <sub>8</sub> | & | .82% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 19'                                 |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 19,000 @  | .012                                | & | .82                                  |
| Area C | average grade  | .034% U <sub>3</sub> O <sub>8</sub> | & | .73% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 44'                                 |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 44,000 @  | .034                                | & | .73                                  |
| Area D | average grade  | .11% U <sub>3</sub> O <sub>8</sub>  | & | 1.07% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 31'                                 |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 31,000 @  | .11                                 | & | 1.07                                 |
| Area E | average grade  | .071% U <sub>3</sub> O <sub>8</sub> | & | .77% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 9'                                  |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 9,000 @   | .071                                | & | .77                                  |

SECTION 5540ED.D.H.'s 13, 16, U29, U30, U42.

|        |                |                                     |   |                                      |
|--------|----------------|-------------------------------------|---|--------------------------------------|
| Area A | average grade  | .061% U <sub>3</sub> O <sub>8</sub> | & | .70% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 32'                                 |   |                                      |
|        | assumed depth  | 152'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 24,300 @  | .061                                | & | .70                                  |
| Area B | average grade  | .14% U <sub>3</sub> O <sub>8</sub>  | & | 1.21% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 21'                                 |   |                                      |
|        | assumed depth  | 132'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 13,850 @  | .14                                 | & | 1.21                                 |
| Area C | average grade  | .107% U <sub>3</sub> O <sub>8</sub> | & | 1.11% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 32'                                 |   |                                      |
|        | assumed depth  | 90'                                 |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 14,400 @  | .107                                | & | 1.11                                 |

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SECTION 5540E

D.D.H.'s 13, 16, U29, U30, U42.

|        |                |                                     |   |                                      |
|--------|----------------|-------------------------------------|---|--------------------------------------|
| Area A | average grade  | .061% U <sub>3</sub> O <sub>8</sub> | & | .70% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 32'                                 |   |                                      |
|        | assumed depth  | 152'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons           | 24,300                              | ⊙ |                                      |
|        |                | .061                                | & | .70                                  |
| Area B | average grade  | .14% U <sub>3</sub> O <sub>8</sub>  | & | 1.21% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 21'                                 |   |                                      |
|        | assumed depth  | 132'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons           | 13,850                              | ⊙ |                                      |
|        |                | .14                                 | & | 1.21                                 |
| Area C | average grade  | .107% U <sub>3</sub> O <sub>8</sub> | & | 1.11% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 32'                                 |   |                                      |
|        | assumed depth  | 90'                                 |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons           | 14,400                              | ⊙ |                                      |
|        |                | .107                                | & | 1.11                                 |



SECTION 5590ED.D.H.'s U33.

|        |                |       |                               |   |      |                                |
|--------|----------------|-------|-------------------------------|---|------|--------------------------------|
| Area A | average grade  | .054% | U <sub>3</sub> O <sub>8</sub> | & | .52% | Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 23'   |                               |   |      |                                |
|        | assumed depth  | 200'  |                               |   |      |                                |
|        | assumed length | 50'   |                               |   |      |                                |
|        | Tons 23,000 @  | .054  |                               | & | .52  |                                |

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SECTION 5590ED.D.H's U33.

|        |                |                                     |   |                                     |
|--------|----------------|-------------------------------------|---|-------------------------------------|
| Area A | average grade  | .054% U <sub>3</sub> O <sub>8</sub> | & | .52% Co <sub>2</sub> O <sub>5</sub> |
|        | true width     | 23'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 50'                                 |   |                                     |
|        | Tons 23,000    | .054                                | & | .52                                 |

SECTION 5640ED.D.H.'s 33, U32, U35, U41.

|        |                |                                     |   |                                      |
|--------|----------------|-------------------------------------|---|--------------------------------------|
| Area A | average grade  | .085% U <sub>3</sub> O <sub>8</sub> | & | .41% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 17'                                 |   |                                      |
|        | assumed depth  | 120'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 10,200 @  | .085                                | & | .41                                  |
| Area B | average grade  | .058% U <sub>3</sub> O <sub>8</sub> | & | 1.29% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 13'                                 |   |                                      |
|        | assumed depth  | 110'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 7,150 @   | .058                                | & | 1.29                                 |
| Area C | average grade  | .045% U <sub>3</sub> O <sub>8</sub> | & | 1.22% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 24'                                 |   |                                      |
|        | assumed depth  | 130'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 15,600 @  | .045                                | & | 1.22                                 |

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SECTION 5610ED.D.H.'s 33, U32, U35, U41.

|        |                |                                     |   |                                      |
|--------|----------------|-------------------------------------|---|--------------------------------------|
| Area A | average grade  | .085% U <sub>3</sub> O <sub>8</sub> | & | .41% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 17'                                 |   |                                      |
|        | assumed depth  | 120'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 10,200 @  | .085                                | & | .41                                  |
| Area B | average grade  | .058% U <sub>3</sub> O <sub>8</sub> | & | 1.29% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 13'                                 |   |                                      |
|        | assumed depth  | 110'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 7,150 @   | .058                                | & | 1.29                                 |
| Area C | average grade  | .045% U <sub>3</sub> O <sub>8</sub> | & | 1.22% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 24'                                 |   |                                      |
|        | assumed depth  | 130'                                |   |                                      |
|        | assumed length | 50'                                 |   |                                      |
|        | Tons 15,600 @  | .045                                | & | 1.22                                 |

SECTION 5690ED.D.H.'s U37, U38.

Due to lack of drilling on this section ore intersection used to substantiate masses outlined on Section 5740E. Ore calculated on Section 5740E projected to Section 5690E.

|        |                |                                     |   |                                     |
|--------|----------------|-------------------------------------|---|-------------------------------------|
| Area A | average grade  | .045% U <sub>3</sub> O <sub>8</sub> | & | .60% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 34'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 25'                                 |   |                                     |
|        | Tons 17,000 @  | .045                                | & | .60                                 |
| Area B | average grade  | .05% U <sub>3</sub> O <sub>8</sub>  | & | .51% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 19'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 25'                                 |   |                                     |
|        | Tons 9,500 @   | .05                                 | & | .51                                 |

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SECTION 5690ED.D.H.'s U37, U38.

Due to lack of drilling on this section ore intersection used to substantiate masses outlined on Section 5740E. Ore calculated on Section 5740E projected to Section 5690E.

|        |                |                                     |   |                                     |
|--------|----------------|-------------------------------------|---|-------------------------------------|
| Area A | average grade  | .045% U <sub>3</sub> O <sub>8</sub> | & | .60% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 34'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 25'                                 |   |                                     |
|        | Tons 17,000 @  | .045                                | & | .60                                 |
| Area B | average grade  | .05% U <sub>3</sub> O <sub>8</sub>  | & | .51% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 19'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 25'                                 |   |                                     |
|        | Tons 9,500 @   | .05                                 | & | .51                                 |

SECTION 5740ED.D.H.'s 15, 18, 20. U43, U44.

Due to lack of drill holes on adjacent sections, ore masses on this section are projected 50' E & to' W.

|        |                |                |   |                 |
|--------|----------------|----------------|---|-----------------|
| Area A | average grade  | .01% $U_3O_8$  | & | 1.31% $Cb_2O_5$ |
|        | true width     | 18'            |   |                 |
|        | assumed depth  | 200'           |   |                 |
|        | assumed length | 100'           |   |                 |
|        | Tons 36,000 @  | .01            | & | 1.31            |
| Area B | average grade  | .01% $U_3O_8$  | & | .54% $Cb_2O_5$  |
|        | true width     | 40'            |   |                 |
|        | assumed depth  | 225'           |   |                 |
|        | assumed length | 100'           |   |                 |
|        | Tons 90,000 @  | .01            | & | .54             |
| Area C | average grade  | .037% $U_3O_8$ | & | .91% $Cb_2O_5$  |
|        | true width     | 42'            |   |                 |
|        | assumed depth  | 140'           |   |                 |
|        | assumed length | 100'           |   |                 |
|        | Tons 58,800 @  | .037           | & | .91             |
| Area D | average grade  | .05% $U_3O_8$  | & | .71% $Cb_2O_5$  |
|        | true width     | 40'            |   |                 |
|        | assumed depth  | 170'           |   |                 |
|        | assumed length | 100'           |   |                 |
|        | Tons 68,000 @  | .05            | & | .71             |
| Area E | average grade  | .066% $U_3O_8$ | & | .62% $Cb_2O_5$  |
|        | true width     | 64'            |   |                 |
|        | assumed depth  | 222'           |   |                 |
|        | assumed length | 100'           |   |                 |
|        | Tons 142,000 @ | .066           | & | .62             |
| Area F | average grade  | .063% $U_3O_8$ | & | .78% $Cb_2O_5$  |
|        | true width     | 46'            |   |                 |
|        | assumed depth  | 262'           |   |                 |
|        | assumed length | 100'           |   |                 |
|        | Tons 120,200 @ | .063           | & | .78             |
| Area G | average grade  | .055% $U_3O_8$ | & | .71% $Cb_2O_5$  |
|        | true width     | 54'            |   |                 |
|        | assumed depth  | 268'           |   |                 |
|        | assumed length | 100'           |   |                 |
|        | Tons 144,000 @ | .055           | & | .71             |

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SECTION 5740ED.D.H.'s 15, 18, 20, U43, U44.

Due to lack of drill holes on adjacent sections, ore masses on this section are projected 50' E & 50' W.

|        |                |                                     |   |                                      |
|--------|----------------|-------------------------------------|---|--------------------------------------|
| Area A | average grade  | .01% U <sub>3</sub> O <sub>8</sub>  | & | 1.31% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 18'                                 |   |                                      |
|        | assumed depth  | 200'                                |   |                                      |
|        | assumed length | 100'                                |   |                                      |
|        | Tons           | 36,000                              | ⊙ |                                      |
|        |                | .01                                 | & | 1.31                                 |
| Area B | average grade  | .01% U <sub>3</sub> O <sub>8</sub>  | & | .54% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 40'                                 |   |                                      |
|        | assumed depth  | 225'                                |   |                                      |
|        | assumed length | 100'                                |   |                                      |
|        | Tons           | 90,000                              | ⊙ |                                      |
|        |                | .01                                 | & | .54                                  |
| Area C | average grade  | .037% U <sub>3</sub> O <sub>8</sub> | & | .91% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 42'                                 |   |                                      |
|        | assumed depth  | 140'                                |   |                                      |
|        | assumed length | 100'                                |   |                                      |
|        | Tons           | 58,800                              | ⊙ |                                      |
|        |                | .037                                | & | .91                                  |
| Area D | average grade  | .05% U <sub>3</sub> O <sub>8</sub>  | & | .71% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 40'                                 |   |                                      |
|        | assumed depth  | 170'                                |   |                                      |
|        | assumed length | 100'                                |   |                                      |
|        | Tons           | 68,000                              | ⊙ |                                      |
|        |                | .05                                 | & | .71                                  |
| Area E | average grade  | .066% U <sub>3</sub> O <sub>8</sub> | & | .62% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 64'                                 |   |                                      |
|        | assumed depth  | 222'                                |   |                                      |
|        | assumed length | 100'                                |   |                                      |
|        | Tons           | 142,000                             | ⊙ |                                      |
|        |                | .066                                | & | .62                                  |
| Area F | average grade  | .063% U <sub>3</sub> O <sub>8</sub> | & | .78% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 46'                                 |   |                                      |
|        | assumed depth  | 262'                                |   |                                      |
|        | assumed length | 100'                                |   |                                      |
|        | Tons           | 120,200                             | ⊙ |                                      |
|        |                | .063                                | & | .78                                  |
| Area G | average grade  | .055% U <sub>3</sub> O <sub>8</sub> | & | .71% Cb <sub>2</sub> O <sub>5</sub>  |
|        | true width     | 54'                                 |   |                                      |
|        | assumed depth  | 268'                                |   |                                      |
|        | assumed length | 100'                                |   |                                      |
|        | Tons           | 144,000                             | ⊙ |                                      |
|        |                | .055                                | & | .71                                  |



SECTION 5740E Cont'dD.D.H.'s 15, 18, 20, U43, U44.

|        |                |                                    |   |                                     |
|--------|----------------|------------------------------------|---|-------------------------------------|
| Area H | average grade  | .04% U <sub>3</sub> O <sub>8</sub> | & | .60% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 21'                                |   |                                     |
|        | assumed depth  | 167'                               |   |                                     |
|        | assumed length | 100'                               |   |                                     |
|        | Tons 35,070    | .04                                | & | .60                                 |

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SECTION 5740E Cont'd

U.D.H.'s 15, 18, 20, U43, U44.

Area H    average grade  
          true width  
          assumed depth  
          assumed length  
  
          Tons 35,070 ●

.04%  $U_3O_8$     &    .60%  $CO_2O_5$   
21'  
167'  
100'  
  
.04                    &    .60

SECTION 5790E

Due to lack of drilling on this section ore outlined on section 5740E projected to this section.

|        |                |                                     |   |                                     |
|--------|----------------|-------------------------------------|---|-------------------------------------|
| Area A | Average grade  | .054% U <sub>3</sub> O <sub>8</sub> | & | .80% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 25'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 25'                                 |   |                                     |
|        | Tons 12,500 @  | .054                                | & | .80                                 |

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SECTION 5790E

Due to lack of drilling on this section ore outlined on section 5740E projected to this section.

|        |                |                                     |   |                                     |
|--------|----------------|-------------------------------------|---|-------------------------------------|
| Area A | average grade  | .054% U <sub>3</sub> O <sub>8</sub> | & | .80% Co <sub>2</sub> O <sub>5</sub> |
|        | true width     | 25'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 25'                                 |   |                                     |
|        | Tons 12,500 @  | .054                                | & | .80                                 |

SECTION 5840E

D.D.H.'s U49, U52, U54.

|        |                |       |                 |   |       |                   |
|--------|----------------|-------|-----------------|---|-------|-------------------|
| Area A | average grade  | .013% | U <sub>30</sub> | & | .89%  | Cb <sub>205</sub> |
|        | true width     | 30'   |                 |   |       |                   |
|        | assumed depth  | 110'  |                 |   |       |                   |
|        | assumed length | 50'   |                 |   |       |                   |
|        | Tons 16,500 @  | .031  |                 | & | .89   |                   |
| Area B | average grade  | .077% | U <sub>30</sub> | & | 1.16% | Cb <sub>205</sub> |
|        | true width     | 28'   |                 |   |       |                   |
|        | assumed depth  | 140'  |                 |   |       |                   |
|        | assumed length | 50'   |                 |   |       |                   |
|        | Tons 19,600 @  | .077  |                 | & | 1.16  |                   |

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SECTION 5840E

D.D.H.'s 149, U52, U54.

Area A    average grade  
           true width  
           assumed depth  
           assumed length

          Tons 16,500 @

.013%  $U_3O_8$     &    .89%  $Cb_2O_5$   
 30'  
 110'  
 50'

.031                    &    .89

Area B    average grade  
           true width  
           assumed depth  
           assumed length

          Tons 19,600 @

.077%  $U_3O_8$     &    1.16%  $Cb_2O_5$   
 28'  
 140'  
 50'

.077                    &    1.16

SECTION 5890E

D.D.H.'s U56, U57.

|        |                |       |                               |   |       |                                |
|--------|----------------|-------|-------------------------------|---|-------|--------------------------------|
| Area A | average grade  | .052% | U <sub>3</sub> O <sub>8</sub> | & | 1.00% | Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 35'   |                               |   |       |                                |
|        | assumed depth  | 200'  |                               |   |       |                                |
|        | assumed length | 50'   |                               |   |       |                                |
|        | Tons 35,000 @  | .052  |                               | & | 1.00  |                                |

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SECTION 5990E

D.D.H.'s U56, U57.

|        |                |                |   |                 |
|--------|----------------|----------------|---|-----------------|
| Area A | average grade  | .052% $U_3O_8$ | & | 1.00% $Cb_2O_5$ |
|        | true width     | 35'            |   |                 |
|        | assumed depth  | 200'           |   |                 |
|        | assumed length | 50'            |   |                 |
|        | Tons 35,000 @  | .052           | & | 1.00            |



SECTION 5940ED.D.H.'s 17, 31.

|        |                |                                     |   |                                     |
|--------|----------------|-------------------------------------|---|-------------------------------------|
| Area A | average grade  | .015% U <sub>3</sub> O <sub>8</sub> | & | .75% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 26'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 100'                                |   |                                     |
|        | Tons 52,000 @  | .015                                | & | .75                                 |
| Area B | average grade  | .044% U <sub>3</sub> O <sub>8</sub> | & | .61% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 26'                                 |   |                                     |
|        | assumed depth  | 245'                                |   |                                     |
|        | assumed length | 125'                                |   |                                     |
|        | Tons 79,600 @  | .044                                | & | .61                                 |
| Area C | average grade  | .04% U <sub>3</sub> O <sub>8</sub>  | & | .70% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 5'                                  |   |                                     |
|        | assumed depth  | 230'                                |   |                                     |
|        | assumed length | 125'                                |   |                                     |
|        | Tons 17,250 @  | .04                                 | & | .70                                 |
| Area D | average grade  | .007% U <sub>3</sub> O <sub>8</sub> | & | .56% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 11'                                 |   |                                     |
|        | assumed depth  | 180'                                |   |                                     |
|        | assumed length | 125'                                |   |                                     |
|        | Tons 22,800 @  | .007                                | & | .56                                 |

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SECTION 59,0E

D.D.H.'s 17, 31.

|        |                |                                     |   |                                     |
|--------|----------------|-------------------------------------|---|-------------------------------------|
| Area A | average grade  | .015% U <sub>3</sub> O <sub>8</sub> | & | .75% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 26'                                 |   |                                     |
|        | assumed depth  | 200'                                |   |                                     |
|        | assumed length | 100'                                |   |                                     |
|        | Tons 52,000 @  | .015                                | & | .75                                 |
| Area B | average grade  | .044% U <sub>3</sub> O <sub>8</sub> | & | .61% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 26'                                 |   |                                     |
|        | assumed depth  | 245'                                |   |                                     |
|        | assumed length | 125'                                |   |                                     |
|        | Tons 79,600 @  | .044                                | & | .61                                 |
| Area C | average grade  | .04% U <sub>3</sub> O <sub>8</sub>  | & | .70% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 6'                                  |   |                                     |
|        | assumed depth  | 230'                                |   |                                     |
|        | assumed length | 125'                                |   |                                     |
|        | Tons 17,250 @  | .04                                 | & | .70                                 |
| Area D | average grade  | .007% U <sub>3</sub> O <sub>8</sub> | & | .56% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 11'                                 |   |                                     |
|        | assumed depth  | 180'                                |   |                                     |
|        | assumed length | 125'                                |   |                                     |
|        | Tons 22,800 @  | .007                                | & | .56                                 |

SECTION 6140E

D.D.H.'s 19, 38.

|        |                |                                    |   |                                     |
|--------|----------------|------------------------------------|---|-------------------------------------|
| Area A | average grade  | .01% U <sub>3</sub> O <sub>8</sub> | & | .93% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 19'                                |   |                                     |
|        | assumed depth  | 200'                               |   |                                     |
|        | assumed length | 150'                               |   |                                     |
|        | Tons 57,000 @  | .01                                | & | .93                                 |
| Area B | average grade  | .02% U <sub>3</sub> O <sub>8</sub> | & | .86% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 12'                                |   |                                     |
|        | assumed depth  | 200'                               |   |                                     |
|        | assumed length | 150'                               |   |                                     |
|        | Tons 36,000 @  | .02                                | & | .86                                 |

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SECTION 6140ED.D.H.'s 19,38.

|        |                |                                    |   |                                     |
|--------|----------------|------------------------------------|---|-------------------------------------|
| Area A | average grade  | .01% U <sub>3</sub> O <sub>8</sub> | & | .93% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 19'                                |   |                                     |
|        | assumed depth  | 200'                               |   |                                     |
|        | assumed length | 150'                               |   |                                     |
|        | Tons 57,000 @  | .01                                | & | .93                                 |
| Area B | average grade  | .02% U <sub>3</sub> O <sub>8</sub> | & | .86% Cb <sub>2</sub> O <sub>5</sub> |
|        | true width     | 12'                                |   |                                     |
|        | assumed depth  | 200'                               |   |                                     |
|        | assumed length | 150'                               |   |                                     |
|        | Tons 36,000 @  | .02                                | & | .86                                 |

## APPENDIX I

| Columbium Oxide % |        | Analysis Checks |      |          |     | TS.L Mines Branch<br>Col. X-Ray Fl. |
|-------------------|--------|-----------------|------|----------|-----|-------------------------------------|
| Sample No.        | McGill | X-Ray           | USGS | Battelle |     |                                     |
| 78                |        | .38             |      | .47      |     |                                     |
| 561               | Ins.   | .15             |      | .16      |     |                                     |
| 710               | "      | .96             |      | 1.15     |     |                                     |
| 3017              | "      | .23             |      | .27      |     |                                     |
| 3024              | "      | .39             |      | .50      |     |                                     |
| 3038              | "      | .39             |      | .51      |     |                                     |
| 3043              | "      | .80             |      | .96      | .76 |                                     |
| 3005              | "      | .60             |      | .89      |     |                                     |
| 3024              | "      | .39             |      | .73      | .53 |                                     |
| 3196              | "      | .48             |      | .74      | .63 |                                     |
| 5313              | "      | 1.60            |      | 1.80     |     |                                     |
| 3533              | "      | 1.56            |      | 1.40     |     |                                     |
| 3704              | "      | .52             |      | .66      |     |                                     |
| 4293              | "      | 2.20            |      | 2.20     |     |                                     |
| 3792              | "      | .48             |      | .54      | .52 |                                     |
| 3814              | "      | .50             |      | .76      | .49 |                                     |
| 3814              | "      | .78             |      | 1.00     | .86 |                                     |
| 3767              | "      | .62             |      |          | .79 |                                     |
| 3921              | "      | 1.03            |      | 1.30     | .93 |                                     |
| 3969              | "      | .24             |      | .36      |     |                                     |
| 3984              | "      | .81             |      | .83      |     |                                     |
| 4017              | "      | .68             |      | .63      |     |                                     |
| 4097              | "      | .51             |      | .70      |     |                                     |
| 4109              | "      | 5.21            |      | 5.00     |     |                                     |
| 500               | "      | .64             | .72  |          |     |                                     |
| 659               |        | .36             | .43  |          |     |                                     |
| 660               |        | .29             | .52  |          |     |                                     |
| 661               |        | .48             | .52  |          |     |                                     |
| 693               |        | 1.00            | 1.14 |          |     |                                     |
| 695               |        | .90             | 1.09 |          |     |                                     |
| 696               |        | .65             | .74  |          |     |                                     |
| 697               |        | .82             | .95  |          |     |                                     |
| 698               |        | .50             | .62  |          |     |                                     |
| 699               |        | .14             | .14  |          |     |                                     |
| 70                |        | .40             | .48  |          |     |                                     |
| 691               |        | .44             | .48  |          |     |                                     |
| 692               |        | .95             | 1.08 |          |     |                                     |
| 693               |        | 1.00            | 1.11 |          |     |                                     |
| 694               |        | 1.08            | 1.35 |          |     |                                     |
| 1374              |        | 2.01            | 2.20 |          |     |                                     |
| 3911              | Ins.   | 1.24            | 1.57 |          |     |                                     |
| 2645              | "      | .63             | .85  |          |     |                                     |
| 734               | "      | .84             | .86  |          |     |                                     |
| 1385              | "      | .76             | .92  |          |     |                                     |
| 3812              | "      | .25             | .30  |          |     |                                     |
| 3813              | "      | .50             | .60  |          |     |                                     |
| 3816              | "      | .26             | .34  |          |     |                                     |

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## APPENDIX I

| Sample No. | Columbian Oxide % | Analysis Checks |       |      |   |
|------------|-------------------|-----------------|-------|------|---|
|            |                   | McGill          | X-Ray | USGS | Battelle TS.L. Mines Branch<br>Col. X-Ray Fl. |
| 78         | .38               |                 |       | .47  |   |
| 561 Ins.   | .15               |                 |       | .16  |   |
| 710 "      | .96               |                 |       | 1.15 |   |
| 3017 "     | .23               |                 |       | .27  |   |
| 3024 "     | .39               |                 |       | .50  |   |
| 3038 "     | .39               |                 |       | .51  |   |
| 3043 "     | .80               |                 |       | .96  | .76   |
| 3005 "     | .60               |                 |       | .89  |   |
| 3024 "     | .39               |                 |       | .73  | .53   |
| 3196 "     | .46               |                 |       | .74  | .63   |
| 5313 "     | 1.60              |                 |       | 1.80 |   |
| 3533 "     | 1.56              |                 |       | 1.40 |   |
| 3704 "     | .52               |                 |       | .66  |   |
| 4293 "     | 2.20              |                 |       | 2.20 |   |
| 3792 "     | .48               |                 |       | .54  | .52   |
| 3814 "     | .50               |                 |       | .76  | .49   |
| 3814 "     | .78               |                 |       | 1.00 | .86   |
| 3767 "     | .62               |                 |       |      | .79   |
| 3921 "     | 1.03              |                 |       | 1.30 | .93   |
| 3969 "     | .24               |                 |       | .36  |   |
| 3984 "     | .81               |                 |       | .83  |   |
| 4017 "     | .68               |                 |       | .63  |   |
| 4094 "     | .51               |                 |       | .70  |   |
| 4109 "     | 5.21              |                 |       | 5.00 |   |
| 500 "      | .64               |                 | .72   |      |   |
| 659 "      | .36               |                 | .43   |      |   |
| 660 "      | .29               |                 | .52   |      |   |
| 661 "      | .48               |                 | .52   |      |   |
| 693 "      | 1.00              |                 | 1.14  |      |   |
| 695 "      | .90               |                 | 1.09  |      |   |
| 696 "      | .65               |                 | .74   |      |   |
| 697 "      | .82               |                 | .95   |      |   |
| 698 "      | .50               |                 | .62   |      |   |
| 699 "      | .14               |                 | .14   |      |   |
| 701 "      | .40               |                 | .48   |      |   |
| 691 "      | .44               |                 | .48   |      |   |
| 692 "      | .95               |                 | 1.08  |      |   |
| 693 "      | 1.00              |                 | 1.11  |      |   |
| 694 "      | 1.08              |                 | 1.35  |      |   |
| 1374 "     | 2.01              |                 | 2.20  |      |   |
| 3921 Ins.  | 1.24              |                 | 1.57  |      |   |
| 2645 "     | .63               |                 | .85   |      |   |
| 734 "      | .84               |                 | .86   |      |   |
| 1385 "     | .76               |                 | .92   |      |   |
| 3812 "     | .25               |                 | .30   |      |   |
| 3813 "     | .50               |                 | .60   |      |   |
| 3816 "     | .26               |                 | .34   |      |   |

| Sample No. | McGill | X-Ray | USGS | Battelle | T.S.L. | Mines Branch<br>Col. X-Ray Fl. |
|------------|--------|-------|------|----------|--------|--------------------------------|
| 16M        | .60    | .83   |      |          | .62    | .72 .75                        |
| 2331       | .72    | .94   |      |          | .85    | .74 .80                        |
| 77M        | .72    | .93   |      |          | .88    |                                |
| 2344       | 1.43   | 1.86  |      |          | 1.60   |                                |
| 915        |        | .58   |      |          | .66    | .62 .63                        |
| 928        |        | 1.18  |      |          | 1.35   | 1.42 1.32                      |
| 984        |        | 1.17  |      |          | 1.20   | 1.29 1.32                      |
| 1392       |        | 2.25  |      |          | 2.30   | 2.35 2.55                      |
| 1458       |        | .67   |      |          | .72    | .78 .81                        |
| 2567       |        | .80   |      |          | .75    | .73 .73                        |
| 2687       |        | .74   |      |          | .65    | .70 .78                        |
| 96M        |        | .62   |      |          | .55    | .53 .52                        |

McGill = McGill University X-ray Laboratory.

X-Ray = X-Ray Laboratories, Ltd., Toronto.

USGS = United States Geological Survey.

Battelle = Battelle Memorial Institute, Columbus, Ohio.

T.S.L. = Technical Service Laboratories, Toronto.

Col. = Colorimetric method.

X-Ray Fl. = X-Ray Fluorescence.

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APPENDIX I

Page 2

| Sample No. | McGill | X-Ray | USGS | Battelle | T.S.L. | Mines Branch<br>Col. X-Ray Fl. |
|------------|--------|-------|------|----------|--------|--------------------------------|
| 16M        | .60    | .83   |      |          | .62    | .72 .75                        |
| 2331       | .72    | .94   |      |          | .85    | .74 .80                        |
| 77N        | .72    | .93   |      |          | .88    |                                |
| 2344       | 1.43   | 1.86  |      |          | 1.60   |                                |
| 915        |        | .58   |      |          | .66    | .62 .63                        |
| 923        |        | 1.18  |      |          | 1.35   | 1.42 1.32                      |
| 984        |        | 1.17  |      |          | 1.20   | 1.29 1.32                      |
| 1392       |        | 2.25  |      |          | 2.30   | 2.35 2.55                      |
| 1458       |        | .67   |      |          | .72    | .78 .81                        |
| 2567       |        | .80   |      |          | .75    | .73 .73                        |
| 2587       |        | .74   |      |          | .65    | .70 .78                        |
| 96M        |        | .62   |      |          | .55    | .53 .52                        |

McGill = McGill University X-ray Laboratory.

X-Ray = X-Ray Laboratories, Ltd., Toronto.

USGS = United States Geological Survey.

Battelle = Battelle Memorial Institute, Columbus, Ohio.

T. S. L. = Technical Service Laboratories, Toronto.

Col. = Colorimetric method.

X-Ray Fl. = X-Ray Fluorescence.



URANIUM ANALYSIS CHECKS

Page 3

Uranium Oxide %

| <u>Sample No.</u> | <u>Insp</u> | Mines Branch, Ottawa |              |                 |                | <u>T.S.L.</u> | <u>Prob.<br/>ThO<sub>2</sub></u> |
|-------------------|-------------|----------------------|--------------|-----------------|----------------|---------------|----------------------------------|
|                   |             | <u>Chem.</u>         | <u>Calc.</u> | <u>Eq gamma</u> | <u>Eq beta</u> |               |                                  |
| 2969              | .081        | .077                 | .074         | .076            | .075           | .051          |                                  |
| 3742              | .028        | .023                 | .028         | .030            | .029           | Tr            |                                  |
| 3766              | .069        | .059                 | .064         | .067            | .066           | .031          |                                  |
| 3815              | .136        | .12                  | .12          | .141            | .135           |               |                                  |
| 3909              | .186        | .18                  | .17          | .164            | .168           |               |                                  |
| 4072              | .10         | .094                 | .10          | .094            | .097           |               |                                  |
| 4163              | .033        | .029                 | .034         | .029            | .031           |               |                                  |
| 3151              | .102        |                      |              |                 |                | .098          |                                  |
| 3194              | .08         |                      |              |                 |                | .072          |                                  |
| 3533              | .01         |                      |              |                 |                | nil           |                                  |
| 3610              | .005        |                      |              |                 |                | nil           |                                  |
| 3737              | .015        |                      |              |                 |                | Tr            |                                  |
| 781               |             | .044                 |              |                 |                |               |                                  |
| 782               |             | .026                 |              |                 |                |               |                                  |
| 783               |             | .062                 |              |                 |                |               |                                  |
| 784               |             | .029                 |              |                 |                |               |                                  |
| Bulk Sample       |             | .15                  | .15          |                 |                |               |                                  |
| 53                | .10         |                      | .06          | .06             | .06            |               |                                  |
| 62                | .10         |                      | .086         | .090            | .088           |               |                                  |
| 996               | .05         |                      | .060         | .063            | .062           |               |                                  |
| 1106              | nil         |                      | .032         | .034            | .033           |               |                                  |
| 1751              | .042        |                      | .037         | .044            | .041           |               |                                  |
| 1921              | .046        |                      | .050         | .042            | .046           |               |                                  |
| 926               | .062        |                      | .070         | .075            | .072           |               |                                  |
| 2873              | .138        |                      | .11          | .124            | .117           |               |                                  |
| 2874              | .049        |                      | .047         | .045            | .046           |               |                                  |
| 2888              | .08         |                      | .072         | .081            | .077           |               |                                  |
| 2889              | .136        |                      | .11          | .129            | .121           |               |                                  |
| 1967              | .08         |                      | .077         | .086            | .082           |               |                                  |
| 2230              | .16         |                      |              |                 |                | .19           |                                  |
| 815               | .015        | .012                 | .016         | .016            | .016           | .019          |                                  |
| 865               | .083        | .083                 | .083         | .074            | .078           | .082          |                                  |
| 882               | .046        | .041                 | .045         | .045            | .045           | .043          |                                  |
| 889               | .065        | .058                 | .059         | .073            | .067           | .059          | .036                             |
| 915               | .072        | .072                 | .068         | .079            | .074           | .061          | .02                              |
| 928               | .07         | .070                 | .073         | .073            | .073           | .064          |                                  |
| 9884              | .111        | .12                  | .12          | .12             | .12            | .12           |                                  |
| 1392              | .106        | .11                  | .10          | .108            | .105           | .080          |                                  |
| 1458              | .059        | .054                 | .054         | .063            | .059           | .042          |                                  |
| 2567              | .041        | .035                 | .037         | .039            | .038           | .043          |                                  |
| 2587              | .068        | .063                 | .065         | .067            | .066           | .066          |                                  |
| 96M               | .062        | .055                 | .059         | .061            | .060           | .065          |                                  |
| 3163              | .075        | .070                 | .069         | .074            | .072           | .074          |                                  |
| 3164              | .08         |                      |              |                 |                | .085          |                                  |
| 3165              | .043        | .037                 | .043         | .045            | .044           | .037          |                                  |
| 3166              | .047        |                      |              |                 |                | .052          |                                  |

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URANIUM ANALYSIS CHECKS

Page 3

Uranium Oxide %

| <u>Sample No.</u> | <u>Insp</u> | <u>Mines Branch, Ottawa</u> |              |                 |                | <u>T. S. L.</u> | <u>Prob.<br/>ThO<sub>2</sub></u> |
|-------------------|-------------|-----------------------------|--------------|-----------------|----------------|-----------------|----------------------------------|
|                   |             | <u>Chem.</u>                | <u>Calc.</u> | <u>Eq gamma</u> | <u>Eq beta</u> |                 |                                  |
| 2969              | .081        | .077                        | .074         | .076            | .075           | .051            |                                  |
| 3742              | .028        | .023                        | .028         | .030            | .029           | Tr              |                                  |
| 3766              | .069        | .059                        | .064         | .067            | .066           | .031            |                                  |
| 3815              | .136        | .12                         | .12          | .141            | .135           |                 |                                  |
| 3909              | .186        | .18                         | .17          | .164            | .168           |                 |                                  |
| 4072              | .10         | .094                        | .10          | .094            | .097           |                 |                                  |
| 4163              | .033        | .029                        | .034         | .029            | .031           |                 |                                  |
| 3157              | .102        |                             |              |                 |                | .098            |                                  |
| 3194              | .08         |                             |              |                 |                | .072            |                                  |
| 3533              | .01         |                             |              |                 |                | nil             |                                  |
| 3610              | .005        |                             |              |                 |                | nil             |                                  |
| 3737              | .015        |                             |              |                 |                | Tr              |                                  |
| 781               |             | .044                        |              |                 |                |                 |                                  |
| 782               |             | .026                        |              |                 |                |                 |                                  |
| 783               |             | .062                        |              |                 |                |                 |                                  |
| 784               |             | .029                        |              |                 |                |                 |                                  |
| Bulk Sample       |             | .15                         | .15          |                 |                |                 |                                  |
| 53                | .10         |                             | .06          | .06             | .06            |                 |                                  |
| 62                | .10         |                             | .086         | .090            | .088           |                 |                                  |
| 996               | .05         |                             | .060         | .063            | .062           |                 |                                  |
| 1106              | nil         |                             | .032         | .034            | .033           |                 |                                  |
| 1751              | .042        |                             | .037         | .044            | .041           |                 |                                  |
| 1921              | .046        |                             | .050         | .042            | .046           |                 |                                  |
| 926               | .062        |                             | .070         | .075            | .072           |                 |                                  |
| 2873              | .138        |                             | .11          | .124            | .117           |                 |                                  |
| 2874              | .049        |                             | .047         | .045            | .046           |                 |                                  |
| 2888              | .08         |                             | .072         | .081            | .077           |                 |                                  |
| 2889              | .136        |                             | .11          | .129            | .121           |                 |                                  |
| 1967              | .08         |                             | .077         | .086            | .082           |                 |                                  |
| 2230              | .16         |                             |              |                 |                | .19             |                                  |
| 815               | .015        | .012                        | .016         | .016            | .016           | .019            |                                  |
| 865               | .083        | .083                        | .083         | .074            | .078           | .082            |                                  |
| 882               | .046        | .041                        | .045         | .045            | .045           | .043            |                                  |
| 889               | .065        | .058                        | .059         | .073            | .067           | .059            | .036                             |
| 915               | .072        | .072                        | .068         | .079            | .074           | .061            | .03                              |
| 928               | .07         | .070                        | .073         | .073            | .073           | .064            |                                  |
| 9834              | .111        | .12                         | .12          | .12             | .12            | .12             |                                  |
| 1392              | .106        | .11                         | .10          | .108            | .105           | .080            |                                  |
| 1452              | .059        | .054                        | .054         | .063            | .059           | .042            |                                  |
| 2567              | .041        | .035                        | .037         | .039            | .038           | .043            |                                  |
| 2587              | .068        | .063                        | .065         | .067            | .066           | .066            |                                  |
| 96M               | .062        | .055                        | .059         | .061            | .060           | .065            |                                  |
| 3163              | .075        | .070                        | .069         | .074            | .072           | .074            |                                  |
| 3164              | .08         |                             |              |                 |                | .085            |                                  |
| 3165              | .043        | .037                        | .043         | .045            | .044           | .037            |                                  |
| 3166              | .047        |                             |              |                 |                | .052            |                                  |

Composition Pyrochlore

Information based on semi-quantitative spectrographic analyses and calculations by E.H. Nickel, Department of Mines and Technical Surveys, Mines Branch, Ottawa, Ontario.

|                                |     |
|--------------------------------|-----|
| Na <sub>2</sub> O              | 58  |
| CaO                            | 13  |
| FeO                            | 5   |
| MgO                            | 7   |
| La <sub>2</sub> O <sub>3</sub> | 0.3 |
| U <sub>3</sub> O <sub>8</sub>  | 7   |
| ThO <sub>2</sub>               | 0.8 |
| TiO <sub>2</sub>               | 4   |
| Nb <sub>2</sub> O <sub>5</sub> | 56  |

The specific gravity is reported by S. Kaiman as being 5.2.

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Composition Synchlore

Information based on semi-quantitative spectrographic analyses and calculations by E. H. Nickel, Department of Mines and Technical Surveys, Mines Branch, Ottawa, Ontario.

|                                |     |
|--------------------------------|-----|
| Na <sub>2</sub> O              | 5%  |
| CeO                            | 13  |
| FeO                            | 5   |
| MgO                            | 7   |
| La <sub>2</sub> O <sub>3</sub> | 0.3 |
| U <sub>3</sub> O <sub>8</sub>  | 7   |
| ThO <sub>2</sub>               | 0.2 |
| TiO <sub>2</sub>               | 4   |
| Nb <sub>2</sub> O <sub>5</sub> | 56  |

The specific gravity is reported by S. Kaiman as being 5.2.

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