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MINING LANDS SECTION CONTROLLED SOURCE AUDIOFREQUENCY MAGNETOTELLURIC SURVEY ON GRID C14 CLIFFORD TOWNSHIP, ONTARIO LARDER LAKE MINING DIVISION DISTRICT OF TIMISKAMING

2.12955

NTS 32D/5 Latitude 48° 17'N Longitude 79° 80'W

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2,10571 John Kovala December 1989

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1.0 INTRODUCTION

A controlled source Audiofrequency magnetotelluric survey was carried out by Quantech Consulting Inc. for LAC Minerals Ltd. on a continuous block of 44 claims located 20Km north east of Kirkland Lake along the south central boundary of Clifford Township. The survey was conducted between November 1st and November 30th, 1987. The survey was completed in order to evaluate the effectiveness of this survey in outlining the low resistivity zone associated with a previously discovered ultramafic breccia.

Sections 1 through 4 of this report were written by J. Kovala. Sections 5 through 7, CSAMT Technique, Data Presentation and Interpretation Techniques were extracted fro a report written by G. Bogden of Quantech in October 1987 for LAC Minerals. P. Haloff, a consultant for LAC Minerals has interpreted the results of this survey, Section 8.

2.0 PROPERTY

The property consists of a continuous block of 44 unpatented mining claims located in Clifford Township, Larder Lake Mining Division, District of Timiskaming. The claims are given below:

L	803325	\mathbf{to}	803331
	803333	to	803342
	983106	to	983108
	918236	to	918238
1	1014621	\mathbf{to}	1014627
1	L014635	to	1014640
1	L014648	to	1014655

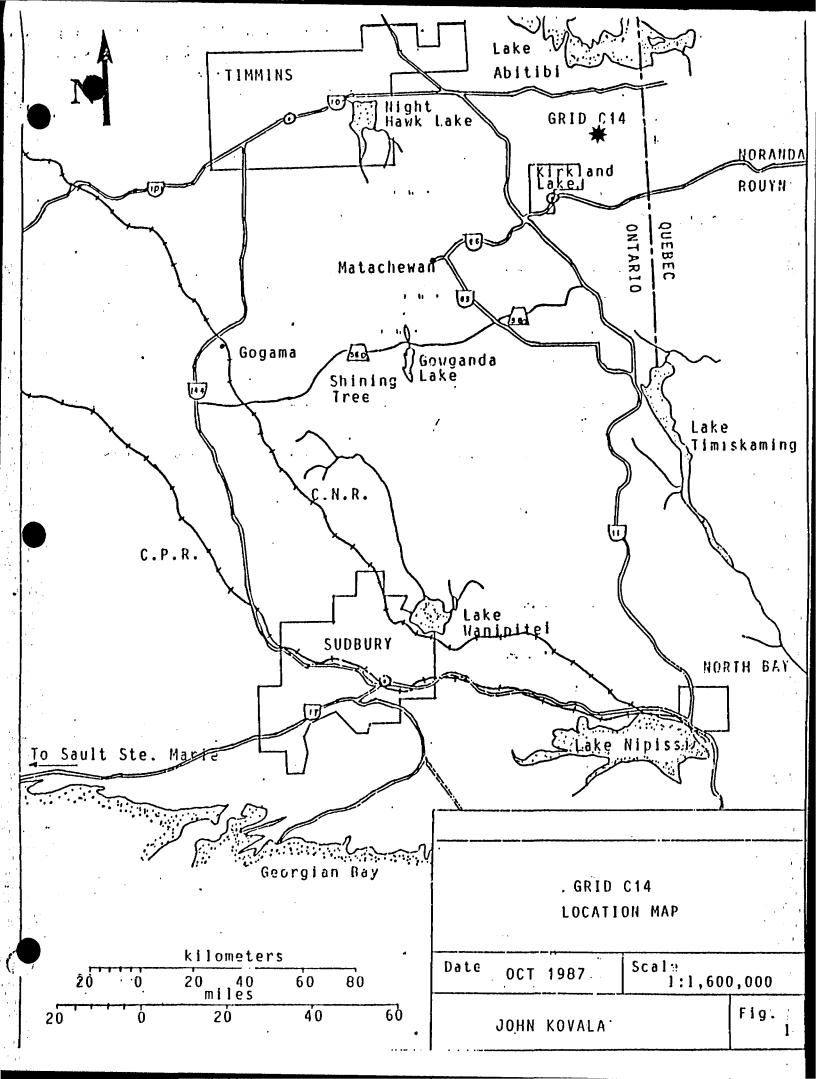
3.0 LOCATION AND ACCESS

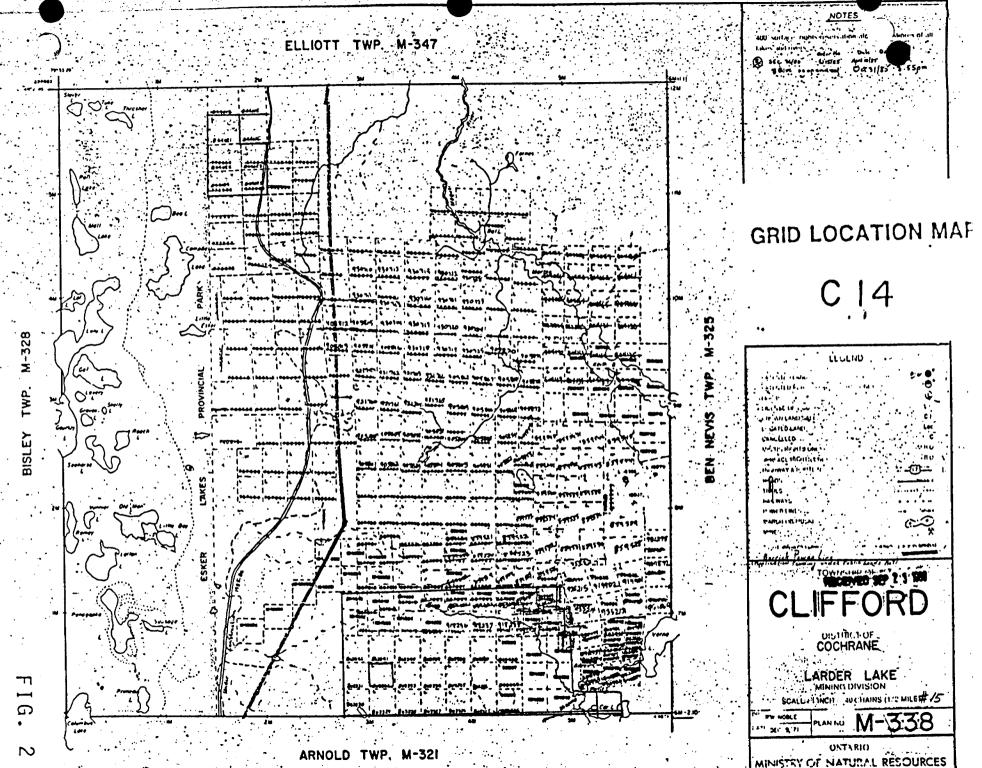
The C14 property is located 20 kilometers northeast of Kirkland Lake in the south central portion of Clifford Township at longitude 79° 80' W and latitude 48° 17'N (NTS 32D/5)

Bush roads originating at the Esker Park and Harker-Holloway roads lead to the south and north boundaries respectively.

4.0 GENERAL GEOLOGY

Regionally the property is located in the west central portion of the Blake River synclinorium. The Blake River group consists of dominantly calc-alkaline series intermediate to felsic volcanic rock occurring in the central portion of Clifford Township. Bodies and sills of mafic intermediate and felsic intrusive rocks cut the volcanics. All of the above are cut by dominantly NW striking diabase.





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In the central portion of the synclinorium in Clifford Township occurs a domal anticline intruded by a granodiorite stock 1 1/4 miles wide. The survey area is located 2 miles south of the above domal anticline over a complimentary WNW syncline. The syncline is centered by felsic volcanics and flanked to the NNE and SSW by intermediate volcanics. A large quartz gabbro intrusive is located along the southeastern boundary of the property.

5.0 CSAMT TECHNIQUE

5.1 Advantages and Disadvantages Over Natural Signal Systems

Natural source electromagnetic (EM) sounding methods such as magnetotellurics (MT) and audiomagnetotellurics (AMT) have been widely used for the exploration of hydrocarbons, groundwater and geothermal sources, but with little application to mineral The MT method measures fluctuations in the earth's exploration. natural electric and magnetic fields over a broad range of frequencies between 10 Hz and 10,000 Hz; the AMT band is slightly higher between 10 Hz and 10,000 Hz. The Bource of these fluctuations originate in the ionosphere for frequencies less than 1 Hz and from thunderstorms for the higher frequencies. The field strength and polarization of the signals vary with the time of day and the season.

The CSAMT technique was introduced to overcome problems and limitations encountered by these natural source methods (Goldstein and Strangeway, 1975). Rather than a natural signal source, CSAMT uses a fixed grounded bipole or current loop on the surface of the earth to produce an EM signal. Some of the advantages of the CSAMT technique over the natural source methods which make CSAMT a viable mineral exploration tool are:

- 1. The polarization of the fields can be selected by the orientation of the transmitting antenna.
- 2. The signal strength does not depend on the time of day or the season.
- 3. Because the signals are stronger, the receiving equipment does not need to be as sensitive as that of MT or AMT.
- 4. Because of the coherent signal, the usual signal processing and enhancement techniques are far more effective.
- 5. CSAMT surveys are much faster and therefore more cost effective than natural source EM surveys.

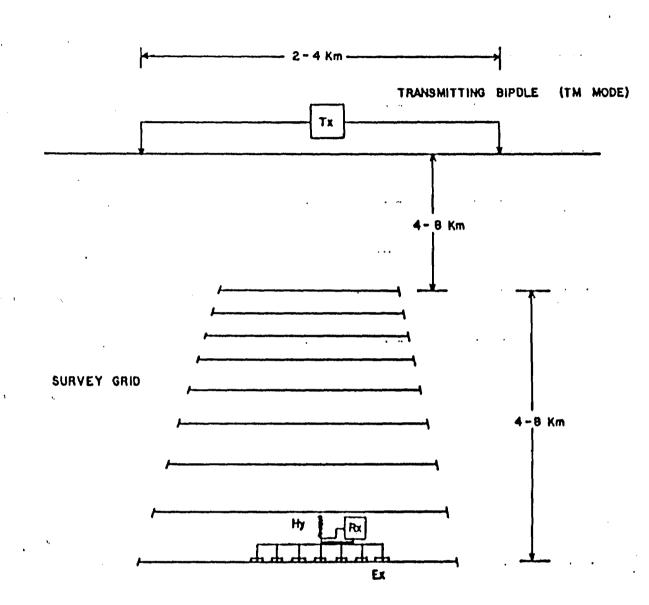
The primary disadvantage of the CSAMT method over natural source EM methods is the closeness of the signal source. For natural source techniques, the signal source is, in effect, infinite such that the EM field is a "plane wave". This assumption greatly simplifies processing and interpretation for MT and AMT data. For CSAMT data, if the transmitting antenna is too close to the survey area, the resistivity of the deep layers cannot be determined accurately since they are no longer energized by this plane wave. Readings measured at the plane wave distance are considered to be in the "far-field", while readings measured at the non-plane wave distance are considered in the "near-field". In order that resistivities of the deep layers be calculated correctly, the measurements must be corrected for this near-field, non-plane wave effect.

5.2 <u>Theory and Instrumentation</u>

The survey was executed using the V4 multichannel universal receiver console, the T30 transmitter and the MG30 (30 kilowatt) motor generator, all manufactured by Phoenix Geophysics Limited, Markham, Ontario. A complete description of the equipment along with technical specifications are contained in Appendix B.

The transmitter operates at sixteen (16), selectable, binary step base frequencies which range from 0.25 Hz to 8192 Hz. An optional alternate frequency set at 2/3 the base frequency set, ranges from 0.17 Hz to 5461 Hz to provide a total of 32 The length of the bipole (or loop transmitting frequencies. edge) may be varied from several hundred meters to several kilometers, depending upon signal strength, the minimum transmitter-receiver distance and the size of the area to be Normally a grounded bipole is preferred to a current surveyed. loop because the bipole requires less wire to produce a comparable signal. The bipole is constructed with lengths of #10 gauge copper wire, which has a resistance of approximately 1 ohm per 1000 feet.

Orthogonal components of the electric field (E) and the magnetic field (H) are measured over the survey area. The E-field components are measured with a dipole using non-polarizable (steel rod) electrodes in the same manner as induced polarization (IP) measurements. The dipole length is a function of the scale of the survey but may also be influenced by the E-field signal strength, which in turn is a function of the transmitter-receiver distance, the transmitter bipole current, the earth resistivity and noise conditions. The H-field components are measured using a magnetic sensor coil placed on the ground. The V4 has the advantage of multiple channels which permits the measurement of six (6) or seven (7) dipoles and one (1) H-field component simultaneously.



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 TYPICAL RECEIVER ARRAY WITH SEVEN E-FIELD COMPONENTS, Rx AND ONE H-FIELD COMPONENT, Hy

FIGURE 5.1 . TYPICAL CSAMT SURVEY CONFIGURATION

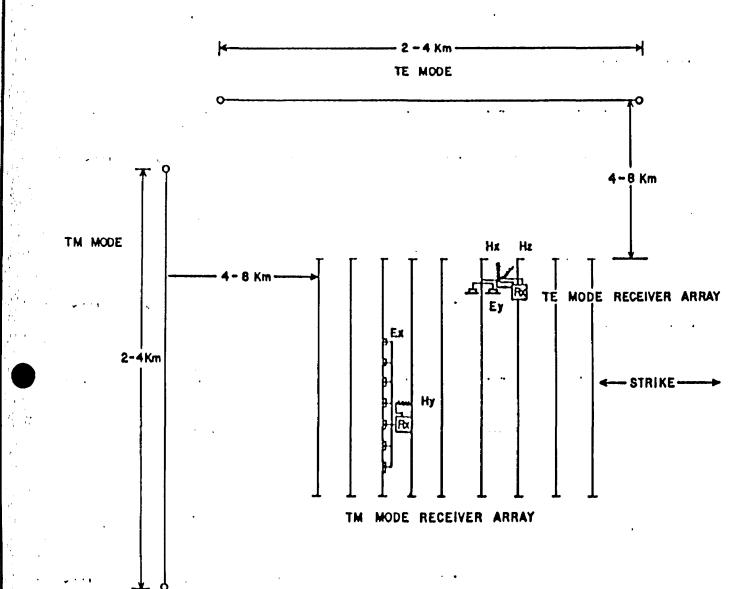


FIGURE 5.2 : TM MODE AND TE MODE ARRAYS

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The survey may be conducted in two survey modes: the transverse magnetic (TM) mode where the transmitting bipole is perpendicular to geologic strike and the transverse electric (TE) mode where the transmitting bipole is parallel to geologic strike. The TM mode is most sensitive to lateral changes in resistivity and is therefore more suitable as a reconnaissance mapping tool whereas the TE mode is preferred as a detailing method because it provides greater resolution of horizontal resistive boundaries. A TM mode survey is also much faster from a logistics standpoint, than a TE mode survey.

Up to three H-field components, Hx, Hy and Hz and two Efield components, Ex and Ey can be measured at each station along with the E-field phase and H-field phase for both modes. The apparent resistivity is calculated from the ratio of orthogonal components of the electric and magnetic fields (eg. Ex/Hy or Ey/Hx) using the following Cagniard equation:

 $p_{a} = \frac{1}{2\pi + 4\sigma} \frac{E}{H} = \frac{1}{2} \frac{E}{2} \frac{1}{2} \frac{E}{2} \frac{1}{2} \frac{1}$

Where μ_c = $4\pi \times 10^{-7}$ H/m ρ_c = apparent resistivity in ohm-meters E = E-field magnitude in mv/km H = H-field magnitude in gammas \emptyset = phase difference in radians

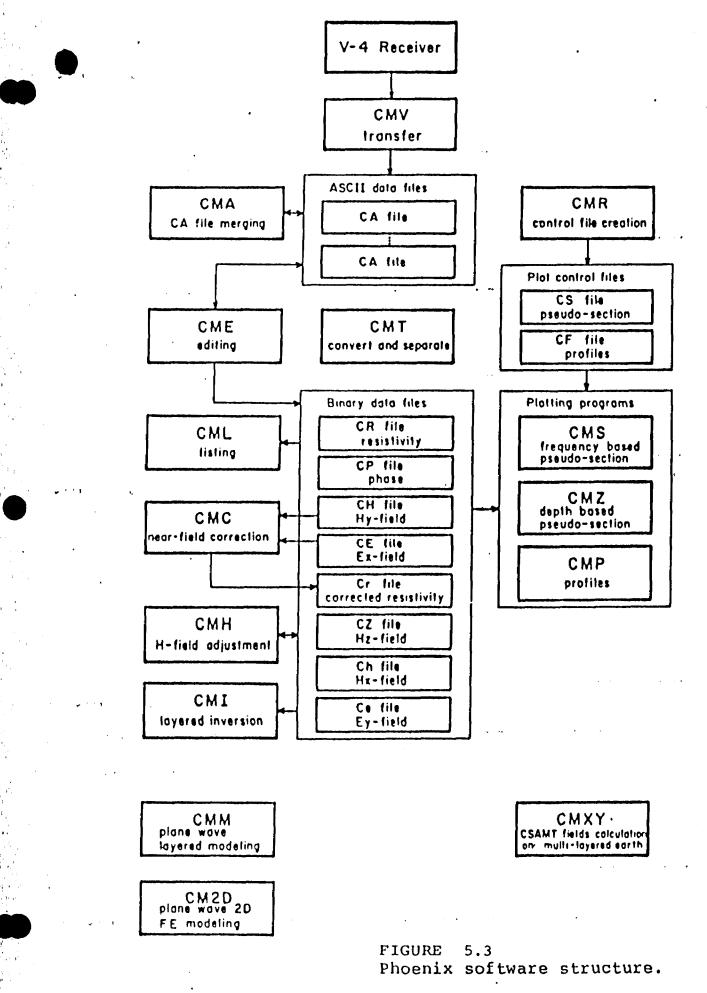
Should only the Ex and Hy components of the electric and magnetic fields respectively be required for the TM mode then only one H-field measurement is necessary for each receiver array since Hy is essentially constant over a significant distance, even for very strong conductors (Yamashita, 1987). Figure 5.1 illustrates a typical configuration for a reconnaissance TM mode and TE mode.

The measured components of the electric and magnetic fields and the calculated apparent resistivity are stored in solid-state memory in the V4 receiver and later transferred to a microcomputer for processing at the end of the field day.

5.3 Computer Software

Data dumping, editing, reduction and presentation was controlled by the CSAMT processing and interpretation programs provided by Phoenix. The software is written in HPBASIC and executes only on a Hewlett Packard HP9845 or HP9000 series machine. Figure 5.3 illustrates the software package structure.

Contours of apparent resistivity values for selected frequencies for the survey grids were prepared using the MAPPLOT system developed by Geosoft Inc., Toronto. The software was controlled by DOS 3.1 written by Compaq Computer Corporation.



5.4 <u>Computer Hardware</u>

In-field processing used the Hewlett Packard HP9845 desk-top computer. The system is equipped with an 8 bit CPU, two cassette tape drives, RS-232C serial port and integral thermal printer.

6.0 DATA PRESENTATION

6.1 Frequency Pseudosections

The contoured apparent resistivity for near-field corrected data for each line surveyed is presented in a frequency pseudosection format (see Appendix A). Contour intervals are logarithmically distributed to compensate for the large dynamic range of the data. Zones of low resistivity (high conductivity) have been shaded at 5,000 ohm-meter intervals.

Other parameters, such as the phase difference, or E-field and H-field magnitude were also presented in the same format, to provide further information when required.

6.2 Frequency Profiles

Profiles of each sounding point were used when necessary by the author to provide more diagnostic information about an individual sounding point.

7.0 INTERPRETATION TECHNIQUES

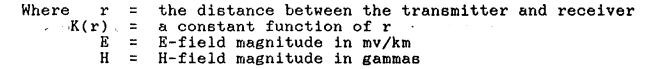
7.1 First Order Correction

In order to use the interpretation methods and modelling techniques common to natural source surveys, CSAMT data must be corrected for the near-field effect.

The Cagniard equation given in Equation (1) is only valid when the transmitted electromagnetic field is far enough from the transmitting bipole such that it is a plane-wave or the far-field This distance is a function of the ground resistivity and case. the transmitter current in the bipole. If the actual distance between the transmitter and the receiver is much less than this far-field distance, the transmitted field is not plane-wave in character, and is considered in the near-field. In the nearthe Cagniard equation overestimates field, the actual Consequently "true" apparent resistivity values resistivity. must be estimated using another technique:

$$p_{Q} = K(r) * r(---)$$
 (2)
H

(Yamashita, 1984)



The area of gradual change between the near-field and the far-field distance is known as the "transition-field". Calculations of apparent resistivities in this case use a "transition-triangle method" (Yamashita, 1984). The combination of the calculations for the near-field, and the transition field is considered the first-order correction.

Considering the high resistivity contrast of rock units in the Abitibi though, apparent resistivities need only be compared *relatively*. Consequently data interpretated using the first order correction (or no correction at all in fact) is considered acceptable for resistivity mapping in this environment.

7.2 QUALITIVE INTERPRETATIONS

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7.2.1 Frequency Pseudosections

The near-field corrected frequency pseudosections provide the starting point for the interpretation of results. By comparing the *relative* apparent resistivities down each line, possible contacts and vertical structure may be interpreted.

The reader must realize when viewing the sections that they do not represent a "slice of the earth", rather they are a convenient means by which to present the data. Each sounding point should be considered individually on the section.

Since the effective depth of investigation of CSAMT is a function of the earth resistivity and the characteristics of the conductor at depth, depth estimates for anomalies cannot be determined with any degree of certainty using qualitative analysis from the frequency sections.

When analyzing CSAMT data, the interpreter must also be aware of several "effects" which, if not considered or understood correctly, can lead to gross misinterpretations:

1) Static Shifts

Small, near-surface resistivity inhomogeneities often strongly affect the calculated apparent resistivity of CSAMT data, the same way that MT and AMT data is affected. When an electrode is placed within, or very near to such a feature, the apparent resistivity curve for that sounding point will be shifted along the resistivity axis. For conductive zones such as swamps, the curve will be shifted *down* the resistivity axis whereas for very resistive zones, such as outcrop, the



curve will be shifted up the resistivity axis.

Static shifts may create interpretation problems when conductors of interest are below near-surface conductors for example. Resistivities from the nearsurface anomaly will pull-down the resistivities above the deeper conductor such that the two anomalies may appear to merge as one long, deep conductor.

2) Undershoot

both MT and CSAMT, In the apparent resistivity increases as frequency decreases over structure of higher resistivity underlying lower resistivity. When the resistivity contrast is high, the apparent resistivity curve usually decreases before beginning to increase. This type of response is more commonly referred to as "undershoot". For data measured in the far-field, the decrease or undershoot is small. For CSAMT data measured in the near-field or the transition field, however, the undershoot is often very large and which can create problems with depth distinct, inversions.

Unfortunately, the undershoot response cannot be corrected using the first order correction. To correct for the effect, the biased data points can simply be removed from the resistivity curve and the curve replotted. However, in some cases it may be difficult to distinguish a true trough of apparent resistivity from an undershoot effect. A simple 1-D forward model may be useful to determine whether the trough is a true response or undershoot.

7.3 MODELLING

7.3.1 <u>1-D Inversions</u>

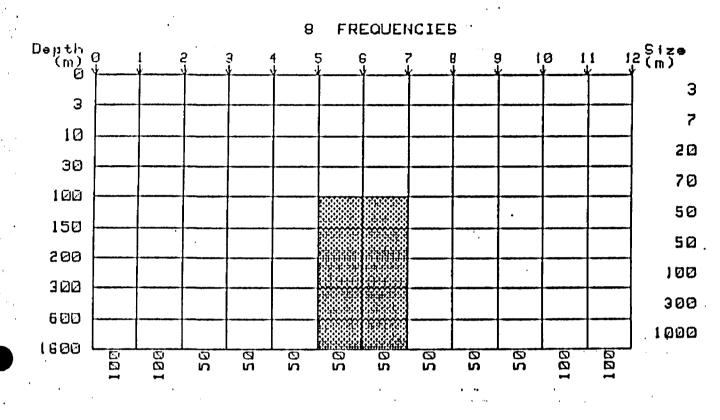
The depth for which the amplitude of the EM field decreases to 1/e (37 percent) of its value at the surface is referred to as the skin depth. The strict definition of skin depth requires a homogeneous medium, however in practical application, such conditions do not exist therefore an apparent skin depth (*skin deptho*) for an inhomogeneous medium may be defined as:

$$\frac{2p_{a}(f)}{2\pi f M_{o}}$$
 skin depth_a= (----) 1/2 (3)

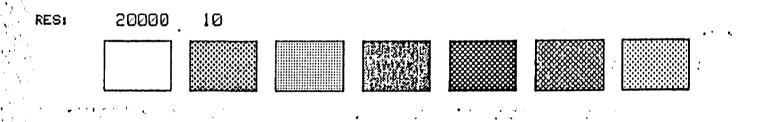
Where apparent resistivity $(p_o(f))$ is the apparent resistivity measured at that frequency. The skin deptho is indicative of the depth of penetration of the EM wave, i.e. the lower the frequency of the transmitted signal, the deeper the depth of penetration.



PHOENIX GEOPHYSICS 2D FINITE ELEMENT CSAMT MODELING



12 X 9 MESH



Execution Time = 2124.18 (MM:SS.SS) on 6 Aug 1987

FIGURE 7.2 2-D forward model at 100 meters.

·····) 		<u>,</u>		·		·	· · · · · · · · · · · · · · · · · · ·					—
52 '	13K	18K	15K	13K	זסאן	172	, ^{א2} ן	10K	13K	TEK	TBK	36K	. 55
3 •	так '	JBK	TEK	זפג	XØ L	אב	яг	ז פא	IJK	тек	IBK	19K	S
· ·	75K	NBI	75K	13K	ז פא	72	ж	1 OK	JET	75K	18K	39K	
2	Iak	18 K	Tek	, 13K	ABL	ЯЗ	ж	. 10K	тэк	Tek	TBK	19K	
ł	13K	18K	IEK	13K	1 OK	ЯZ	ЯZ	TOK	IJK	TEK	78K	39K	
ŝ	так	18K	1eK	13K	зßк	ус	ж	10к	тэк	тек	ABI	18K	
91	13K	38 K	TEK	1 3 K	1 BK	72	ж	төк	13K	TEK	18 K	X 61	9
35	IJK	XBI	IEK	13K	NOI	۶к	Яг	төк	IJK	TEK	XBI	19K	2
64	так	JAK	JEK	34K	HØ C	y2	же	1 OK	J4K	TEK	JBK	NEL	þ
158	IJK	ABI	τśκ	1+K	YOI	8K	ЯЯ	нак	14K	72K	XBI	19K	BS
528	IJK	זפא	JZK	3+K	NON	, BK:	ЯС	pigt	JAK	11K ⁺	IGK	13K	99
215	50K	JBI	12K	1+K	X0 t	8K	ЯК	10K	74K	15K	18K	SDK	15
1054	SOK	Jak	72K] 4 K	אננ	BK	ЯӨ	л тк }	тақ	174	Jak	SOK	954
82048	SOK	IJK	71K	14K	яп	BK	BK	77K	74K	77K	YEI	SBK	848
9604	Iak	JBK	72K) א+נ	אננ }	ақ	ак	ן זזג (ן ^{זאַג}	77K	18K	36K	960
	15	τι	ØI	6	B	2	9	S	* *	Ê	Ś	ī	-
ЕГІИС	IIIOW J	WHSC	<u>5-D (</u>) 				•	<u>INC</u>	<u>'SDIS</u>	<u>57H7G</u>	IX CE	НОЕИ

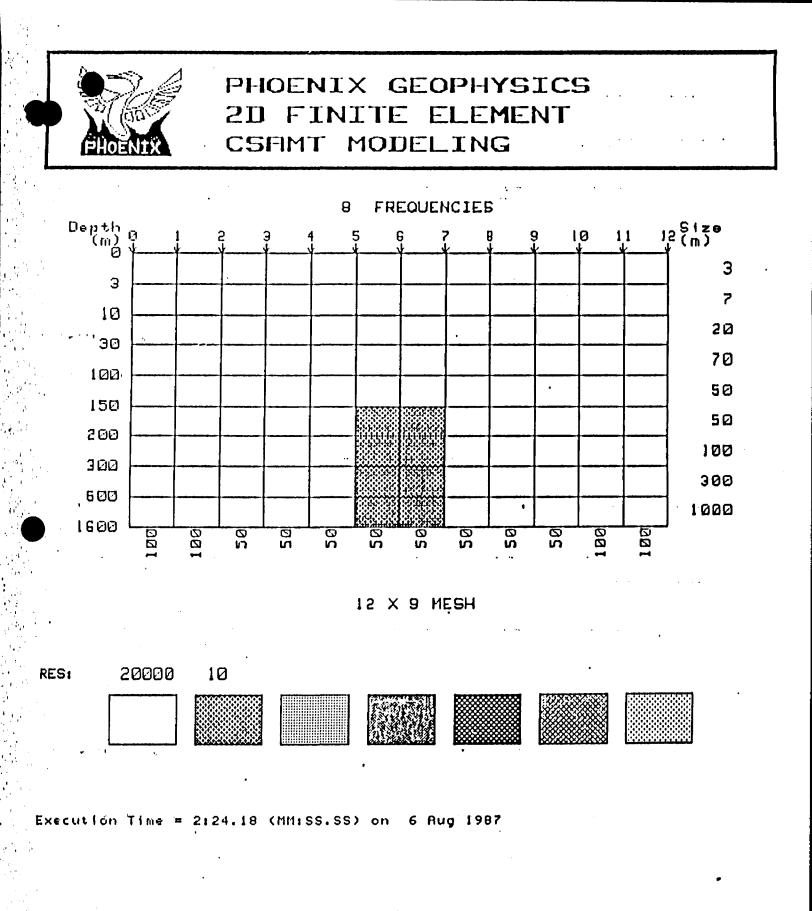


FIGURE 7.3 2-D forward model at 150 meters.

	1	2	3	4	5	6	7	8	9	10	11	12	
1036	19K	18K	17K	15K1	14K	1эк	13K	J4K	1)5K	17K	18K	19K	4096
2048	19K	19K	17K	15K	13K	15K	12K	13K	15K	17K	19K	19K	2048
024	19K	18K	17K	150	13K	12K	IZK	13K	15κ	17K	18K	19K	1024
12	19K	18K	17K	15K	13K	15K	15K	13K	15K	17K	18K	19K	512
156	19K	18K	16к	15K	13K	IZK	IZK	13K	15K	16K	18K	. 18K	. 256
28	19K	18K	16K	14K	12K	I 2K	12K	12K	14K	16K	18K	19K	128
\$ 4	19K	17K	16K	14K	12K	ык	ιιк	12K	J4K	15K	17K	19K	64
32	19K	17K	16K	14K	12K	LIK	IIK	15K	14K	 16K	17K	19K	
16	19K	17K	16K	14K	12K	ык	шк	15K	14K	16K	17K	19K	16
8	19K	17K	16K	14K	12K	ЦК	шк	12K	14K	16K	17K	19K	8
ş	19K	17K	16K	14K	12K	нк	нк	12K	14K	16K	17K	13K	4
2.	19K	17K	16K	14K	12K	11К _	ιιк	15K	14K	16K	17K	19K	2
1	19K	17K	16K	14K	12K	ык	ιικ	12K	14K	16K	17K	19K	·
. 5	19K	17K	15K	14K	12K	шк	ιιк	12K	14K	16K	17K	19K	.5
. 25		17K	16K	14K	12K	цк	11K	12K	14K	16K	17K	13K	. 25

Considering the recorded apparent resistivity for each frequency, the apparent skin depth for a sounding point may be estimated by means of a simple inversion program. The program provides reasonable estimates only for layered, horizontallyhomogeneous stratigraphy, and is therefore not also be exercised to avoid literal interpretation of depth structures, i.e. finite or isolated conductors (Bartel, 1987).

Static effects, as discussed above, may also lead to errors in inverted models. By the apparent skin depth calculation, the inverted resistivities will be shifted proportionally to the shift in the apparent resistivity curve, while the inverted depth will be shifted proportionally to the square root of the shift of the apparent resistivity curve. The interpreter must exercise care when applying inversions under these conditions to avoid misinterpretations.

7.3.2 <u>2-D Forward Modelling</u>

A two dimensional, finite element, forward modelling program was used when necessary to estimate the "best-fit" geology model for a particular frequency pseudosection.

The operator can specify a mesh size and up to seven (7) causative bodies each with an apparent resistivity value. The program was executed on an HP9000 computer by Phoenix Geophysics Ltd. at their facilities in Toronto.

8.0 RESULTS AND INTERPRETATION

The C14 project was undertaken to investigate an ultramafic breccia in Clifford Township, Ontario. Several drill holes have been completed, to evaluate the results of a ground magnetic and an IP and resistivity test survey. The CSAMT Test Survey was completed in an attempt to evaluate the usefulness of this relatively new technique in outlining the low resistivity zone that represents the increased porosity associated with the breccia.

Reconnaissance and detailed ground magnetic surveys clearly show a "kidney shaped" magnetic high. The magnetic high is centered at about 7+00N on line 2000E and line 2125N. This magnetic high correlates closely with the breccia pipe, as it was later outlined by the drill holes completed.

Dipole-dipole IP and resistivity measurements were completed on line 2000E and on line 2125E using X=50 meters; n=1,2,3,4,5. These pseudosections both indicate a region of very high resistivities (greater than 2000 ohm-meters) to the south of about 6+00N to 5+00N. On both sets of data, the dipole-dipole results indicate a relatively narrow zone of lower bedrock resistivities (less than 200 ohm-meters) just to the north of this resistivity contact. This some of lower apparent resistivities is broader on the western line (line 2000E) than it is on line 2125E. To the north of this low resistivity feature, the basement rocks are indicated to have a more moderate resistivity value.

CSAMT measurements were completed on the C14 Grid, with an E-field dipole length of 50 meters. On line 2000E and line 2125E, the CSAMT apparent resistivity pseudosections show resistivity lows that correlate exactly with those detected by the X=50 meters, dipole-dipole measurements. The zone of low resistivities in the bedrock is broader on line 2000E than on line 2125E. The plan map, contoured presentation of the apparent resistivities measured at 64Hz, shows a region of low bedrock apparent resistivities that correlates closely with the magnetic high and the location of the breccia pipe.

The association of a magnetic high and an apparent resistivity low is unusual. Alteration in the bedrock will produce an apparent resistivity low, due to increased porosity. However, most alteration phenomena decrease, or totally destroy, the magnetite content of the rocks. This will result in the measurement of a magnetic low during a survey.

It would appear that magnetic and resistivity surveys would be useful in the search for breccia pipes. However, care must be exercised in the interpretation of these results in regions of deep glacial overburden. The magnetic anomalies may be reduced, due to the greater distance to the source. The apparent resistivity results will be drastically influenced by the presence of the thick, conductive, overburden layer.

The CSAMT pseudosections from line 2500E and line 125 exhibit the type of apparent resistivity pattern that can be encountered.

CERTIFICATION

I John M. Kovala certify:

- 1. That I reside at 7 Teck Hughes Property Kirkland Lake Ontario.
- 2. That I have completed the B.Sc. program in Geology at Laurentian University.
- 3. That I have been employed in the exploration Industry since 1983.

Signed

John M. Kovala Project Geologist

Qual 2.10571

APPENDIX A

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TECHICAL SPECIFICATIONS --- PHOENIX V4, T30, MG30

	SIGNAL PROCESSING, A-D Conversion	16 bits, giving a resolution of 3 part in 65,000.	I/O Ports	The memory may be transferred into a computer by an 8-bit parallel 1/0 port or by an optional serial RS-232 port.
		Controlled by miroprocessor to a maximum of 12.5 kHz (16 kHz by early 1985).	Printer	A vest pocket-sized, 20 column, dot matrix printer operates through the 8 bit porallel 1/O
•	TEST AND CALIBRATIC Calibration	A test signal output is provided to perform test and calibration functions. There is also a processor controlled internal test mode that		port. Power for the printer is supplied by the V-4; no additional batteries are required. The external printer configuration permits better environmental protection.
ł		allows automatic precise calibration of all filters. Calibration responses may be stared in the instrument and automatically removed from the measurements.	Analog Meters	A meter for each channet provides continuous monitoring of the signals. These meters are also used for bottery monitoring.
	Test Signal	The externally available test signal can be either:	GENERAL	
,	•	a frequency domain signal of \pm SV, 200 ohm Impedance, frequency 4 kHz - 1/128 Hz, or a time domain signal with a S0% duty cycle.	Temperature	The storage temperature range is -50°C to +70°C. The operating temperature range is -60°C to +50°C, [-10°C to +50°C without LCD heater option).
	Display and Controls	The display is a 64 character dat matrix LCD and the computer results presented are the mean and standard deviation as well as the	Humidity	The instrument is moisture proof and may be operated during rain.
		stack number.	Altitude	-1600 m to 5000 m.
		All modes of operation and parameter control entries may be displayed and the display will	Vibration	Suitable for transport in light aircraft and bush vehicle.
		prompt the operator to make the oppropriate keypod entries.	Weight	13 kg.
		The LCD will operate to a temperature of -10°C. For lower temperature operation on LCD heater is required (optional).	Case	The case is made of an Acrylic PVC elloy, which is vacuum formed, extremely tough, resilient, weather resistant and a good electrical insulator, it is equipped with a removable iid, carrying
	Memory	Non-volatile memory for data logging is provi- ded. This is sufficient for storage of 36 SIP sta-	N 1 1 1	handle and packboard tie down loops.
	Share and the second	tions with a full complement of channels over the	Dimensions	32 cm x 36 cm, 27 cm high.
	, ,	entire frequency range. Although this is sufficient for approximately three days operation, a further memory extension is optionally available.	Batteries	The standard instrument is equipped with three 6 volt rechargeable gel cells. The battery charger circuit (less transformer) is built-in.
on	trolling Firm	ware		
	Programs	The standard version of the V-4 includes the control program for Spectral Induced Polarization operation (SIP).	Optional Programs available	Controlled Source Audio Magnetatelluric (CSAMT, Time domain induced polarization Others: Consult Phoenix for details,

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Spectral I.P. [SIP] Operation

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Frequencles	2. ¹⁰ Hz to 2 ¹² HZ (1/1024 to 4096 Hz) in binary steps. An automatic frequency scan is initiated by selecting Fhigh and Flow to be different values. The scan can step by a factor of 4, 2, or	· .	ENTER is pressed after each of the operating parameters is input through the keypod. A averaging time
	values. The scall call step by a factor of a , a , or $\sqrt{2}$.		6 number of channels
Transmitter Links	For spectral IP, two highly isolated RF communication links are provided:		C current in amperes D dipole identification E electrode interval in meters
	 A: Transmitter drive link for transmitter switching control via a twisted pair cable. 		F frequency range (Fhigh, Flow) The six parameters are held in memory. Only
	 Current Monitor link, This link provides an occurate seplica of 		a few are usually changed from station to station to station to station to station afong a line.
	the transmitter current to one of the eight chonnel inputs. This allows real-time deconvolution of the transmitter waveform from the other input chonnels. The required Isolation transformer and demodulation circuits are built into the V-4.		PRINT prints out the six operating parameters if It is desired to check their values. RUN starts the automatic frequency scan. The unit first measures, colculates and prints the resistivity at 1 Hz. It then proceeds to Fhigh makes the required measurements, displays
Deconvolution	The physical quantity which we are attempting to determine is the resistivity transfer function. Since it is not possible to control kilowatts of power passing through unstable current		and prints the results, proceeds to the next frequency and so on, down to flow. \$10RE is pressed if the scon is satisfactory and It is desired to slore the results in memory.
	electrodes to an accuracy of 1 part in 10000, it is necessary to monitor both current and voltage and then to deconvolve the current from the voltage to obtain the true spectral IP response. This deconvolution is carried out automatically in the V-4 at each frequency by dividing the voltage amplitude by the current amplitude and by	Software	Phoenix supplies complete applications software for transferring spectral IP data to a computer; litting the Cole-Cole model to spectral IP data; calculation of Cole-Cole parameters; removal of electromognetic coupling; and plotting and contouring data pseudosections.
	subtracting the current phase from the voltage phase for all six voltage channels.		in addition, Phoenix supplies 2-dimensional modelling programs for both forward and
Operating Sequence	START sets the receiver and transmitter to 1 Hz and allows the System to cancel SP and adjust		inverse problems, to aid in interpretation.
	gain for each channel.		All programs pre-written in SASIC.

CSAMT Operation

Frequencies

Productivity

2.2 to 212 (0.25 Hz - 4096 Hz) in binary steps (or 72 steps).

Since the horizontal H field varies slowly, it is possible to measure only one H field for six electric dipoles. Thus production rates are six times greater than those of older, conventional, 2-channel instruments.

Real-time Calibration

Software

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The standard procedure is to store the transfer function of the instrument in memory and remove it from the signal in real time.

In addition to the CSAMT control program, BASIC software utilities are available for plotting and contouring pseudosections of Cogniard apparent resistivity, and correcting for the near-field situation.

	₩.4	·
	 Versatility 	Instrument may be used for spectral IP, CSAMT, and conventional IP in either frequency or time domain.
	Productivity	Simultaneous measurement of eight input channels.
	Microprocessor Control	Microprocessor-controlled real-time filtering, signal stacking and averaging in time or frequency domain.
	Reliability	Data logging in solid state non-volatile memory.
• '• '•: 1	• Standard 1/0	Output ports for a vest pocket printer and computer or data link.
•	 Automated Operation 	Automatic gain control and self-potential (SP) cancellation.

Eight Channel Universal Receiver



Features

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EXTREMELY BROAD FREQUENCY RANGE

The V-4 was designed to cover the frequency range of most interest for electrical measurements. Its complete frequency range is six decades. With a top frequency of 4096 HZ it is a multifrequency EM unit as well as a spectral IP unit. High frequency measurements may be made very quickly, and provide useful, detailed data about the resistivity section. Pseudosection plots of the high frequency phase angles provide geometric as well as parametric EM information. The Intermediate frequencies allow very accurate removal of electromagnetic coupling from IP data, and provide information on mineral type, which in certain situations can result in considerably more cost-effective exploration programs. Alternatively the high-frequency measurements may be made in CSAMT mode, providing rapid reconnaissance measurements of resistivity from 0.25-4096 Hz.

DESIGNED FOR BOTH RESEARCH AND PRODUCTION

The V-4 has been designed to be both an extremely powerful research instrument as well as the fastest production IP unit available. The conversion is accomplished simply by changing the limits of the frequency scan. Reconnaissance work might be carried out at a single frequency in which case the measurements are extremely fast and accurate. If an anomaly is encountered, the scan may be widened to provide additional data useful for the evaluation and removal of inductive coupling, and for purposes of mineral discrimination.

EIGHT CHANNEL CAPABILITY

The multichannel capability of the V-4 can decrease measurement time by a factor of six over conventional units.

1000 Megohms

REAL TIME DECONVOLUTION

Any variations in the transmitter waveform are closely monitored and accurately compensated for. This is equivalent to continuous calibration of the transmitter electrodes. All calculations are made in real time. No measurement time is wasted waiting for the processor, even at 4 kHz

MEAN/STANDARD DEVIATION

Both mean and standard deviation are continuously displayed and recorded. Thus a constant record is maintained of the precision of the measurement. If the desired accuracy is achieved early, time can be save by pressing NEXTF. The processor then prints the results and proceed with the next frequency.

VERSATILITY

The V-4 can be used for spectral IP, conventional IP in time or frequenc domain, and CSAMT, resulting in an extremely cost-effective instrumen package.

OPTIONS

Goins

- . Dipole preamplifiers for spectral IP operation in high resistivity areas.
- . RS-232 1/0 port.
- LCD heater for extended cold temperature operation.
- Memory extension.

Power Line Filtering

Anti-Alias Filter

Sp Concellation

SIGNAL PROCESSING, ANALOG

- Operating firmware for CSAMT, time domain IP, and others to b onnounced.

I to 640, under microprocessor control.

may be switched in or out.

corner frequencies.

of ±2.5V.

Triple notch filter for 1st, 3rd and 5th hormonic of

50 or 60 Hz. Notch depth 40 db minimum. Filter

7 pole fow pass filter with processor controlled

Under microprocessor control up to a range

Specifications,	Hardware
-----------------	----------

INPUT Channels

Impedance Protection

Ranaes

DHOEND

PHOENIX GEOPHYSICS LIMITED

Geophysical Consulting and Contracting, Instrument Manufacture, Sale and Lease.



Tel: (418) 477-8588

High input impedance differential amplifiers. Eight input channels may be measured

simultaneously. Six channels are combined in

one input connector. The other two inputs are

The input is protected from excessive voltages by a 10,000 ohm fuse resistor.

To ±10V maximum input signal.

equipped with isolated power supplies to pov external devices such as coil preamplifiers.

Telex: 06-986856, Fax: 418-477-9251

Markham, Ontario, Canada L3R 5M7

TORONTO 7100 Warden Ave., Unit 7



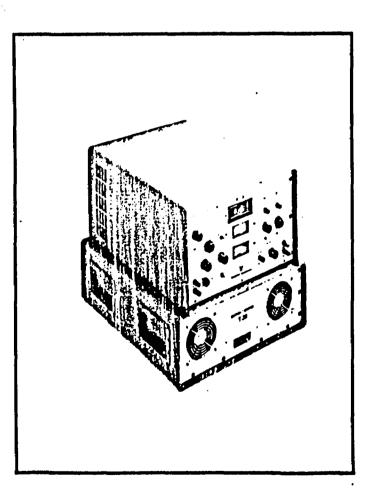
PHOENIX Geophysics Limited

7100 WARDEN AVENUE, UNIT 7, MARKHAM, ONTARIO CANADA L3R 5M7

TELEPHONE(416) 477-8588 Telex: 06-986856 Cable: PHEXCO TORONTO



MULTIPURPOSE CONTROLLED SOURCE



THE T-30 IS THE MOST ADVANCED CONTROLLED CURRENT SOURCE AVAILABLE FOR ELECTRICAL METHODS EXPLORATION. IT COMBINES MODERN GTO TECHNOLOGY WITH THIRTY YEARS OF TRANSMITTER DESIGN EXPERIENCE.

THE T-30 (30 KW) IS ONE OF TWO UNITS, IDENTICAL IN ALL SPECIFICATIONS EXCEPT FOR POWER AND WEIGHT. THE LIGHTWEIGHT VERSION OF THE T-30 IS DESIGNATED THE T-15. THE 15 kw T-15kw IS DESIGNED FOR END-USERS WHOSE APPLICATION PLACES A PREMIUM ON PORTABLILITY.

THESE TRANSMITTERS CAN BE USED FOR A VARIETY OF DEOPHYSICAL TECHNIQUES, INCLUDING CONVENTIONAL IP IN THE TIME OR FREQUENCY DOMAIN; TRUE WIDEBAND SPECTRAL IP; CSAMT (CONTROLLED SOURCE AUDIO MAGNETOTELLURICS); AND TDEM (TIME DOMAIN ELECTROMAGNETICS).

THE TRANSMITTER LOAD MAY BE EITHER A GROUNDED DIPOLE OR A LOOP, DEPENDING ON THE REQUIREMENTS OF THE APPLICATION. THE RAPID CONTROLLED TURN-OFF INTO INDUCTIVE LOADS IS SUITABLE FOR TDEM APPLICATIONS.

A VERY WIDE RANGE OF STANDARD BINARY-RELATED TIMING OPTIONS IS PROVIDED, AS WELL AS AN INPUT CONNECTION FOR AN ARBITRARY EXTERNAL TIMING DRIVE.

THESE UNITS ALSO FEATURE A VARIETY OF PROTECTIVE CIRCUITS, BUILT IN RECEIVER CALIBARION CIRCUITRY, CURRENT MONITOR OUTPUT FOR EXTERNAL DECONVOLUTION, CONSTANT SURRENT CONTROL, AND SEMI-INFINITE IMPEDANCE IN THE "OFF-TIME" WHEN USED FOR TIME-DOMAIN IP.

SUMMARY SPECIFICATIONS FOR THE TRANSMITTERS ARE DIVEN BELOW:

FREQUENCY	: DC - 10 kHZ.
MAX. YOLTAGE	: 800 YOLTS.
MAX. CURRENT	: 40 AMPERES.
WEIOHT	: T-15 75 KO.
	: T-30 120 KO.

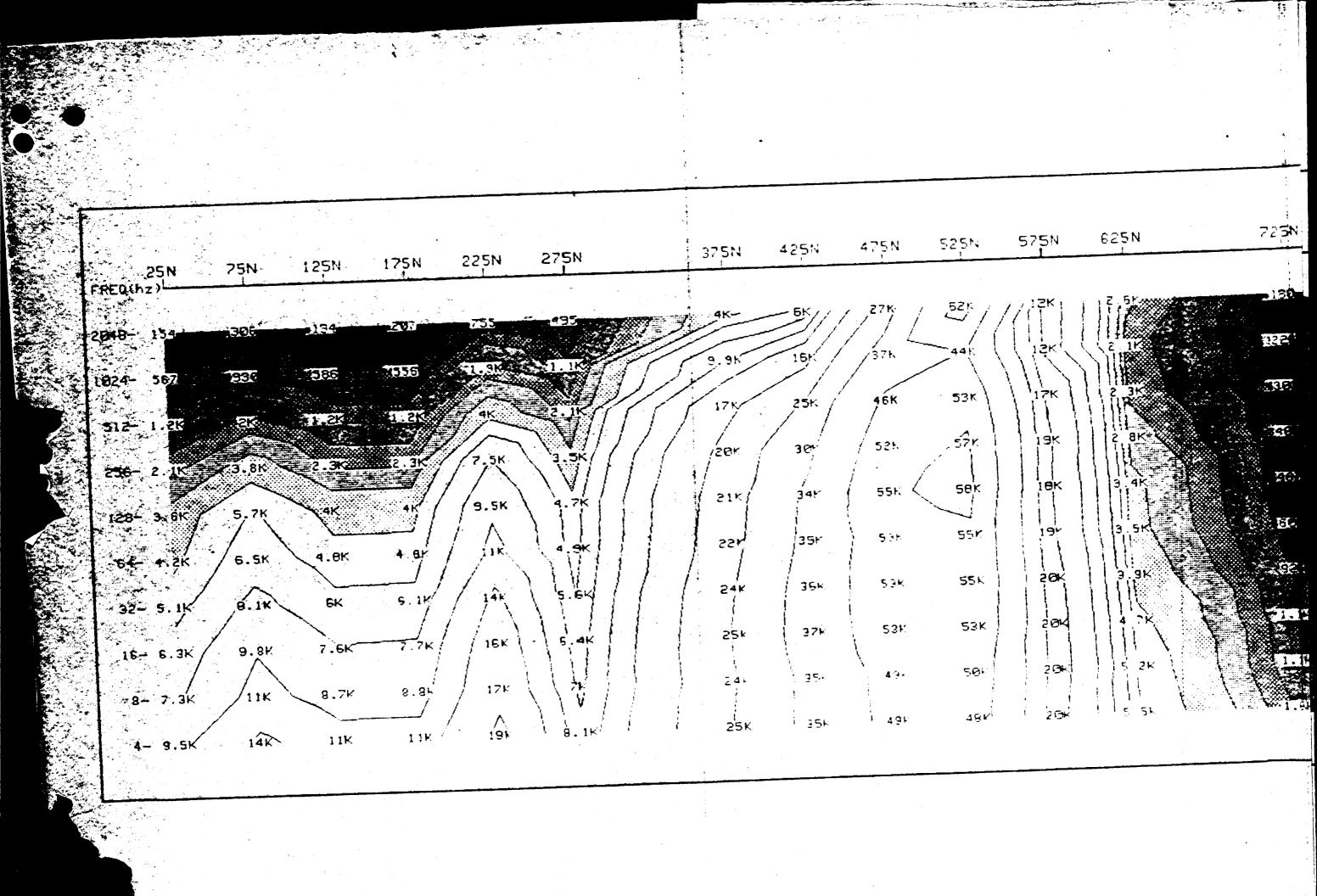
THE STANDARD POWER SOURCE FOR BOTH UNITS IS THE MO-30 MOTOR OENERATOR. HOWEVER, AS ANY SUITABLE MO UNIT MAY BE USED, IT IS NOT NECESSARY TO PURCHASE THE MO UNIT FROM PHOENIX.

IN ADDITION TO THE MO-30, WHICH EMPHASIZES HIGH POWER/LOW WEIGHT, PHOENIX OFFERS A VARIETY OF MO OPTIONS. THE USER MAY REQUEST GASOLINE OR DIESEL ENGINES; 60 HZ. OR 400 HZ. ALTERNATORS; AND 110/208 V OR HIGHER VOLTAGE OUTPUT.

APPENDIX B

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CSAMT FREQUENCY PSEUDOSECTIONS



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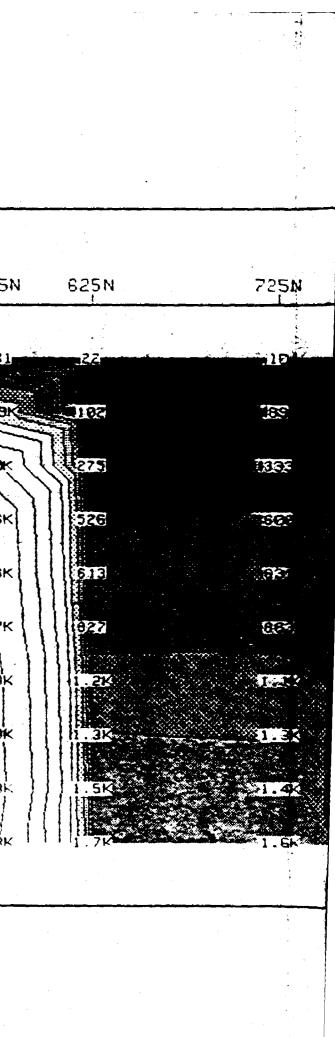
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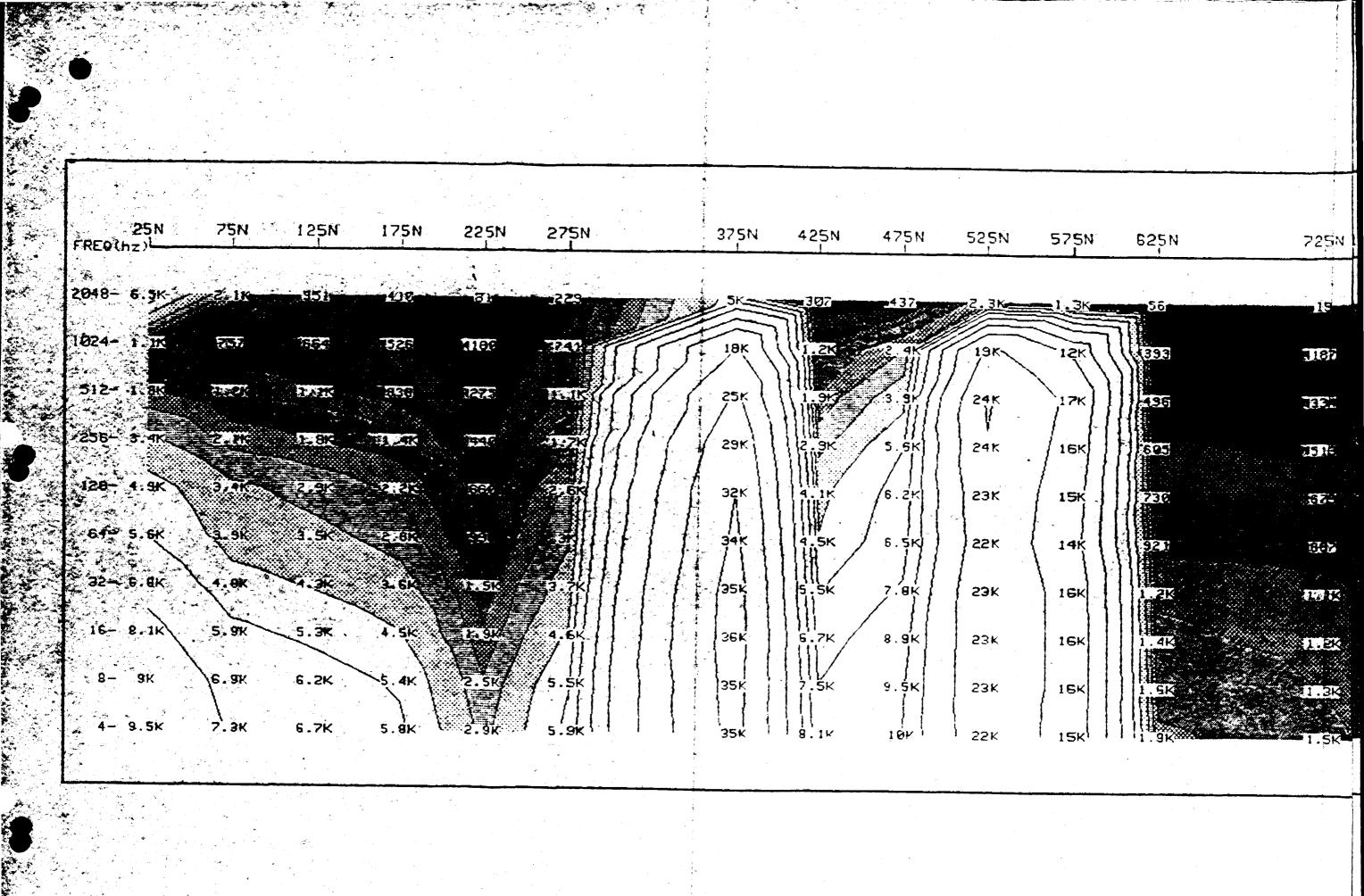
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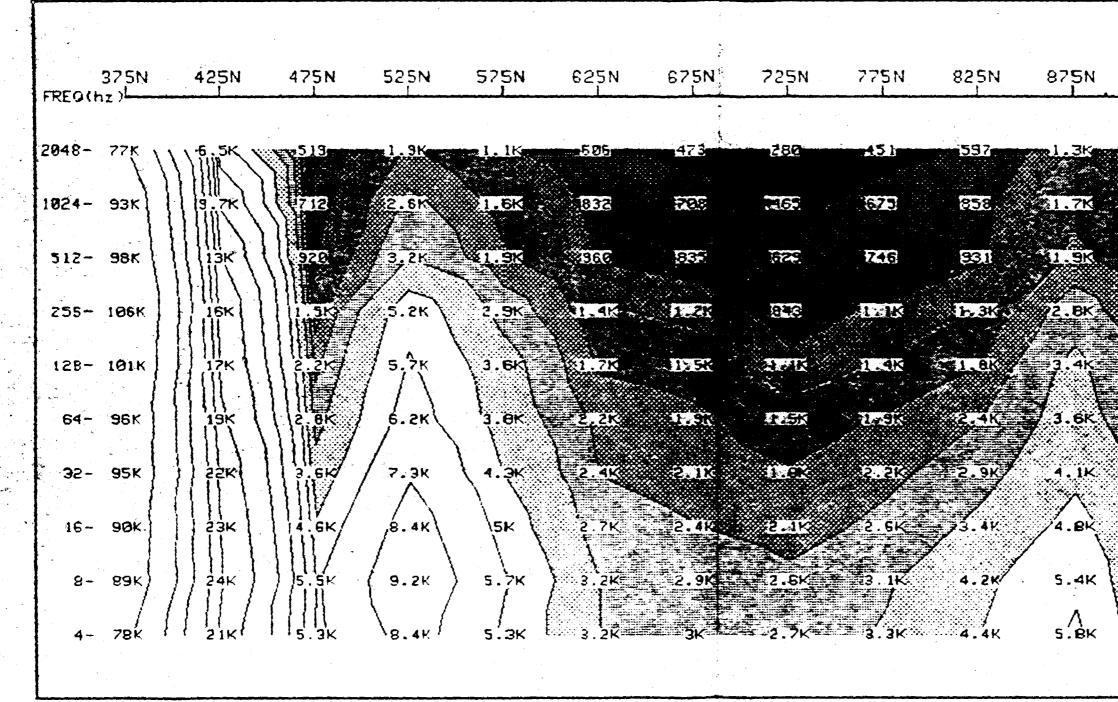
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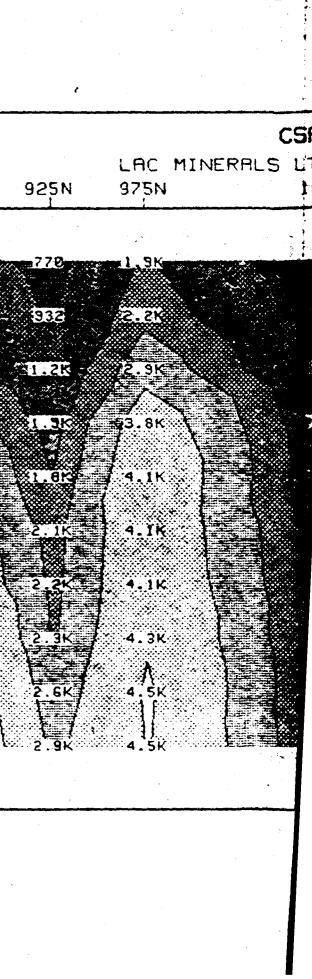
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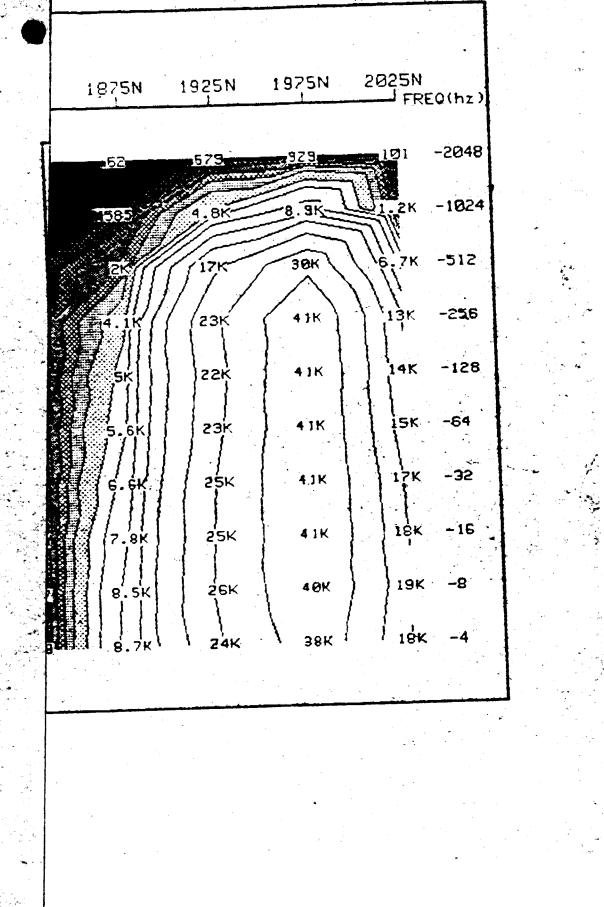
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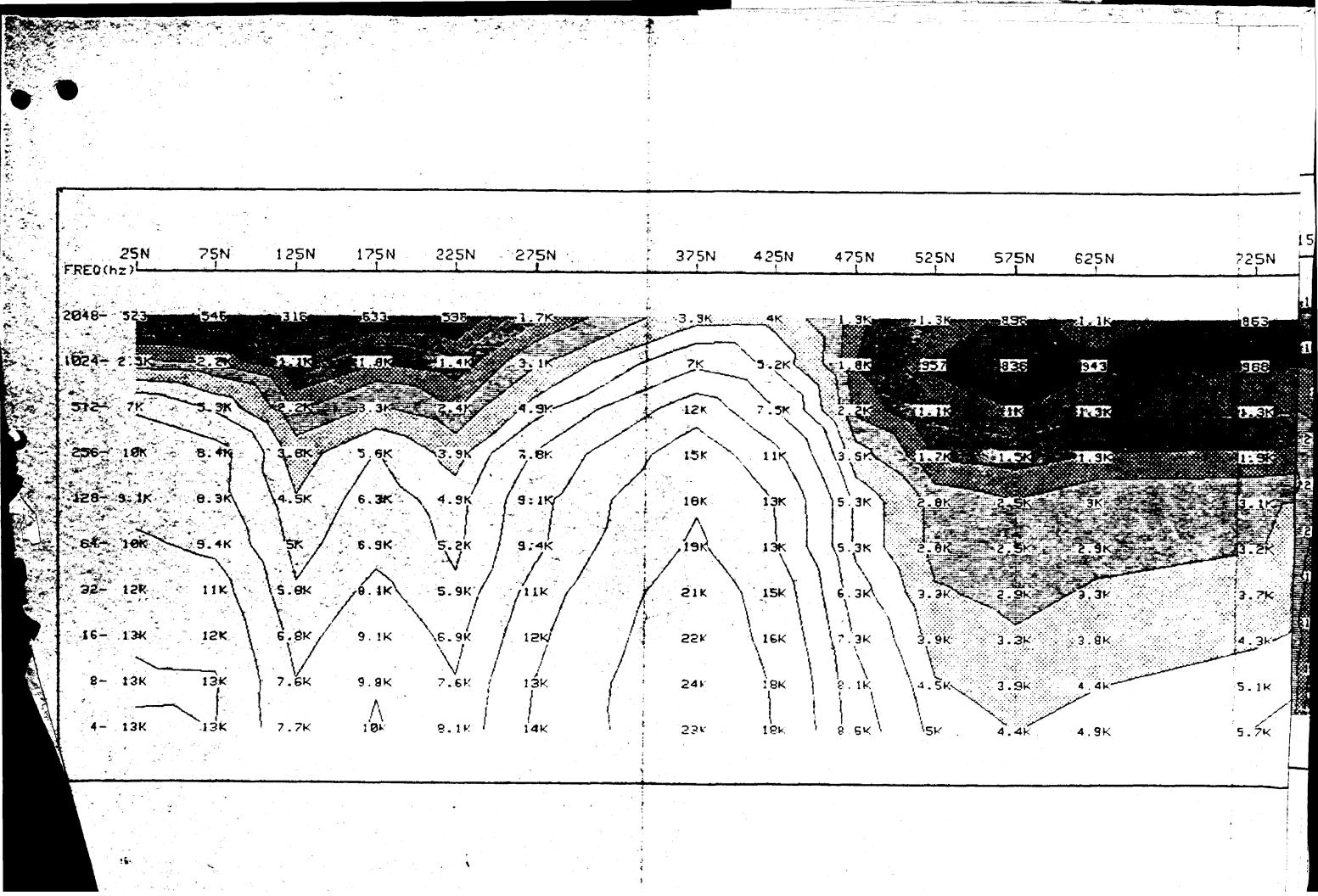


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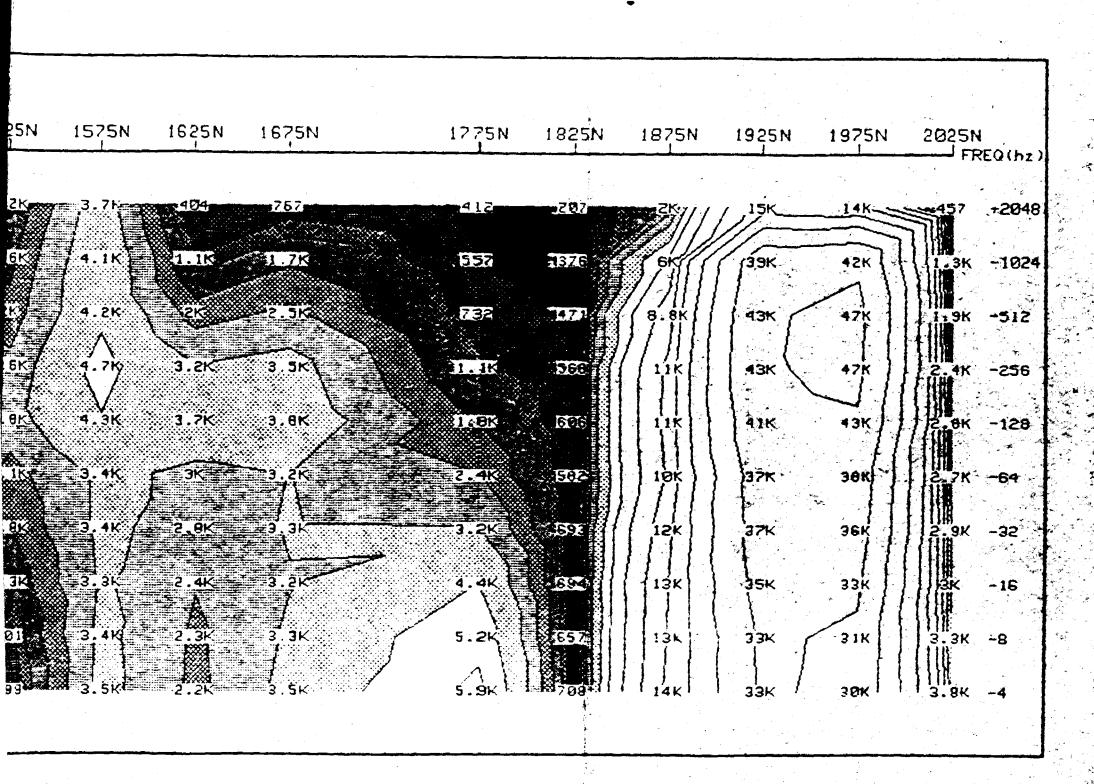
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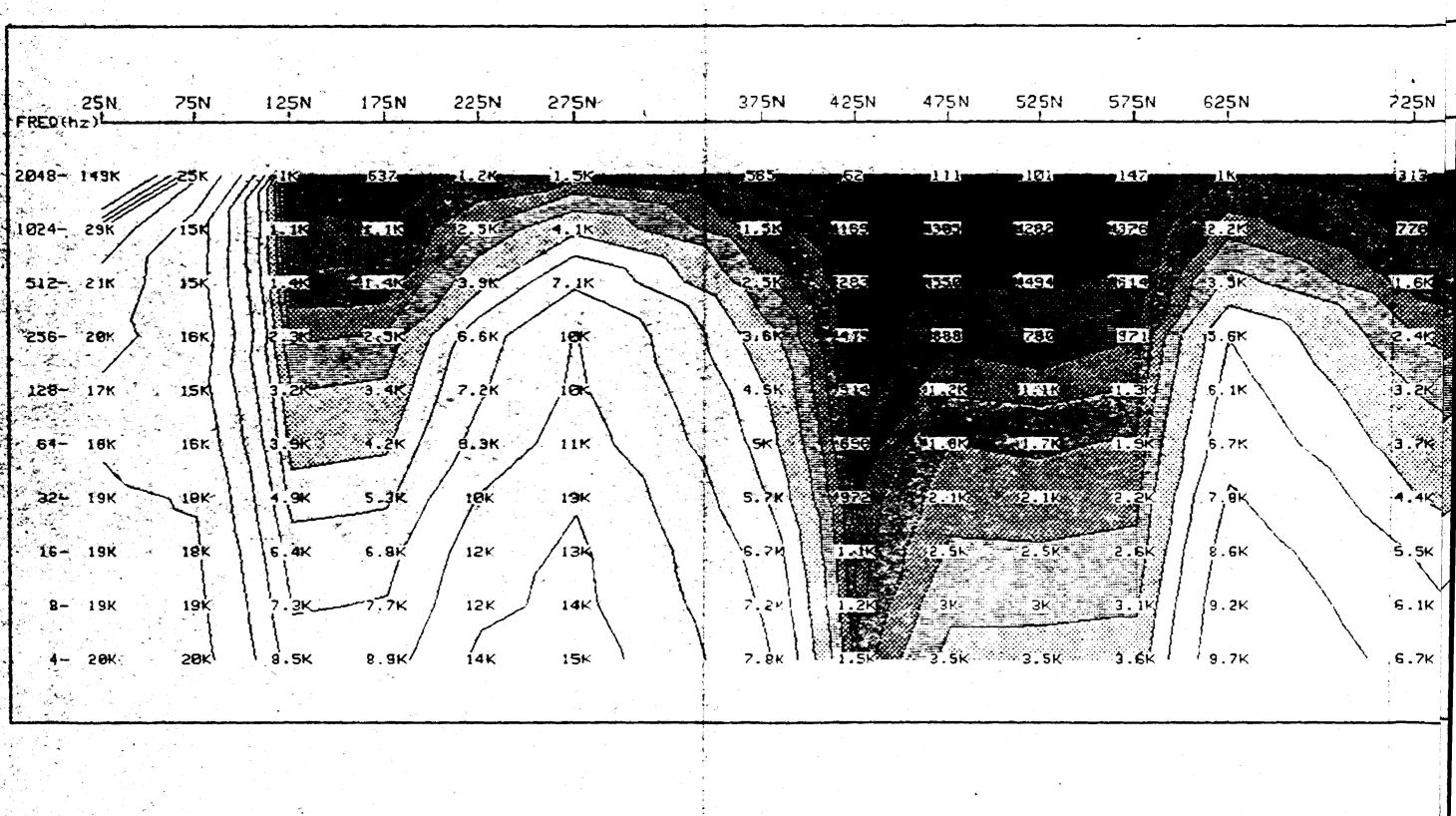
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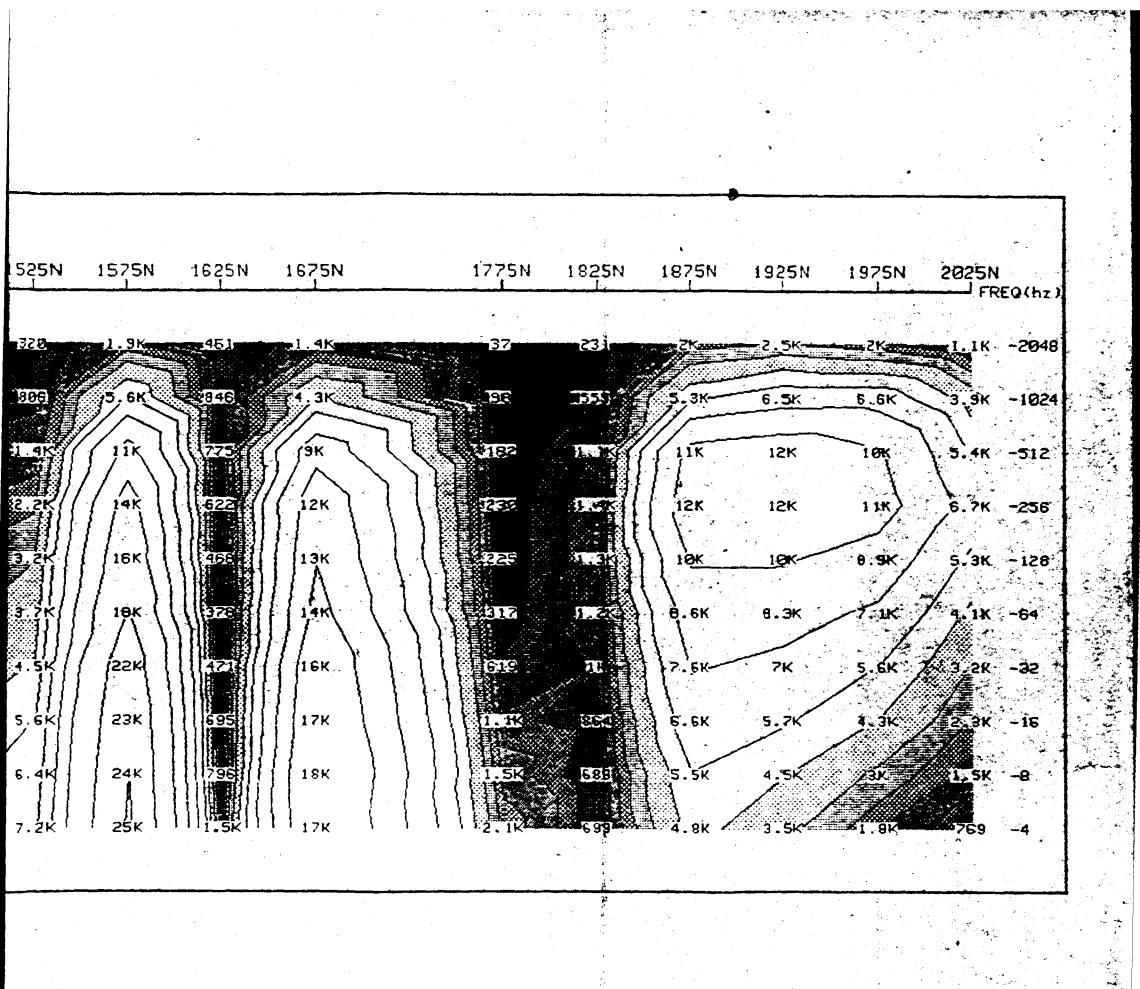


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э.5K	3.50		- 2 . 5K	EX.		5 .000 .00						4.2K	Ì
4.2K	4.3K	1.34.1	2.9K		N						1.98	4.8K	
5K	5.3K	3.74	3. 3 K	2. C. 7. M						972	1.8K	5.4	
5.9K	6.24	4.5K	3.9K	X 3K.			1		94 8 ⁻	568	1.9	5.7	ĸ
6.7K	7.1K	5.4K	4.5K	3.5K	in ohm-m	INC. NOV-	1.5K-	33-				- - 	

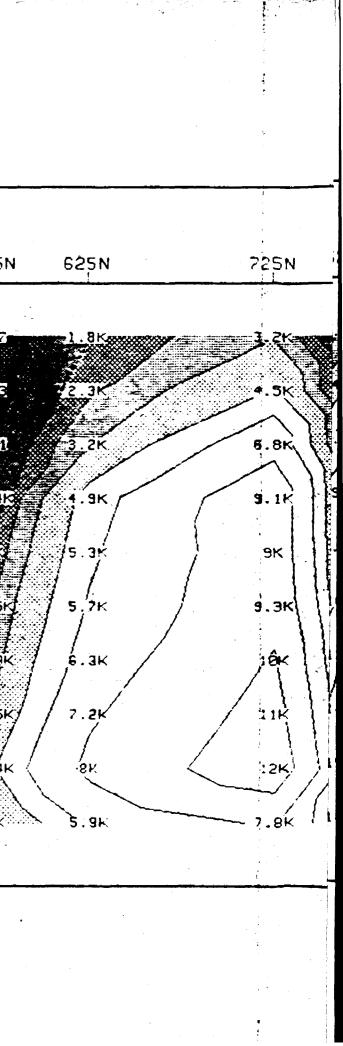




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		CSRI	MT RPPP	RENT RES	SISTIVITY (CORREC	TED				1. *	•
275N	C MINER	144	D_ C14 925N	LINE=625E 975N			ft Tx-R> 1175N			1325N	1425N	1475N
•	345	302	217-	187	355	243	251	158	400	288	355	283
				ж.ж [.] д п								
794	131	1399	1923	TEDT			14.95	1318	897	669	1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -	549
	555	1980	.38			<u>, 2 – 4 – 1 – 1 – 1 – 1 – 1 – 1 – 1 – 1 – 1</u>	2259	14.95	1.4K		1.6K	
21.8K	<u>, 572</u>	335	612			in see		228	2.2K	1.7K	2. SK	1.76
2457			255	TER					2,98	2.46	ЪŔ	2.46
			- 153 s.									
-3K								TAR	ЭТЭК	2.15K	Э.4К	2.90
3.5K							7 3 67	ne z -	3.9K	3.6K 🦟	4K ***	3,5K
			and the second secon	n na Sana Anna Anna Anna Anna Anna Anna Anna A								
4.2K	5.16		I.SK				2.6K	2 3%	4.64	4.4K	4.8K	4.3K
4.7K	12.5P	2.3%	1 94	2.14	36:	5.98	3.3%	2 9r	5.34	SK	5.5K	4.9K
								V	1			
\5.2K ₩	2.9K	2.7	2.3K	2.54	134	с -экур	3.76	3.34	S. 8K	5.7K	6.14	`s.бк
· · ·			Surveyed b	W Resistiv	CONSULTING	EL NOV 198	2.7					



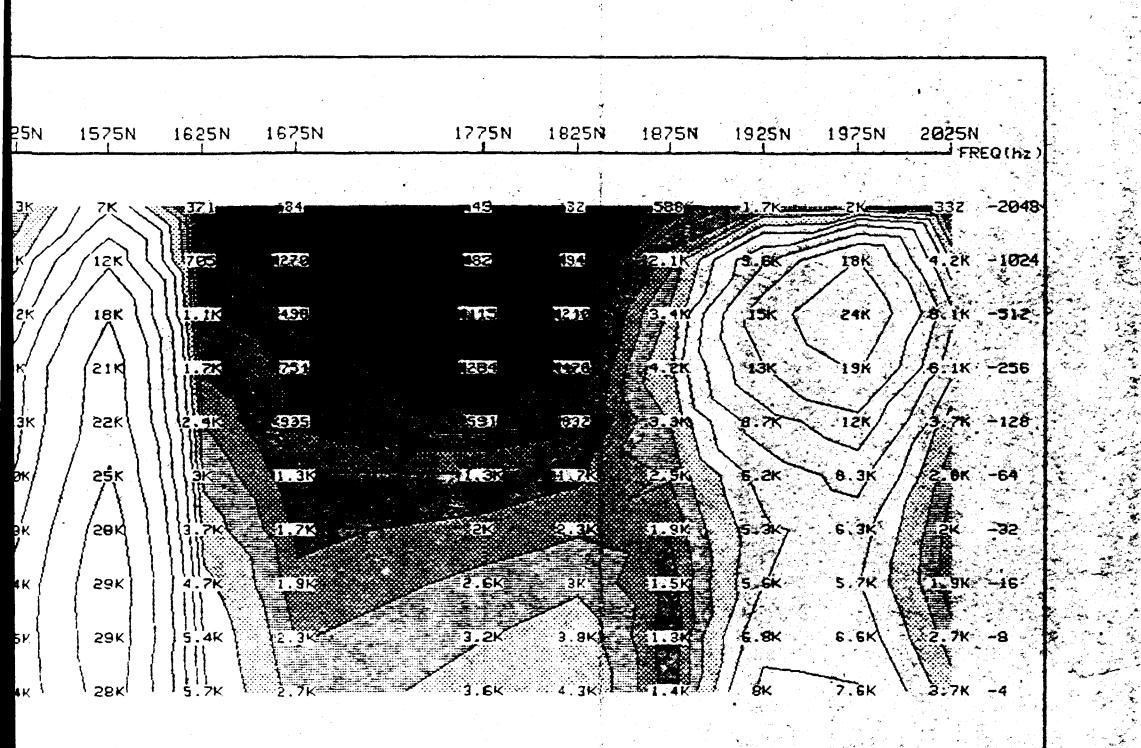
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									7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2				
		25N	75N	125N	175N_	225N	275N		375N	425N	475N	525N	575N
	FREQ()	ע די			•								
1961 - 1985 - 1985 - 1985 1986 - 1986 - 1985 - 1985 1986 - 1986 - 1986 - 1986 - 1986 - 1986 - 1986 - 1986 - 1986 - 1986 - 1986 - 1986 - 1 1986 - 1986	2048-	14 <u>K</u>	15K		1.6K	3K	- 3.3K		.553	635	604	272	487
	1024-	38K	38K	253	3.3K	5.81		f / f	1. 3N	1. IK	894	1489	693
	-215-	33K	34K:	- 255 · ·	3.9K	7.3K-	7.7K		1.9K	1.46	1.2K	543	951
	-256-	34K	39K	1324	7 (5, 9K	9.5K	9.7K	$\left\{ \right\}$) 2.9K.	ak	1.7K	762	1.4k
		201	29K		5.8K								
	120-	29K	234		J. OK) 9.1K	9 .3 K		3.41				
1	64-	Sak	281	464	6.3K	9.6K	9.5K		3.76	2.96	2.78	1.41	2.5K
					1//								
	-35-	ЭВК	20K	720	7.5K	11K	11K		4.1 <i>R</i>	а.эк	- 1K	1.68	💥 2.9K
													1-1
	16-	30K	27K	973	8.5K	12×	11K \		4.8K	لي €.9	3.6K	(1.9K)	3.5K
			27K		11/		·						/ /
	8-	29K	27K		19.6K	13K	12K		5.5K	4.7K	_4.4K	/ 2.4K= (4.4K
	4-	30K*	25K		8.6K	<u> </u>	-9.6K		4.24	3.5к	3.14	1. 6K	× 3K
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	l principalitation de la companya de												



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	an si												
94	55		525	355	500	24642	424	3	498	576	2425	1851z.	
245		1522	1340	-481	737		354	33	616	318	575 1).4).4	
								10					ŧ7,
66		1576		<u>(</u> ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					87.1			2.16.	[]/
83	1468	215		7755	REF		•		1.31	I SER .	1.5%	3.41 9	
1 <u>6</u> 2	er-F	UEE	776						1. 58	745	1.9K	4 4K 1	
				IN IN A		EKC K		2K	2.16		2. 3K	4.3K1	1
78		HEIEX	1.4K	STREEK S	3.16		2.2K	<u>.</u>	- 2MAK-	2.6K	2 + + 2.5K	5.2K1	11
													1.1.
	3 1.5 4	1.94					Y.		2.8K		2.9K	6.2Ki	
7K	31.9P	2.3K	2.28	2.6K	4.4k	5.2K.2	3.2K	3 (3.3K	3.3K	3.24	6.7K1	
			2.6K	3.14	4 34	5.48.5	1 3.5+	3 <	3.5K	3.5K	3.4K	6.8K1	
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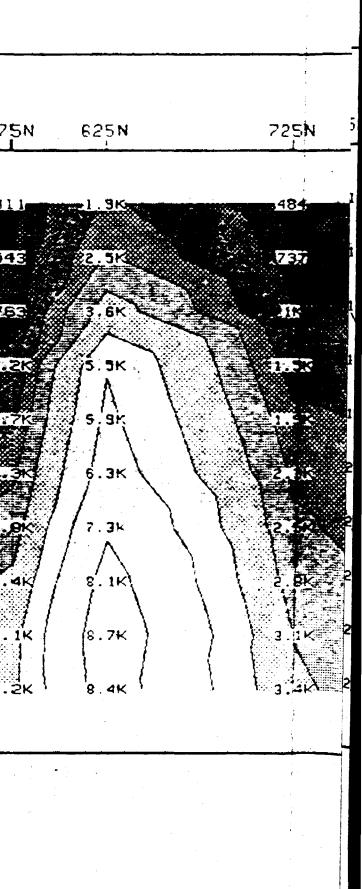
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25 FREQ(hz)	· · · · · · · · · · · · · · · · · · ·	125N	175N	225N	275N	375N	425N	475N	525N	575
2048- 1.	1K 1.5H	(Z.1K.		1.5K	1.7 Kita	332	255	
1024- 1		ZGK-	2.96.	2.6K	2 . .7K		8.8X		8628	*54
512-2.	xic= <u></u>	3.7K*	46	<u>3.9</u> K	<u>9.1</u> K	2.96		616	2427	75
236-4.	5K 4-91	6.2%	6.4 K	6.1 K	6.3K	4.85	5.5k		531	1.2
1284 5.4		6.9K	78	6.5K	6.7K	5.5K	6.3K			
64 - 6.	۴K <u>6</u> , 5)	K 7,5K	7.6K	-7K	7K i	5_9K	7.1K	2.4K		
			9.5 K	7 .5 %	?.BK 】	6.6K	- 8 - 41X	13. JK		
16- 8.		~~~		9.1K	8.5K	7.3K	9.5К \ 10К	3.9%	2.74	3.4
8- 97 4- 18			10K	Э.3К	8.9K	7.7K 7.8K	10	4.9K 5.1K	З.4К 3.6к	4.1
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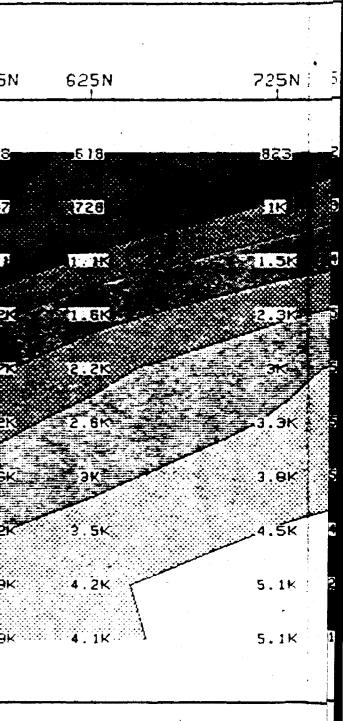
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		CSAN	MT RPP	ARENT RE	SISTIVITY (C	CORREC	TED)	<u></u>			 			
LA 775N	C MINER	RALS LTE	D. C14 925N	LINE=8758 975N	E E-dipol 1075N	1 e= 5000 1 125N	1175N	×=10.62 1225N	5km 1275N	1325N		1425N	1475N	15
522	325 -	437	279	475	2.1K	645	357	782	590	290	8	1 7.1K	15K	
760	727	573	1363	261.6	1.4K	910	DEE	912	ट्राइ			бк	17K	Í
	972	7755	7185		¥.7X	1.2.	न्हर		335		4	7.36	2000	
	J.A.A.K		26.3	RIE		J.C.F.		18K		TTE		8.8K	22K	1
.1.7K	1.76		046 	JERT	WK	त्विम्स र	116 -12	7 48 975	11 95	327		8.5K	23K	j,
2X	enk	erez	ALC: NOTE: N	1051	Jan X	2.9K	2.44	3K) -	2.44			8.8K	27К	*
3.16			. 375F		y	3.5		5. 3. 7K .				100	30K	~
2.2%	- 22 rik- 	2.74V 2.74V	31831C		4. 7K	-4.3K	3. <i>7</i> ×	4.5K	3.76			11K	31K	
2.5K	3.2K	73.3K	2.3K3	23.1K	5.4K	5K	à.śk	5.3K	4.4K			12k	31K	i
ma∑ ' PK	₩°₩7 3.4 ₩.57665	а .5 к че 5	Surveyed	Pesistiv by OUGNTECH	Solution of the second	5.2K	<i>₄.9</i> + 387	5 3K ∖	5.16	resona 1 Guno rez	- A I I	1 12K 1	1 32K	ē
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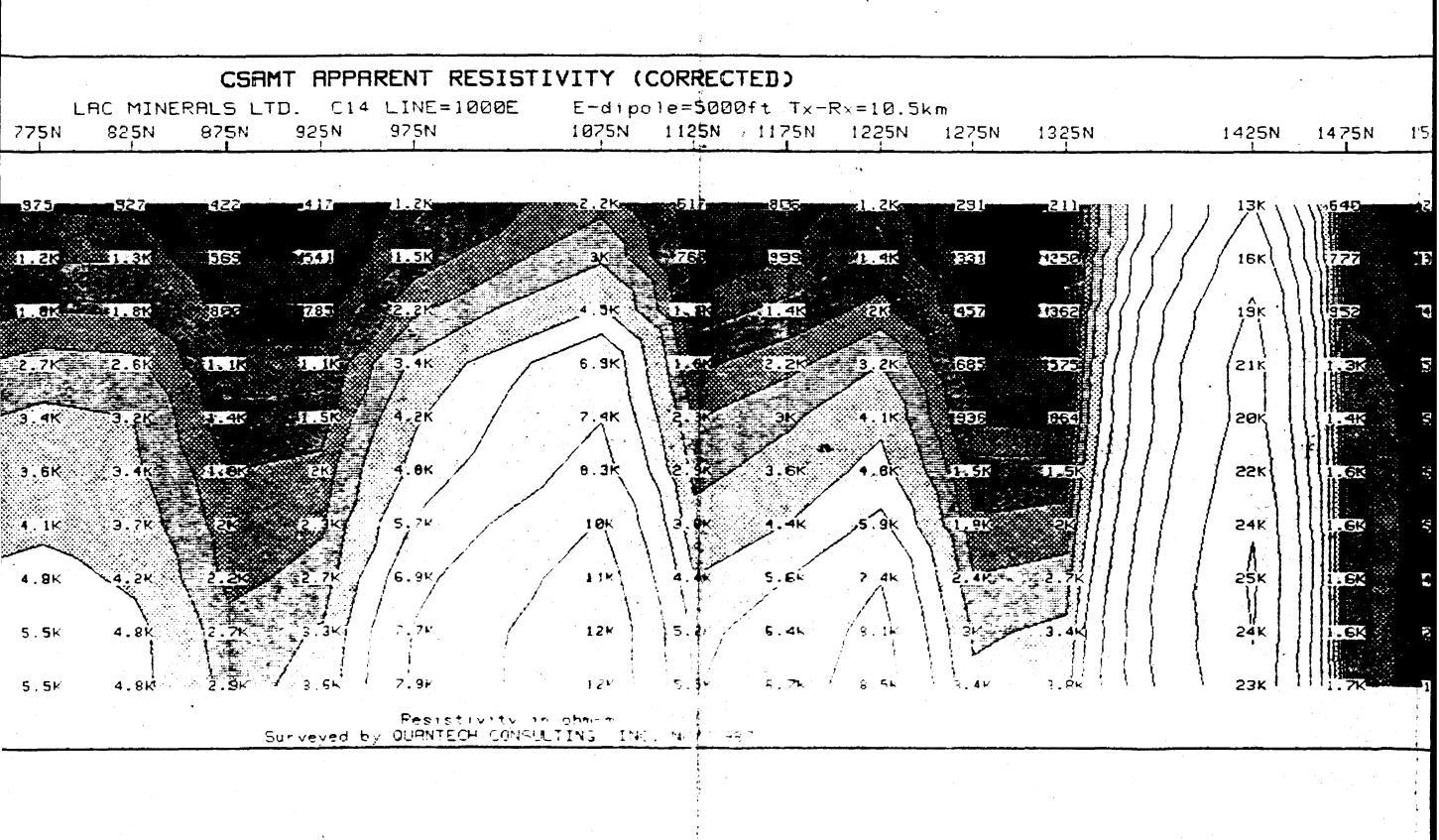
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		· · · · ·			- 	9 4		
	1575N	1625N	1675N	1775N	1825N	1875N	1925N 1975N	2025N
		436	741			ł		
1			24)	587	375,*		215 3 6K	9.3 K -2048
	552	1331	262	5.17	4.47		955 - 5 K	16K -1824
	598	5701	1354		FILE		ाजन (s. ak	15k -512
	745	1435		7.55	144	1997 1. 8 7. 1.	THE JICK	13K -256
	735	522					J. 1745 - 244 - 3FQ	5.8K -128
	956	97K			Stork			7.6K -64
	1.16			3.7 K	5. SK			
	-11K		1. SK	्र इ.	с. 9К. С. 9К.	С. АК 		4.6K -16
	1.1K	1.94	1.eK	2.4K	3.5K		3.58 11.38	3,3K -8
	1.38	2.3K	2.2K	2.8K	4K *	3.74	4.2%	2.6K -4

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25N FREQ(hz)	.25N	125N	175N	225N	275N	<u> </u>	375N	425N	475N	525N	
2048- 455	502	785	14.3K	5.18			- 1 - 5km	2K-	53}	35.8	
1024905	1.7 K	11.5%	(7.2K-	8.2K	(2.9 <u>K</u> *		2.5K	2.96	3 <mark>851</mark>	438	
512- 4.JK	2.8K	2.4%	(izh	-19K	5.1K		3.9K	4.4K	31.3 K	63 1	
-256- 2.7%	4.9K	4.1K	15K	16K)7. šk-		6.5K	6.9K	119K		
128- 3.SK	5.4K	4.7K	15K	17K	6.5K		6.9К	7.1K	2.GK	41.3 K	
64- 4.1K	6.1K	5.24	16K	18K	9.4K	and Second	7.6K	7.5K	2.9K	21-0 K	
- 32- 4 .8K	7. 1K	EK	17K	20K			9K	8.6K	3.2K	2.271K	Z
16- S.SK	7.7%	6.7K	17K	50K	12K		.a.ak	9.3K	3.76	*2.4K -1	
8- 6. IK	8.2K	7.1K	184	20K	13K		111	9.9K	4 3K	Y3K /	
4- 7.3K	9.4K	8ĸ	184	20K	13K		11K	9.7K	4.26	3K	

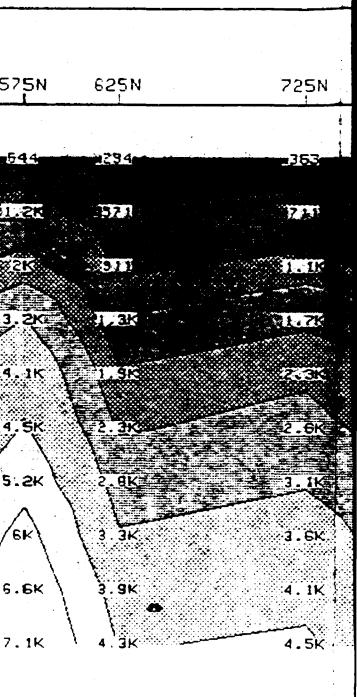


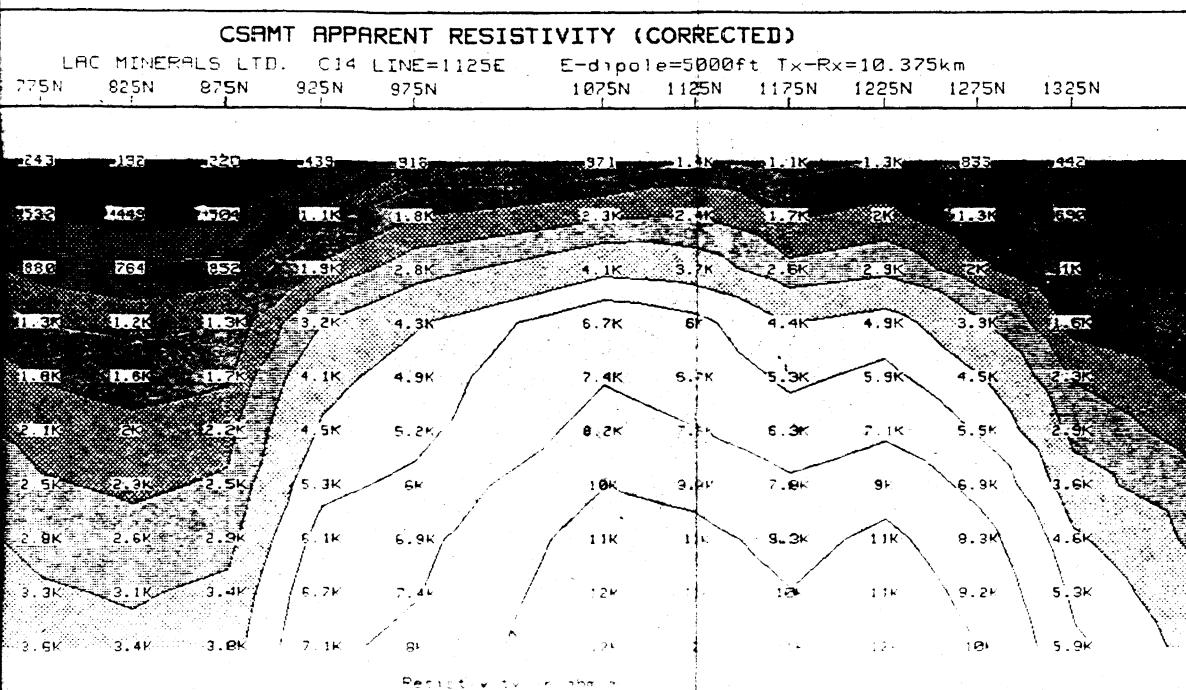


25N	1575N	1625N	1675N	1775N	1825N	1875N	1925N	1975Ň	2025N
	¢ 1								
34	285	693	583	385	563/	318	421-0	.757	200 2048
31	1335	1955	7710	466	8377	(RSE	-18.53.5		11.1K -1024,
21	THE PARTY	- 31.2 AK	9.15	634	B67	AZE			1.3 K -512
	1528	्र गाइन्स् र	1.2 K		I. K		- 733	FREEZE C	1.74K -256
(2)	2532	U.GK	₩1.4 K	315-91					5K -128-
	-486	1575	AT A SEK	41.64	1. AK		TE IN THE	TLGK	₩
	154.0	1.5K	1	≈1. <u></u> si≮	.I.S.				SK -32
æ	7450	2 41.3 K	11.7K	2.2.	LAK	Neak	E.S.		1.5K -16
	1317	1.1K	1.9K	2.66	-11.4K	2.31. SK	1225	2.02	€1.5K8
67	188	1.1K	2.1K	3.1K	1.5K	2K	2.3K	2.4K	7K -4

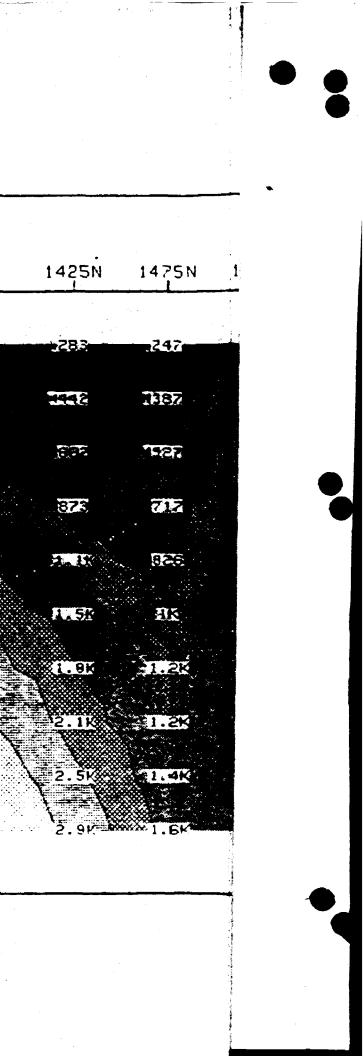
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	с. н. 1. с. ж.										
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	<u> </u>	 	<u> </u>			· · · · · · · · · · · · · · · · · · ·	· · ·	·			<u></u>
	25N 75N	125N	175N	225N	275N		375N	425N	475N	525N	ł
FREQ	(hz)					· · · · · · · · · · · · · · · · · · ·					
2048-	55		935	2. 4K	2.3K		52	235	336	376	
	488 2334	1255	5.6K	15K				295	642	A.ak	
	1.88		16K	29K	21K		1449.5			1.6%	
312-									• 1 2		
) - 3 56- 2	3.9K	1.8K	20K	35K	24K			Jork II.	1. SK	2.3K	
n († 128-	4.6K 34	2.6K	20K	Эбк	24K		1. TT	3.967	-mec	ЭК /	
64-	4.8% 3.3		2 JK	35K	24K		1. EK	4.2K .	2.3X E	3.2K	
32-	5.8K 4K	3.84	236	36K	25K				12,7K	Э. ек"	1
								/	廖		7
16-	6.5K 4.6H	(4.5K	22K	35K	25K		2.26	5.4K	3 5	4.11	/
8-	- 7K 5.2	5.2K	22K	331	24K		2.7K	EK	3.5K	4.6K	(
4-	7.6K 5.6H	5.7K	228	32K	2 3 K		3.2K	6.4K	3.9K	4.8K	/
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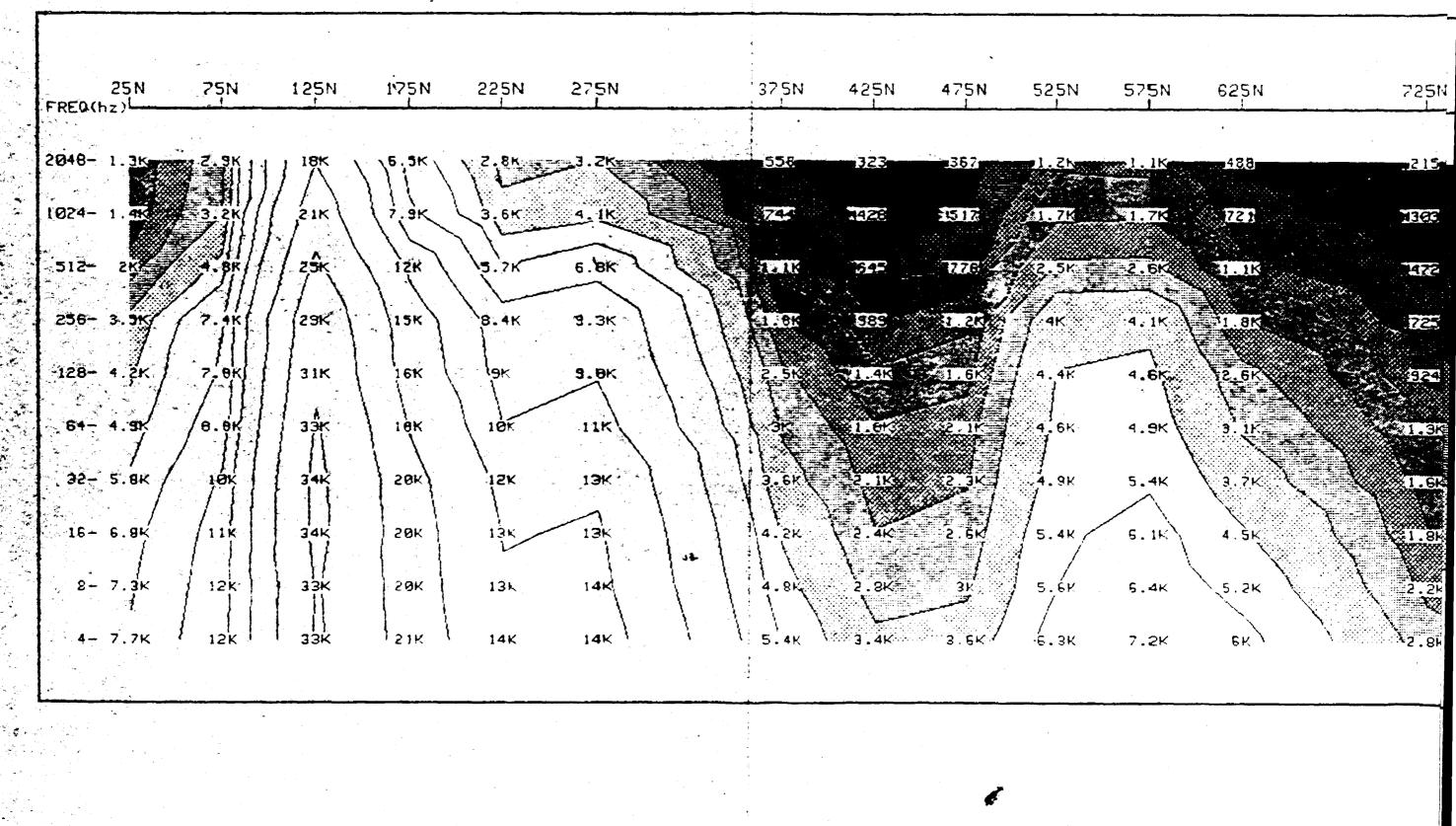




SURVEYED BUIDDANTECH OCHSULTEN . INC. MA 1920



525N	1575N	1625N	1675N		1775N	1825N	1875N	1925N	1975N	2025N
617			55	49	114	.225	203	G 17	170	3 92, -2048
1.1K	(7,5K	1.6K	11-26		अवस्	1392		<u> </u>	19398	681
1.5 K	1119	2.7K	1 		<u></u>	1772				511 -512
NB	12K	4.2%	0 228			<u></u>				7.6K -256
2. IK	10K	4.6				272.	a Car			<u>ск.</u> –128
2.1K	ө. 6К	4.7K	100 EX4-							2 18 -64
1,9K	BK	ş.3K	105		1.	36	e v	\$7.5 J		SK - 35
1.7K	6.9к	6.1K	(321)		MES		FEE			2K16
1.7K	6.1K	е.ек	2272 2		(JE)	2459	536			2K -8
1.8K	5.6К	6.9K	\$885 •		317-		454	894	1.26	₩₩₩¥2.2K -4



2 2 							- - -							
LF 775N	RC MINE 825N	CSAN RALS LTI 875N	1T RPPA D. C14 925N			VITY (C E-dipol 1075N	e=5000			km - 1275N	1325N		1425N	1475N
179	233	353	554	9.2K			1.24	3	2	7	115		475	536
1267	1389	III	1. 1K	15к			33	22	10	141	172		741	312
1395	1520		IV: DK	216			ग्रहत	æ	193	IF	2		F.F.P	
594	352		12 . 4K	25K		17	9.2K				हरस		1.3K	1.58
228	655	1.56	2.94 1995 - 5	26K		JE	F A A 5.9K	526					1.6I	2.48
IK	1.38	1.6%	3.1K	28K		E S	6.00	D ECK	555	THE	1361		n-sk	
I.	S1.4K		3.4K	30K		DZE MA	9. GR	12.2X	1.2K	219	ाहाःस्		5.56	
11.5K	21.6K	21116	73.9K	35K		440	101	3.3K	1.9K	498	1459		2.4K	73.96
1.8K	1.9K	2.5K	4.51	32K		1.214		4.4K	12.5K	s 1752	.489		2.9K	4. 6K
2.2K	2.3K	2.9K	5ĸ	32K	-	3 K	12K		, \ _{3K}	IK-	536		і <i>І</i> 3.2к	4.9K
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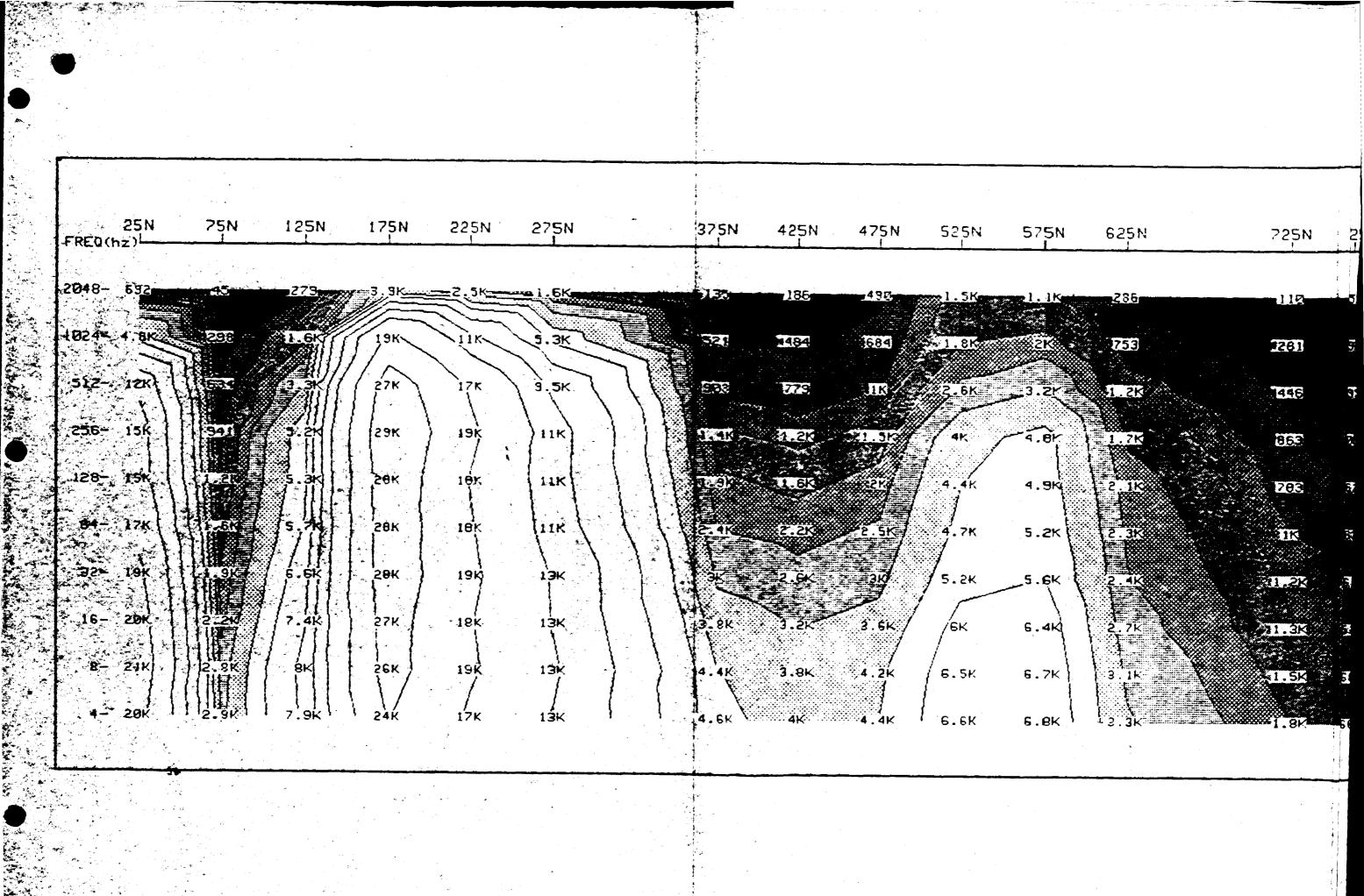
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25N 1575N	1625N	1675N	1775 1	5N 1825N	1875N	1925N	1975N	2025N	EQINZY
,		·							
31 3. ZK	-3.1K	54	154	401-1	452		1365	583	-2048
55 5K	4.8K	81	245	35972	THE REAL		598	827	-1024
6.1K	бК		1286	5 7000	EEE			S.K	-542
ятка (с.9К	6.8K		(3 4)	1 <u>703</u>			J	J.SK	-256-
.5K 5.5K	5.3K	ંગાર	1401	n 5.25	D RK			1. SK	-128
.gk 4.2K		i IIGE	13	5 059	ERS X			J98	-64
I 7									
.1K= 3.3K	EX	3 .	1257	6 (70 7)	Sector Sector			1. SK	-32
4K (2.3K	2.24	132	1255	3	835 8	1.25		12.74	-16
5K	22K	242	14 10	G <u>1500</u>	523	* E	IR	1. 6K	-8
5.4K		321	313	3-469	362	\$24			-4

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75N	AC MINAR 825N	875N	925N	LINE=1375E 975N	1075N	1e=50001	1175N		1275N	1325N	1425N	1475N	152
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Surveyed by QUANTECH CONSULTING INC. NOV/1987

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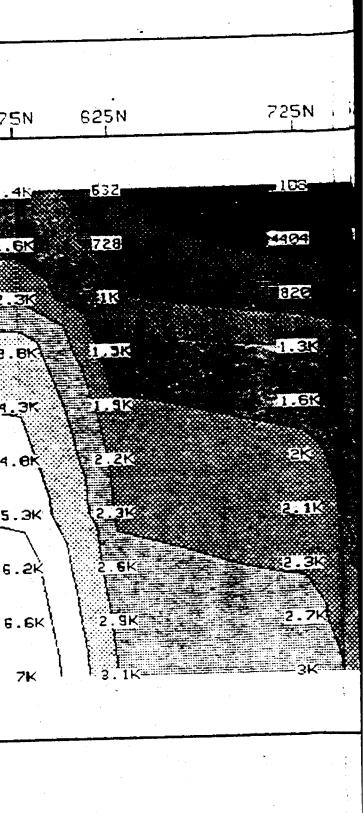
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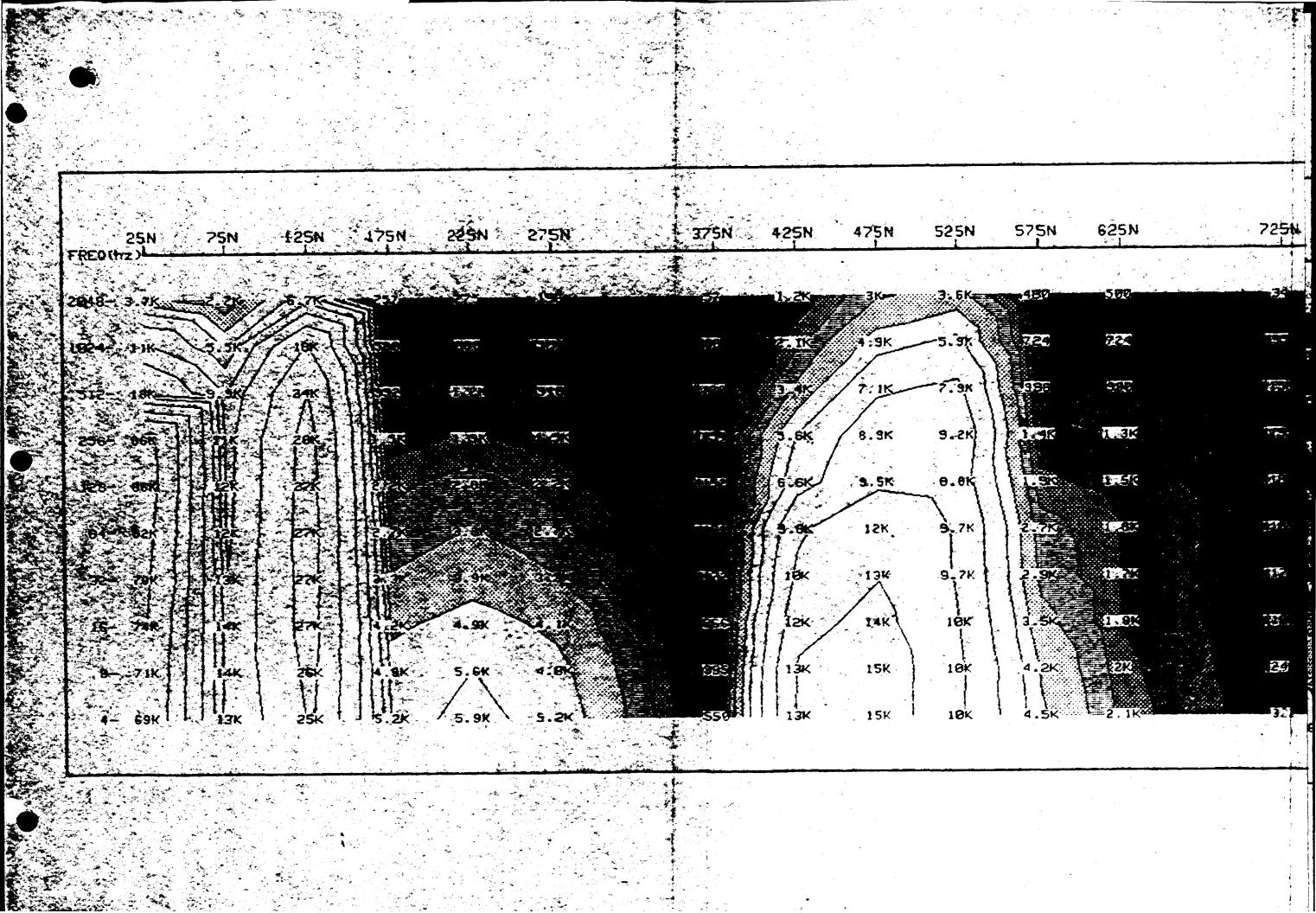
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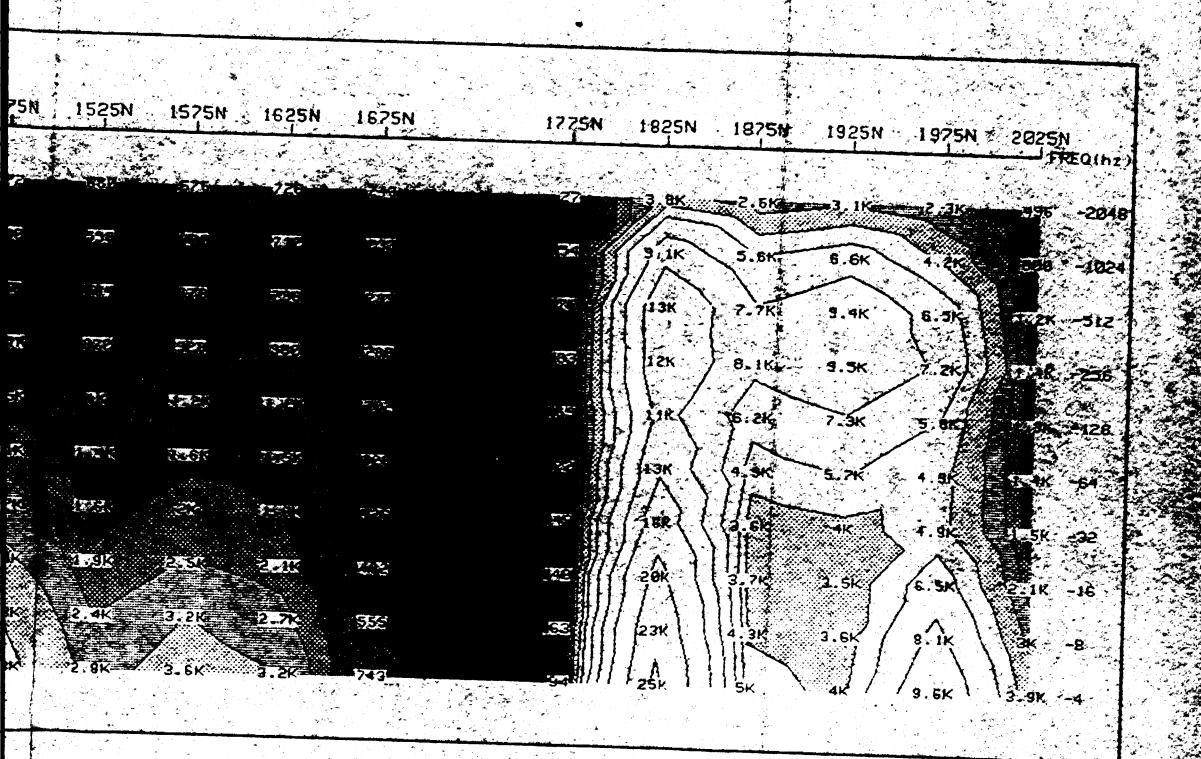
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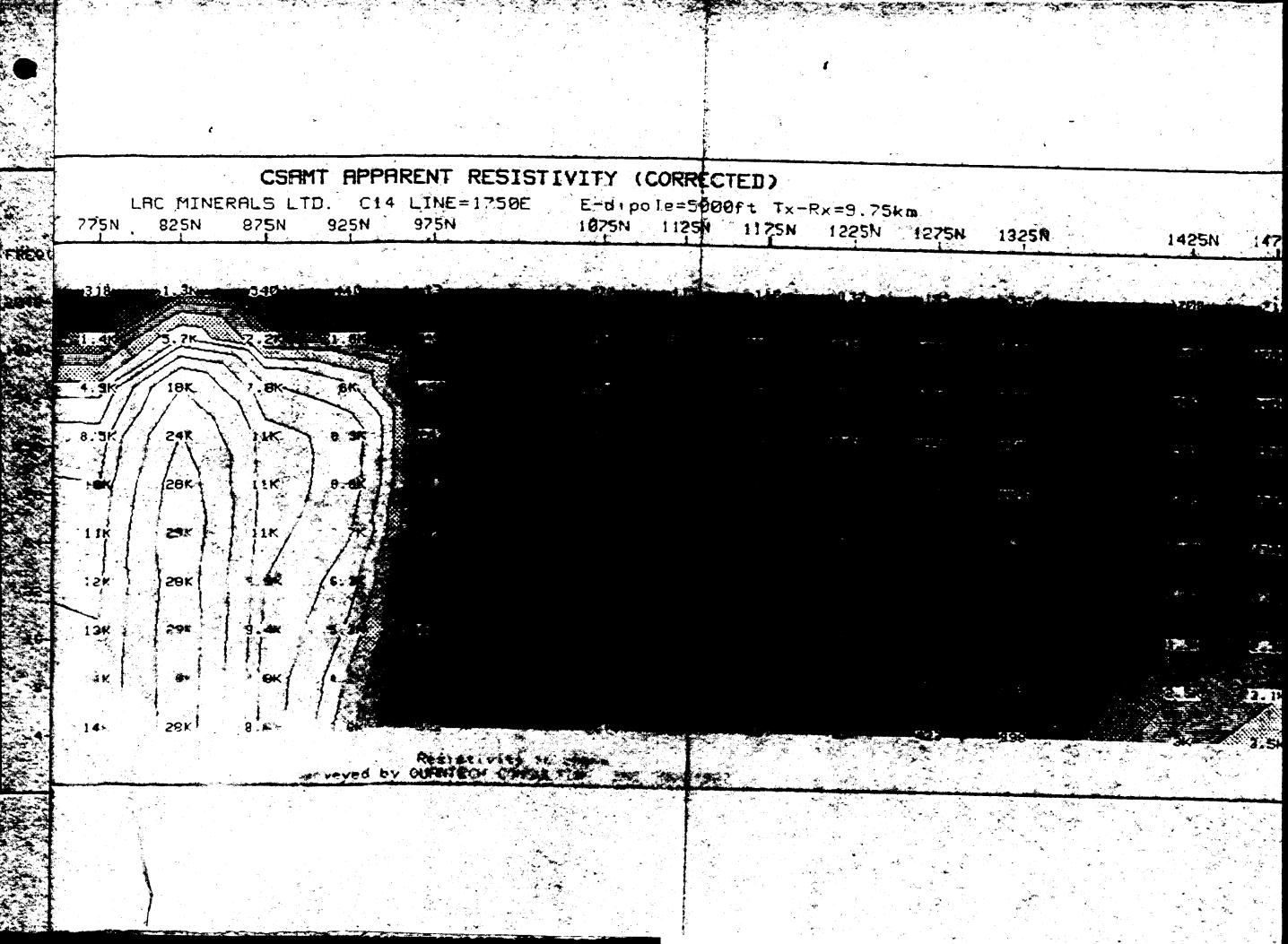
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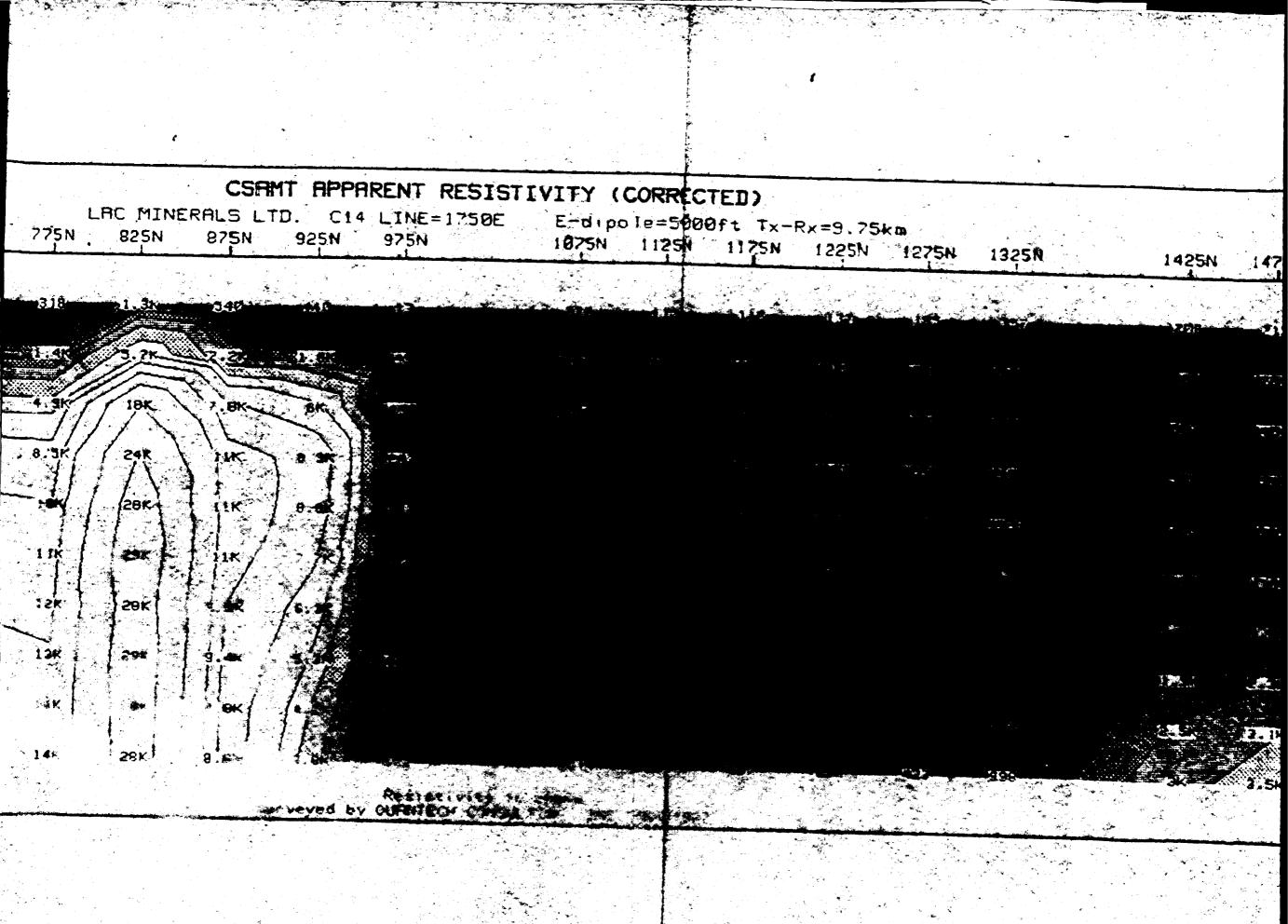


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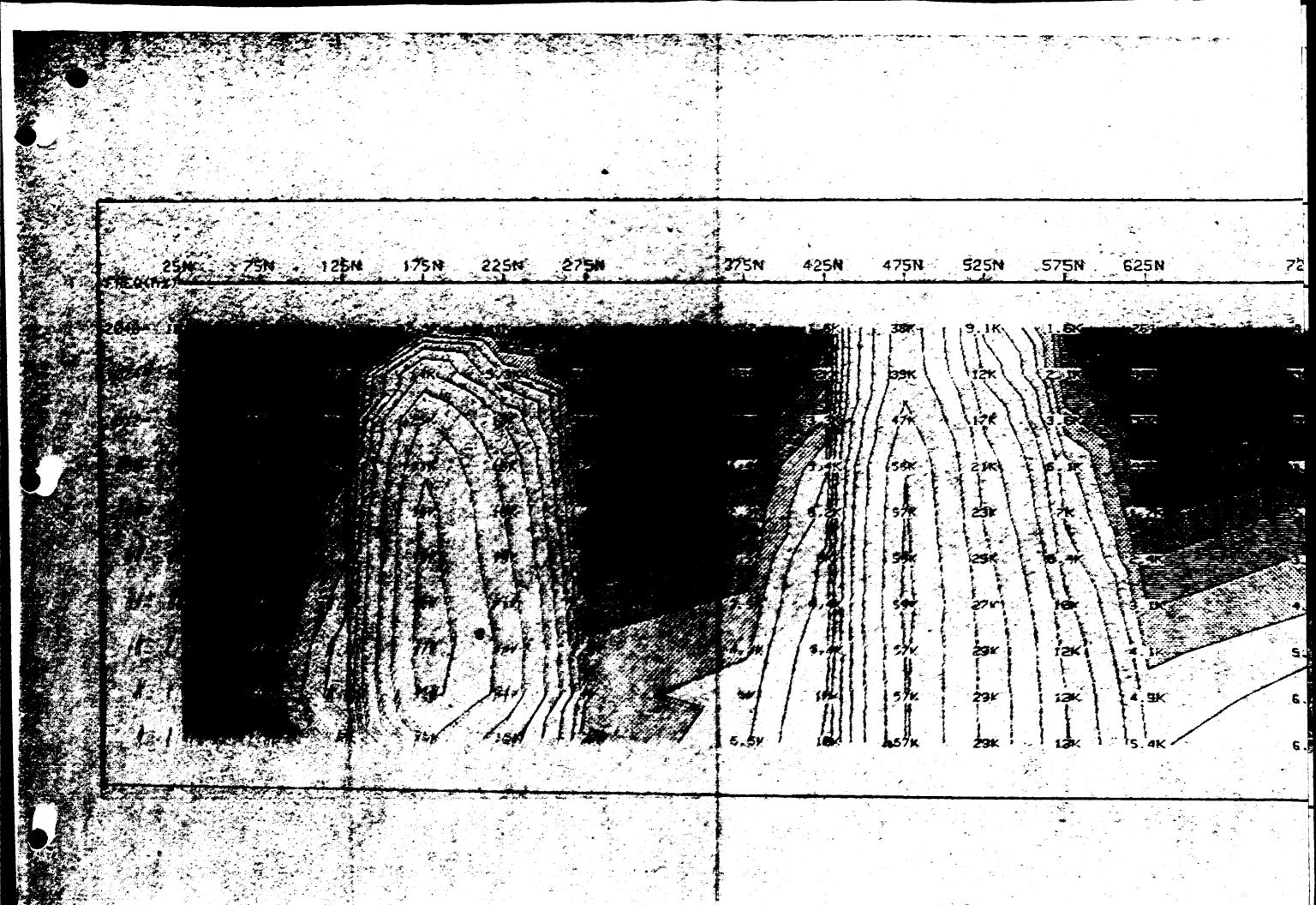




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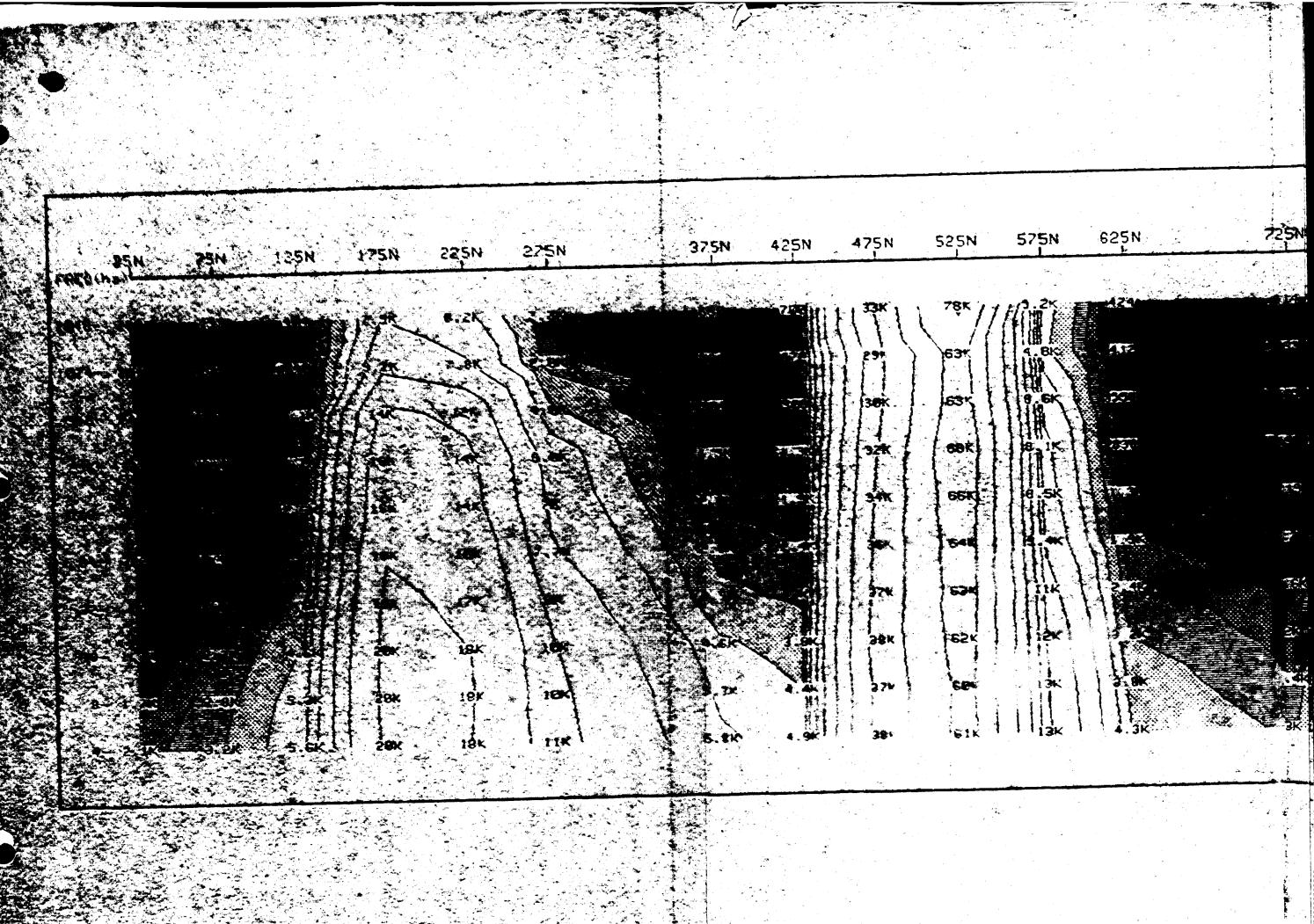
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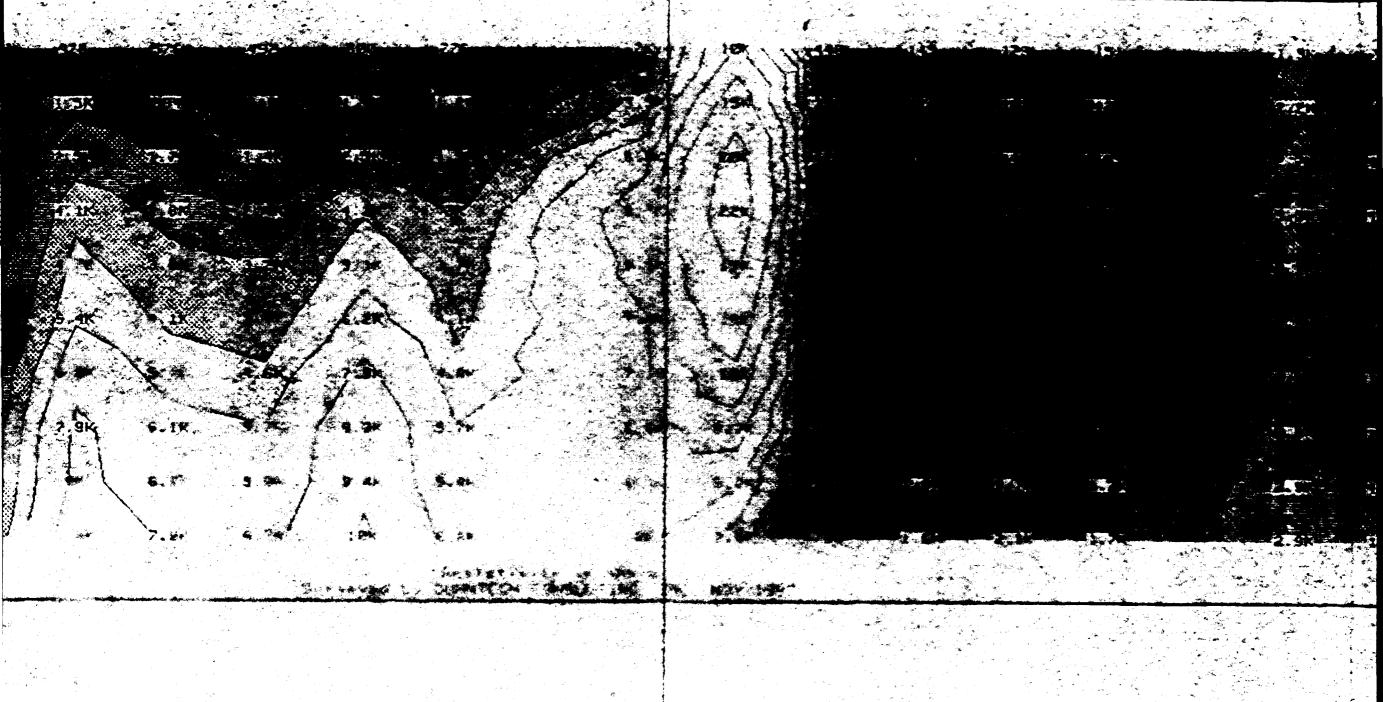
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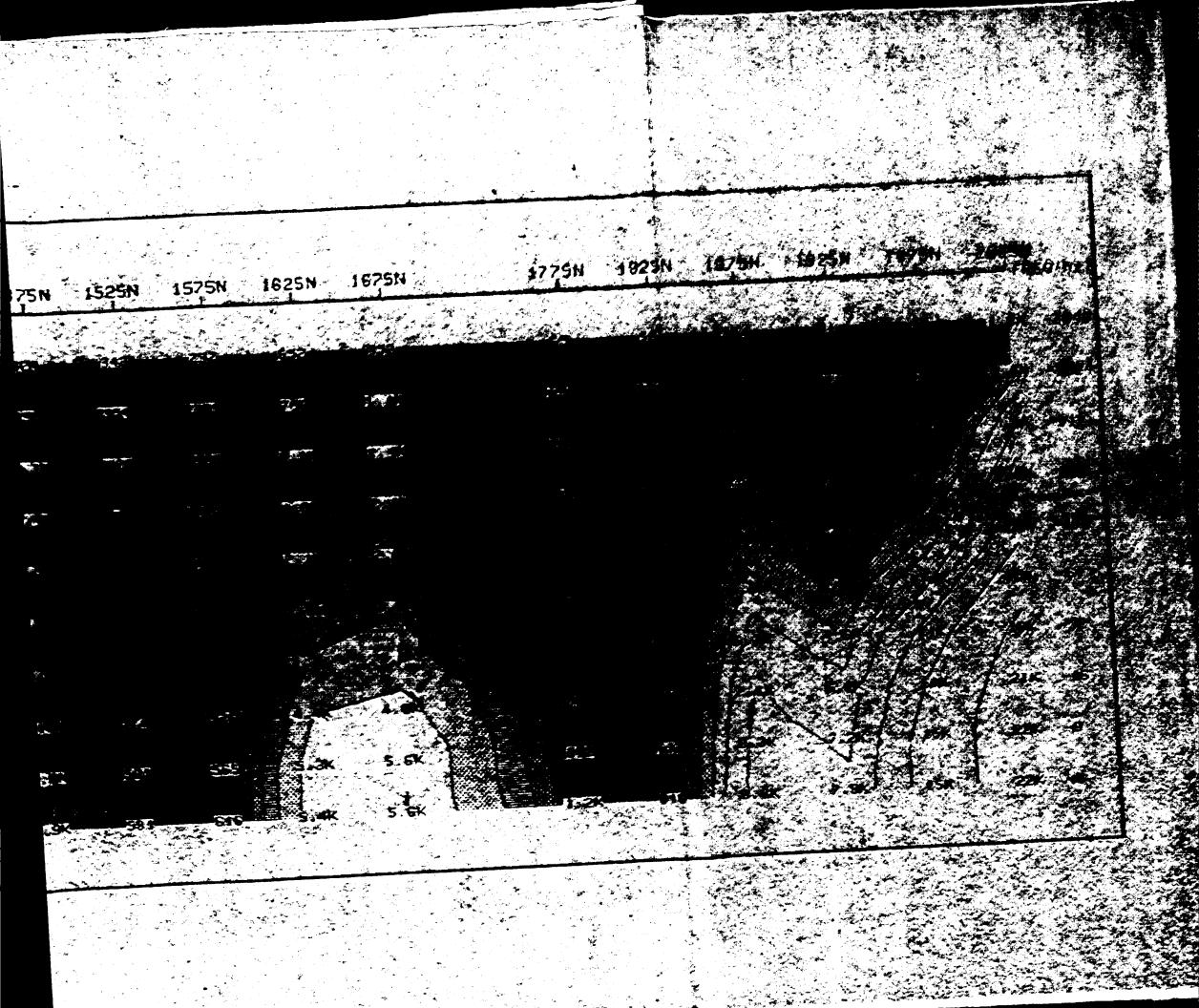
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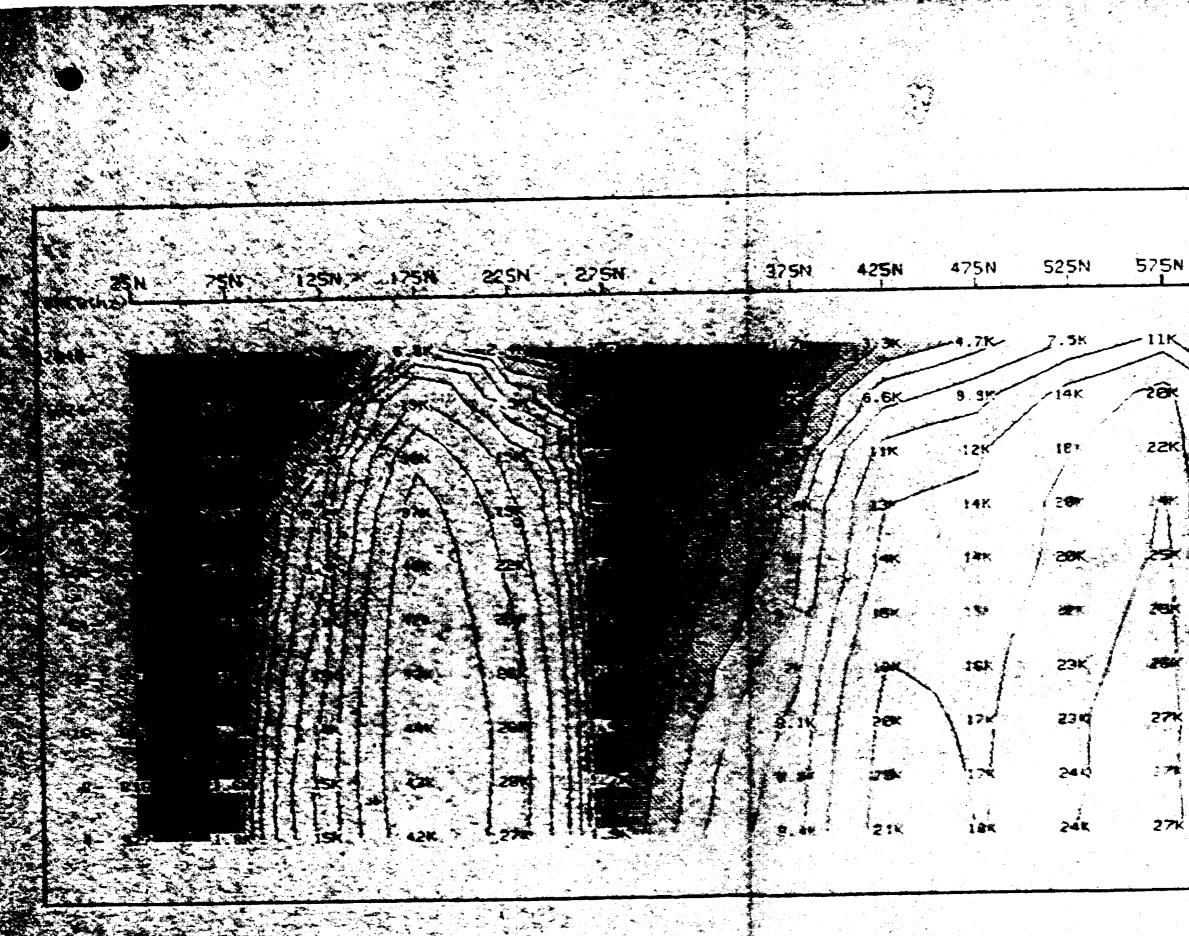


CSAMT APPARENT RESISTIVITY (CORRECTED)

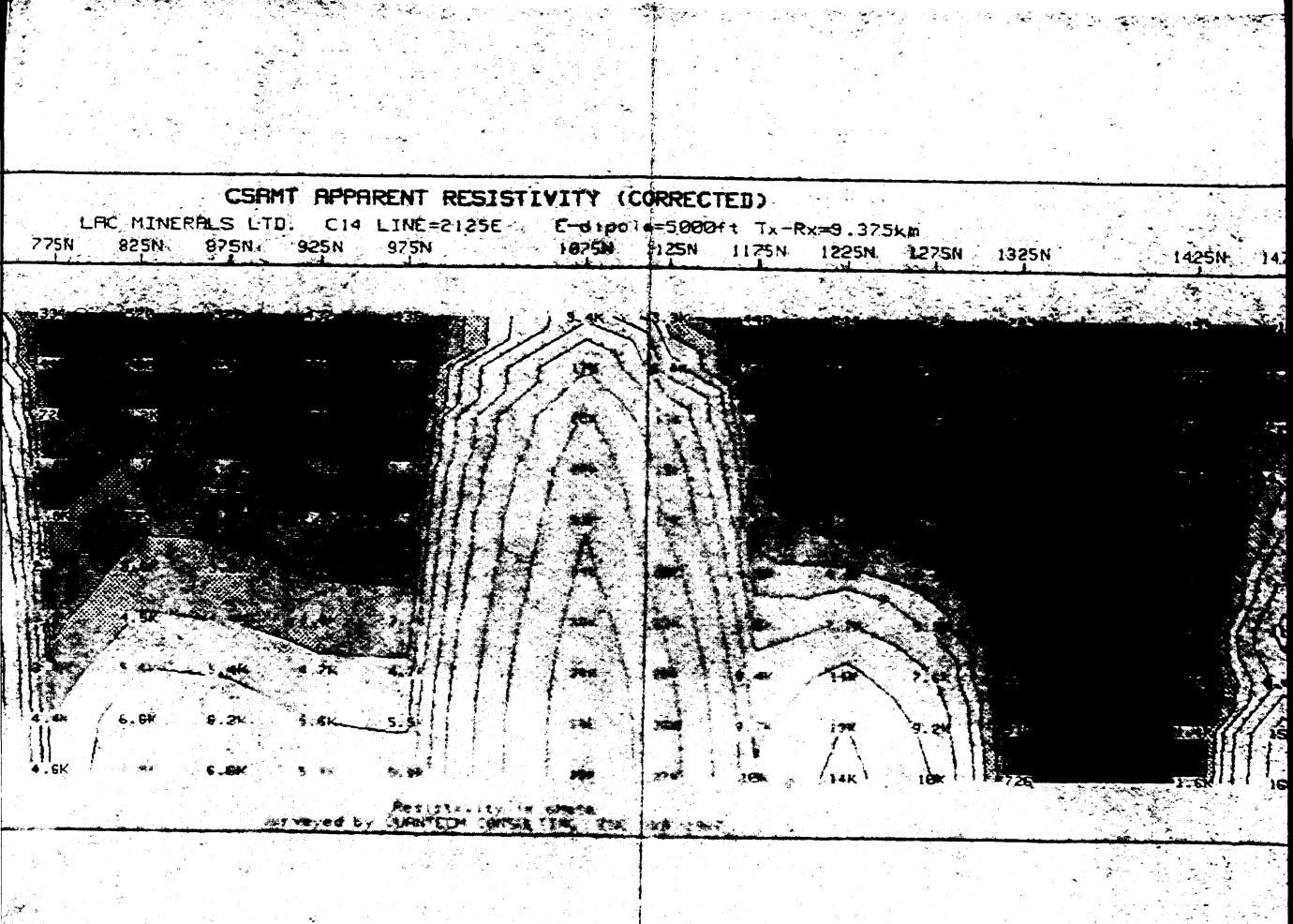
LAC MINERALS LTD. CI4 LINE=2000E E-d pole=5000ft Tx-Rx=9.5km 775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N

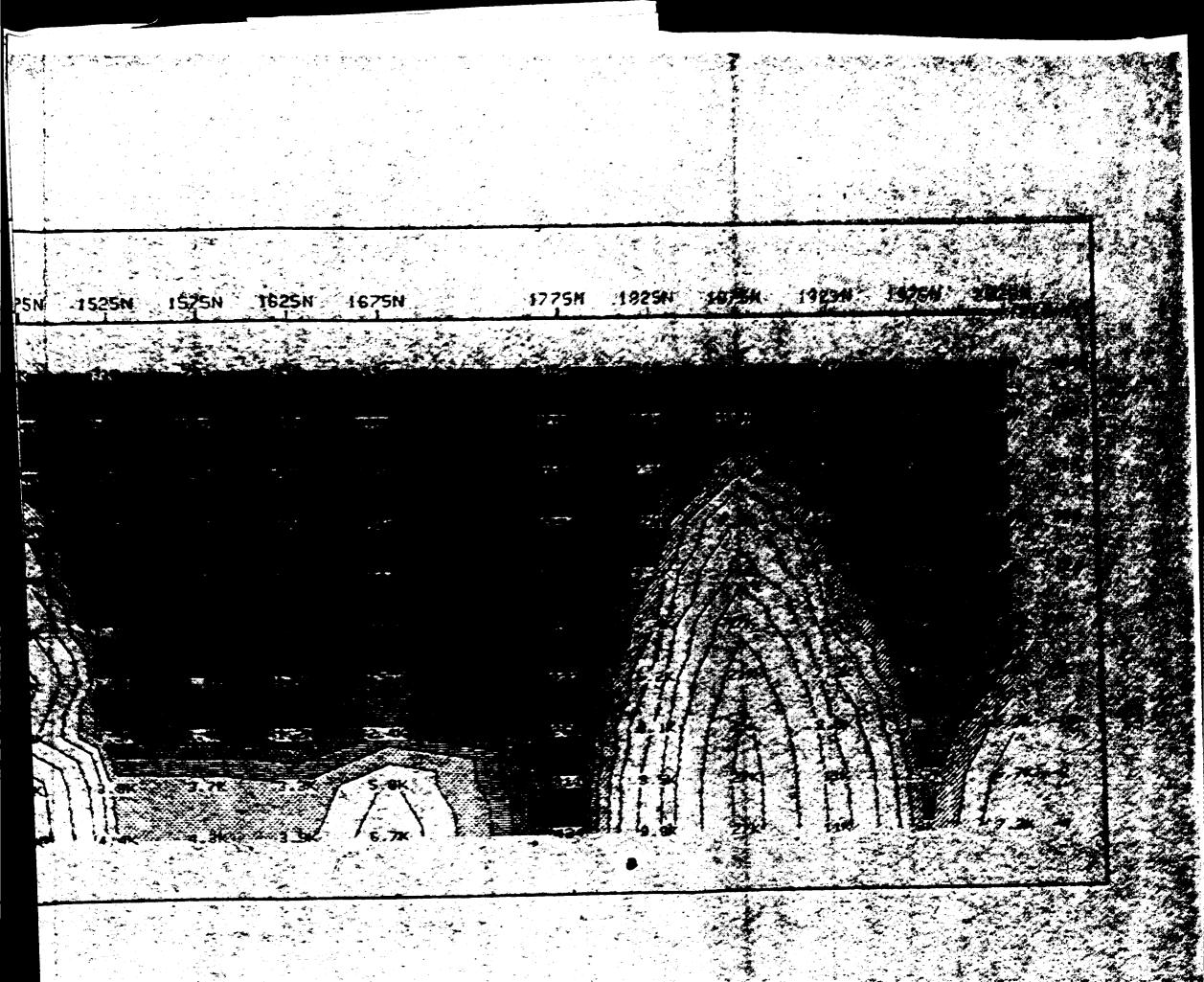


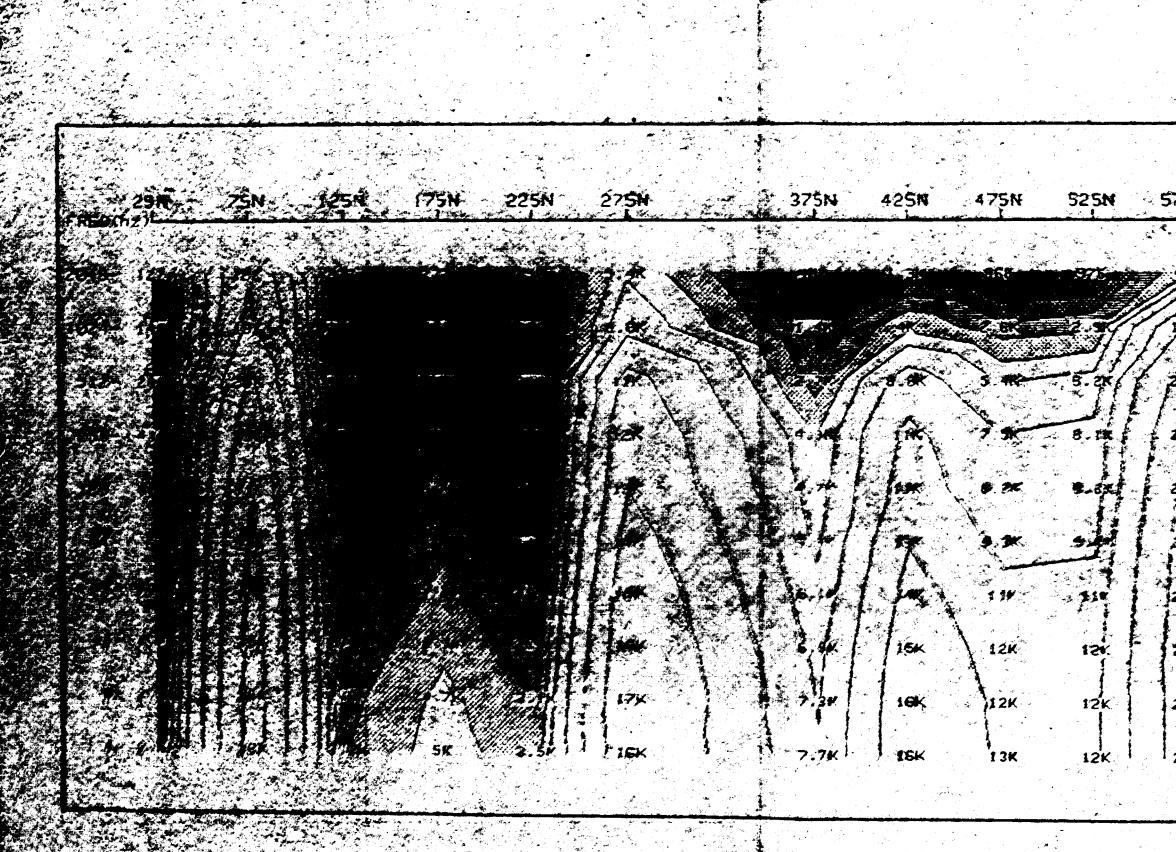


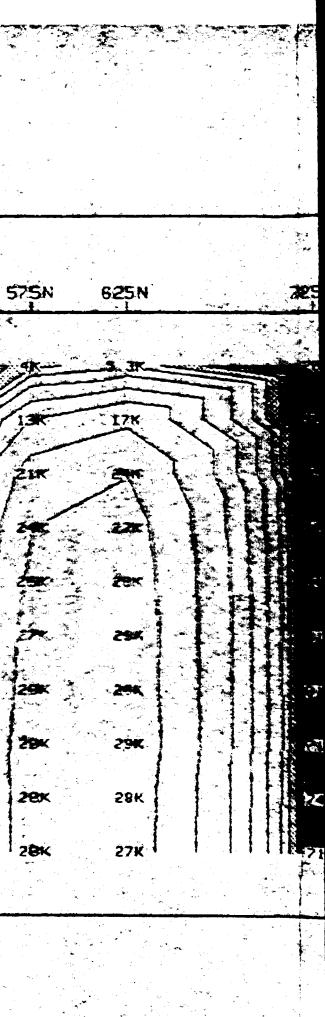


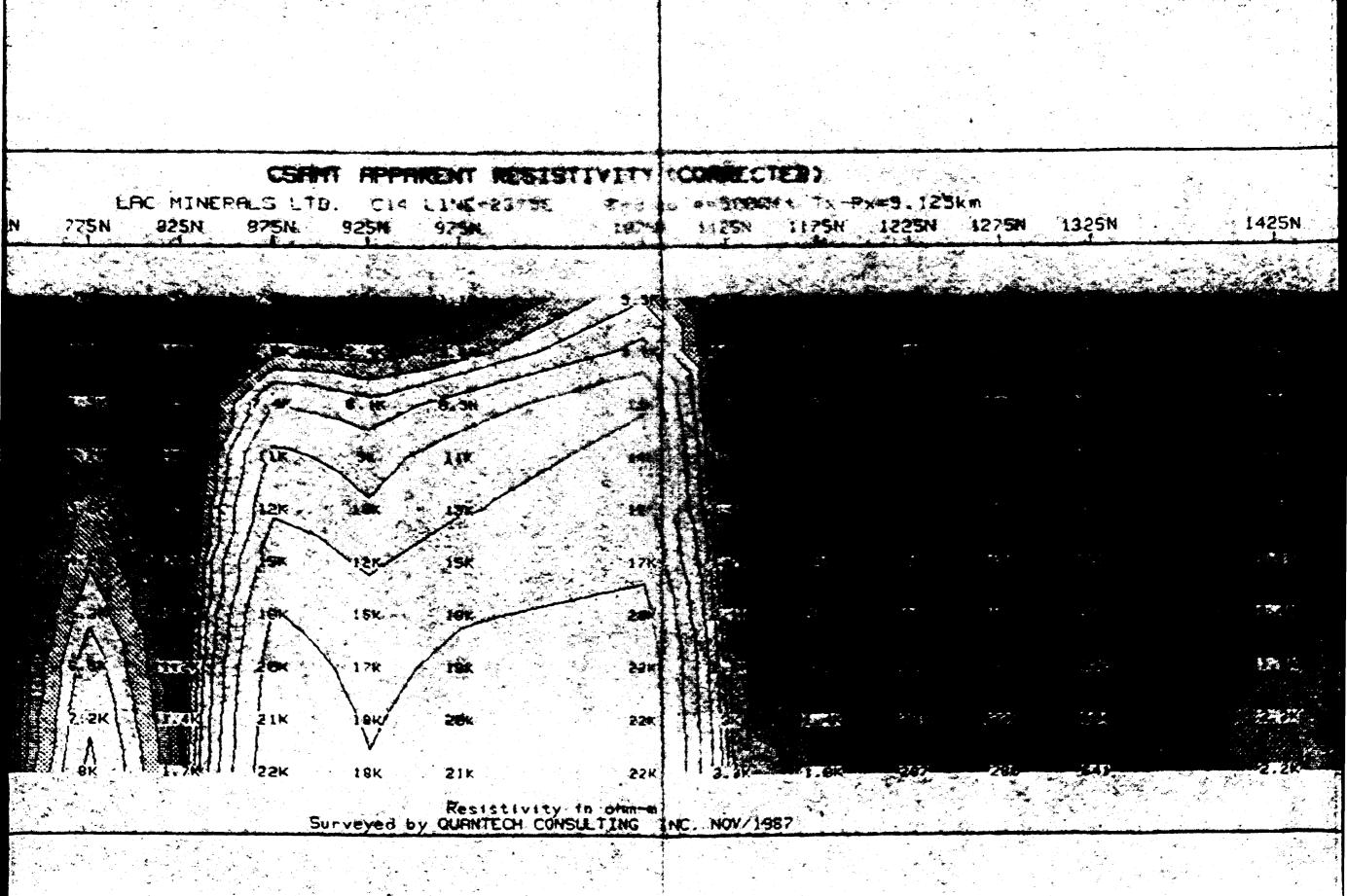
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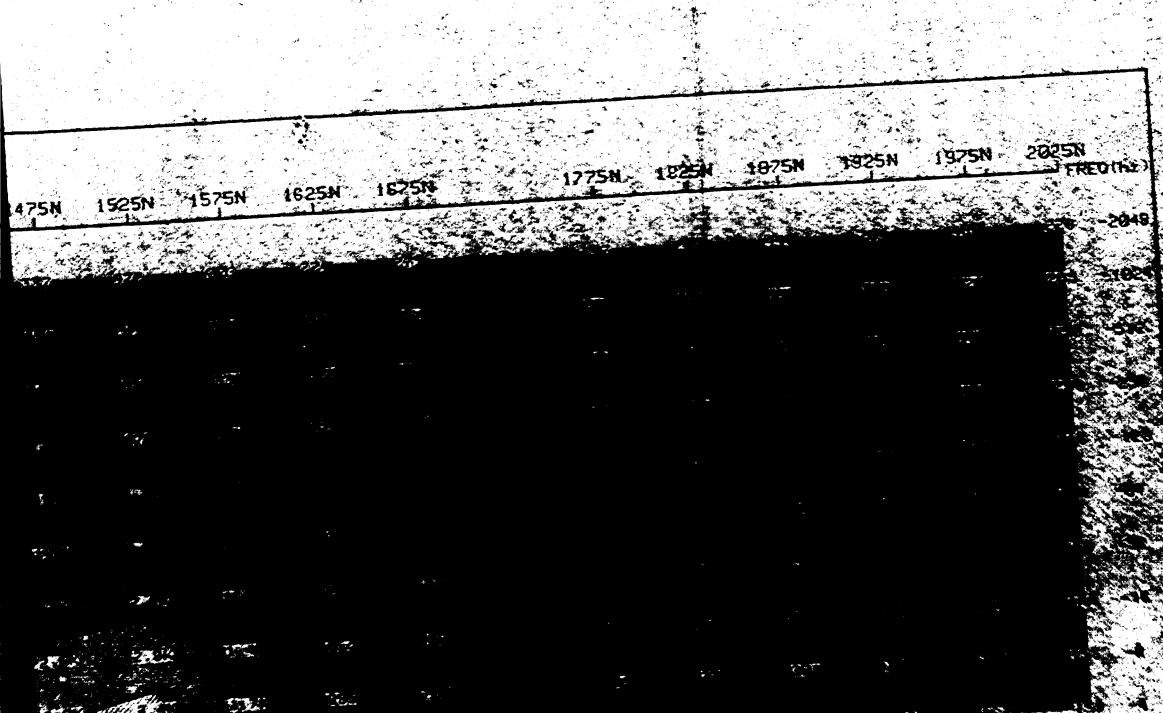


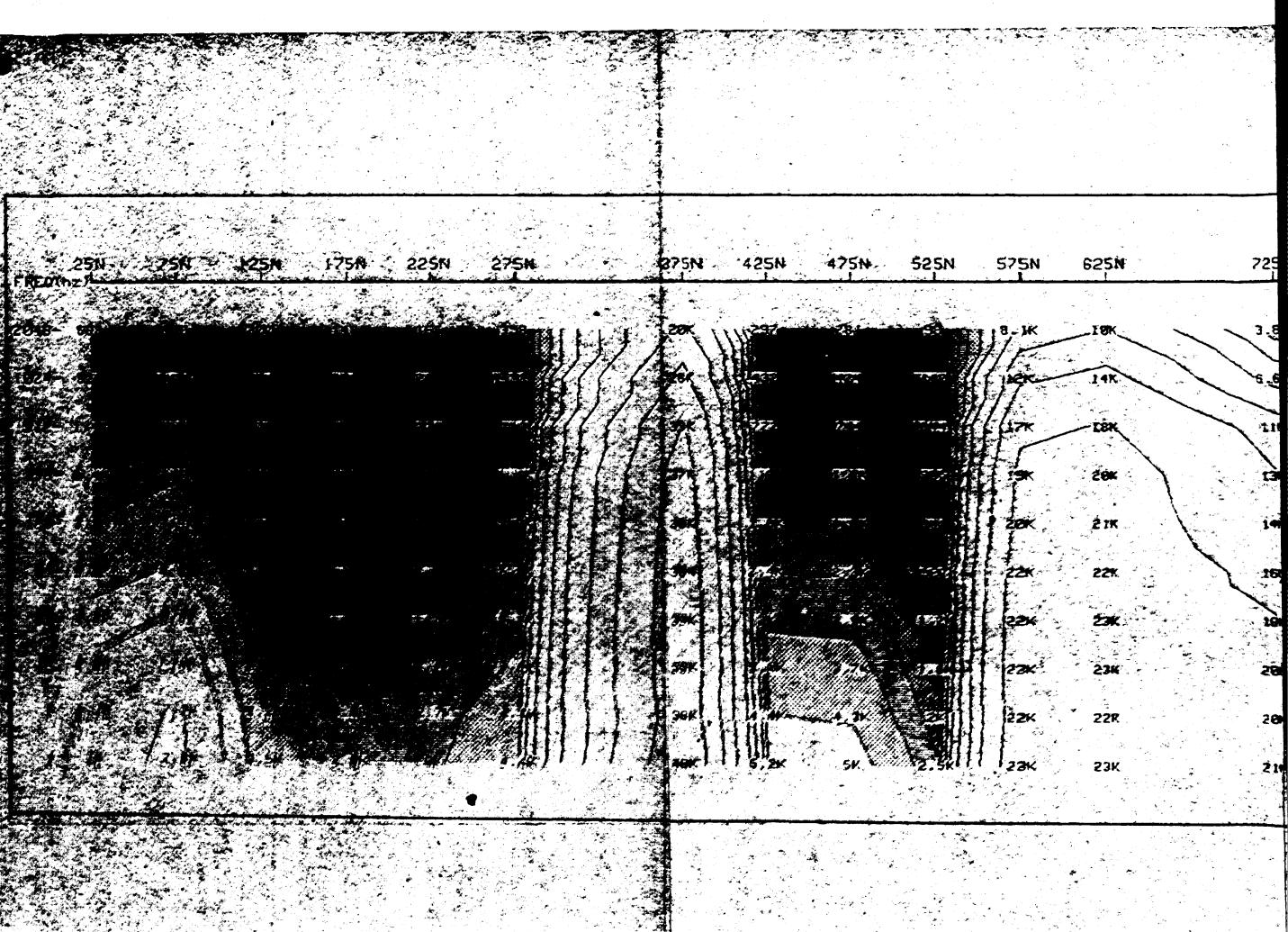






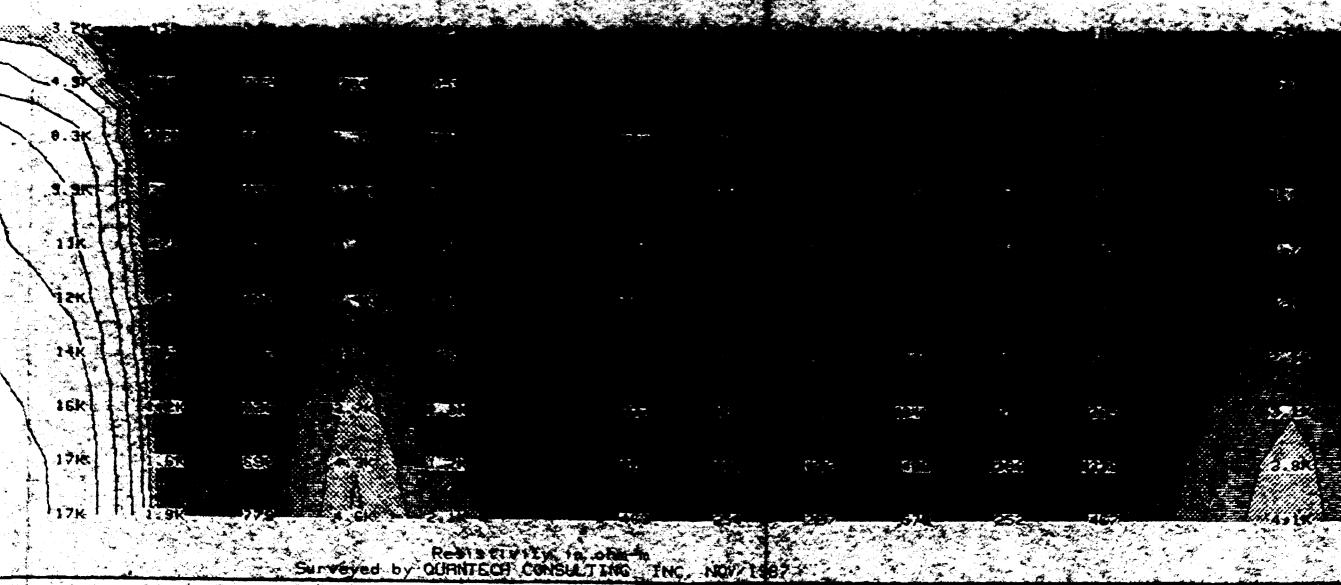


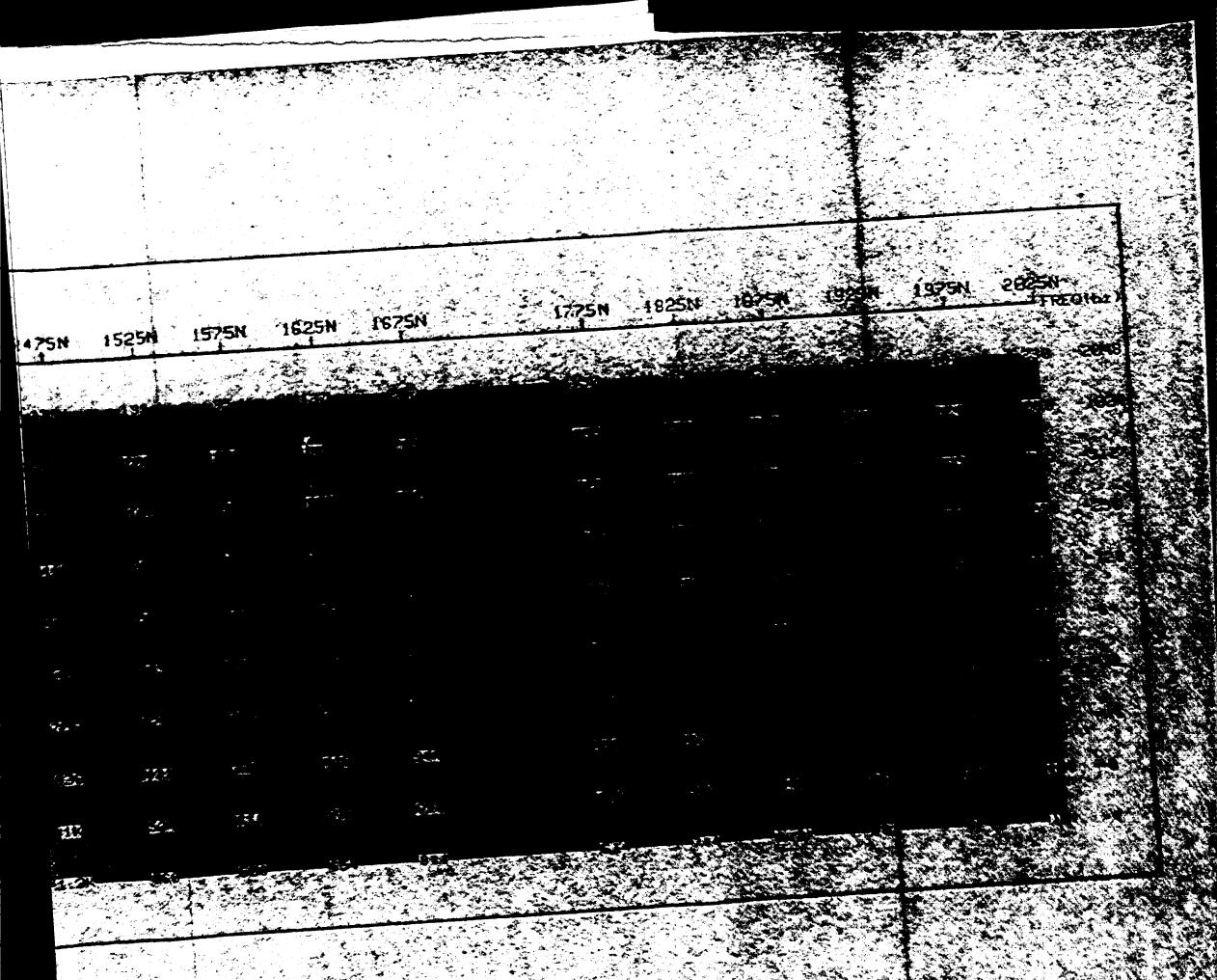


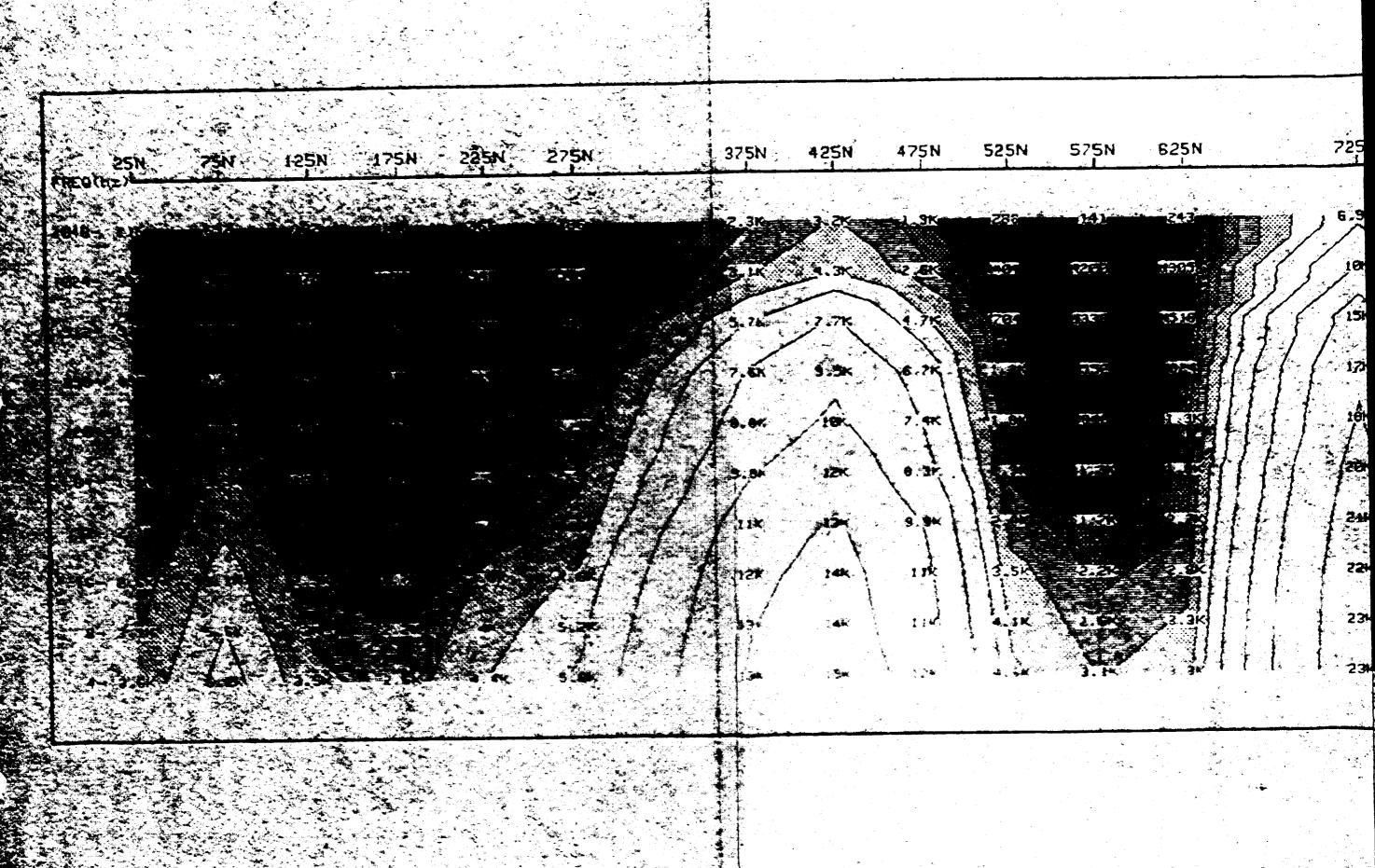


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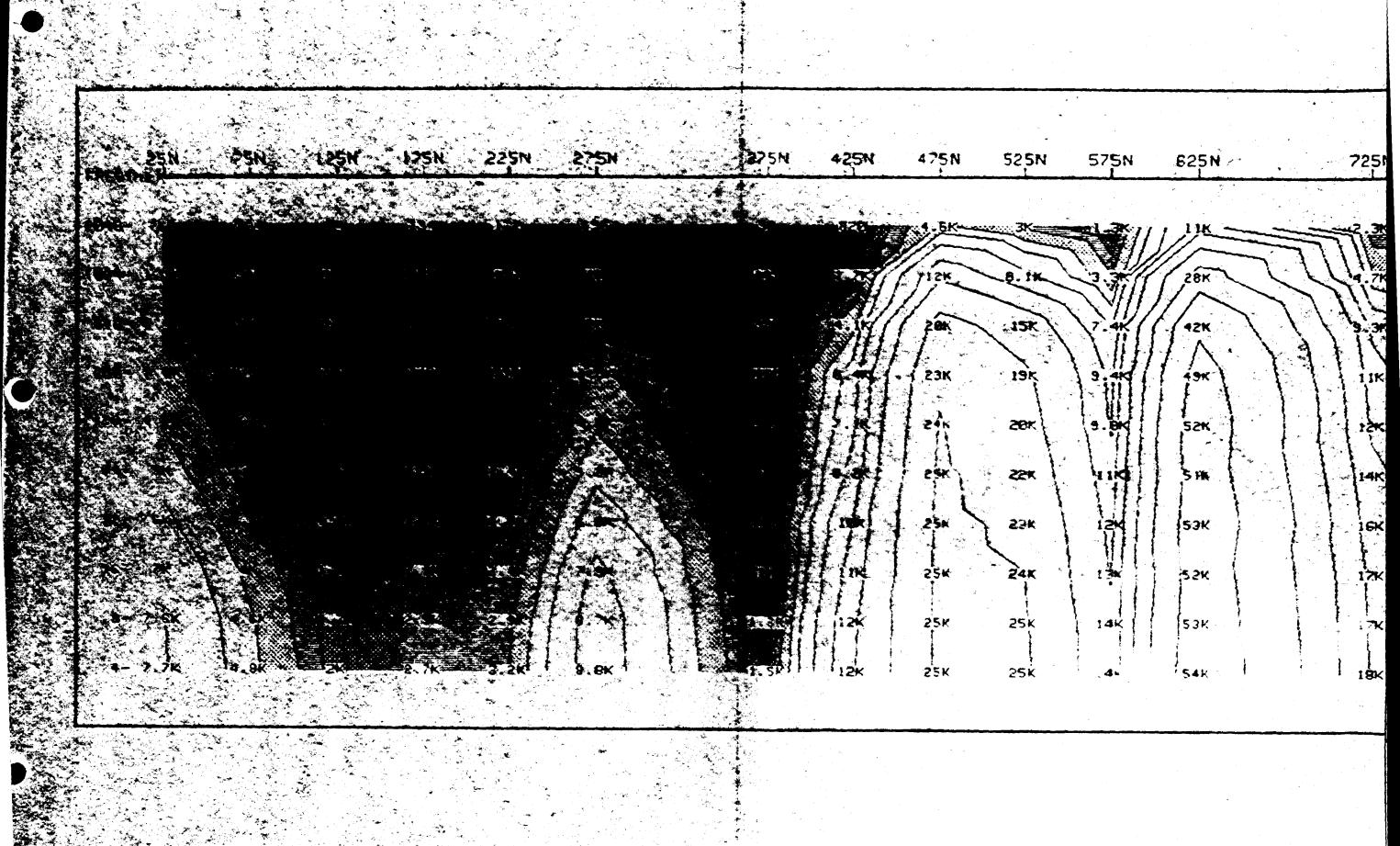


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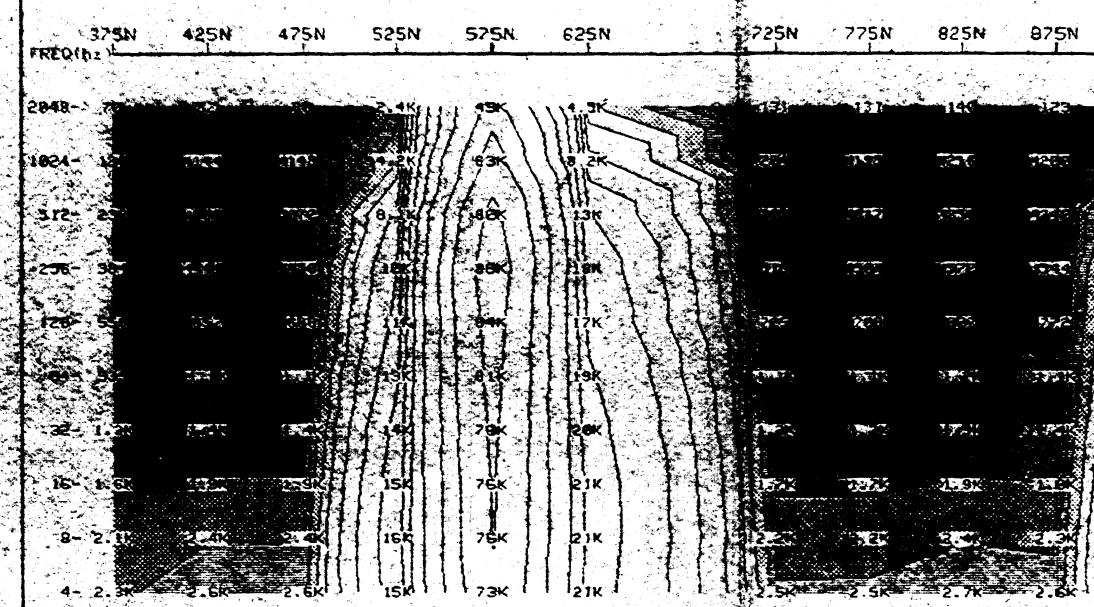
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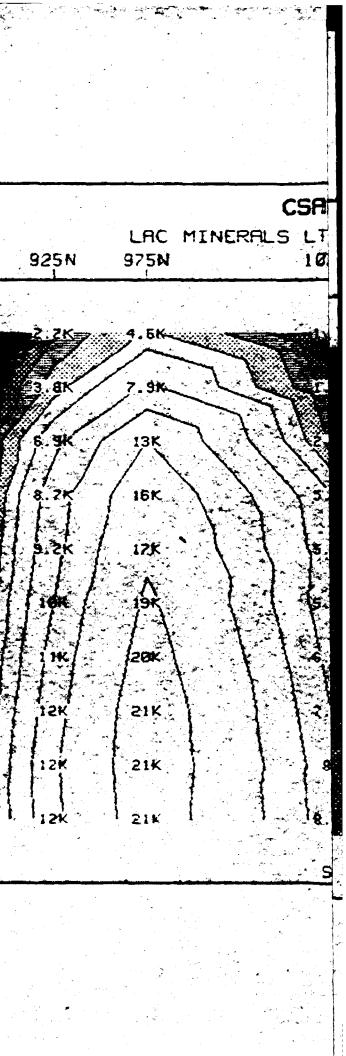
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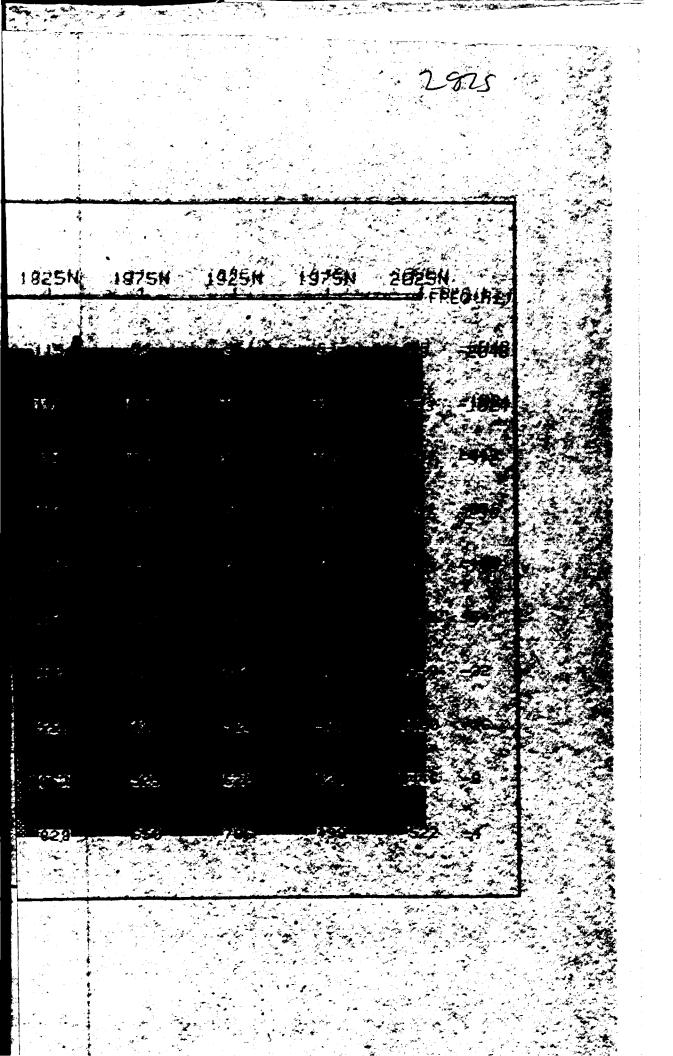


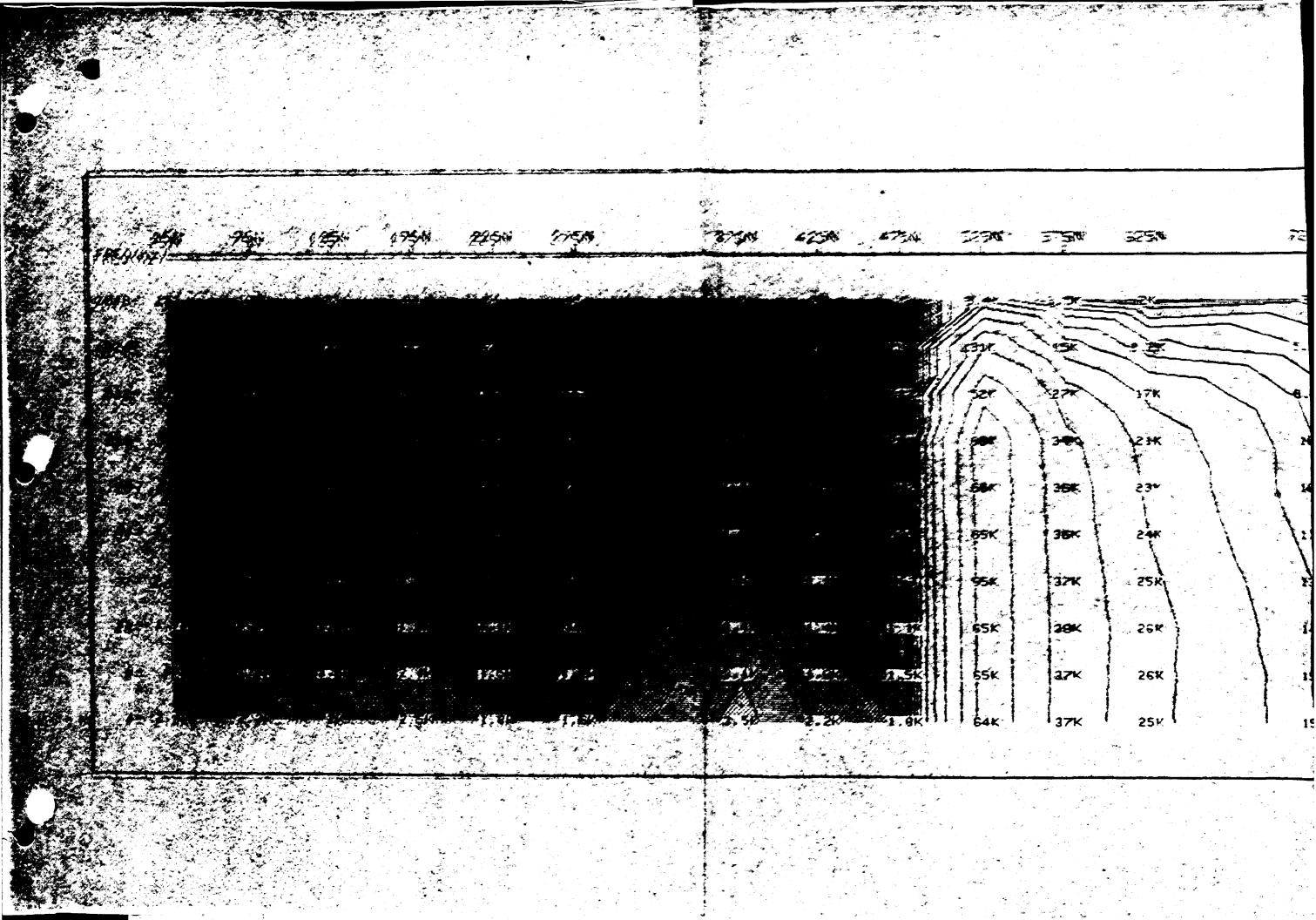


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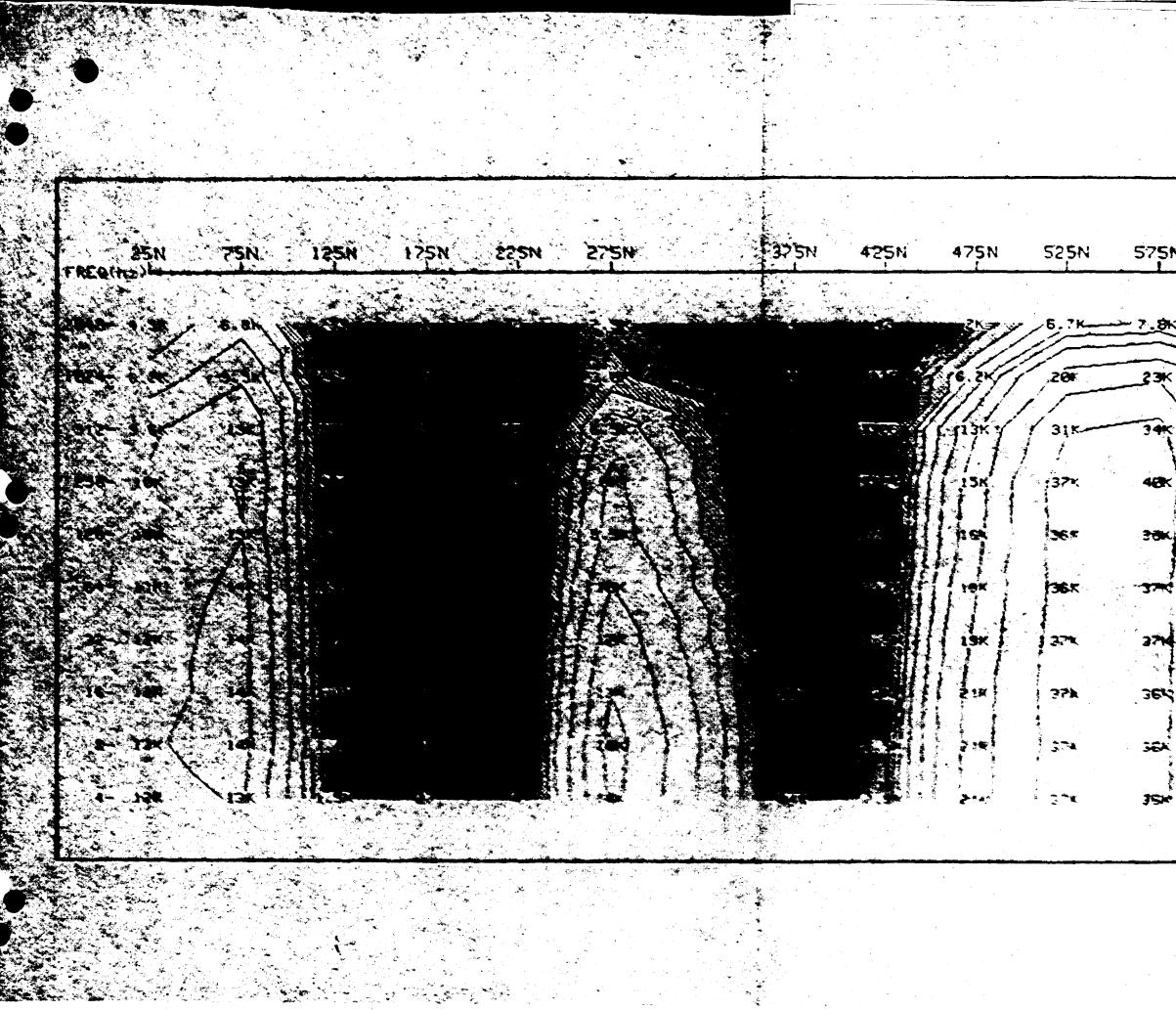
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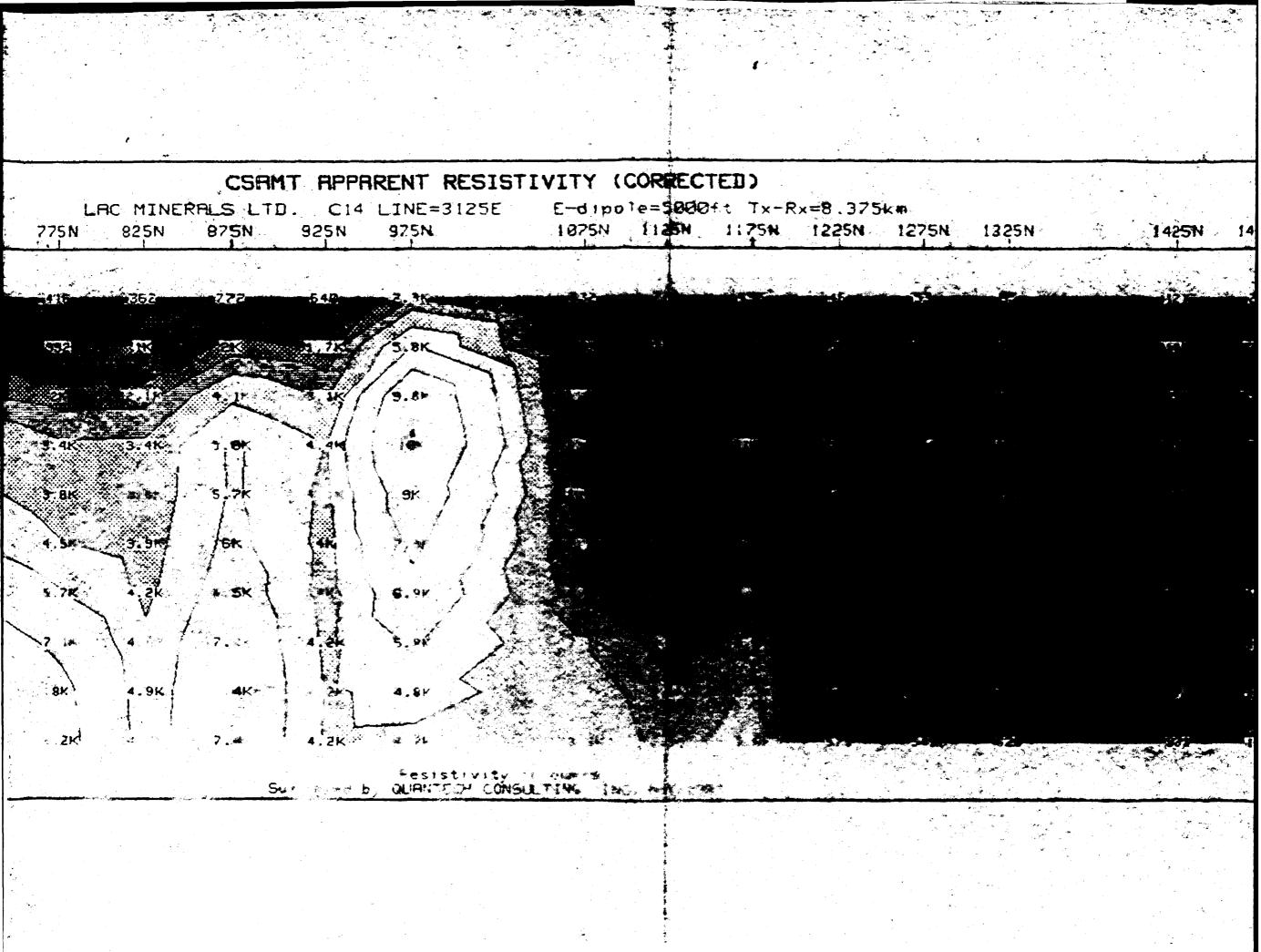


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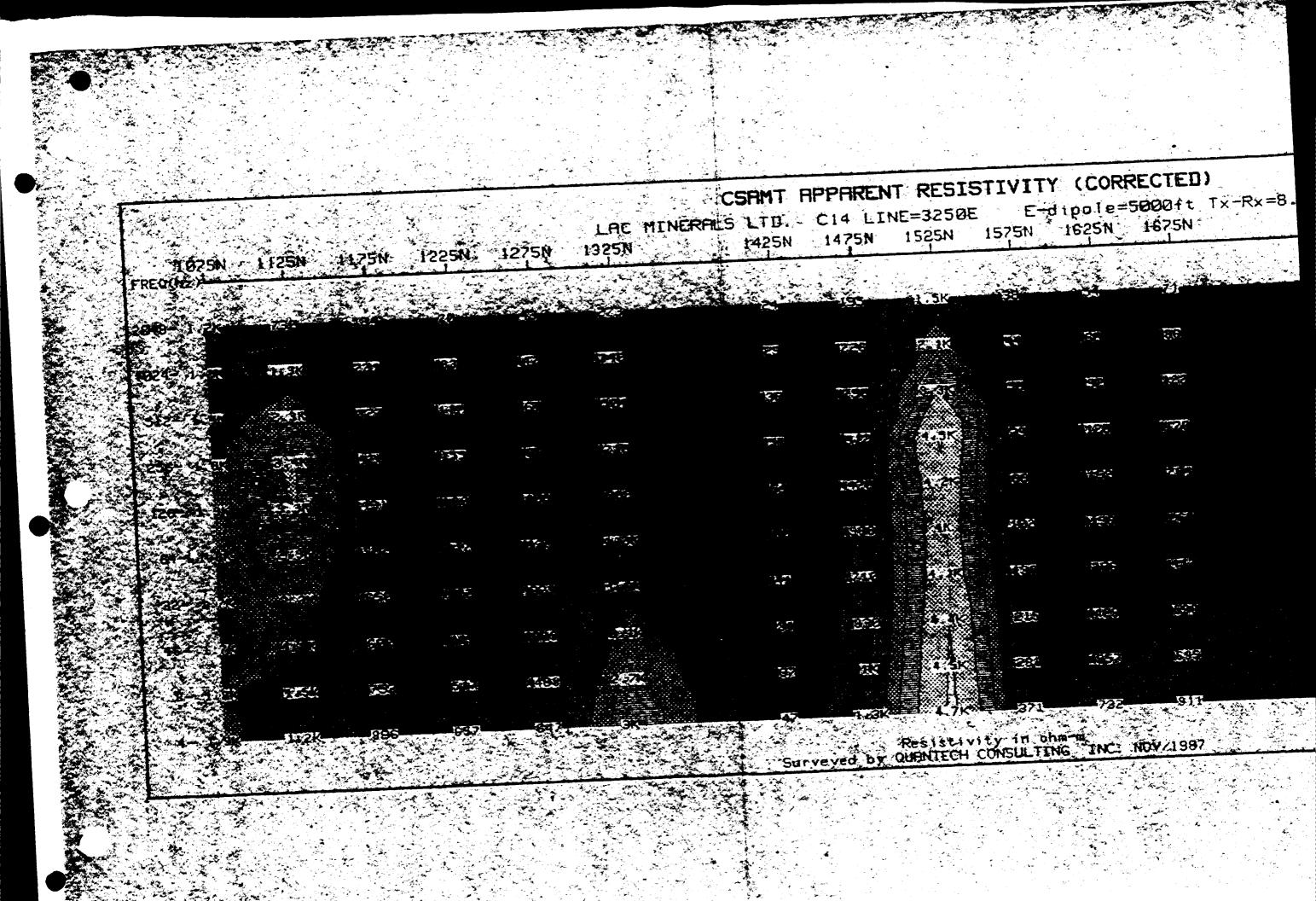
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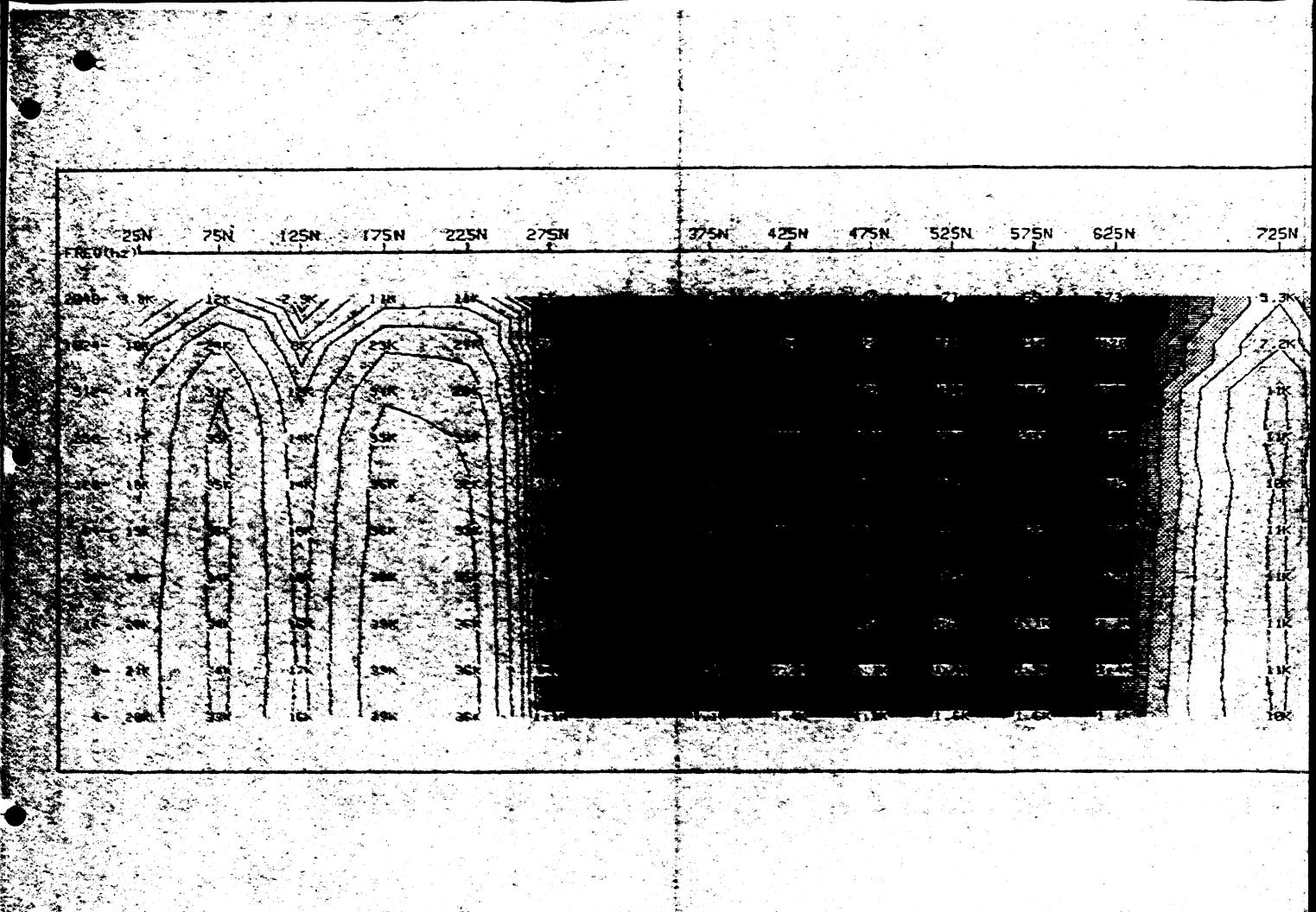
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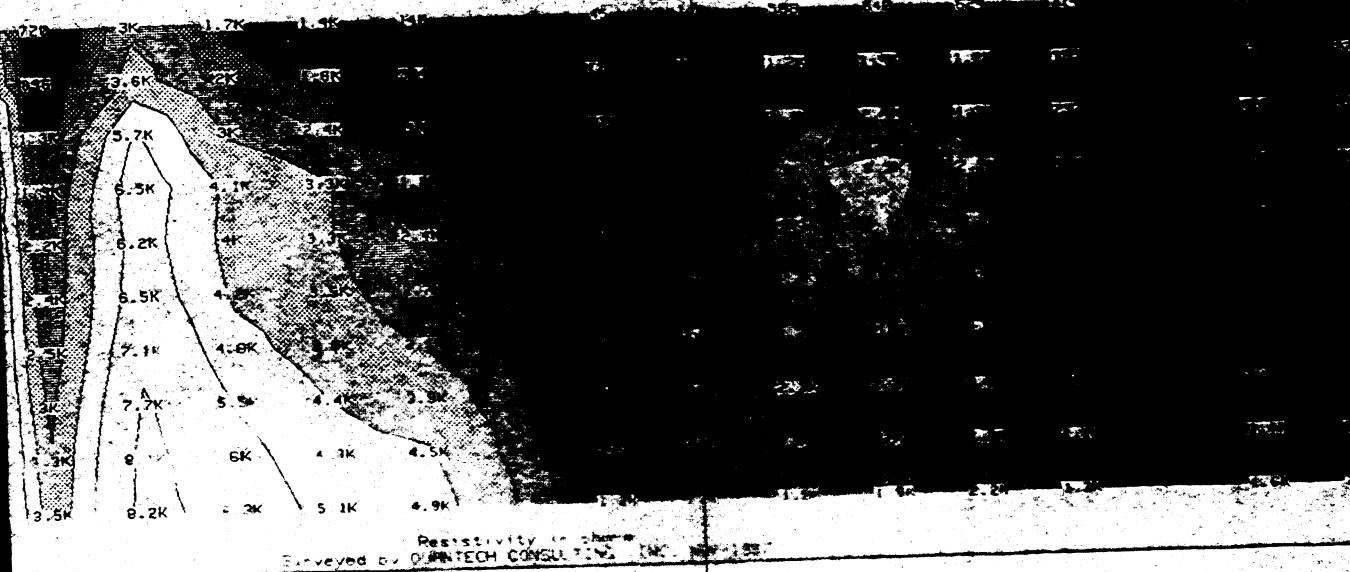
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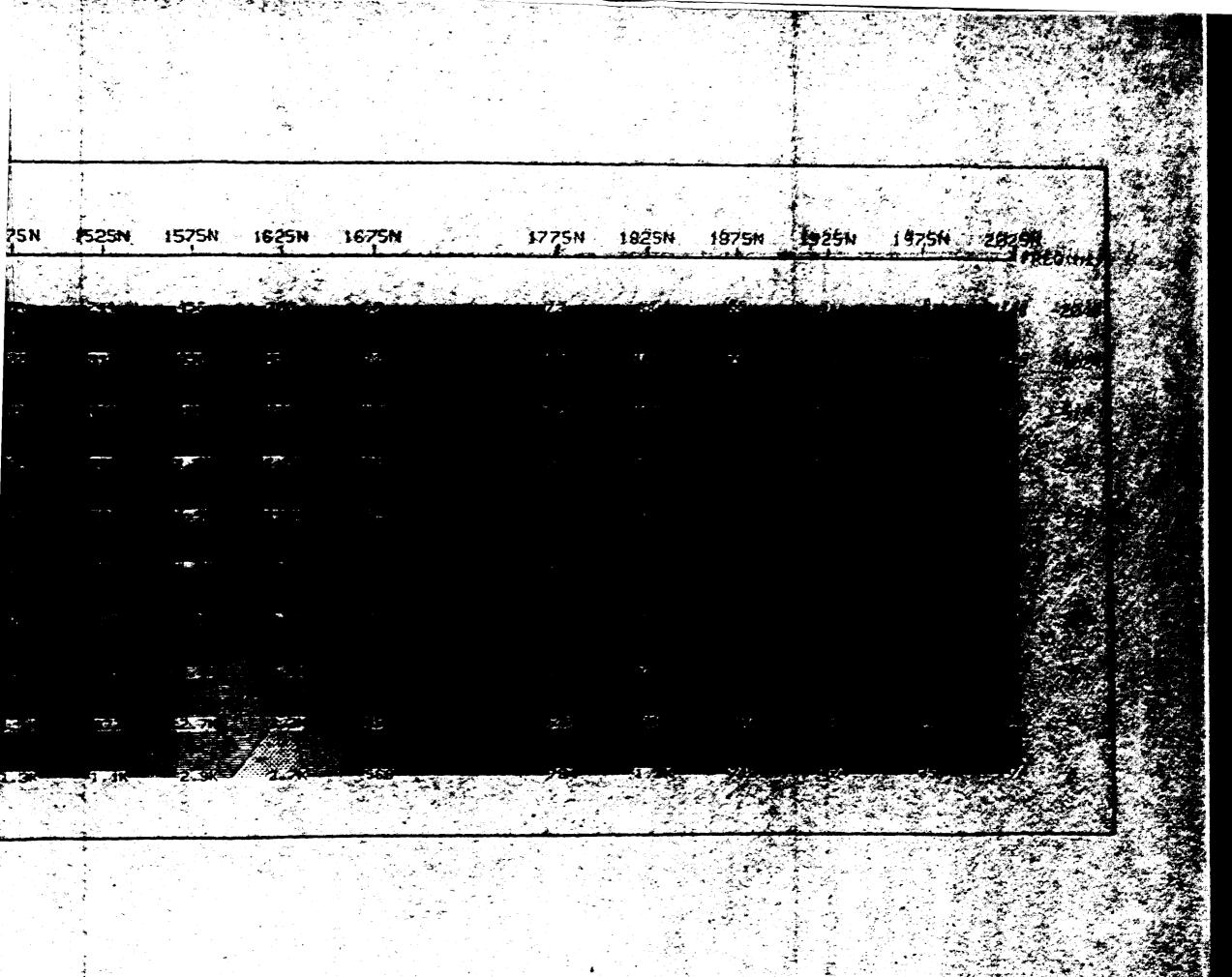
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CSAMT APPARENT RESISTIVITY (CORRECTED)

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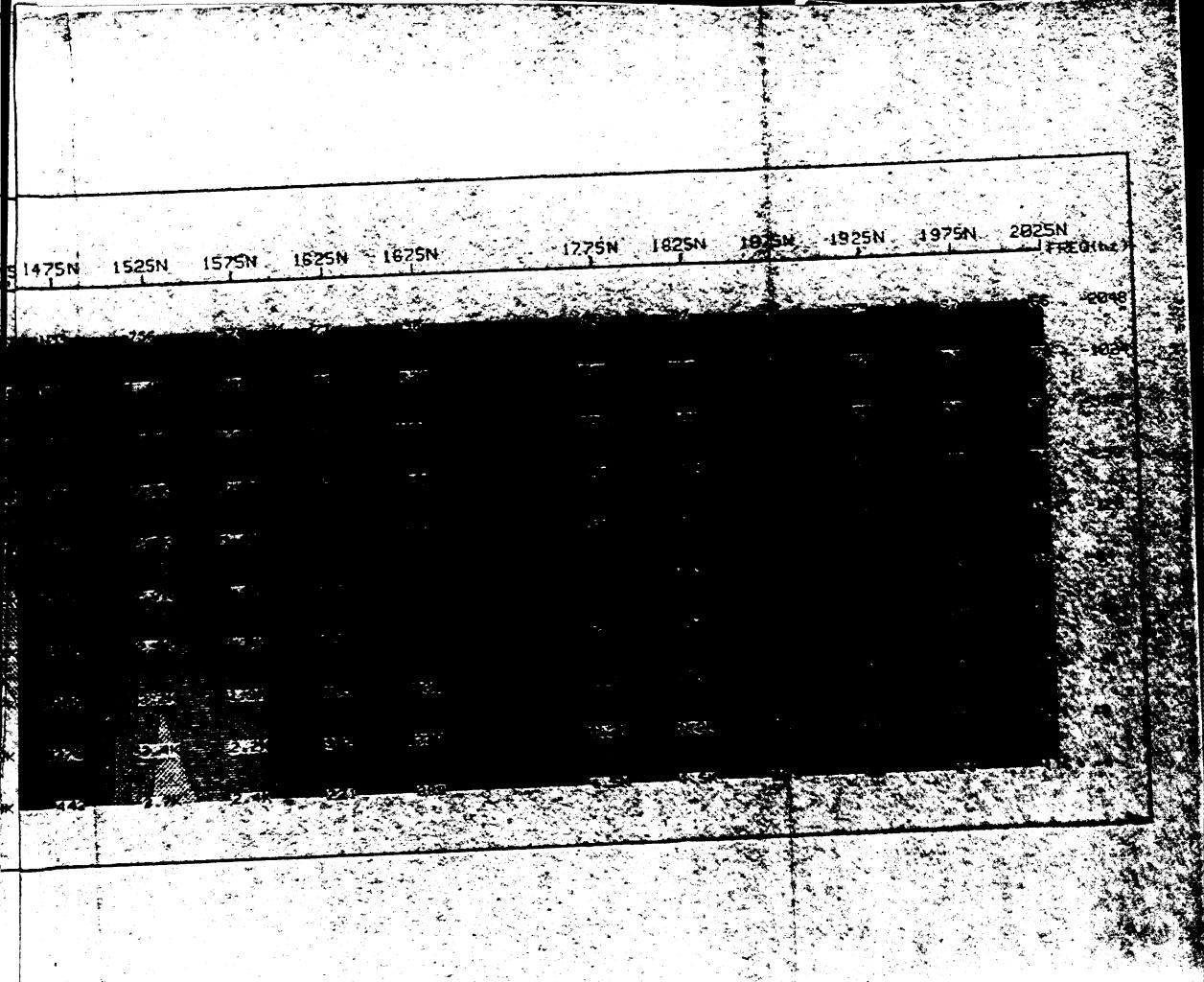
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		Mining Act	Report of Wor		Gaaabami		02 2.12955				900	d to
رد ۲۰ را ر	Type of	-	(Geophysical, Geo			Mining Division	Mining	Lands Section		velopment	and Lands Bri	anch:
in in Sec Sec		Survey(s) CSAMT		í.		Larder La	ake	1 '	ford			
	Recorde	d Holder(s)	inerals Ltd.	•	12	955))	/	Prospector			
	Address	DAC M	inerais Ltd.	<u></u>	<u>, rw</u>			-/	Telephone	T-664 No.		
	6 A1	Wende Ave	., P.O. Box	670, KI	RKLAN	D LAKE, (Ont. P	N 3K1			5656	
and. State	Survey C	ompany Ouant	ech Consulti	na		\mathbf{N}						
		d Address of Author (of Geo-Technical Report)		$\overline{}$	$\overline{}$	/		Date of Su 01 1	rvey (from	& to)	
,	John	Kovala, P	.O. Box 334,	KIRKLA					Day Mo). Yr.	30 11 Day Mo.	87 Yr.
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		tion Verifying Rep	rsonal and intimate knowle	day of the fact	e est forth in	this Deport of Wo	we having as	dormod the w	wk or witnes	cad came	during and/or	· · · · · · · · · · · · · · · · · · ·
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•		Address of Person C Kovala, P	ertifying	KIRKLAN	D LAKE	E, Ontari	lo					
		/		Telephon	ne No.	Dale			Certified B	y (Signaju	(e)	1
	P2N 3			(705)-567-	-5495 Oct	ved Stamp	5, 1989	he	7/6	no	
	For Of	fice Use Only					LAF	R D E R MINING DI	LAKE	1		:
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	- Total Day	ys Date Recorded	Mining A	ecorder			裕二	• ••	····			
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Ministry of Northern Development and Mines

Ministère du Développement du Nord et des Mines Mining Lands Section 880 Bay Street, 3rd Floor Toronto, Ontario M5S 1Z8

Telephone: (416) 965-4888

Your File: W8908-336 Our File: 2.12955

April 10, 1990

Mining Recorder Ministry of Northern Development and Mines 4 Government Road East Kirkland Lake, Ontario P2N 1A2

Dear Sir:

Re: Notice of Intent dated February 23, 1990 for Geophysical (Electromagnetic) Survey submitted on Mining Claims: L 803326 et al in Clifford Township.

The assessment work credits, as listed with the above-mentioned Notice Intent have been approved as of the above date.

Please inform the recorded holder of these mining claims and so indicate on your records.

Yours sincerely,

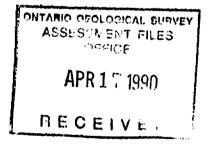
W.R. Cowan Provincial Manager, Mining Lands Mines & Minerals Division

JLS:pt Enclosure

> cc: Mr. G.H. Ferguson Mining and Lands Commissioner Toronto, Ontario

> > LAC Minerals Limited Kirkland Lake, Ontario

> > John Kovala Kirkland Lake, Ontario



Resident Geologist Kirkland Lake, Ontario



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Ministry of Northern Development and Mines

Technical Assessment Work Credits

	File				
	2,12955				
Dete	Mining Recorder's Report of				
Feb 23/90	2,12955 Work No. W8908.336				

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Recorded Holder						
Lac Minerals Limited						
Clifford						
Type of survey and number of Assessment days credit per claim	Mining Cleims Assessed					
Geophysical						
Electromagnetic <u>20</u> days	L 803326 to 331 incl.					
Magnetometer days	803333 to 335 incl. 803337 to 342 incl. 918236					
Radiometric days	918238					
Induced polarization days	1014621 1014623 to 627 incl.					
Other days	1014635 to 637 incl					
Section 77 (19) See "Mining Claims Assessed" column	1014639 1014648 to 655 incl.					
Geological						
Geochemical days						
Man days 🗌 🛛 Airborne 🗌						
Special provision 🛛 Ground 🕱						
Credits have been reduced because of partial coverage of claims.						
Credits have been reduced because of corrections to work dates and figures of applicant.						
Special credits under section 77 (16) for the following m	ining claims					
15 days Elctromagnetics L 10146	38, 1014640					
10 days Electromagnetics L 803325, 803336, 918237, 1014622						
to credits have been allowed for the following mining cla	aims					
not sufficiently covered by the survey	insufficient technical data filed					
Note: Credits were reduced because L 2250 E was not Surveyed and L3250 E was not surveyed from BLO to 1075N.						
	1					

The Mining Recorder may reduce the above credits if necessary in order that the total number of approved assessment days recorded on each claim does not exceed the maximum allowed as follows: Geophysical - 80; Geologocal - 40; Geochemical - 40; Section 77(19) - 60.

Norsty of Norstern Developm and Mines		DOCUME W8908	3•336		 Refer to S and maxi 	ns pe or print. Section 77, the Mining A mum credits allowed r of mining claims trai	per survey t	ment work requirement
Mining Act	Geophysical, Geo	rk plogical and	2.129 Geochem	ical Surveys)	- Technica	Reports and maps i		should be submitted t and Lands Branch:
Type of Survey(s) CSAMT				Mining Division Larder Lak		Township or Area	}	
Recorded Holder(s)					<u> </u>		lor's Licence	No.
LAC Minerals Ltd.						T-664		
Address 6 Al Wende Ave	. P.O. Box	670. кл	RKLAN	D LAKE, On	t. P2	1		-5656
Survey Company	······································						/ 00/	
Quante Name and Address of Author (o	ech Consulti	Ing				Data of	Supray Ilea	m 8 to)
John Kovala, P		KIRKL	AND LA	KE, Ontari	O P2N	3J1 01	Survey (from 11 87	30 11 87 Day Mo Yr
Credits Requested per Ea		and the second		Claims Traversed				- 02) - MC - 1
Special Provisions	Geophysical	Days per Claim		Mining Claim		Mining Claim		Mining Claim
For first survey:			Prefix	Number	Prefix	Number	Prefix	Number
Enter 40 days. (This includes	- Electromagnetic	20	L	803325	L	918236	LL	1014640
line cutting)	- Magnetometer			803326		918237	· .	1014648
For each additional survey: using the same grid:	- Other			803327		918238		1014649
Enter 20 days (for each)	Geological			803328		1014621		1014650
	Geochemical			803329		1014622		1014651
Man Days	Geophysical	Days per Claim		803330		1014623	1	1014652
Complete reverse side and	- Electromagnetic	Cidwir		803331	<u> </u>			
enter total(s) here	Magnetometer			1		1014624		1014653
				803333	}	1014625		1014654
	Other			803334	<u> </u>	1014626	·	1014655
	Geological			803335		1014627		
	Geochemical			803336	<u> </u>	1014635		
Airborne Credits		Days per Claim		803337		1014636	REC	EIVED
Note: Special provisions credits do not	Electromagnetic			803338		1014637	MOU	0.0 1000
apply to Airborne Surveys.	Magnetometer			803339		1014638	1 11/0 1	00 1505
00.0010.	Other							ANDS SECTIO
Total miles flown over cl				803340	<u> </u>	1014639 M		ANDS SECTIO
	(Signature)		803341	ł	Total number of			
Oct 1 graf	the know			803342]	mining claims covered 4 by this report of work.		
Certification Verifying Rep	<u> </u>							
I hereby certify that I have a per after its completion and annexed Name and Address of Person C	d report is true.	edge of the fact	is set forth in	this Report of Work, I	having perfo	ormed the work or wit	nessed same	e during and/or
John Kovala, P.					······	····		
P2N 3J1		Telepho (705	ne No. 5)-567:	-5495 Octol	ber 5,	, 1989	By (Signat	nie)
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