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MINING LANDS SECTION

CONTROLLED SOURCE AUDIOFREQUENCY

MAGNETOTELLURIC SURVEY

ON GRID C14

CLIFFORD TOWNSHIP, ONTARIO

LARDER LAKE MINING DIVISION

DISTRICT OF TIMISKAMING

2.12955

NTS 32D/5

Latitude 48° 17' N

Longitude 79° 80' W

2,10571

John Kovala

December 1989

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## 1.0 INTRODUCTION

A controlled source Audiofrequency magnetotelluric survey was carried out by Quantech Consulting Inc. for LAC Minerals Ltd. on a continuous block of 44 claims located 20km north east of Kirkland Lake along the south central boundary of Clifford Township. The survey was conducted between November 1st and November 30th, 1987. The survey was completed in order to evaluate the effectiveness of this survey in outlining the low resistivity zone associated with a previously discovered ultramafic breccia.

Sections 1 through 4 of this report were written by J. Kovala. Sections 5 through 7, CSAMT Technique, Data Presentation and Interpretation Techniques were extracted from a report written by G. Bogden of Quantech in October 1987 for LAC Minerals. P. Haloff, a consultant for LAC Minerals has interpreted the results of this survey, Section 8.

## 2.0 PROPERTY

The property consists of a continuous block of 44 unpatented mining claims located in Clifford Township, Larder Lake Mining Division, District of Timiskaming. The claims are given below:

L 803325 to 803331  
803333 to 803342  
983106 to 983108  
918236 to 918238  
1014621 to 1014627  
1014635 to 1014640  
1014648 to 1014655

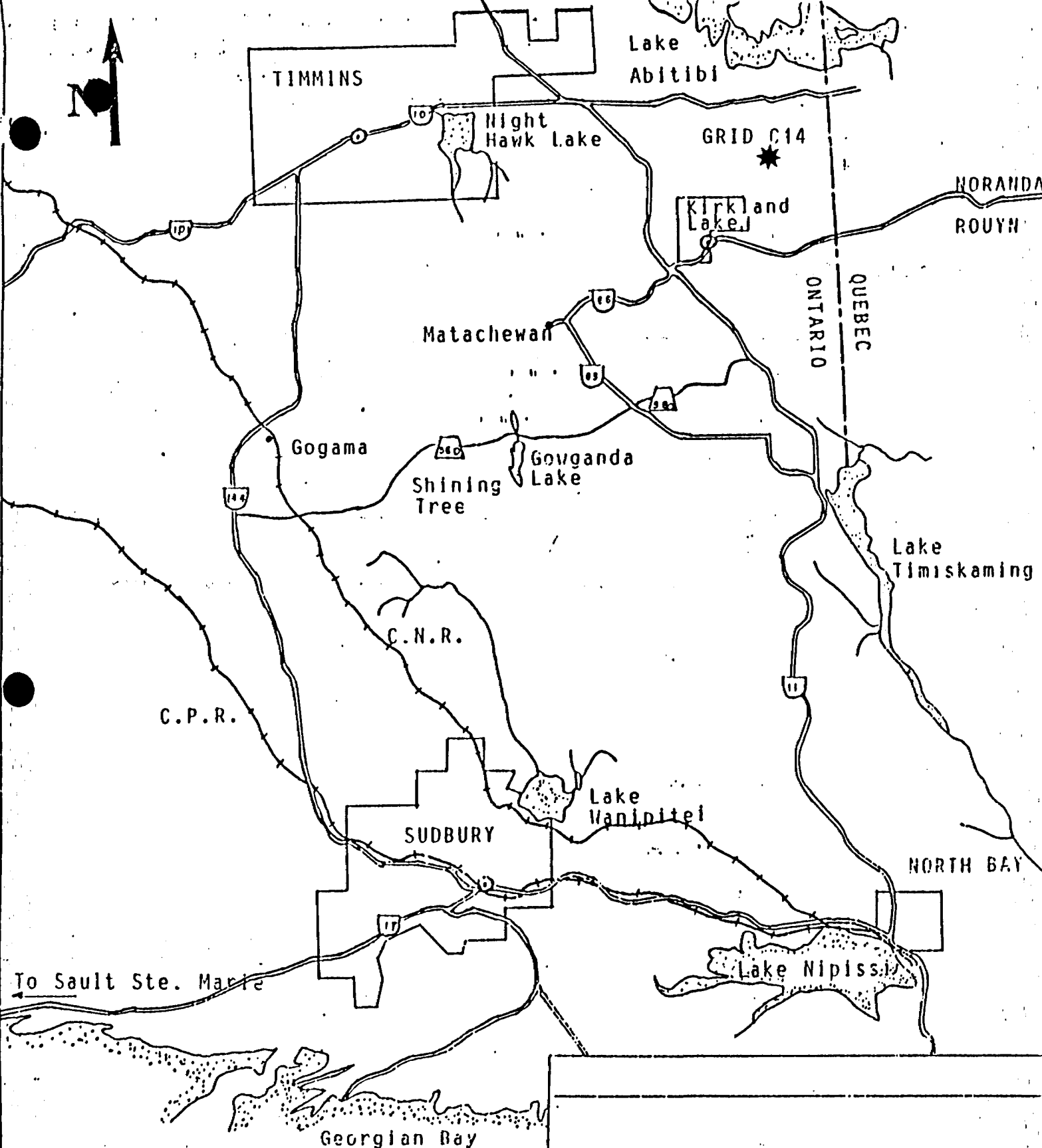
## 3.0 LOCATION AND ACCESS

The C14 property is located 20 kilometers northeast of Kirkland Lake in the south central portion of Clifford Township at longitude 79° 80' W and latitude 48° 17' N (NTS 32D/5)

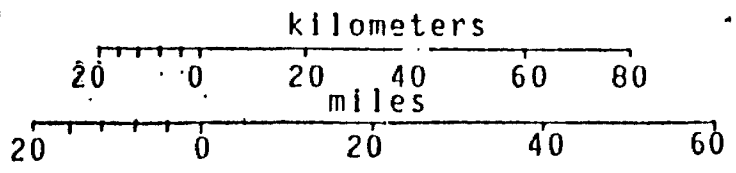
Bush roads originating at the Esker Park and Harker-Holloway roads lead to the south and north boundaries respectively.

## 4.0 GENERAL GEOLOGY

Regionally the property is located in the west central portion of the Blake River synclinorium. The Blake River group consists of dominantly calc-alkaline series intermediate to felsic volcanic rock occurring in the central portion of Clifford Township. Bodies and sills of mafic intermediate and felsic intrusive rocks cut the volcanics. All of the above are cut by dominantly NW striking diabase.



To Sault Ste. Marie



GRID C14 LOCATION MAP	
Date	OCT 1987
Scale	1:1,600,000
JOHN KOVALA	Fig. 1





In the central portion of the synclinorium in Clifford Township occurs a domal anticline intruded by a granodiorite stock 1 1/4 miles wide. The survey area is located 2 miles south of the above domal anticline over a complimentary WNW syncline. The syncline is centered by felsic volcanics and flanked to the NNE and SSW by intermediate volcanics. A large quartz gabbro intrusive is located along the southeastern boundary of the property.

## 5.0 CSAMT TECHNIQUE

### 5.1 Advantages and Disadvantages Over Natural Signal Systems

Natural source electromagnetic (EM) sounding methods such as magnetotellurics (MT) and audiomagnetotellurics (AMT) have been widely used for the exploration of hydrocarbons, groundwater and geothermal sources, but with little application to mineral exploration. The MT method measures fluctuations in the earth's natural electric and magnetic fields over a broad range of frequencies between 10 Hz and 10,000 Hz; the AMT band is slightly higher between 10 Hz and 10,000 Hz. The source of these fluctuations originate in the ionosphere for frequencies less than 1 Hz and from thunderstorms for the higher frequencies. The field strength and polarization of the signals vary with the time of day and the season.

The CSAMT technique was introduced to overcome problems and limitations encountered by these natural source methods (Goldstein and Strangeway, 1975). Rather than a natural signal source, CSAMT uses a fixed grounded bipole or current loop on the surface of the earth to produce an EM signal. Some of the advantages of the CSAMT technique over the natural source methods which make CSAMT a viable mineral exploration tool are:

1. The polarization of the fields can be selected by the orientation of the transmitting antenna.
2. The signal strength does not depend on the time of day or the season.
3. Because the signals are stronger, the receiving equipment does not need to be as sensitive as that of MT or AMT.
4. Because of the coherent signal, the usual signal processing and enhancement techniques are far more effective.
5. CSAMT surveys are much faster and therefore more cost effective than natural source EM surveys.

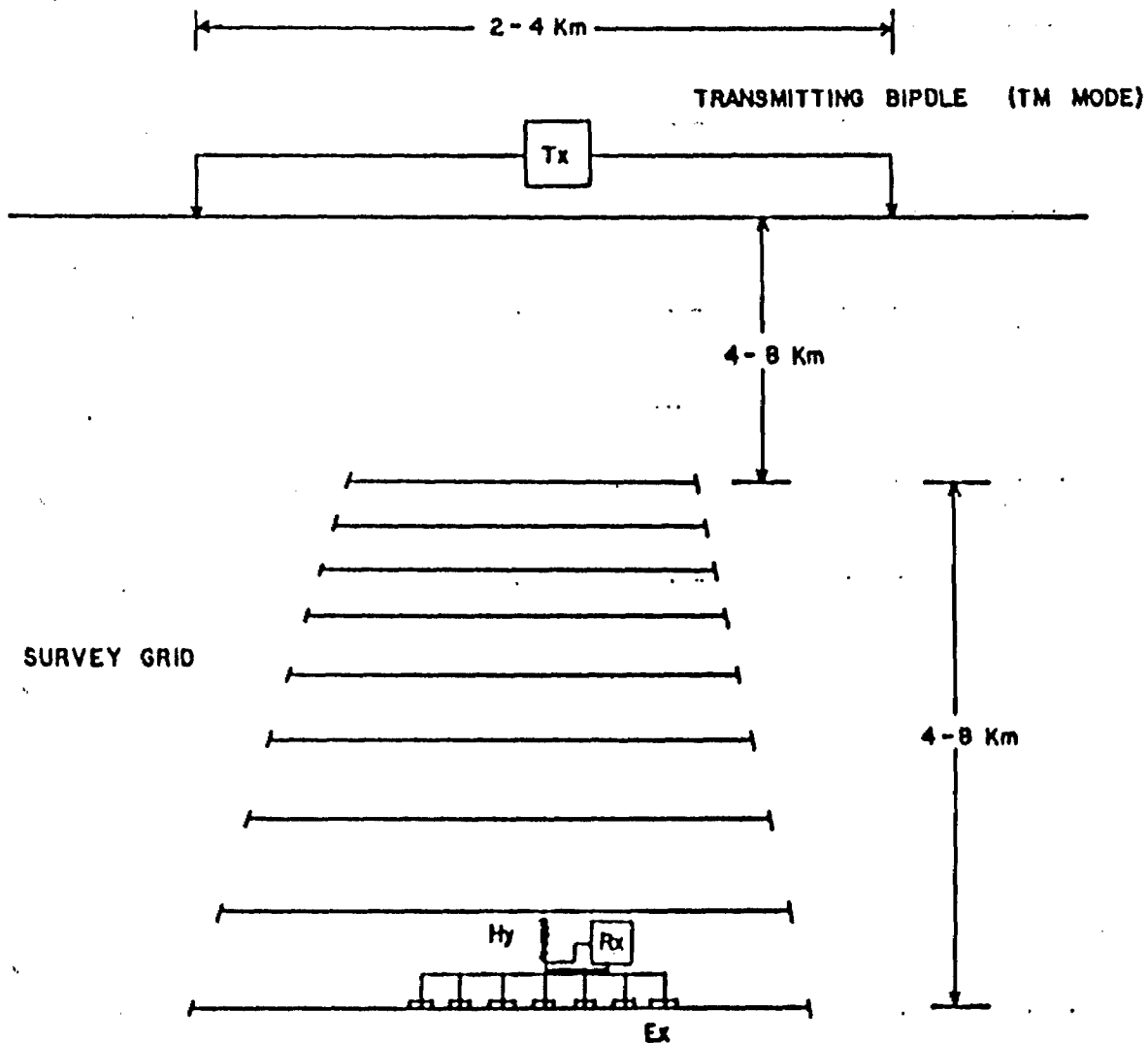
The primary disadvantage of the CSAMT method over natural source EM methods is the closeness of the signal source. For natural source techniques, the signal source is, in effect, infinite such that the EM field is a "plane wave". This assumption greatly simplifies processing and interpretation for MT and AMT data. For CSAMT data, if the transmitting antenna is too close to the survey area, the resistivity of the deep layers cannot be determined accurately since they are no longer energized by this plane wave. Readings measured at the plane wave distance are considered to be in the "far-field", while readings measured at the non-plane wave distance are considered in the "near-field". In order that resistivities of the deep layers be calculated correctly, the measurements must be corrected for this near-field, non-plane wave effect.

## 5.2 Theory and Instrumentation

The survey was executed using the V4 multichannel universal receiver console, the T30 transmitter and the MG30 (30 kilowatt) motor generator, all manufactured by Phoenix Geophysics Limited, Markham, Ontario. A complete description of the equipment along with technical specifications are contained in Appendix B.

The transmitter operates at sixteen (16), selectable, binary step base frequencies which range from 0.25 Hz to 8192 Hz. An optional alternate frequency set at  $2/3$  the base frequency set, ranges from 0.17 Hz to 5461 Hz to provide a total of 32 transmitting frequencies. The length of the bipole (or loop edge) may be varied from several hundred meters to several kilometers, depending upon signal strength, the minimum transmitter-receiver distance and the size of the area to be surveyed. Normally a grounded bipole is preferred to a current loop because the bipole requires less wire to produce a comparable signal. The bipole is constructed with lengths of #10 gauge copper wire, which has a resistance of approximately 1 ohm per 1000 feet.

Orthogonal components of the electric field (E) and the magnetic field (H) are measured over the survey area. The E-field components are measured with a dipole using non-polarizable (steel rod) electrodes in the same manner as induced polarization (IP) measurements. The dipole length is a function of the scale of the survey but may also be influenced by the E-field signal strength, which in turn is a function of the transmitter-receiver distance, the transmitter bipole current, the earth resistivity and noise conditions. The H-field components are measured using a magnetic sensor coil placed on the ground. The V4 has the advantage of multiple channels which permits the measurement of six (6) or seven (7) dipoles and one (1) H-field component simultaneously.



TYPICAL RECEIVER ARRAY WITH SEVEN  
E-FIELD COMPONENTS,  $R_x$   
AND ONE H-FIELD COMPONENT,  $H_y$

FIGURE 5.1 • TYPICAL CSAMT SURVEY CONFIGURATION

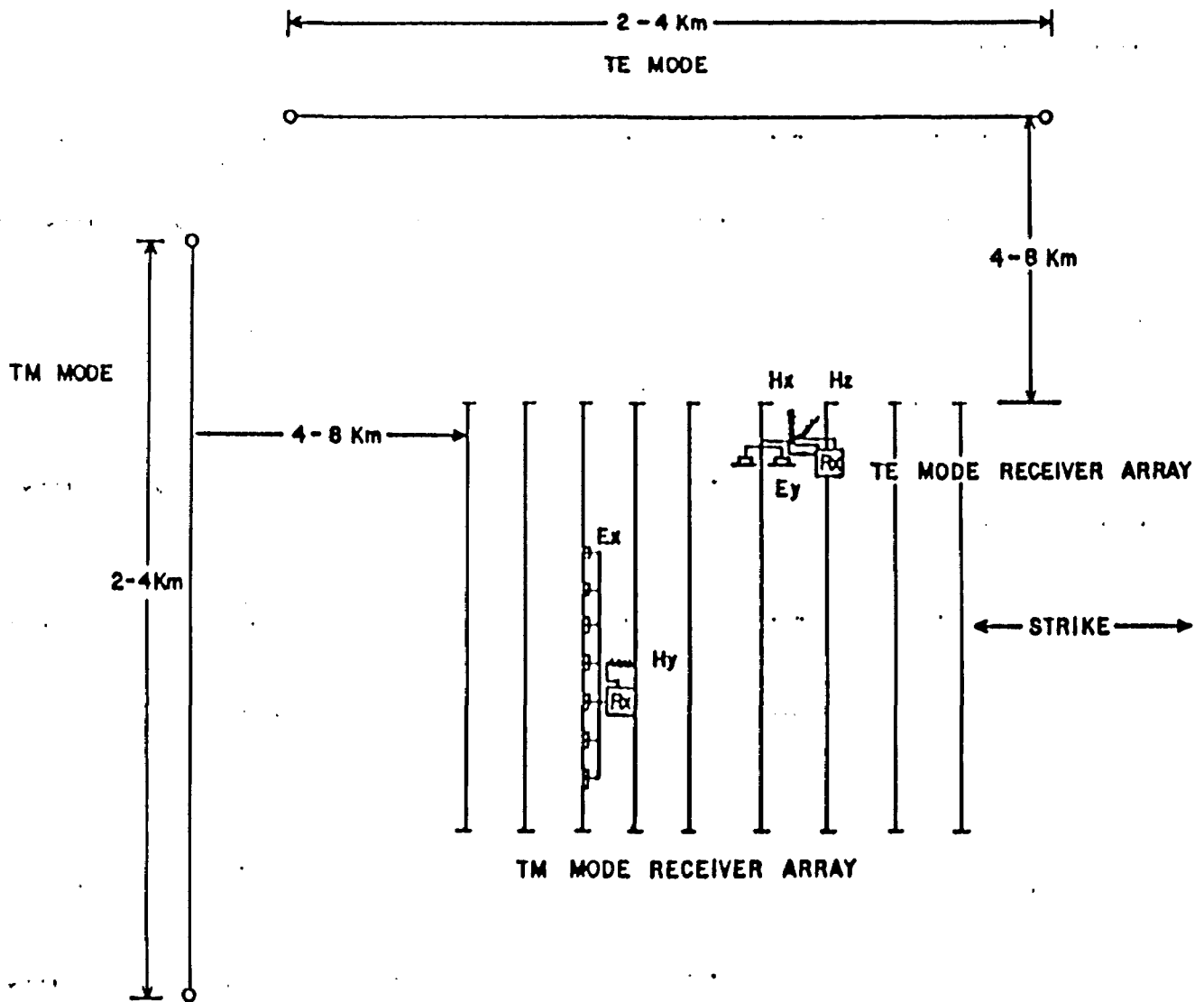


FIGURE 5.2 : TM MODE AND TE MODE ARRAYS

The survey may be conducted in two survey modes: the transverse magnetic (TM) mode where the transmitting bipole is perpendicular to geologic strike and the transverse electric (TE) mode where the transmitting bipole is parallel to geologic strike. The TM mode is most sensitive to lateral changes in resistivity and is therefore more suitable as a reconnaissance mapping tool whereas the TE mode is preferred as a detailing method because it provides greater resolution of horizontal resistive boundaries. A TM mode survey is also much faster from a logistics standpoint, than a TE mode survey.

Up to three H-field components, H<sub>x</sub>, H<sub>y</sub> and H<sub>z</sub> and two E-field components, E<sub>x</sub> and E<sub>y</sub> can be measured at each station along with the E-field phase and H-field phase for both modes. The apparent resistivity is calculated from the ratio of orthogonal components of the electric and magnetic fields (eg. E<sub>x</sub>/H<sub>y</sub> or E<sub>y</sub>/H<sub>x</sub>) using the following Cagniard equation:

$$\rho_a = \frac{1}{2\pi f \mu_0} \left( \frac{E}{H} \right)^2, \quad \phi = E_\phi - H_\phi \quad (1)$$

Where  $\mu_0 = 4\pi \times 10^{-7}$  H/m  
 $\rho_a$  = apparent resistivity in ohm-meters  
 E = E-field magnitude in mv/km  
 H = H-field magnitude in gammas  
 $\phi$  = phase difference in radians

Should only the E<sub>x</sub> and H<sub>y</sub> components of the electric and magnetic fields respectively be required for the TM mode then only one H-field measurement is necessary for each receiver array since H<sub>y</sub> is essentially constant over a significant distance, even for very strong conductors (Yamashita, 1987). Figure 5.1 illustrates a typical configuration for a reconnaissance TM mode and TE mode.

The measured components of the electric and magnetic fields and the calculated apparent resistivity are stored in solid-state memory in the V4 receiver and later transferred to a microcomputer for processing at the end of the field day.

### 5.3 Computer Software

Data dumping, editing, reduction and presentation was controlled by the CSAMT processing and interpretation programs provided by Phoenix. The software is written in HPBASIC and executes only on a Hewlett Packard HP9845 or HP9000 series machine. Figure 5.3 illustrates the software package structure.

Contours of apparent resistivity values for selected frequencies for the survey grids were prepared using the MAPLOT system developed by Geosoft Inc., Toronto. The software was controlled by DOS 3.1 written by Compaq Computer Corporation.

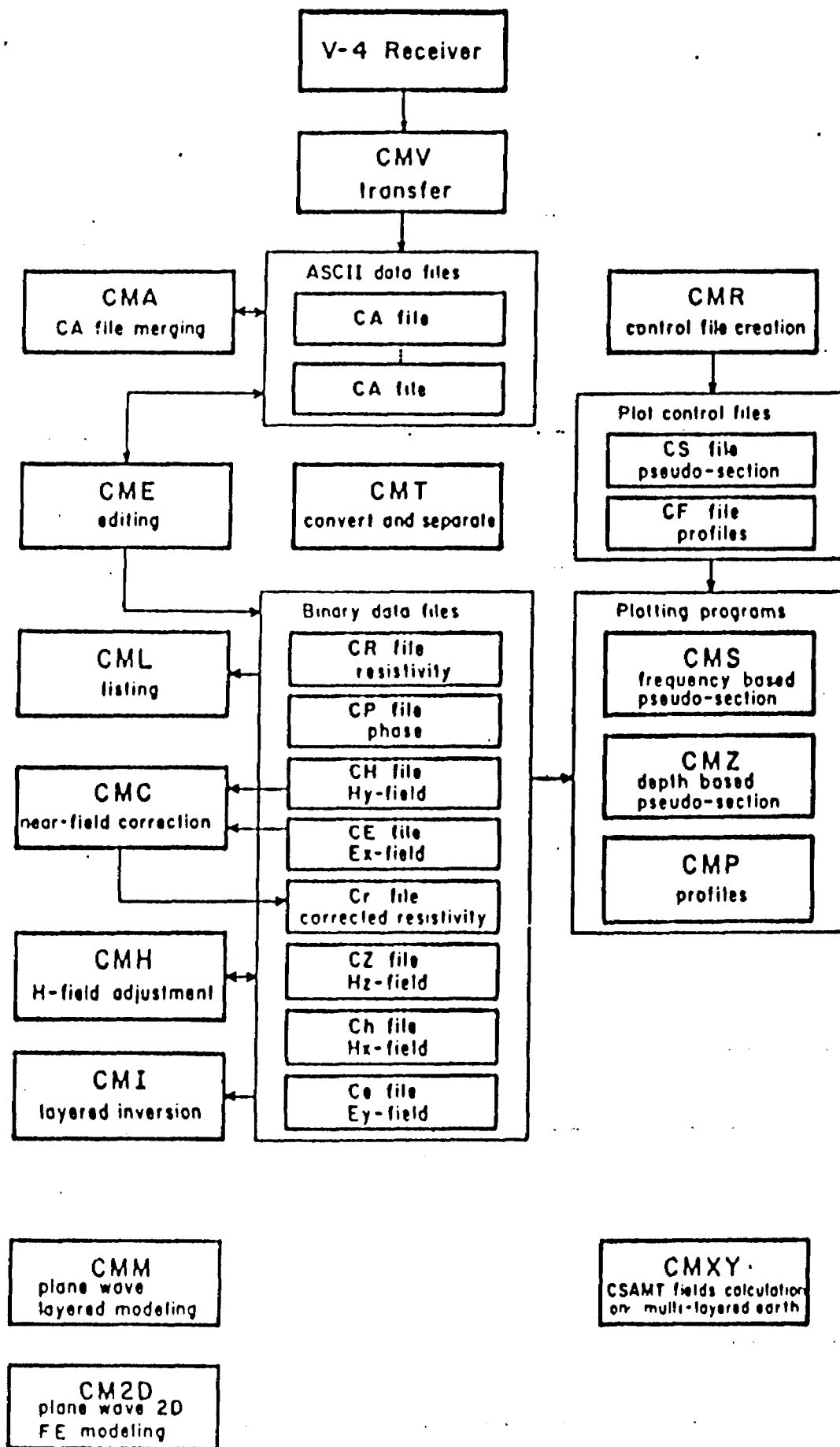


FIGURE 5.3  
Phoenix software structure.

#### 5.4 Computer Hardware

In-field processing used the Hewlett Packard HP9845 desk-top computer. The system is equipped with an 8 bit CPU, two cassette tape drives, RS-232C serial port and integral thermal printer.

### 6.0 DATA PRESENTATION

#### 6.1 Frequency Pseudosections

The contoured apparent resistivity for near-field corrected data for each line surveyed is presented in a frequency pseudosection format (see Appendix A). Contour intervals are logarithmically distributed to compensate for the large dynamic range of the data. Zones of low resistivity (high conductivity) have been shaded at 5,000 ohm-meter intervals.

Other parameters, such as the phase difference, or E-field and H-field magnitude were also presented in the same format, to provide further information when required.

#### 6.2 Frequency Profiles

Profiles of each sounding point were used when necessary by the author to provide more diagnostic information about an individual sounding point.

### 7.0 INTERPRETATION TECHNIQUES

#### 7.1 First Order Correction

In order to use the interpretation methods and modelling techniques common to natural source surveys, CSAMT data must be corrected for the near-field effect.

The Cagniard equation given in Equation (1) is only valid when the transmitted electromagnetic field is far enough from the transmitting bipole such that it is a plane-wave or the far-field case. This distance is a function of the ground resistivity and the transmitter current in the bipole. If the actual distance between the transmitter and the receiver is much less than this far-field distance, the transmitted field is not plane-wave in character, and is considered in the near-field. In the near-field, the Cagniard equation overestimates the actual resistivity. Consequently "true" apparent resistivity values must be estimated using another technique:

$$\rho_a = K(r) * r \left( \frac{E}{H} \right) \quad (2)$$

(Yamashita, 1984)



Where  $r$  = the distance between the transmitter and receiver  
 $K(r)$  = a constant function of  $r$   
 $E$  = E-field magnitude in mv/km  
 $H$  = H-field magnitude in gammas

The area of gradual change between the near-field and the far-field distance is known as the "transition-field". Calculations of apparent resistivities in this case use a "transition-triangle method" (Yamashita, 1984). The combination of the calculations for the near-field, and the transition field is considered the first-order correction.

Considering the high resistivity contrast of rock units in the Abitibi though, apparent resistivities need only be compared *relatively*. Consequently data interpreted using the first order correction (or no correction at all in fact) is considered acceptable for resistivity mapping in this environment.

## 7.2 QUALITATIVE INTERPRETATIONS

### 7.2.1 Frequency Pseudosections

The near-field corrected frequency pseudosections provide the starting point for the interpretation of results. By comparing the *relative* apparent resistivities down each line, possible contacts and vertical structure may be interpreted.

The reader must realize when viewing the sections that they do not represent a "slice of the earth", rather they are a convenient means by which to present the data. Each sounding point should be considered individually on the section.

Since the effective depth of investigation of CSAMT is a function of the earth resistivity and the characteristics of the conductor at depth, depth estimates for anomalies cannot be determined with any degree of certainty using qualitative analysis from the frequency sections.

When analyzing CSAMT data, the interpreter must also be aware of several "effects" which, if not considered or understood correctly, can lead to gross misinterpretations:

#### 1) Static Shifts

Small, near-surface resistivity inhomogeneities often strongly affect the calculated apparent resistivity of CSAMT data, the same way that MT and AMT data is affected. When an electrode is placed within, or very near to such a feature, the apparent resistivity curve for that sounding point will be shifted along the resistivity axis. For conductive zones such as swamps, the curve will be shifted *down* the resistivity axis whereas for very resistive zones, such as outcrop, the

curve will be shifted up the resistivity axis.

Static shifts may create interpretation problems when conductors of interest are below near-surface conductors for example. Resistivities from the near-surface anomaly will pull-down the resistivities above the deeper conductor such that the two anomalies may appear to merge as one long, deep conductor.

## 2) Undershoot

In both MT and CSAMT, the apparent resistivity increases as frequency decreases over structure of higher resistivity underlying lower resistivity. When the resistivity contrast is high, the apparent resistivity curve usually decreases *before* beginning to increase. This type of response is more commonly referred to as "undershoot". For data measured in the far-field, the decrease or undershoot is small. For CSAMT data measured in the near-field or the transition field, however, the undershoot is often very large and distinct, which can create problems with depth inversions.

Unfortunately, the undershoot response cannot be corrected using the first order correction. To correct for the effect, the biased data points can simply be removed from the resistivity curve and the curve replotted. However, in some cases it may be difficult to distinguish a true trough of apparent resistivity from an undershoot effect. A simple 1-D forward model may be useful to determine whether the trough is a true response or undershoot.

## 7.3 MODELLING

### 7.3.1 1-D Inversions

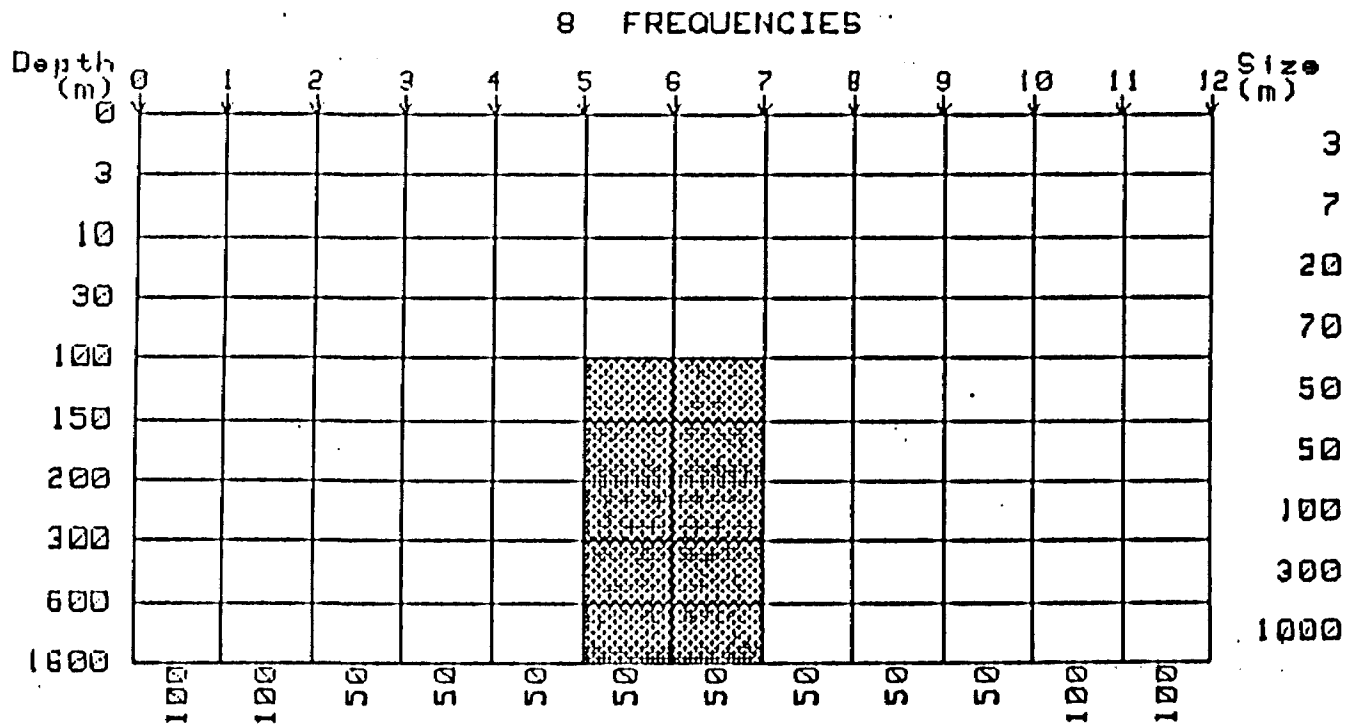
The depth for which the amplitude of the EM field decreases to  $1/e$  (37 percent) of its value at the surface is referred to as the skin depth. The strict definition of skin depth requires a homogeneous medium, however in practical application, such conditions do not exist therefore an apparent skin depth (*skin depth*) for an inhomogeneous medium may be defined as:

$$\text{skin depth}_a = \left( \frac{2\rho_a(f)}{2\pi f \mu_0} \right)^{1/2} \quad (3)$$

Where apparent resistivity ( $\rho_a(f)$ ) is the apparent resistivity measured at that frequency. The *skin depth* is indicative of the depth of penetration of the EM wave, i.e. the lower the frequency of the transmitted signal, the deeper the depth of penetration.



# PHOENIX GEOPHYSICS 2D FINITE ELEMENT CSAMT MODELING



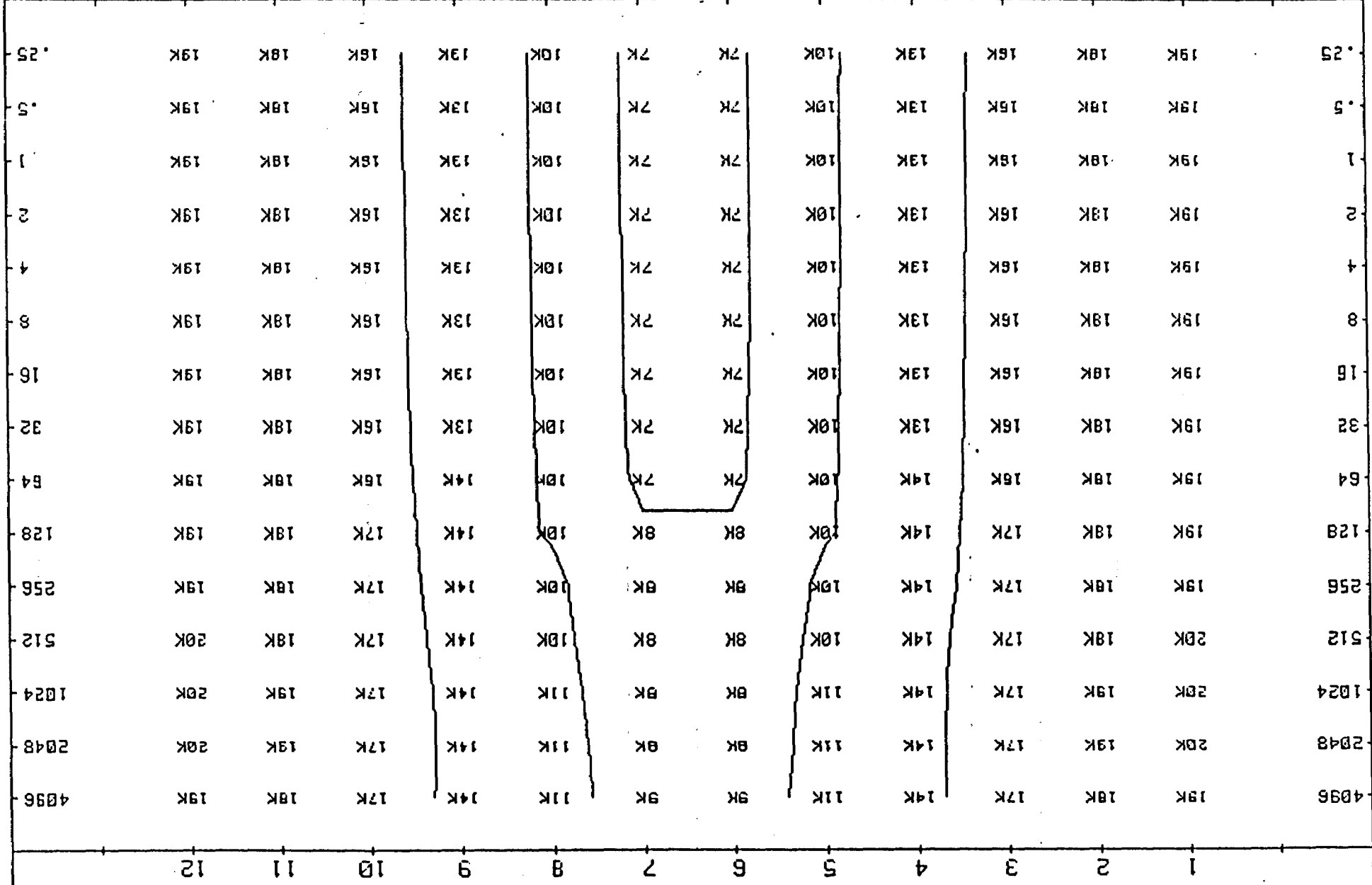
12 X 9 MESH

RES: 20000 10



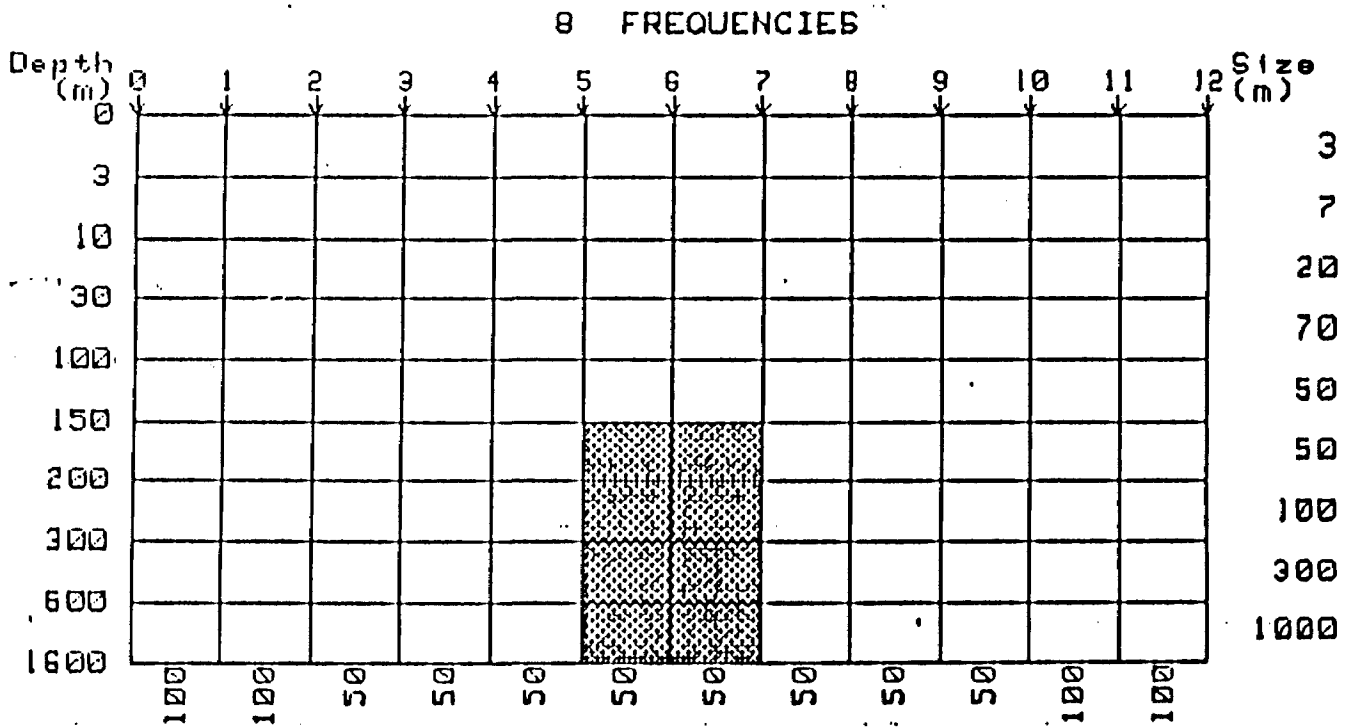
Execution Time = 2:24.18 (MM:SS.SS) on 6 Aug 1987

FIGURE 7.2  
2-D forward model at 100 meters.





# PHOENIX GEOPHYSICS 2D FINITE ELEMENT CSAMT MODELING



12 X 9 MESH

RES: 20000 10



Execution Time = 2:24.18 (MM:SS.SS) on 6 Aug 1987

FIGURE 7.3  
2-D forward model at 150 meters.

PHOENIX GEOPHYSICS, INC.

2-D CSAMT MODELING

	1	2	3	4	5	6	7	8	9	10	11	12	
4096	19K	18K	17K	15K	14K	13K	13K	14K	15K	17K	18K	19K	4096
2048	19K	18K	17K	15K	13K	12K	12K	13K	15K	17K	18K	19K	2048
1024	19K	18K	17K	15K	13K	12K	12K	13K	15K	17K	18K	19K	1024
512	19K	18K	17K	15K	13K	12K	12K	13K	15K	17K	18K	19K	512
256	19K	18K	16K	15K	13K	12K	12K	13K	15K	16K	18K	19K	256
128	19K	18K	16K	14K	12K	12K	12K	12K	14K	16K	18K	19K	128
64	19K	17K	16K	14K	12K	11K	11K	12K	14K	16K	17K	19K	64
32	19K	17K	16K	14K	12K	11K	11K	12K	14K	16K	17K	19K	32
16	19K	17K	16K	14K	12K	11K	11K	12K	14K	16K	17K	19K	16
8	19K	17K	16K	14K	12K	11K	11K	12K	14K	16K	17K	19K	8
4	19K	17K	16K	14K	12K	11K	11K	12K	14K	16K	17K	19K	4
2	19K	17K	16K	14K	12K	11K	11K	12K	14K	16K	17K	19K	2
1	19K	17K	16K	14K	12K	11K	11K	12K	14K	16K	17K	19K	1
.5	19K	17K	16K	14K	12K	11K	11K	12K	14K	16K	17K	19K	.5
.25	19K	17K	16K	14K	12K	11K	11K	12K	14K	16K	17K	19K	.25

Considering the recorded apparent resistivity for each frequency, the apparent skin depth for a sounding point may be estimated by means of a simple inversion program. The program provides reasonable estimates only for layered, horizontally-homogeneous stratigraphy, and is therefore not also be exercised to avoid literal interpretation of depth structures, i.e. finite or isolated conductors (Bartel, 1987).

Static effects, as discussed above, may also lead to errors in inverted models. By the apparent skin depth calculation, the inverted resistivities will be shifted proportionally to the shift in the apparent resistivity curve, while the inverted depth will be shifted proportionally to the square root of the shift of the apparent resistivity curve. The interpreter must exercise care when applying inversions under these conditions to avoid misinterpretations.

### 7.3.2 2-D Forward Modelling

A two dimensional, finite element, forward modelling program was used when necessary to estimate the "best-fit" geology model for a particular frequency pseudosection.

The operator can specify a mesh size and up to seven (7) causative bodies each with an apparent resistivity value. The program was executed on an HP9000 computer by Phoenix Geophysics Ltd. at their facilities in Toronto.

## 8.0 RESULTS AND INTERPRETATION

The C14 project was undertaken to investigate an ultramafic breccia in Clifford Township, Ontario. Several drill holes have been completed, to evaluate the results of a ground magnetic and an IP and resistivity test survey. The CSAMT Test Survey was completed in an attempt to evaluate the usefulness of this relatively new technique in outlining the low resistivity zone that represents the increased porosity associated with the breccia.

Reconnaissance and detailed ground magnetic surveys clearly show a "kidney shaped" magnetic high. The magnetic high is centered at about 7+00N on line 2000E and line 2125N. This magnetic high correlates closely with the breccia pipe, as it was later outlined by the drill holes completed.

Dipole-dipole IP and resistivity measurements were completed on line 2000E and on line 2125E using X=50 meters; n=1,2,3,4,5. These pseudosections both indicate a region of very high resistivities (greater than 2000 ohm-meters) to the south of about 6+00N to 5+00N. On both sets of data, the dipole-dipole results indicate a relatively narrow zone of lower bedrock resistivities (less than 200 ohm-meters) just to the north of this resistivity contact.

This some of lower apparent resistivities is broader on the western line (line 2000E) than it is on line 2125E. To the north of this low resistivity feature, the basement rocks are indicated to have a more moderate resistivity value.

CSAMT measurements were completed on the C14 Grid, with an E-field dipole length of 50 meters. On line 2000E and line 2125E, the CSAMT apparent resistivity pseudosections show resistivity lows that correlate exactly with those detected by the X=50 meters, dipole-dipole measurements. The zone of low resistivities in the bedrock is broader on line 2000E than on line 2125E. The plan map, contoured presentation of the apparent resistivities measured at 64Hz, shows a region of low bedrock apparent resistivities that correlates closely with the magnetic high and the location of the breccia pipe.

The association of a magnetic high and an apparent resistivity low is unusual. Alteration in the bedrock will produce an apparent resistivity low, due to increased porosity. However, most alteration phenomena decrease, or totally destroy, the magnetite content of the rocks. This will result in the measurement of a magnetic low during a survey.

It would appear that magnetic and resistivity surveys would be useful in the search for breccia pipes. However, care must be exercised in the interpretation of these results in regions of deep glacial overburden. The magnetic anomalies may be reduced, due to the greater distance to the source. The apparent resistivity results will be drastically influenced by the presence of the thick, conductive, overburden layer.

The CSAMT pseudosections from line 2500E and line 125 exhibit the type of apparent resistivity pattern that can be encountered.

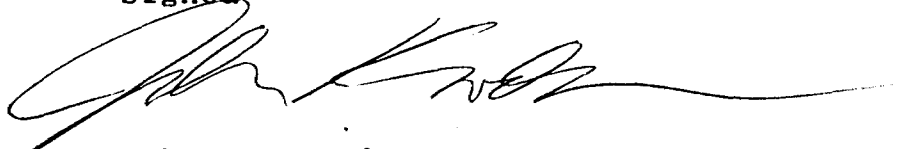


CERTIFICATION

I John M. Kovala certify:

1. That I reside at 7 Teck Hughes Property  
Kirkland Lake Ontario.
2. That I have completed the B.Sc. program in  
Geology at Laurentian University.
3. That I have been employed in the exploration  
Industry since 1983.

Signed



John M. Kovala  
Project Geologist

Qual 2.10571

APPENDIX A

TECHICAL SPECIFICATIONS --- PHOENIX V4, T30, MG30

## SIGNAL PROCESSING, DIGITAL

### A-D Conversion

16 bits, giving a resolution of 1 part in 65,000.

### Sampling Rate

Controlled by microprocessor to a maximum of 12.5 kHz (16 kHz by early 1983).

## TEST AND CALIBRATION

### Calibration

A test signal output is provided to perform test and calibration functions. There is also a processor controlled internal test mode that allows automatic precise calibration of all filters. Calibration responses may be stored in the instrument and automatically removed from the measurements.

### Test Signal

The externally available test signal can be either: a frequency domain signal of  $\pm 5V$ , 200 ohm impedance, frequency 4 kHz - 1/128 Hz, or a time domain signal with a 50% duty cycle.

### Display and Controls

The display is a 64 character dot matrix LCD and the computer results presented are the mean and standard deviation as well as the stack number.

All modes of operation and parameter control entries may be displayed and the display will prompt the operator to make the appropriate keypad entries.

The LCD will operate to a temperature of -10°C. For lower temperature operation an LCD heater is required (optional).

### Memory

Non-volatile memory for data logging is provided. This is sufficient for storage of 36 SIP stations with a full complement of channels over the entire frequency range. Although this is sufficient for approximately three days operation, a further memory extension is optionally available.

## I/O Ports

The memory may be transferred into a computer by an 8-bit parallel I/O port or by an optional serial RS-232 port.

### Printer

A vest pocket-sized, 20 column, dot matrix printer operates through the 8 bit parallel I/O port. Power for the printer is supplied by the V-4; no additional batteries are required. The external printer configuration permits better environmental protection.

### Analog Meters

A meter for each channel provides continuous monitoring of the signals. These meters are also used for battery monitoring.

## GENERAL

### Temperature

The storage temperature range is -50°C to +70°C. The operating temperature range is -40°C to +50°C, (-10°C to +50°C without LCD heater option).

### Humidity

The instrument is moisture proof and may be operated during rain.

### Altitude

-1600 m to 5000 m.

### Vibration

Suitable for transport in light aircraft and bush vehicle.

### Weight

13 kg.

### Case

The case is made of an Acrylic PVC alloy, which is vacuum formed, extremely tough, resilient, weather resistant and a good electrical insulator. It is equipped with a removable lid, carrying handle and packboard tie down loops.

### Dimensions

32 cm x 36 cm, 27 cm high.

### Batteries

The standard instrument is equipped with three 6 volt rechargeable gel cells. The battery charger circuit (less transformer) is built-in.

## Controlling Firmware

### Programs

The standard version of the V-4 includes the control program for Spectral Induced Polarization operation (SIP).

### Optional Programs available

Controlled Source Audio Magnetotelluric (CSAMT)  
Time domain Induced polarization  
Others: Consult Phoenix for details.

## Spectral I.P. [SIP] Operation

### Frequencies

$2^{10}$  Hz to  $2^{12}$  Hz (1/1024 to 4096 Hz) in binary steps. An automatic frequency scan is initiated by selecting Fhigh and Flow to be different values. The scan can step by a factor of 4, 2, or  $\sqrt{2}$ .

### Transmitter Links

For spectral IP, two highly isolated RF communication links are provided:

A: Transmitter drive link for transmitter switching control via a twisted pair cable.

B: Current Monitor link.

This link provides an accurate replica of the transmitter current to one of the eight channel inputs. This allows real-time deconvolution of the transmitter waveform from the other input channels. The required isolation transformer and demodulation circuits are built into the V-4.

### Deconvolution

The physical quantity which we are attempting to determine is the resistivity transfer function. Since it is not possible to control kilowatts of power passing through unstable current electrodes to an accuracy of 1 part in 10000, it is necessary to monitor both current and voltage and then to deconvolve the current from the voltage to obtain the true spectral IP response. This deconvolution is carried out automatically in the V-4 at each frequency by dividing the voltage amplitude by the current amplitude and by subtracting the current phase from the voltage phase for all six voltage channels.

### Operating Sequence

START sets the receiver and transmitter to 1 Hz and allows the System to cancel SP and adjust gain for each channel.

ENTER is pressed after each of the operating parameters is input through the keypad.

A averaging time  
B number of channels  
C current in amperes  
D dipole identification  
E electrode interval in meters  
F frequency range (Fhigh, Flow)

The six parameters are held in memory. Only a few are usually changed from station to station along a line.

PRINT prints out the six operating parameters if it is desired to check their values.

RUN starts the automatic frequency scan. The unit first measures, calculates and prints the resistivity at 1 Hz. It then proceeds to Fhigh, makes the required measurements, displays and prints the results, proceeds to the next frequency and so on, down to Flow.

STORE is pressed if the scan is satisfactory and it is desired to store the results in memory.

## Software

Phoenix supplies complete applications software for transferring spectral IP data to a computer; fitting the Cole-Cole model to spectral IP data; calculation of Cole-Cole parameters; removal of electromagnetic coupling; and plotting and contouring data pseudosections.

In addition, Phoenix supplies 2-dimensional modelling programs for both forward and inverse problems, to aid in interpretation.

All programs are written in BASIC.

## CSAMT Operation

### Frequencies

$2^2$  to  $2^{12}$  (0.25 Hz - 4096 Hz) in binary steps (or  $\sqrt{2}$  steps).

### Productivity

Since the horizontal H field varies slowly, it is possible to measure only one H field for six electric dipoles. Thus production rates are six times greater than those of older, conventional, 2-channel instruments.

## Real-time Calibration

The standard procedure is to store the transfer function of the instrument in memory and remove it from the signal in real time.

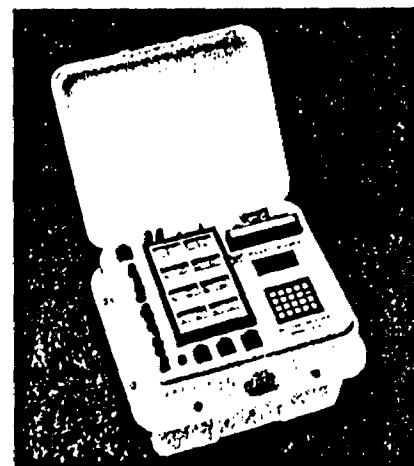
## Software

In addition to the CSAMT control program, BASIC software utilities are available for plotting and contouring pseudosections of Cagniard apparent resistivity, and correcting for the near-field situation.

# V-4

## Eight Channel Universal Receiver

- **Versatility** Instrument may be used for spectral IP, CSAMT, and conventional IP in either frequency or time domain.
- **Productivity** Simultaneous measurement of eight input channels.
- **Microprocessor Control** Microprocessor-controlled real-time filtering, signal stacking and averaging in time or frequency domain.
- **Reliability** Data logging in solid state non-volatile memory.
- **Standard I/O** Output ports for a vest pocket printer and computer or data link.
- **Automated Operation** Automatic gain control and self-potential (SP) cancellation.



### Features

#### EXTREMELY BROAD FREQUENCY RANGE

The V-4 was designed to cover the frequency range of most interest for electrical measurements. Its complete frequency range is six decades. With a top frequency of 4096 HZ it is a multifrequency EM unit as well as a spectral IP unit. High frequency measurements may be made very quickly, and provide useful, detailed data about the resistivity section. Pseudosection plots of the high frequency phase angles provide geometric as well as parametric EM information. The intermediate frequencies allow very accurate removal of electromagnetic coupling from IP data, and provide information on mineral type, which in certain situations can result in considerably more cost-effective exploration programs. Alternatively the high-frequency measurements may be made in CSAMT mode, providing rapid reconnaissance measurements of resistivity from 0.25-4096 Hz.

#### DESIGNED FOR BOTH RESEARCH AND PRODUCTION

The V-4 has been designed to be both an extremely powerful research instrument as well as the fastest production IP unit available. The conversion is accomplished simply by changing the limits of the frequency scan. Reconnaissance work might be carried out at a single frequency in which case the measurements are extremely fast and accurate. If an anomaly is encountered, the scan may be widened to provide additional data useful for the evaluation and removal of inductive coupling, and for purposes of mineral discrimination.

#### EIGHT CHANNEL CAPABILITY

The multichannel capability of the V-4 can decrease measurement time by a factor of six over conventional units.

#### REAL TIME DECONVOLUTION

Any variations in the transmitter waveform are closely monitored and accurately compensated for. This is equivalent to continuous calibration of the transmitter electrodes. All calculations are made in real time. No measurement time is wasted waiting for the processor, even at 4 kHz.

#### MEAN/STANDARD DEVIATION

Both mean and standard deviation are continuously displayed and recorded. Thus a constant record is maintained of the precision of the measurement. If the desired accuracy is achieved early, time can be saved by pressing NEXTF. The processor then prints the results and proceeds with the next frequency.

#### VERSATILITY

The V-4 can be used for spectral IP, conventional IP in time or frequency domain, and CSAMT, resulting in an extremely cost-effective instrument package.

#### OPTIONS

- Dipole preamplifiers for spectral IP operation in high resistivity areas.
- RS-232 I/O port.
- LCD heater for extended cold temperature operation.
- Memory extension.
- Operating firmware for CSAMT, time domain IP, and others to be announced.

### Specifications, Hardware

#### INPUT

##### Channels

High input impedance differential amplifiers. Eight input channels may be measured simultaneously. Six channels are combined in one input connector. The other two inputs are equipped with isolated power supplies to power external devices such as coil preamplifiers.

##### Impedance

1000 Megohms.

##### Protection

The input is protected from excessive voltages by a 10,000 ohm fuse resistor.

##### Ranges

To  $\pm 10V$  maximum input signal.

#### SIGNAL PROCESSING, ANALOG

##### Gains

1 to 640, under microprocessor control.

##### Power Line Filtering

Triple notch filter for 1st, 3rd and 5th harmonic of 50 or 60 Hz. Notch depth 40 db minimum. Filter may be switched in or out.

##### Anti-Alias Filter

7 pole low pass filter with processor controlled corner frequencies.

##### Sp Cancellation

Under microprocessor control up to a range of  $\pm 2.5V$ .



## PHOENIX GEOPHYSICS LIMITED

Geophysical Consulting and Contracting, Instrument Manufacture, Sale and Lease.

Head Office:

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Markham, Ontario, Canada L3R 5M7  
Tel: (416) 477-8588  
Telex: 08-888586, Fax: 416-477-9231



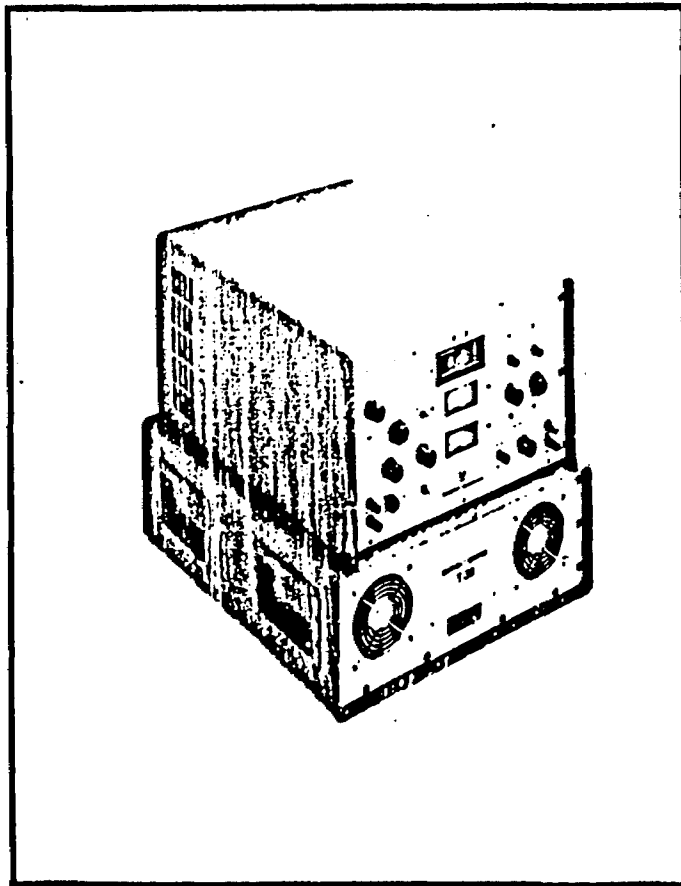
PHOENIX Geophysics Limited

7100 WARDEN AVENUE, UNIT 7, MARKHAM, ONTARIO CANADA L3R 5M7

TELEPHONE (416) 477-8588  
Telex: 06-986856  
Cable: PHEXCO TORONTO

# T-30

## MULTIPURPOSE CONTROLLED SOURCE



THE T-30 IS THE MOST ADVANCED CONTROLLED CURRENT SOURCE AVAILABLE FOR ELECTRICAL METHODS EXPLORATION. IT COMBINES MODERN GTO TECHNOLOGY WITH THIRTY YEARS OF TRANSMITTER DESIGN EXPERIENCE.

THE T-30 (30 KW ) IS ONE OF TWO UNITS, IDENTICAL IN ALL SPECIFICATIONS EXCEPT FOR POWER AND WEIGHT. THE LIGHTWEIGHT VERSION OF THE T-30 IS DESIGNATED THE T-15. THE 15 kw T-15kw IS DESIGNED FOR END-USERS WHOSE APPLICATION PLACES A PREMIUM ON PORTABLILITY.

THESE TRANSMITTERS CAN BE USED FOR A VARIETY OF GEOPHYSICAL TECHNIQUES, INCLUDING CONVENTIONAL IP IN THE TIME OR FREQUENCY DOMAIN; TRUE WIDEBAND SPECTRAL IP; CSAMT (CONTROLLED SOURCE AUDIO MAGNETOTELLURICS); AND TDEM ( TIME DOMAIN ELECTROMAGNETICS ).

THE TRANSMITTER LOAD MAY BE EITHER A GROUNDED DIPOLE OR A LOOP, DEPENDING ON THE REQUIREMENTS OF THE APPLICATION. THE RAPID CONTROLLED TURN-OFF INTO INDUCTIVE LOADS IS SUITABLE FOR TDEM APPLICATIONS.

A VERY WIDE RANGE OF STANDARD BINARY-RELATED TIMING OPTIONS IS PROVIDED, AS WELL AS AN INPUT CONNECTION FOR AN ARBITRARY EXTERNAL TIMING DRIVE.

THESE UNITS ALSO FEATURE A VARIETY OF PROTECTIVE CIRCUITS, BUILT IN RECEIVER CALIBRATION CIRCUITRY, CURRENT MONITOR OUTPUT FOR EXTERNAL DECONVOLUTION, CONSTANT CURRENT CONTROL, AND SEMI-INFINITE IMPEDANCE IN THE "OFF-TIME" WHEN USED FOR TIME-DOMAIN IP.

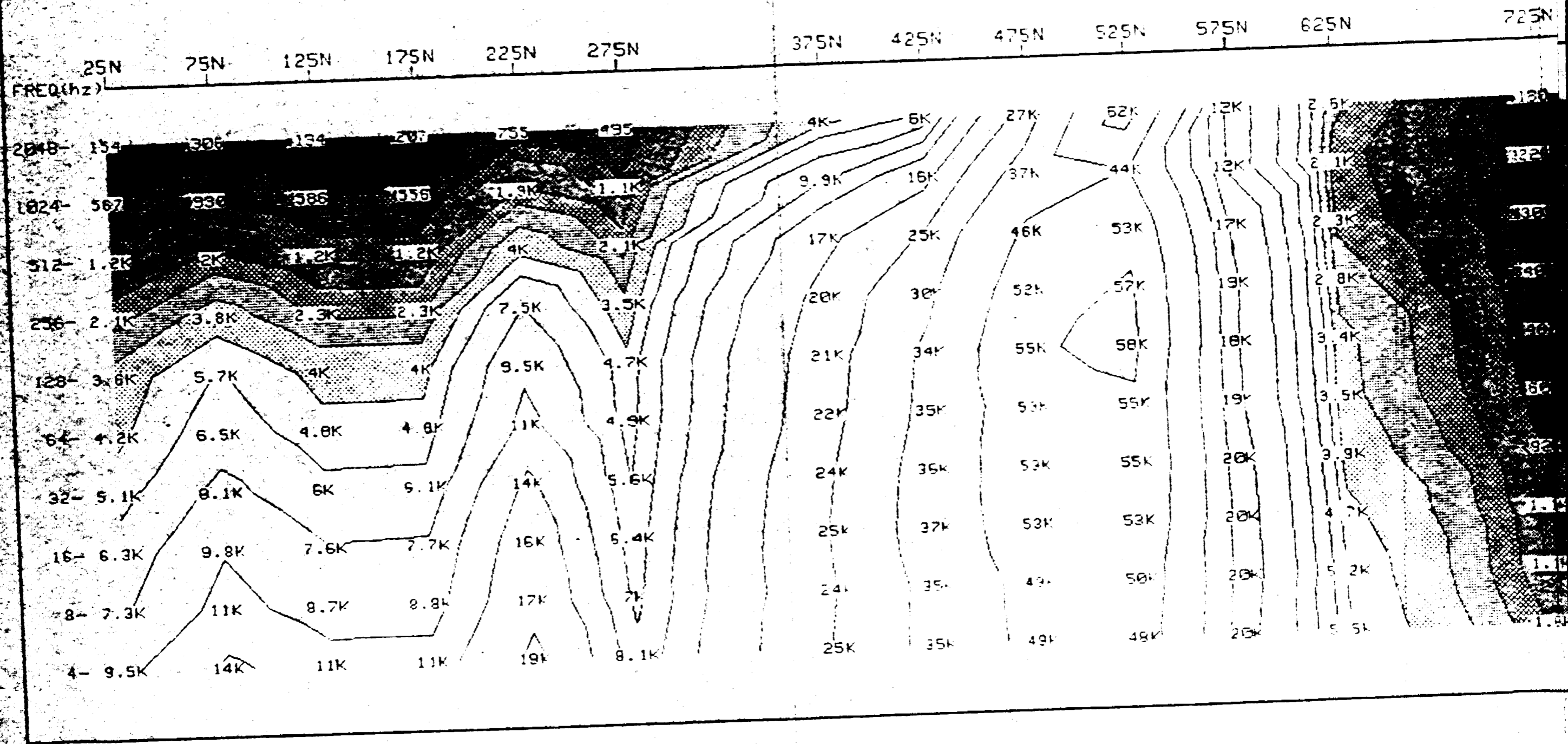
SUMMARY SPECIFICATIONS FOR THE TRANSMITTERS ARE GIVEN BELOW:

FREQUENCY	: DC - 10 KHZ.
MAX. VOLTAGE	: 800 VOLTS.
MAX. CURRENT	: 40 AMPERES.
WEIGHT	: T-15 75 KØ.
	: T-30 120 KØ.

THE STANDARD POWER SOURCE FOR BOTH UNITS IS THE MØ-30 MOTOR GENERATOR. HOWEVER, AS ANY SUITABLE MØ UNIT MAY BE USED, IT IS NOT NECESSARY TO PURCHASE THE MØ UNIT FROM PHOENIX.

IN ADDITION TO THE MØ-30, WHICH EMPHASIZES HIGH POWER/LOW WEIGHT, PHOENIX OFFERS A VARIETY OF MØ OPTIONS. THE USER MAY REQUEST GASOLINE OR DIESEL ENGINES; 60 HZ. OR 400 HZ. ALTERNATORS; AND 110/208 V OR HIGHER VOLTAGE OUTPUT.

APPENDIX B  
CSAMT FREQUENCY PSEUDOSECTIONS



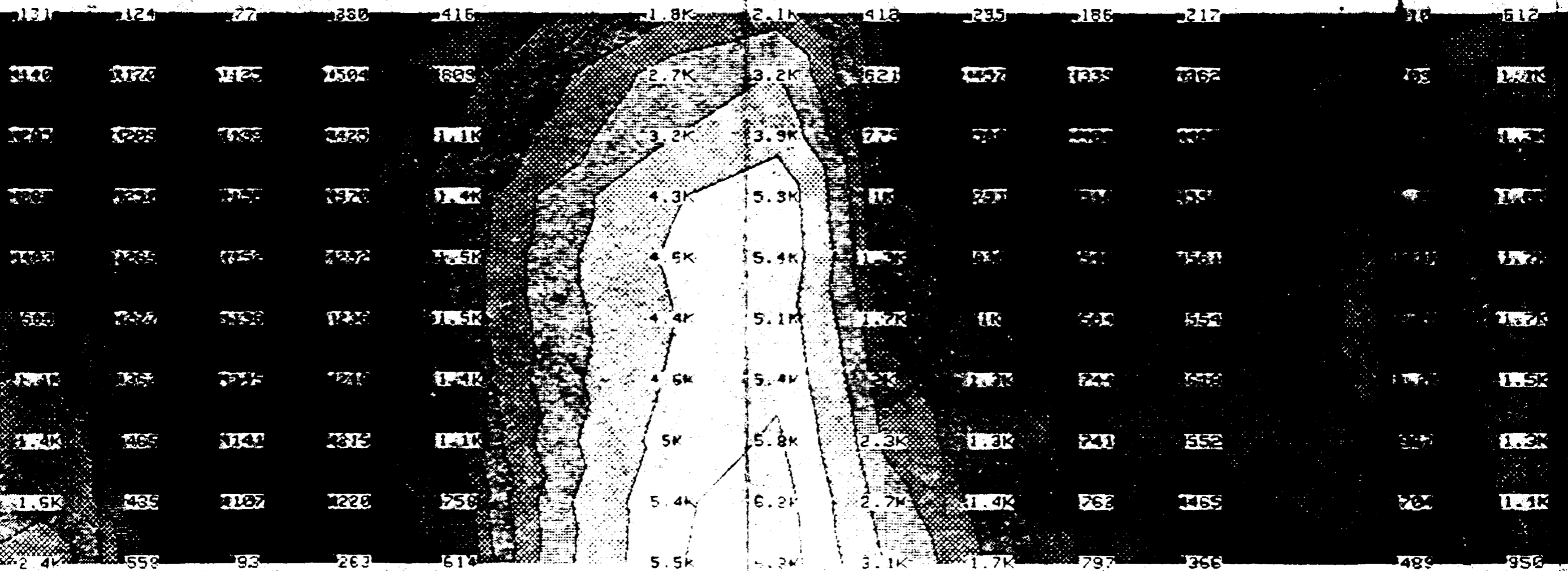


# CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 LINE=0E

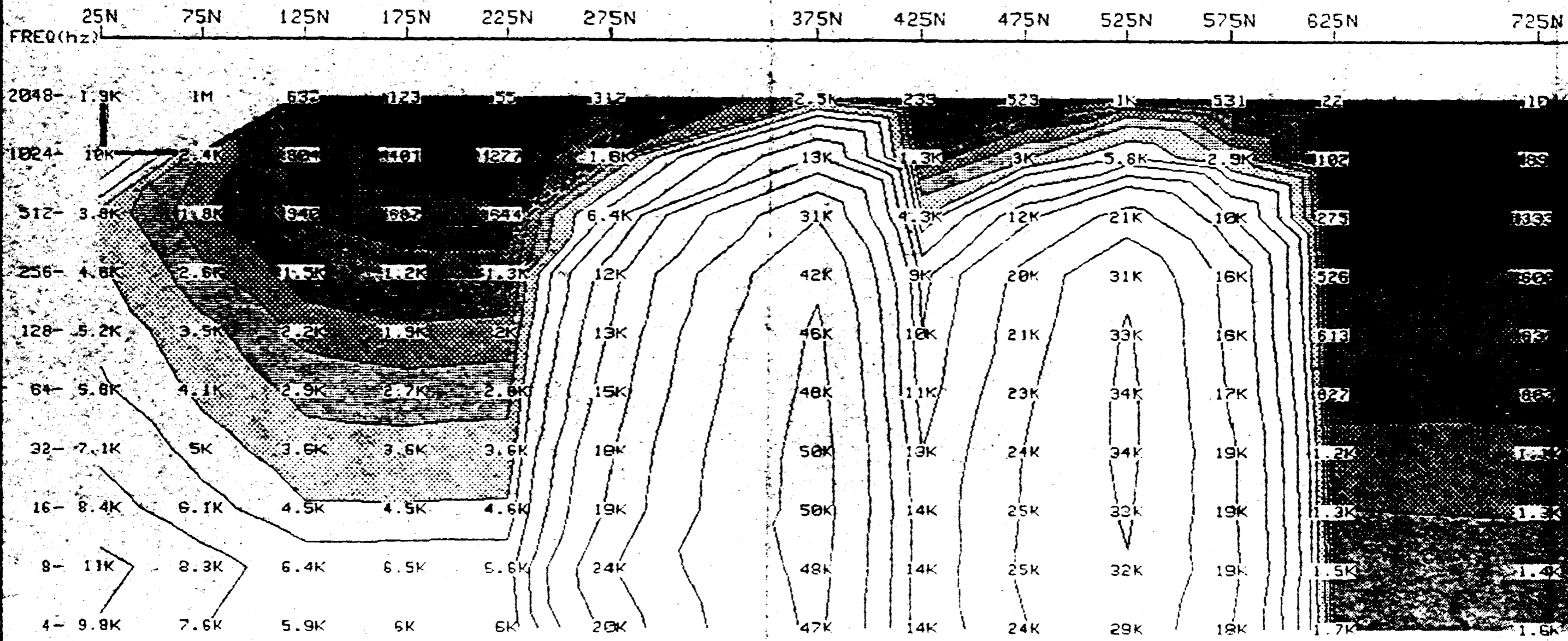
E-dipole = 5000ft Tx-Rx = 11.5km

775N    825N    875N    925N    975N    1075N    1125N    1175N    1225N    1275N    1325N    1425N    1475N



Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV 1987

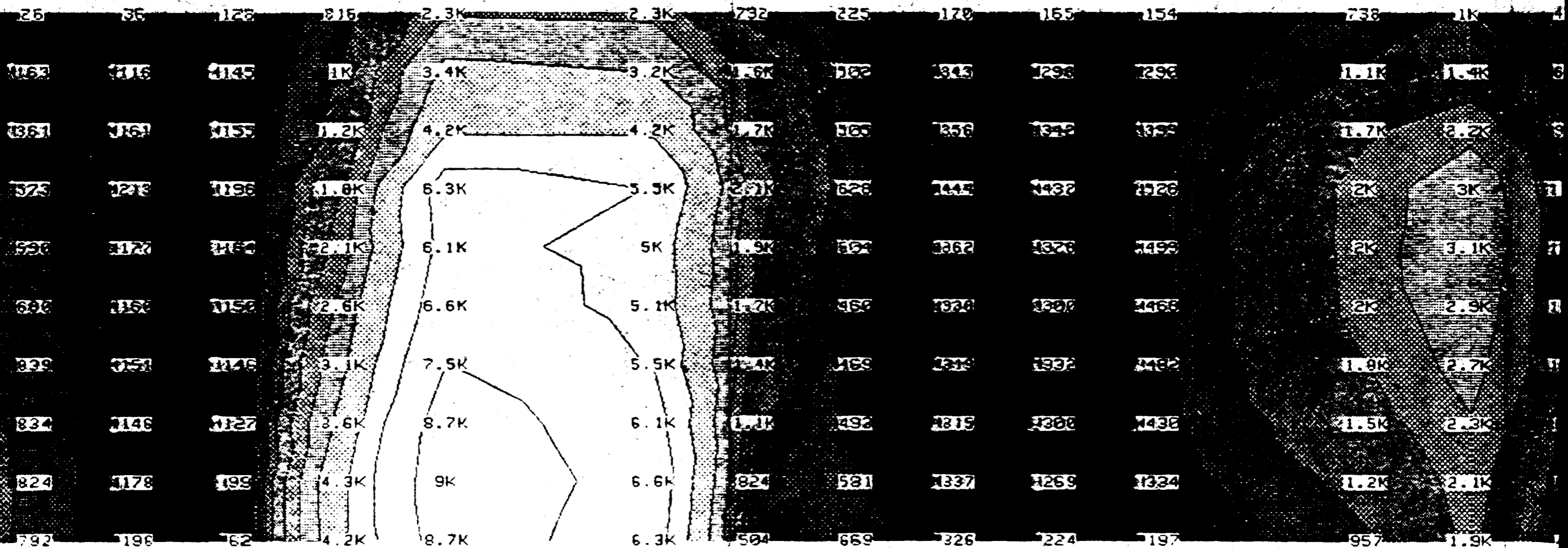
1525N	1625N	1675N	1775N	1825N	1875N	1925N	1975N	2025N	FREQ(hz)
562	205	328	285	390	348	461	807	782	-2048
980	1494	595	1308	743	780	946	1.7K	2K	-1024
1.9K	816	768	728	1.1K	1K	1.2K	2K	2.5K	-512
1.8K	786	852	788	1.3K	1.4K	1.5K	2.7K	3.5K	-256
1.7K	765	1K	891	1.4K	1.4K	1.7K	3K	4K	-128
1.6K	725	1K	898	1.4K	1.5K	1.6K	2.7K	3.7K	-64
1.5K	788	1K	886	1.2K	1.2K	1.3K	2.1K	3.1K	-32
1.3K	576	869	539	930	930	1K	1.7K	2.7K	-16
1K	7455	3608	7483	684	667	712	1.1K	2.2K	-8
845	312	461	382	409	466	453	745	2K	-4



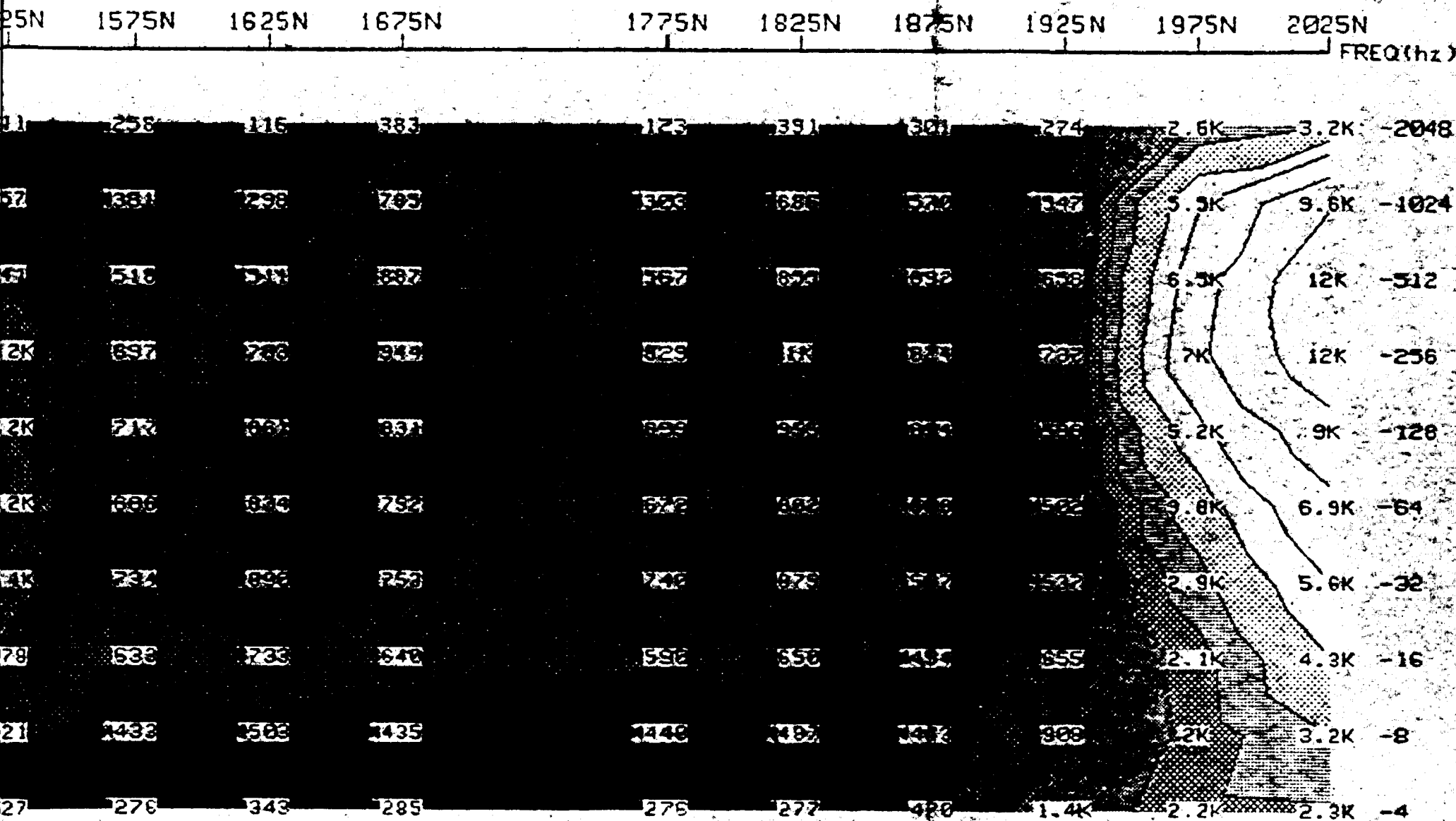
# CSAMT APPARENT RESISTIVITY (CORRECTED)

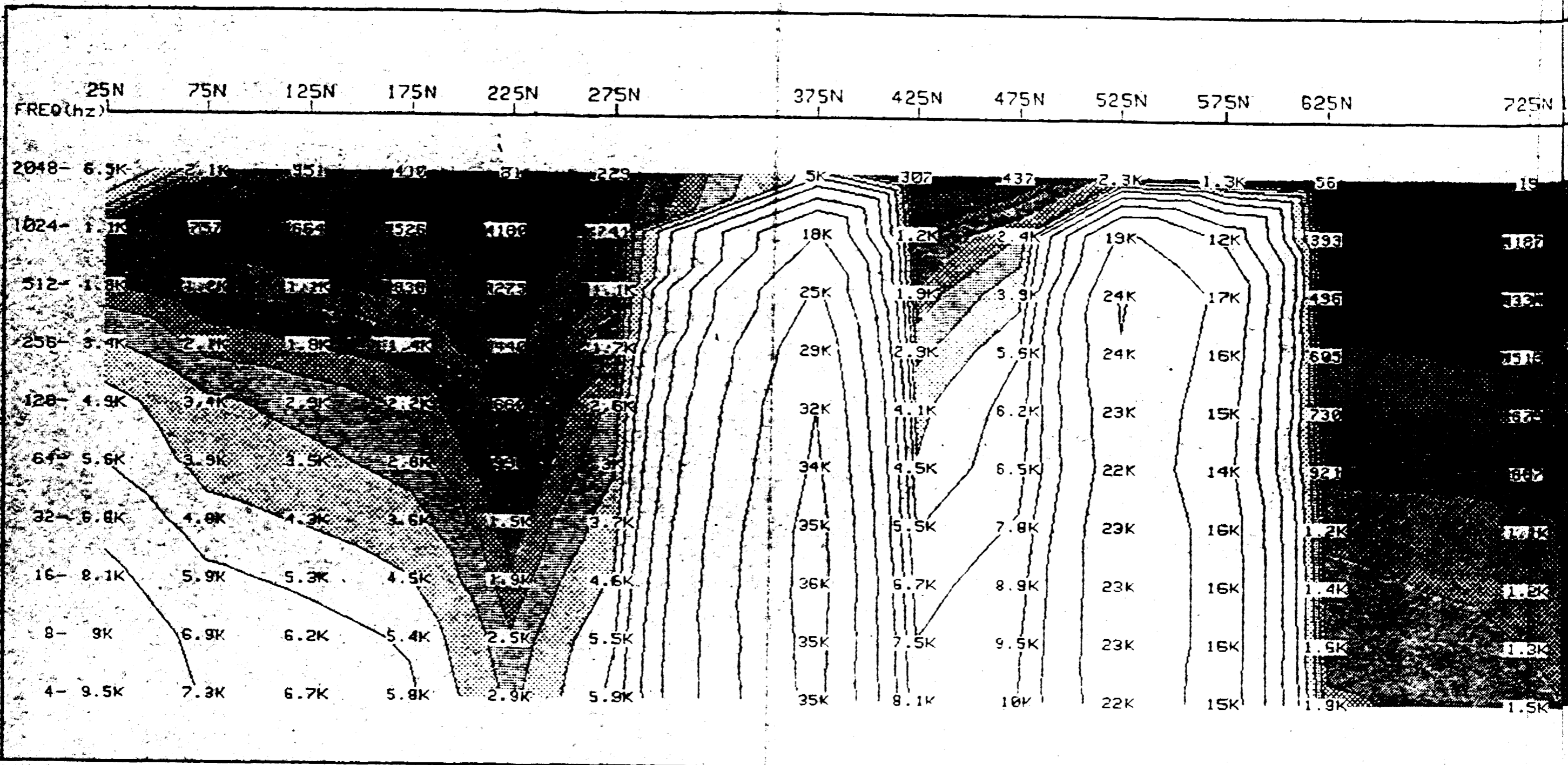
LAC. MINERALS LTD. C14 LINE=125E E-dipole=5000ft Tx-Rx=11.375km

775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N 1475N 1525N



Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV 1987



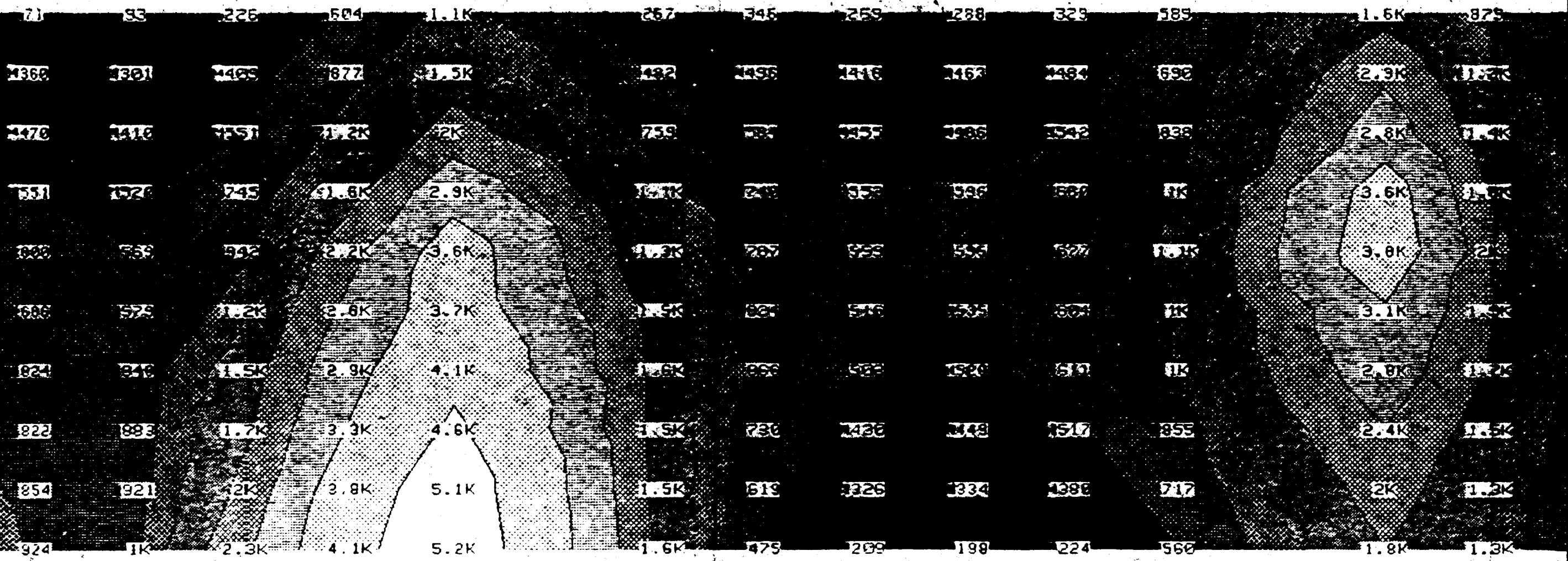


# CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 LINE=250E

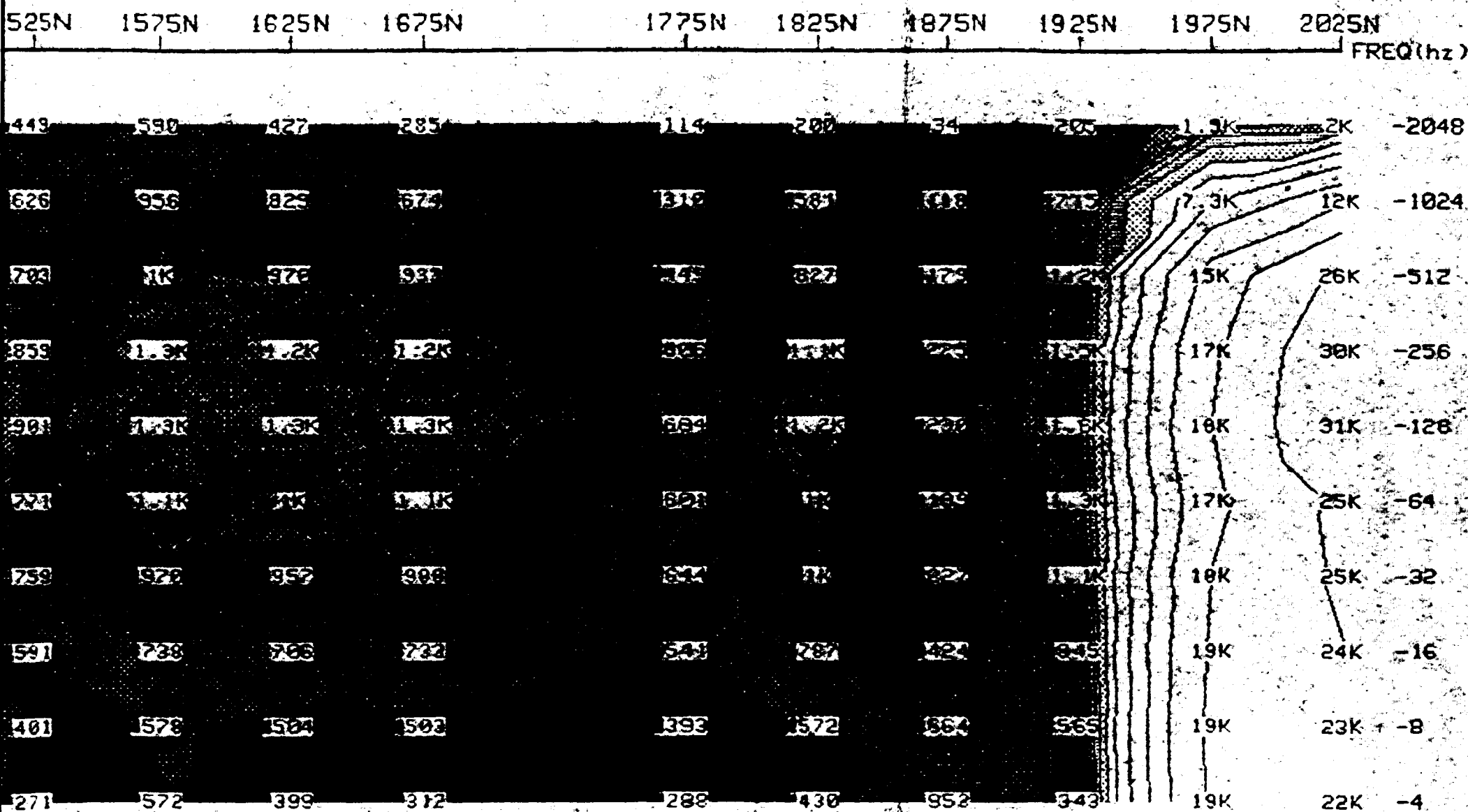
E-dipole=5000ft Tx-Rx=11.25km

775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N 1475N



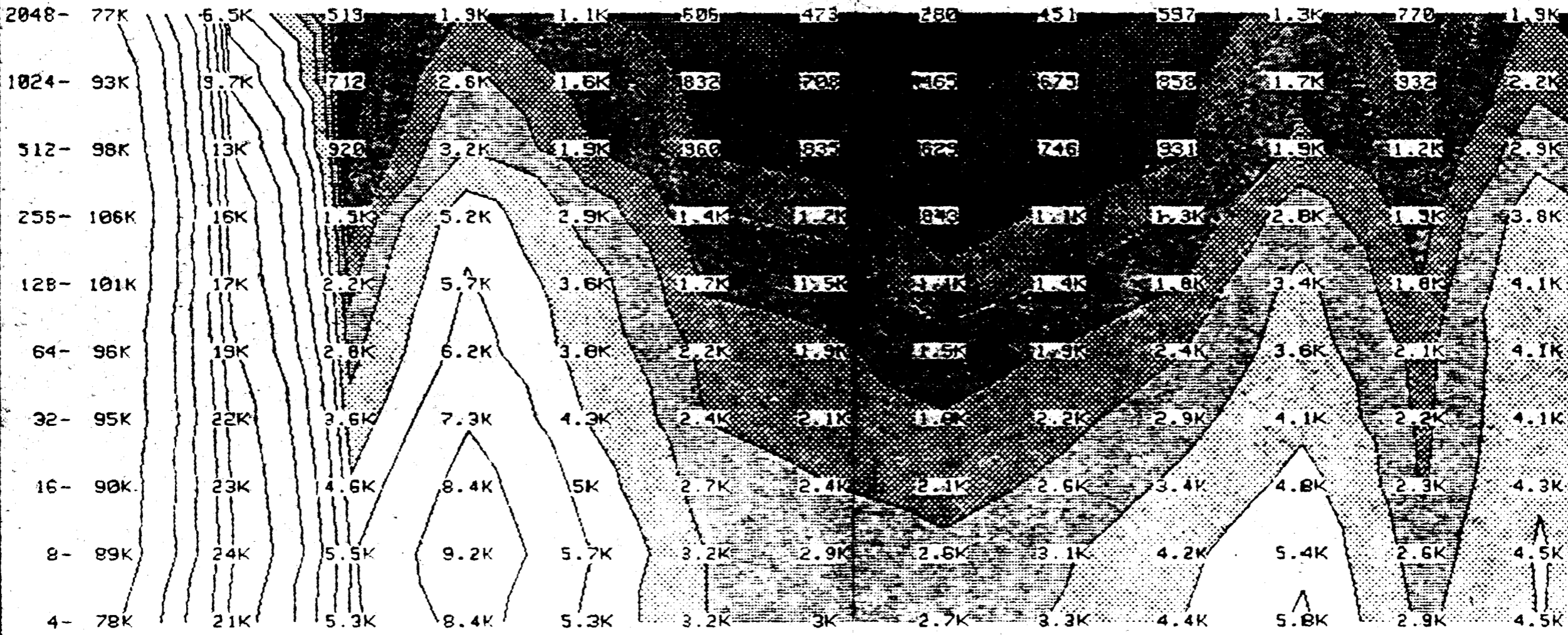
Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV/1987







FREQ (hz)    375N    425N    475N    525N    575N    625N    675N    725N    775N    825N    875N    925N    975N

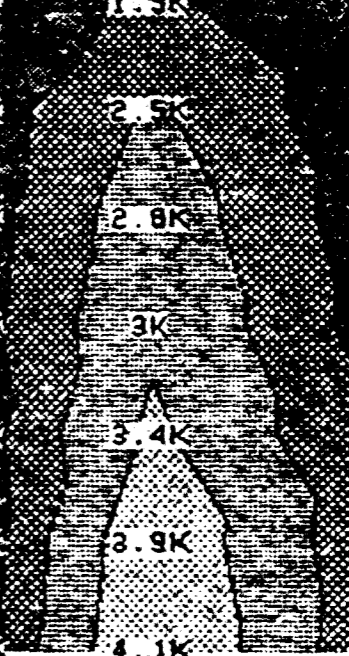


MT APPARENT RESISTIVITY (CORRECTED)

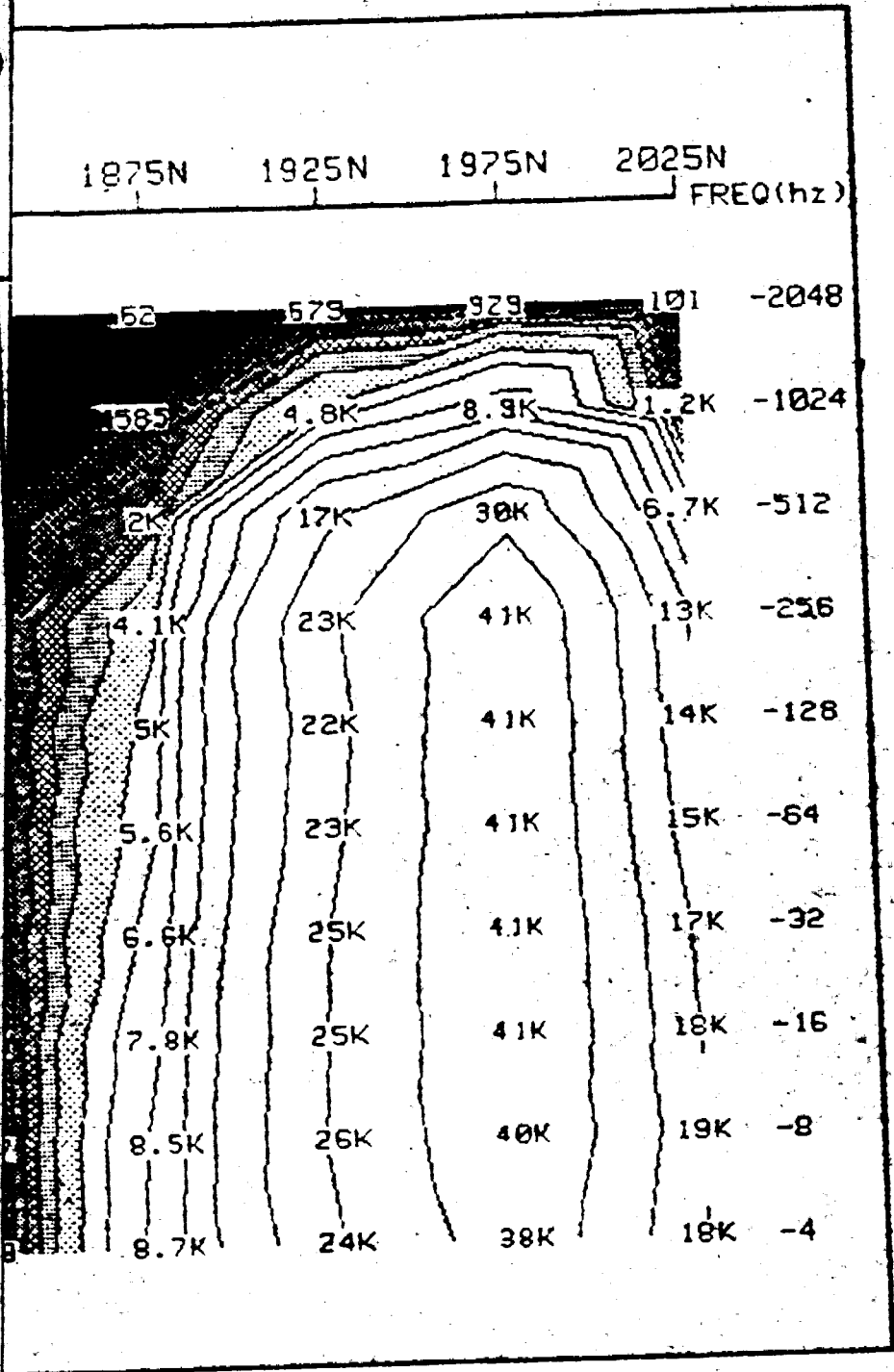
0. C14 LINE=375E E-dipole=5000ft Tx-Rx=11.125km

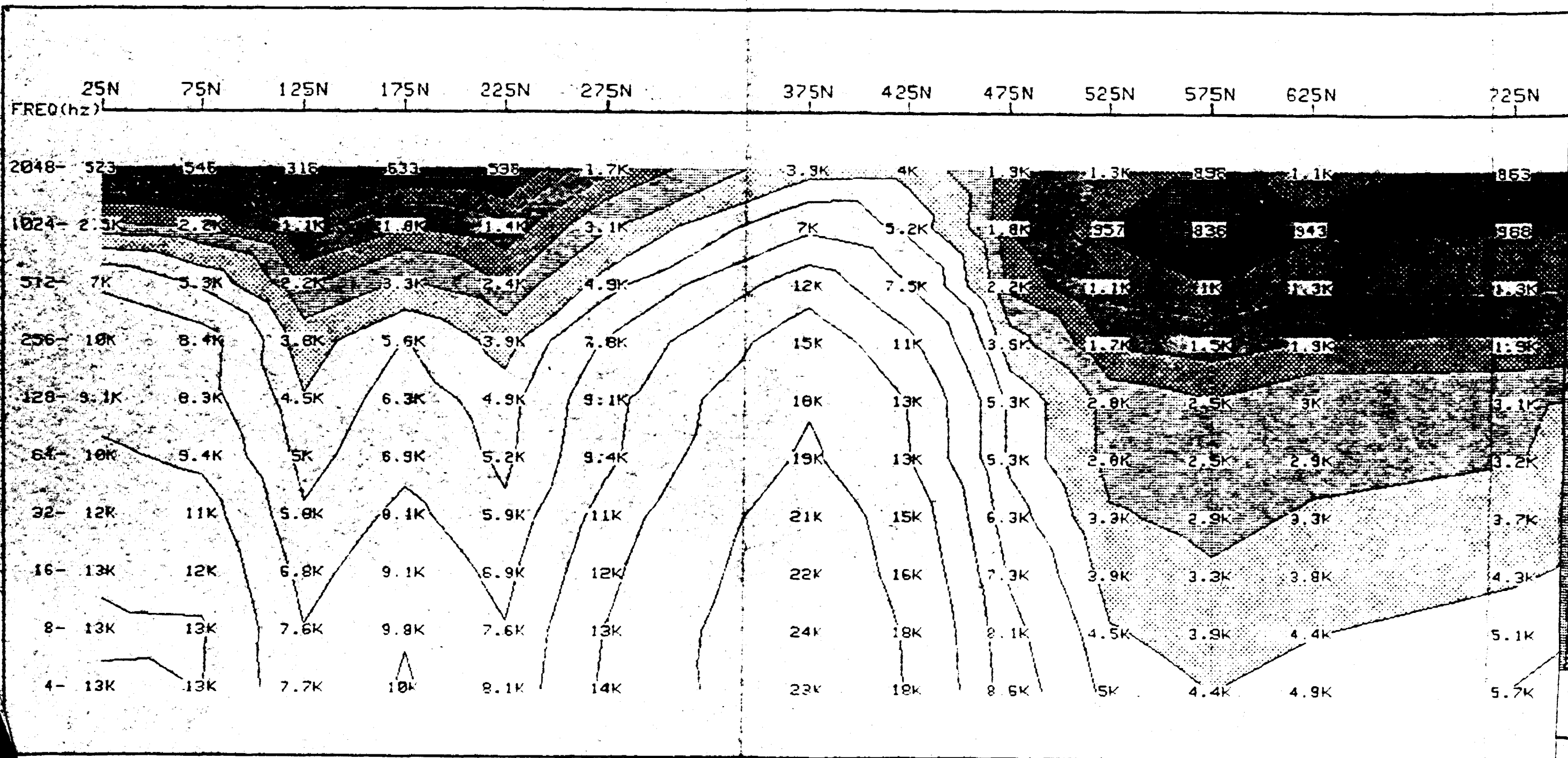
75N 1125N 1175N 1225N 1275N 1325N 1425N 1475N 1525N 1575N 1625N 1675N 1775N 18

55	323	253	345	405	485	534	844	891	514	201	52	35	5
63	7486	7418	7537	691	785	1.1K	1.4K	1.2K	782	664	405	768	12
716	586	7585	7588	690	848	1.4K	1.6K	1.4K	996	1.1K	1.2K	720	14
741K	622	813	692	614	985	1.4K	1.5K	1.7K	1.2K	1.3K	1.9K	543	15
741K	622	693	676	790	890	1.4K	1.9K	1.7K	1.2K	1.4K	2.5K	621	17
741K	677	696	676	815	6K	1.5K	1.6K	1.6K	1.3K	1.5K	2.8K	496	18
1.4K	758	664	696	846	890	1.5K	1.5K	1.4K	1.3K	1.5K	3K	494	19
1.4K	736	623	602	700	818	1.5K	1.5K	1.4K	1.1K	1.4K	3.4K	455	20
1.4K	673	1482	1427	1555	831	88	299	931	1K	1.3K	3.9K	857	21
1.5K	623	382	328	382	443	580	466	580	999	1.4K	4.1K	267	22



Resistivity in ohm-m  
 Surveyed by QUIANTECH CONSULTING INC. NOV/1987



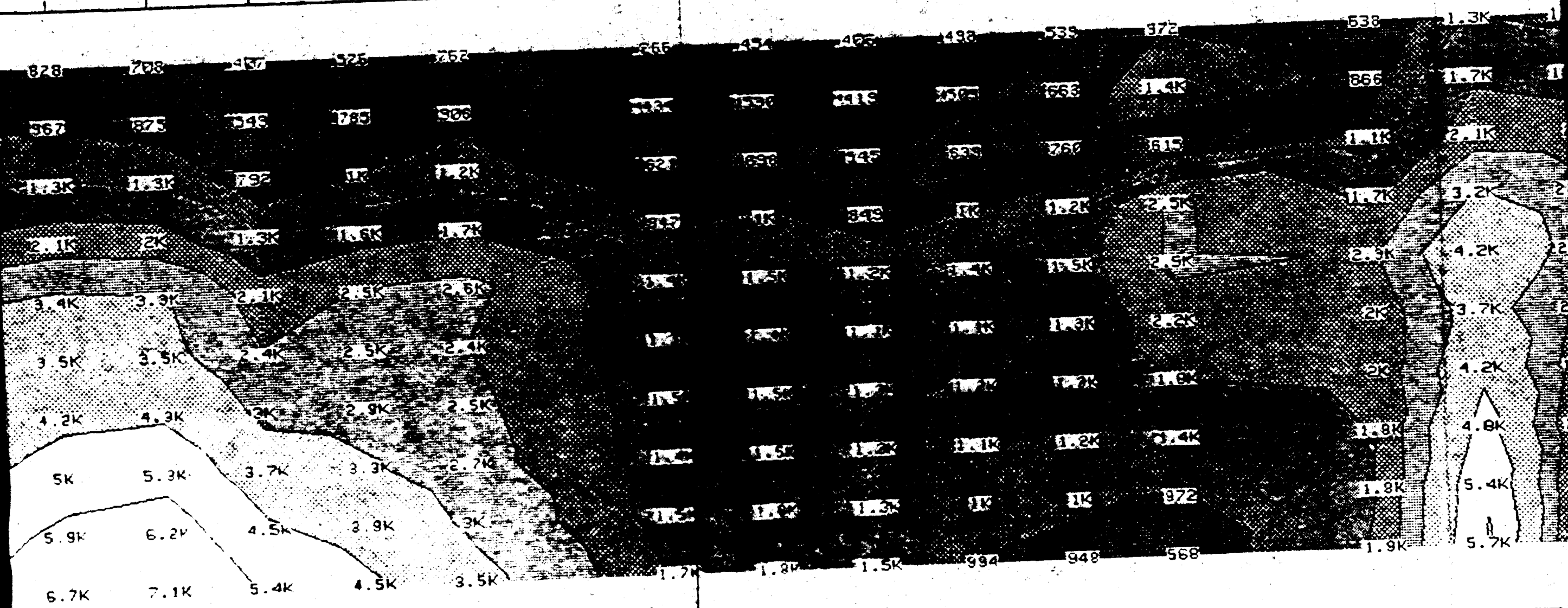


# CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 LINE=500E

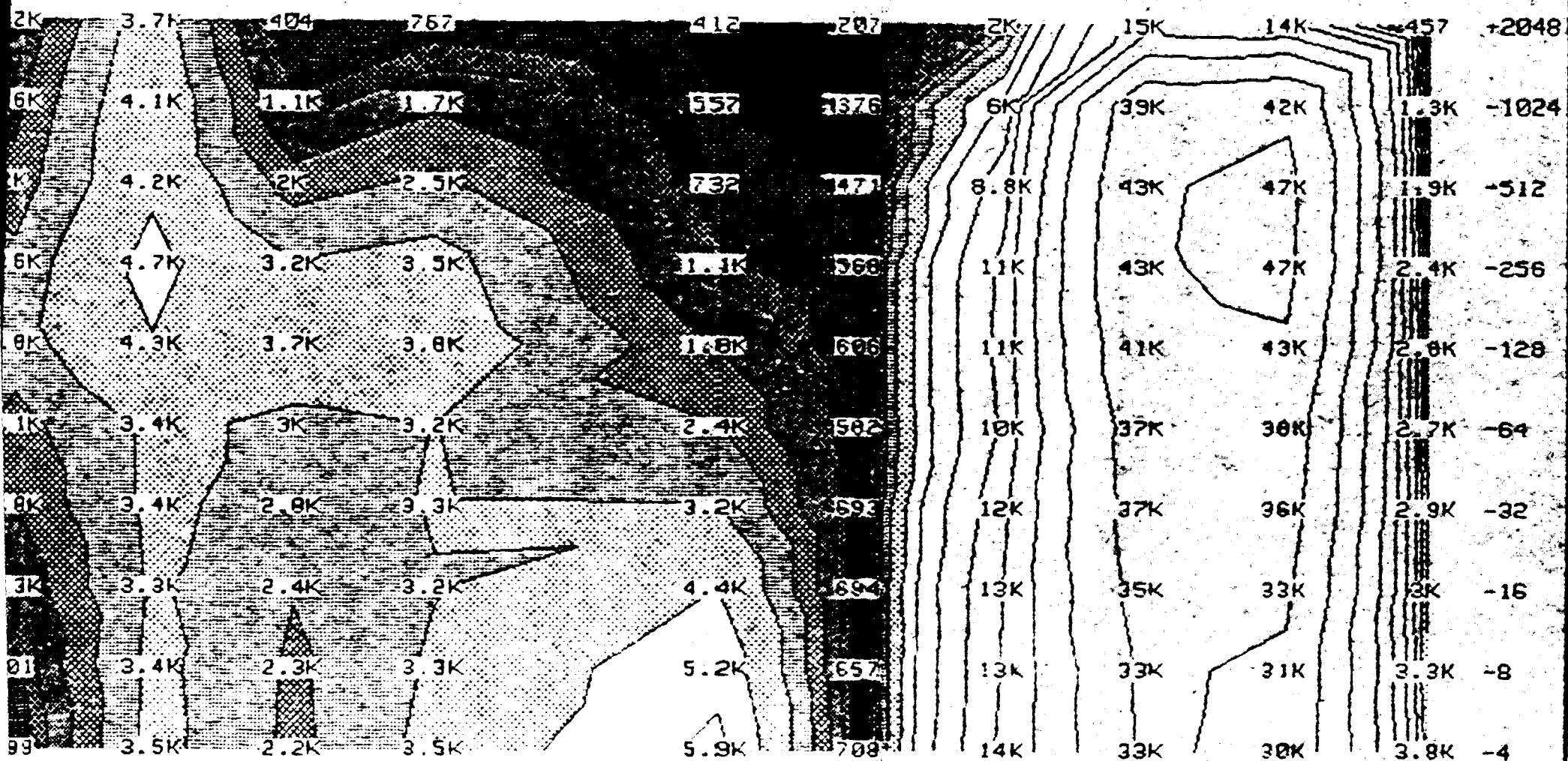
E-dipole=5000ft Tx-Rx=11km

775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N 1475N 15

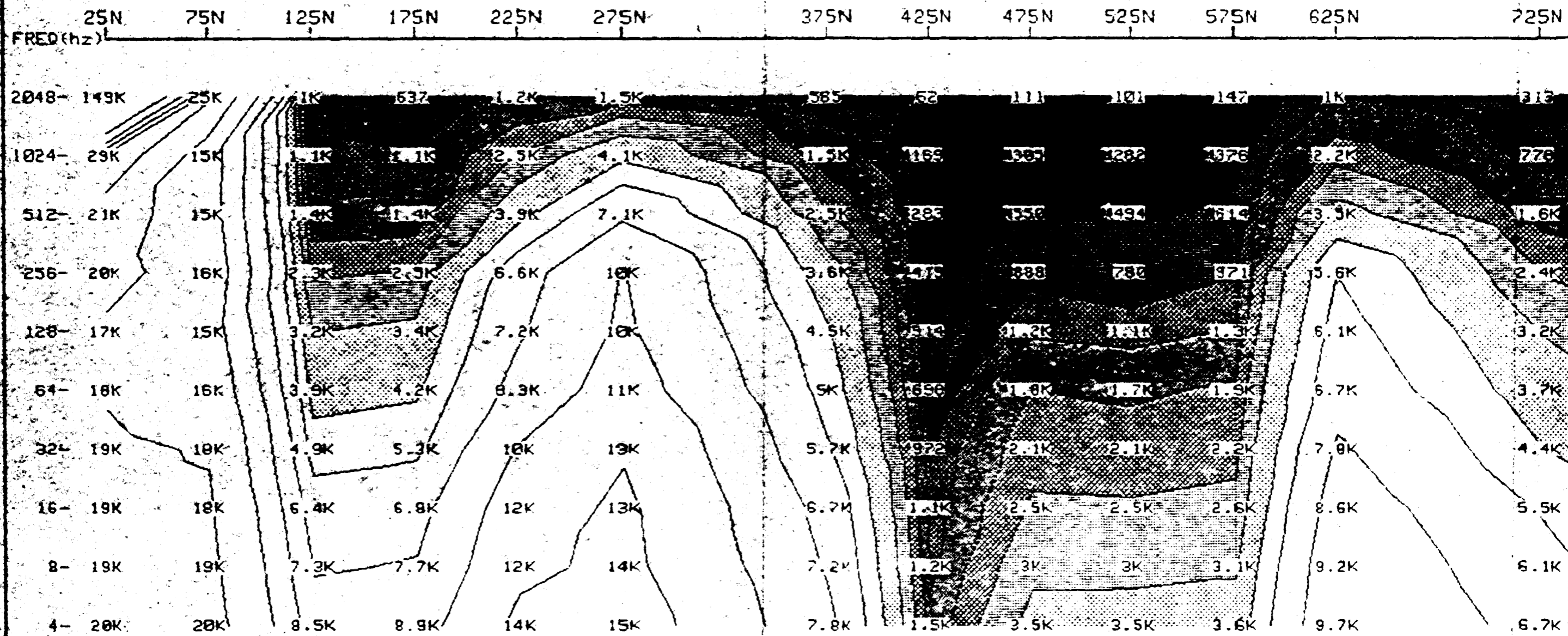


Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV/1987

1525N 1575N 1625N 1675N 1725N 1775N 1825N 1875N 1925N 1975N 2025N  
 FREQ(hz)



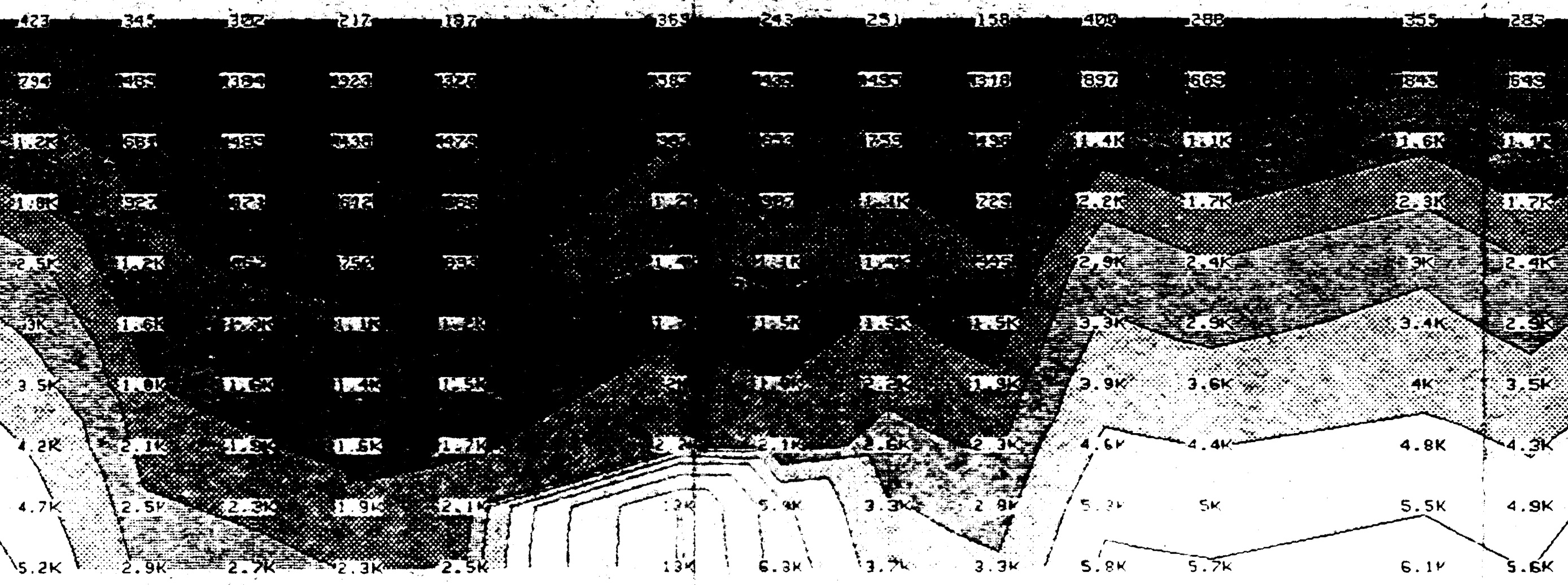




# CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 LINE=625E E-dipole=5000ft Tx-Rx=10.875km

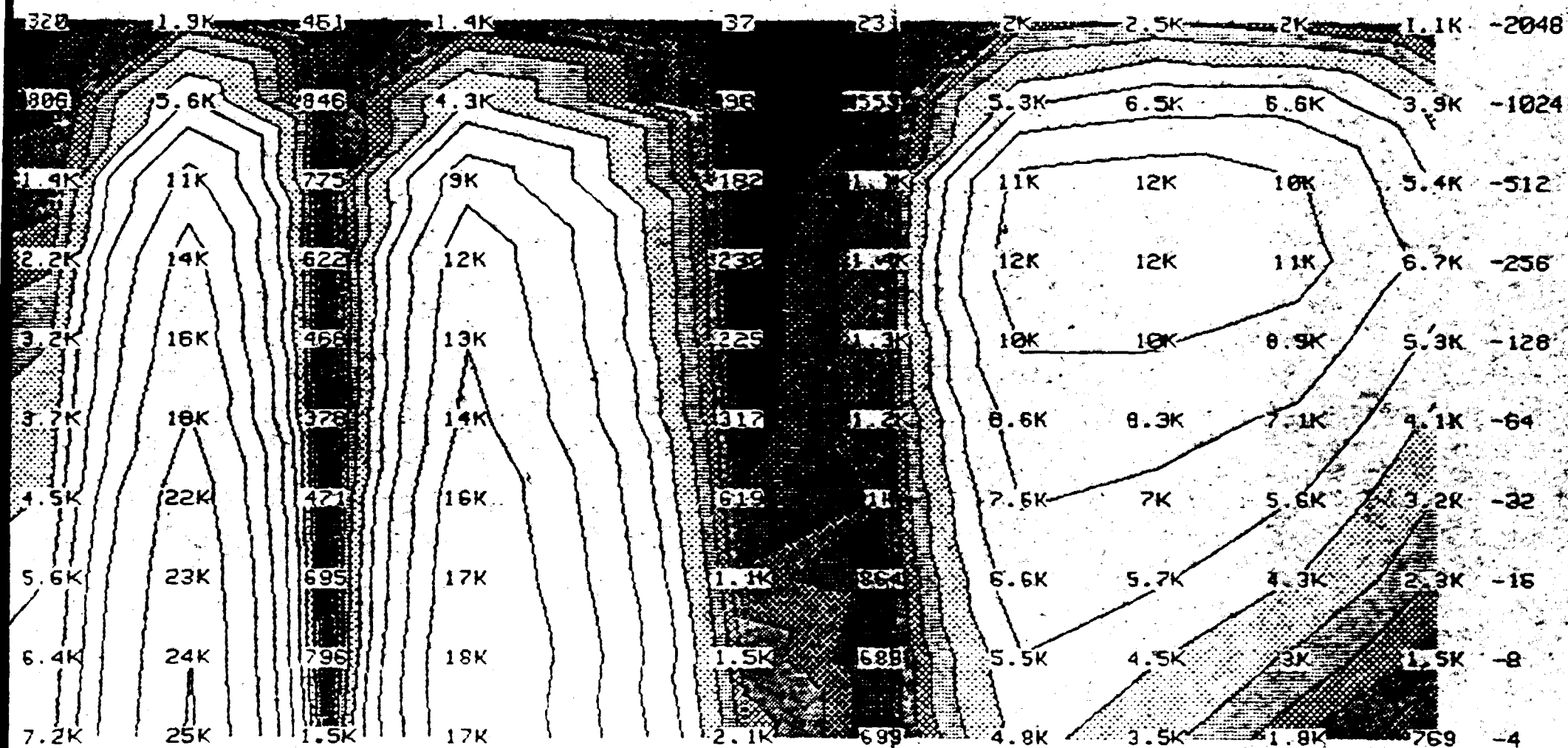
775N    825N    875N    925N    975N            1075N    1125N    1175N    1225N    1275N    1325N            1425N    1475N

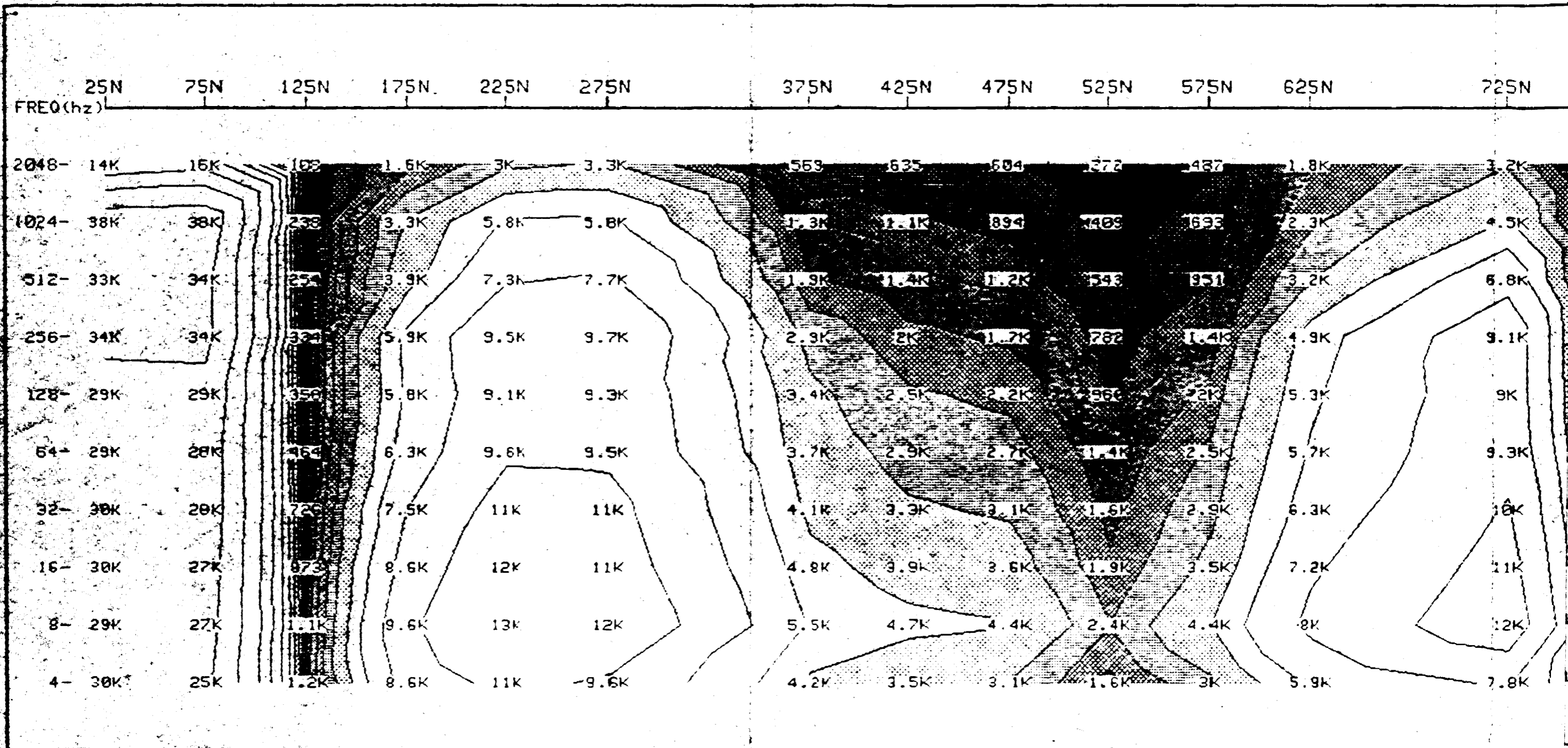


Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV 1997



525N 1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N  
FREQ(hz)



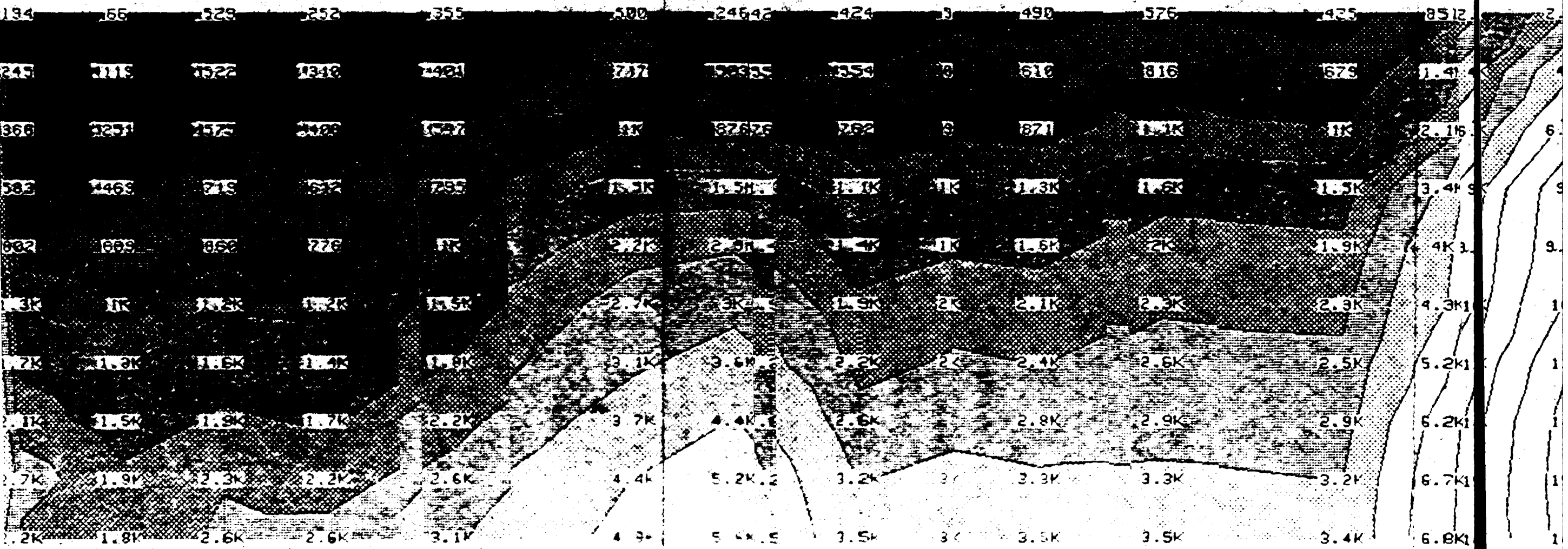


# CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 LINE=71E

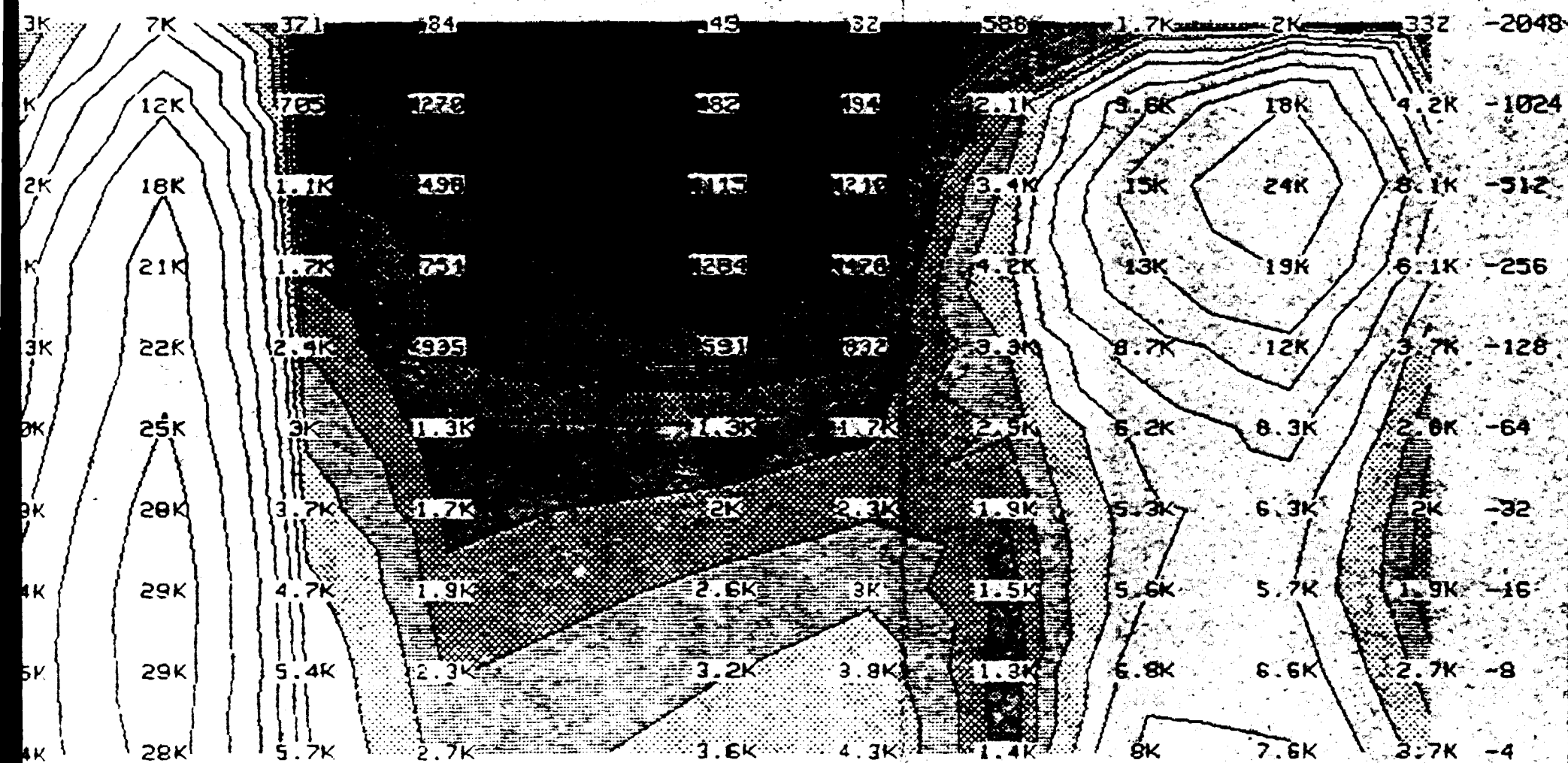
E-dipole=51 000ft Tx-Rx=1.75km

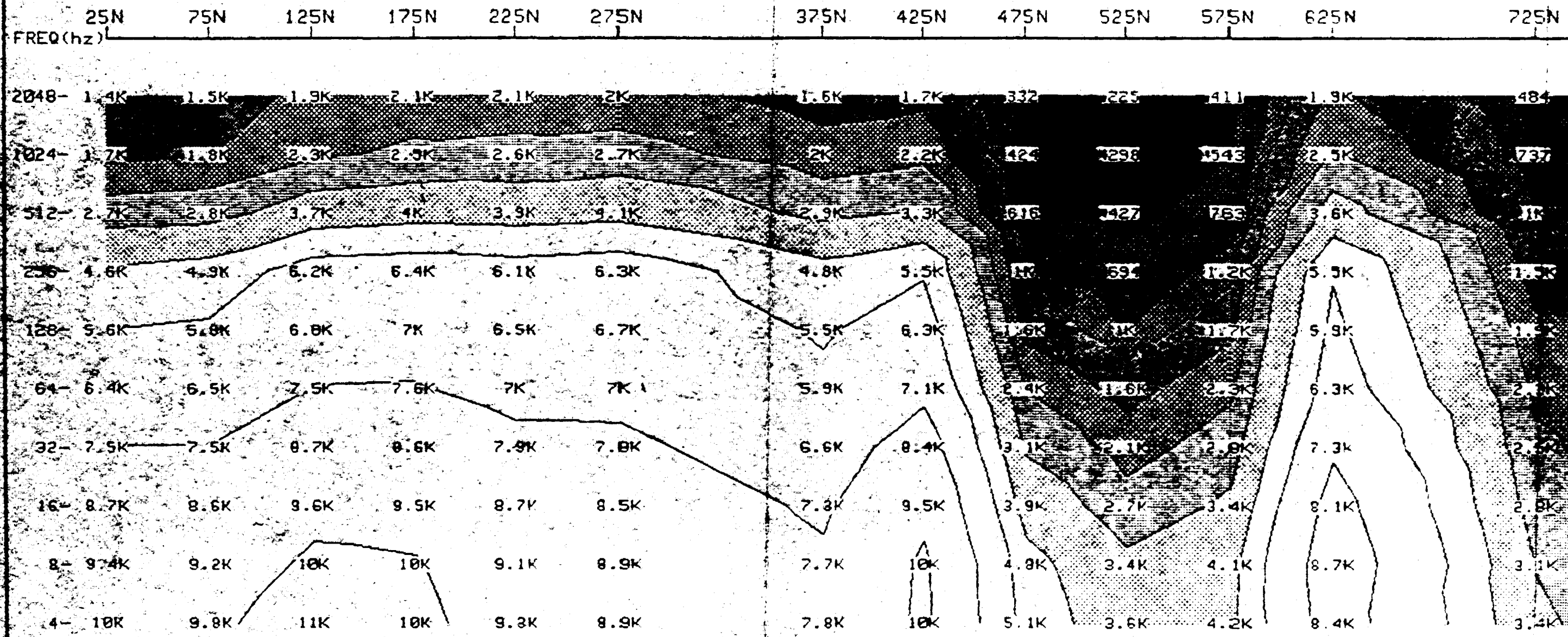
75N 825N 875N 925N 975N 1075N 1125N 1175N 1275N 1325N 1425N 1475N 15



Resistivity in ohm-m  
 Surveyed by EQUANTER CONSULTING INC. NOV 1987

1525N 1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N FREQ (Hz)



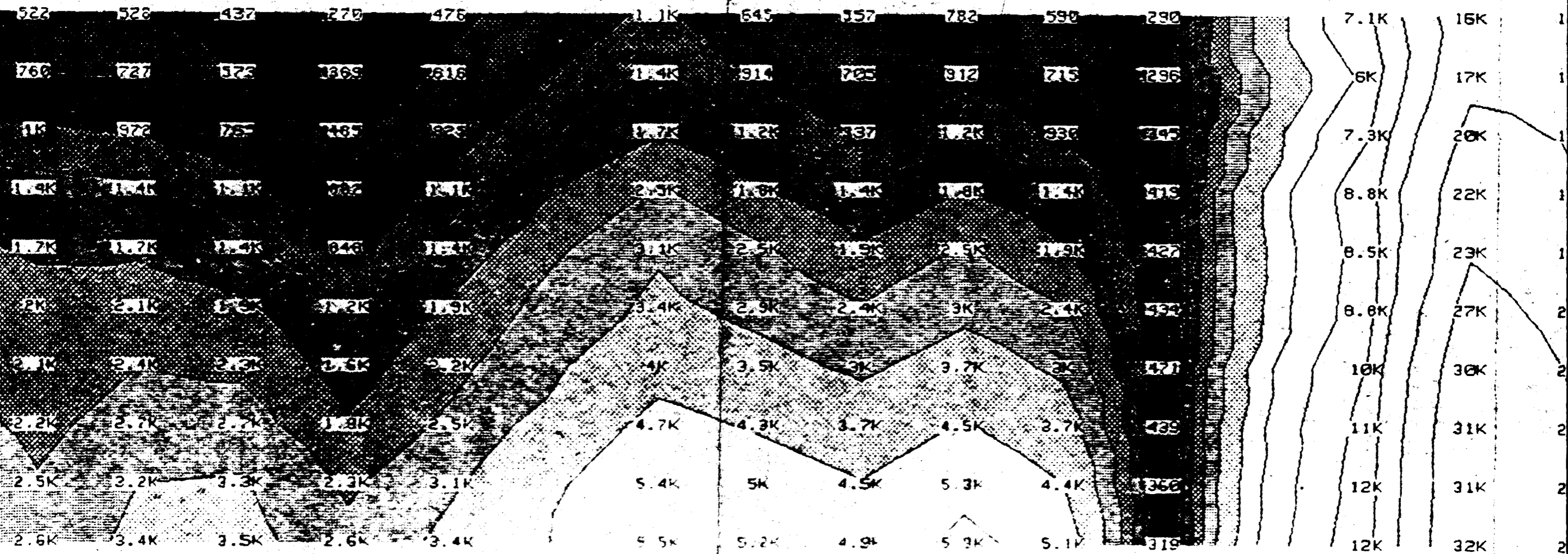




# CSAMT APPARENT RESISTIVITY (CORRECTED)

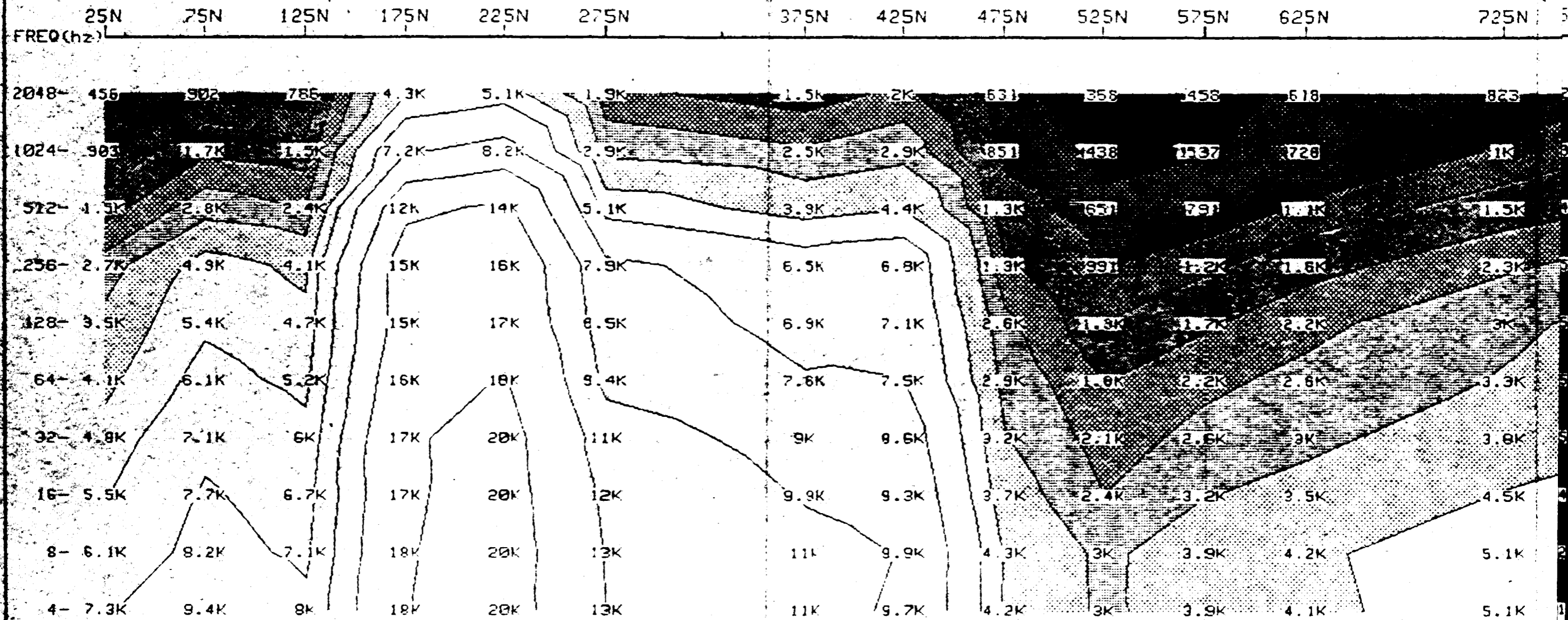
LAC MINERALS LTD. C14 LINE=875E E-dipole=5000ft Tx-Rx=10.625km

775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N 1475N 15



Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV/1987



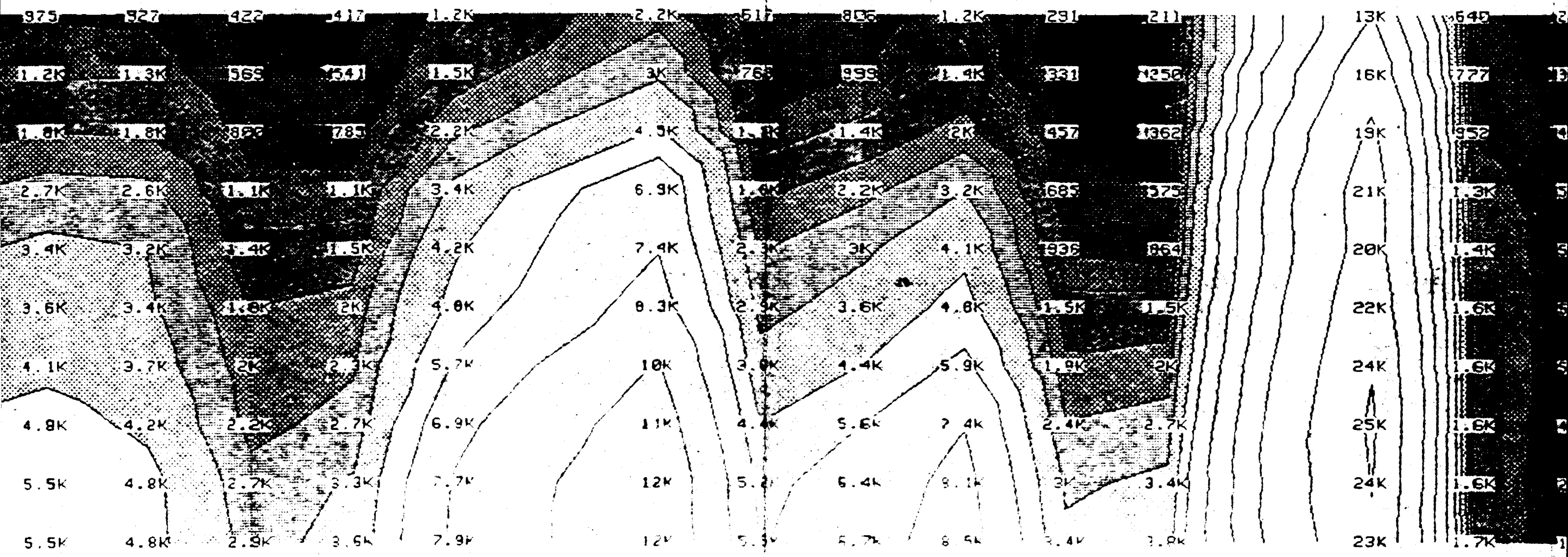




# CSAMT APPARENT RESISTIVITY (CORRECTED)

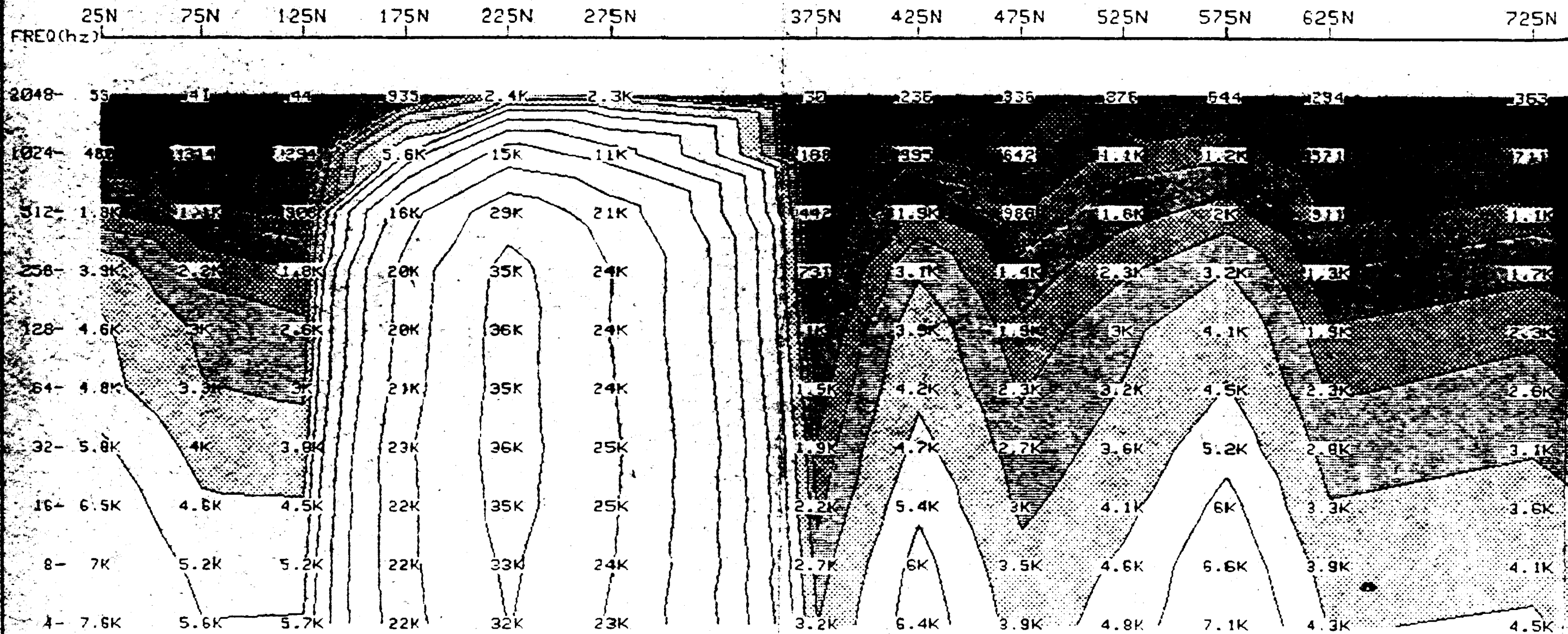
LAC MINERALS LTD. C14 LINE=1000E E-dipole=5000ft Tx-Rx=10.5km

775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N 1475N 15



Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV 1997

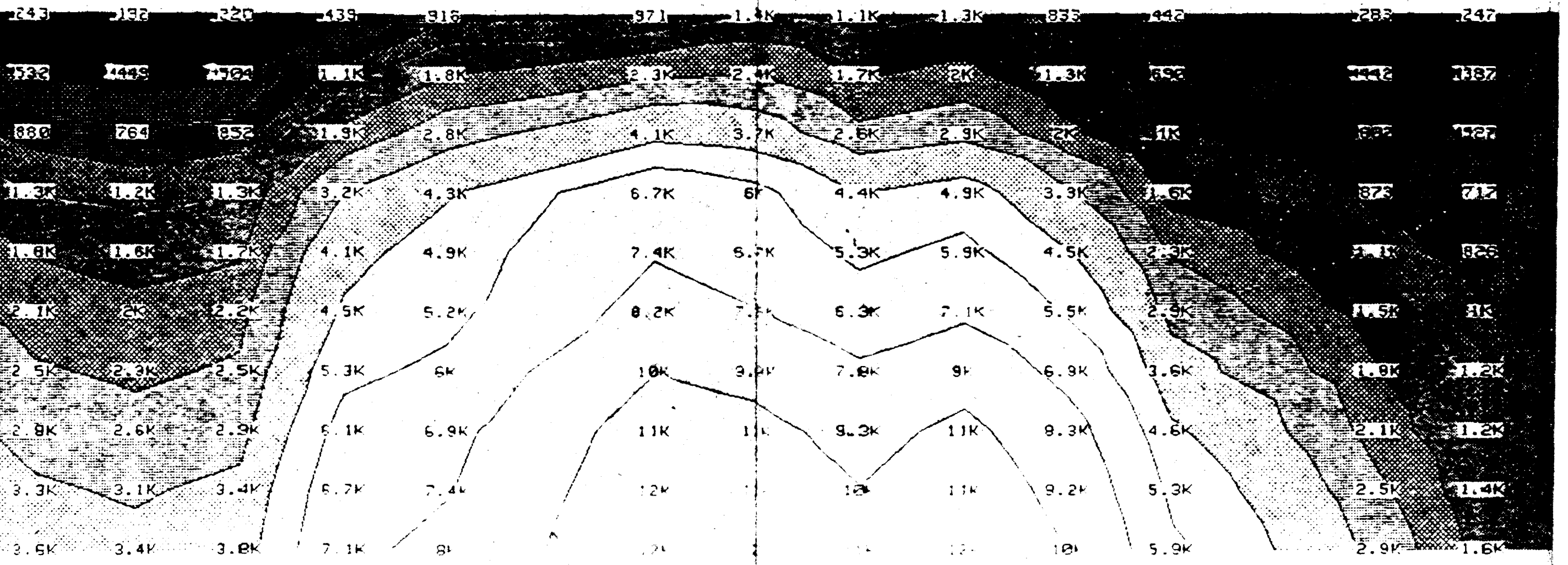
	1575N	1625N	1675N	1775N	1825N	1875N	1925N	1975N	2025N	FREQ(hz)
34	285	693	588	385	563	318	421	757	908	-2048
50	1336	1355	1210	1466	697	1592	1456	924	1.1K	-1024
21	1480	1.1K	919	634	867	1428	757	1K	1.3K	-512
48	1528	1.4K	1.2K	888	1.1K	1686	781	1.2K	1.4K	-256
40	1532	1.6K	1.4K	1.1K	1.2K	217	816	1.2K	1.5K	-128
20	1486	1.7K	1.5K	1.6K	1.4K	362	1211	1.6K	1.6K	-64
31	1540	1.5K	1.2K	1.9K	1.4K	1.2K	1.6K	1.2K	1.5K	-32
35	1450	1.3K	1.7K	2.2K	1.4K	1.2K	1.6K	1.2K	1.5K	-16
92	1317	1.1K	1.8K	2.6K	1.4K	1.6K	1.9K	2.1K	1.5K	-8
67	188	1.1K	2.1K	3.1K	1.6K	2K	2.3K	2.4K	1.7K	-4



# CSAMT APPARENT RESISTIVITY (CORRECTED)

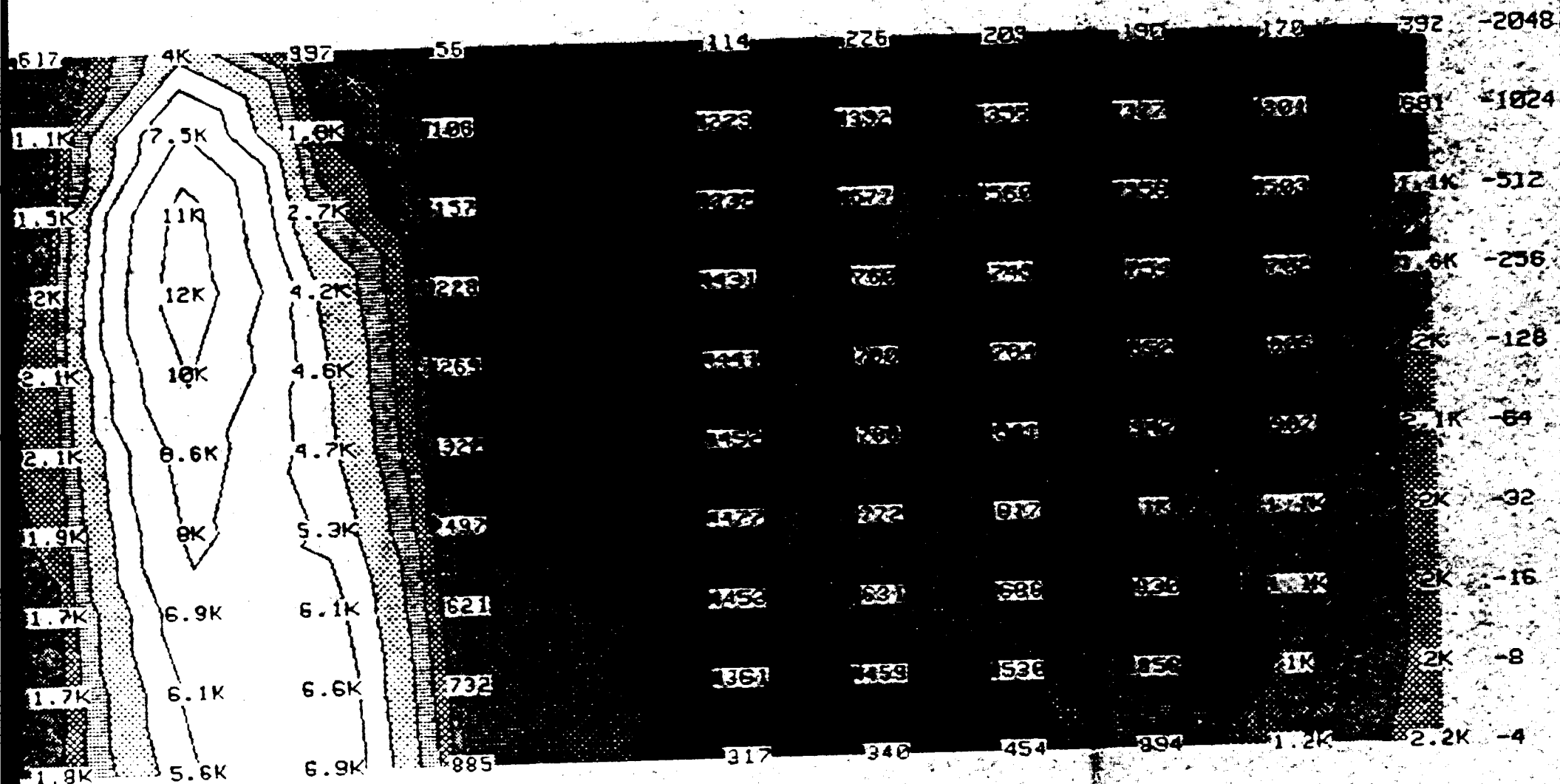
LAC MINERALS LTD. C14 LINE=1125E E-dipole=5000ft Tx-Rx=10.375km

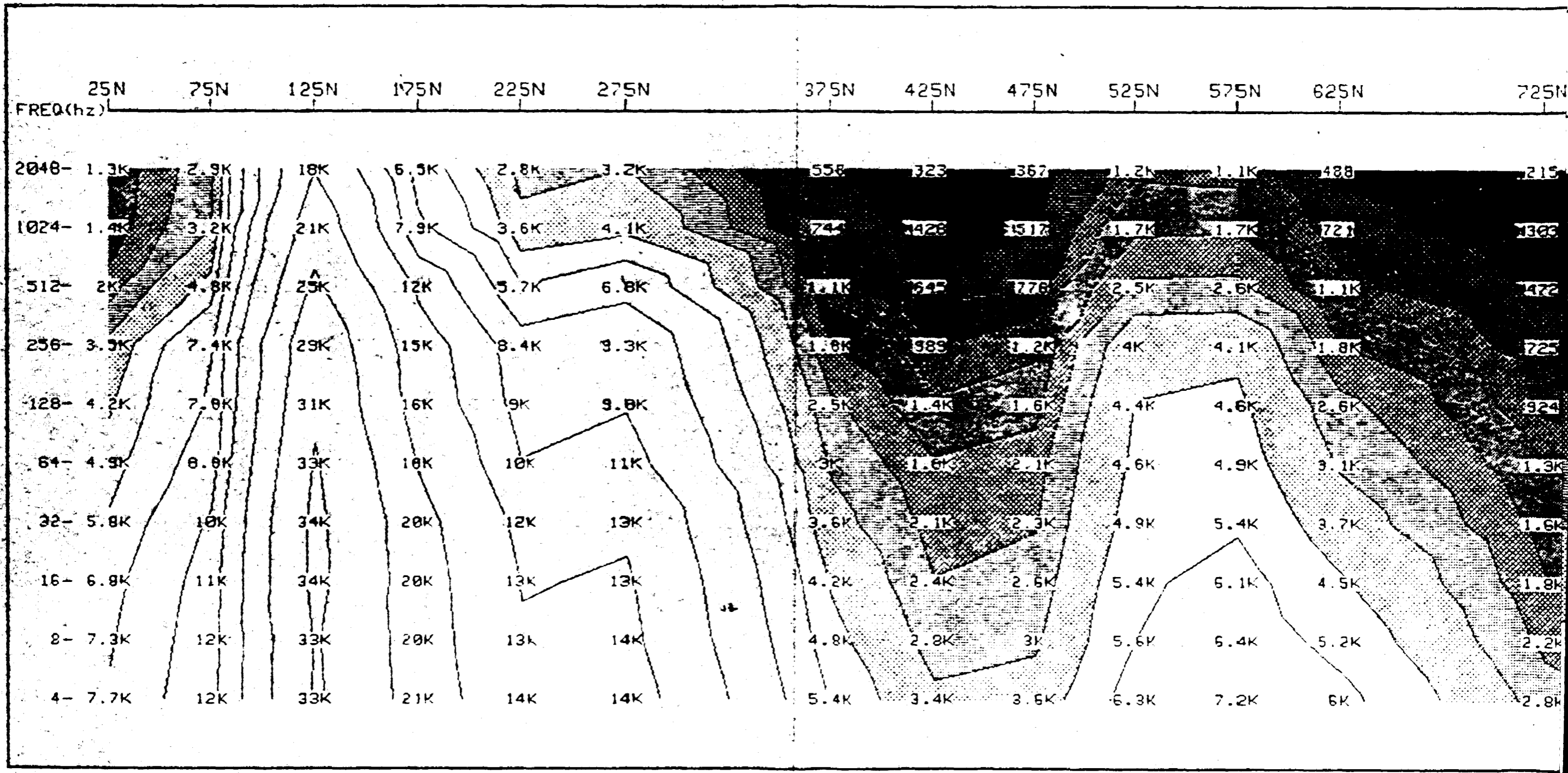
775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N 1475N



Resistivity in Ohm-m  
 Surveyed by QUANTECH CONSULTING INC. 1997

525N 1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N FREQ(hz)





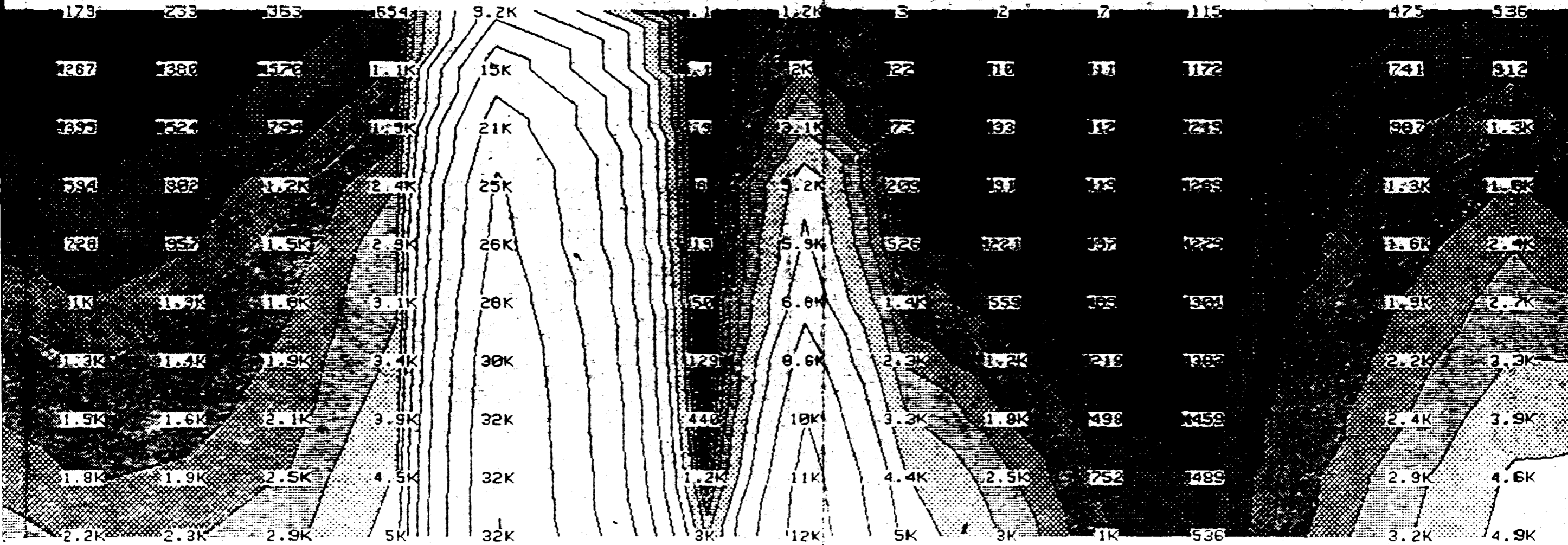


# CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 LINE=1250E

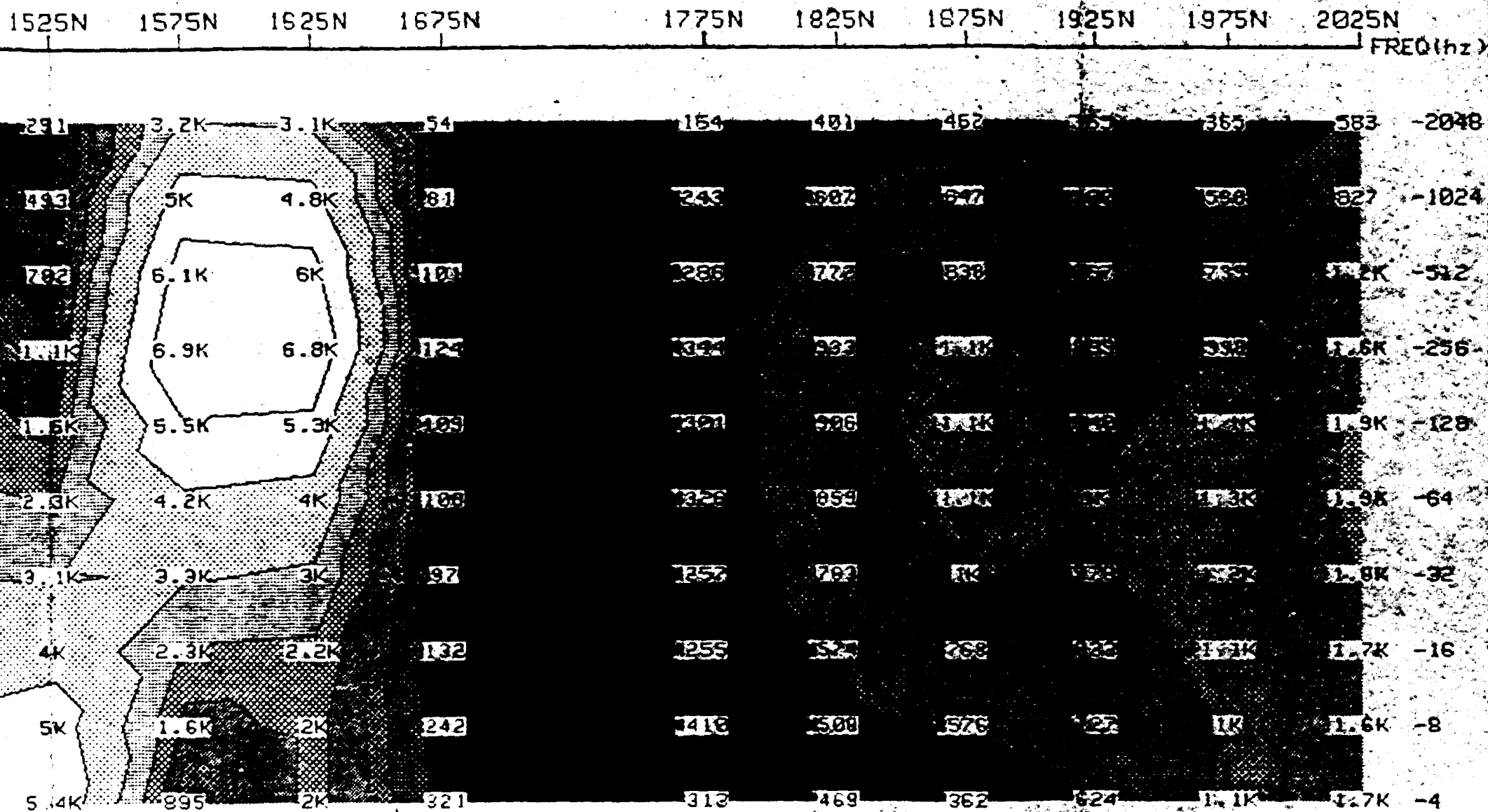
E-dipole=5000ft Tx-Rx=10.25km.

775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N 1475N

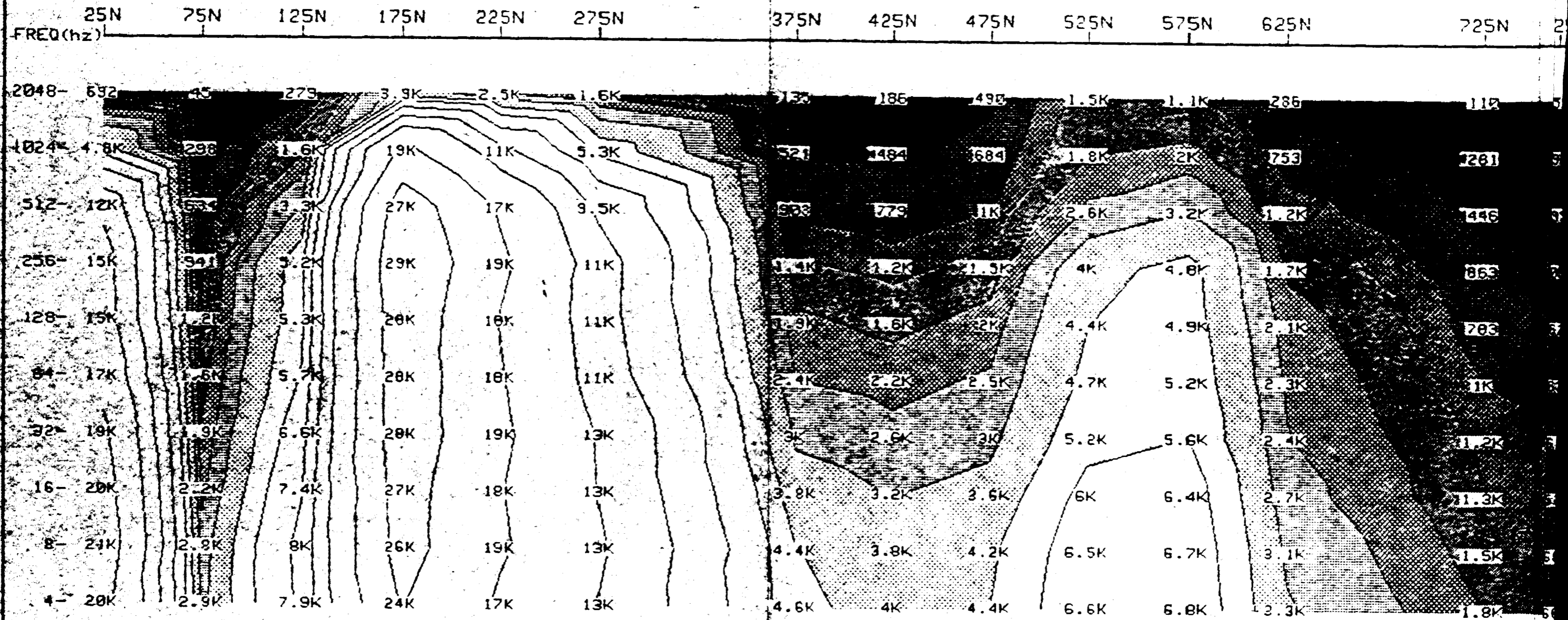


Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV/1987

12 50



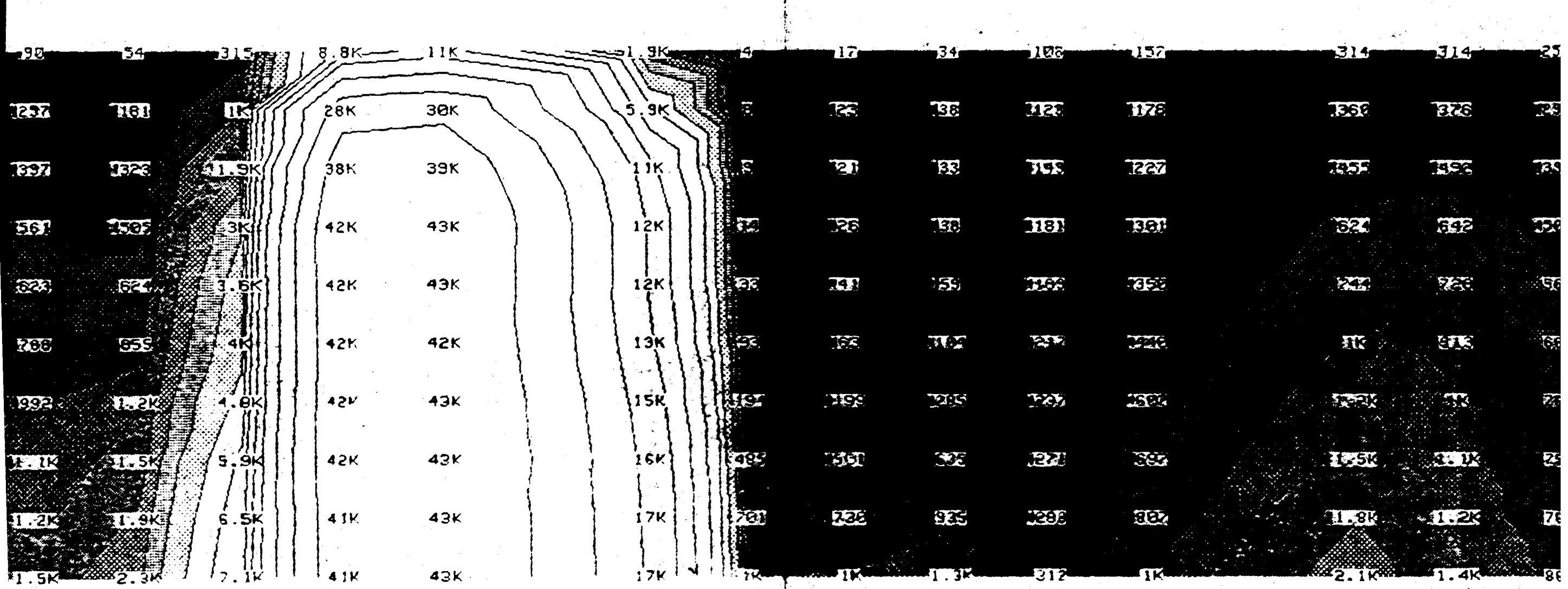




# CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINARALS LTD. C14 LINE=1375E E-dipole=5000ft Tx-Px=10.125km

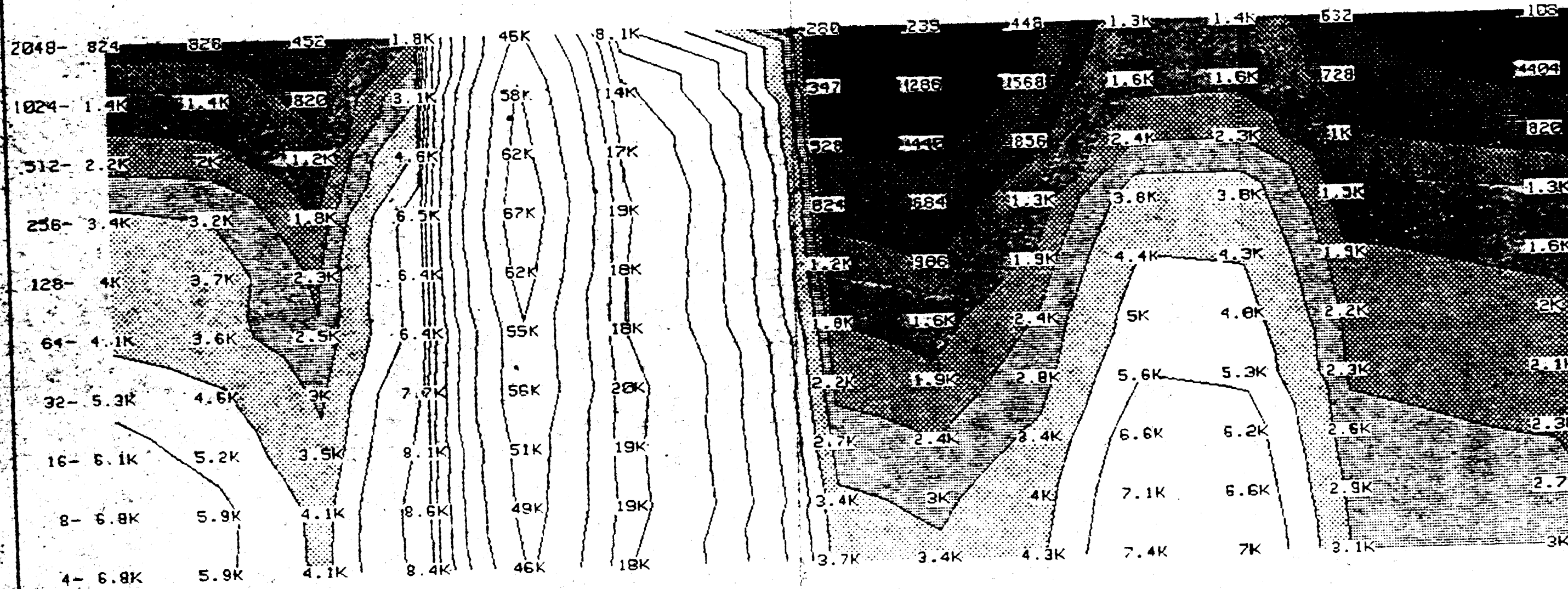
775N	825N	875N	925N	975N	1075N	1125N	1175N	1225N	1275N	1325N	1425N	1475N	1525N
------	------	------	------	------	-------	-------	-------	-------	-------	-------	-------	-------	-------



Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV/1987

	1575N	1625N	1675N	1775N	1825N	1875N	1925N	1975N	2025N	FREQ(hz)
445	877	422	457	806	1.5K	2.8K	1.8K	1.3K	-2048	
504	1K	491	1488	893	1.5K	2.7K	1.9K	1.2K	-1024	
632	1.3K	605	602	1.1K	1.8K	3.2K	2K	3.3K	-512	
806	1.6K	728	732	1.2K	2.3K	4.1K	2.8K	1.6K	-256	
846	1.6K	693	697	1.4K	2.3K	4.5K	2.4K	1.5K	-128	
868	1.5K	648	681	1.3K	1.9K	3.2K	2.7K	1.3K	-64	
795	1.3K	622	598	1.1K	1.5K	3.7K	1.7K	1.1K	-32	
614	1.3K	268	492	785	1.3K	1.2K	1.3K	851	-16	
1416	1.7K	978	1414	1494	1580	957	927	574	-8	
289	2.1K	1.4K	508	398	530	725	968	513	-4	

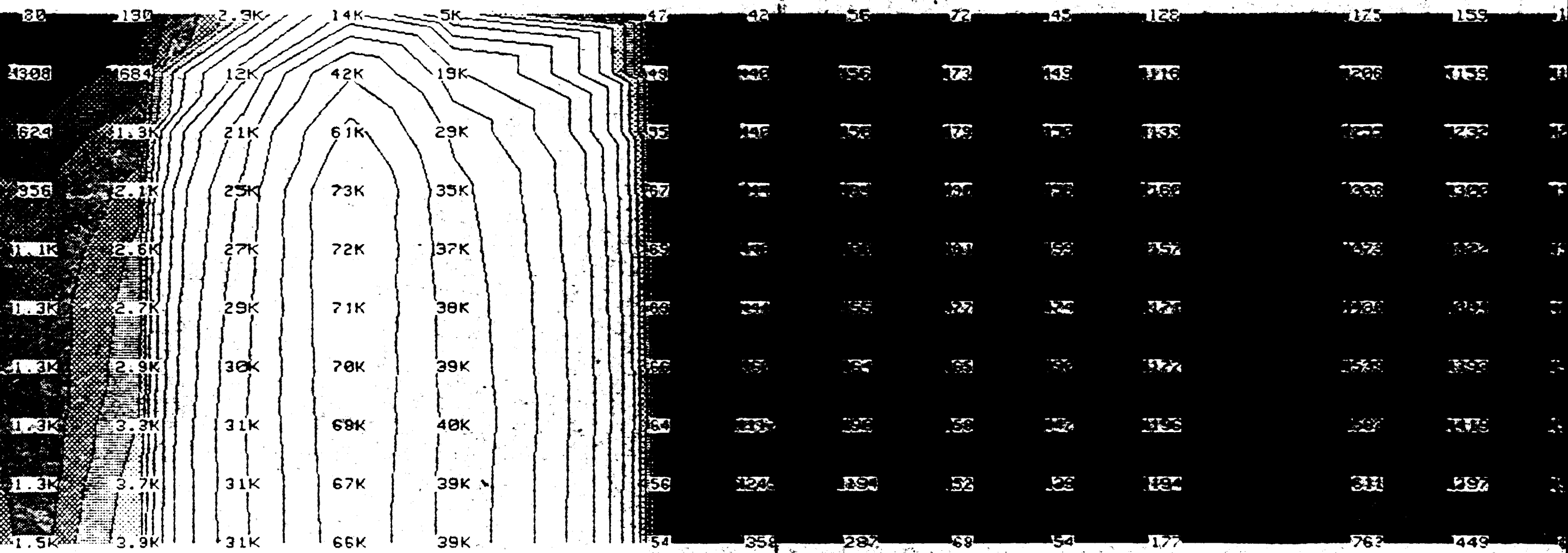
FREQ(hz) 25N 75N 125N 175N 225N 275N 375N 425N 475N 525N 575N 625N 725N



# CSAMT APPARENT RESISTIVITY (CORRECTED)

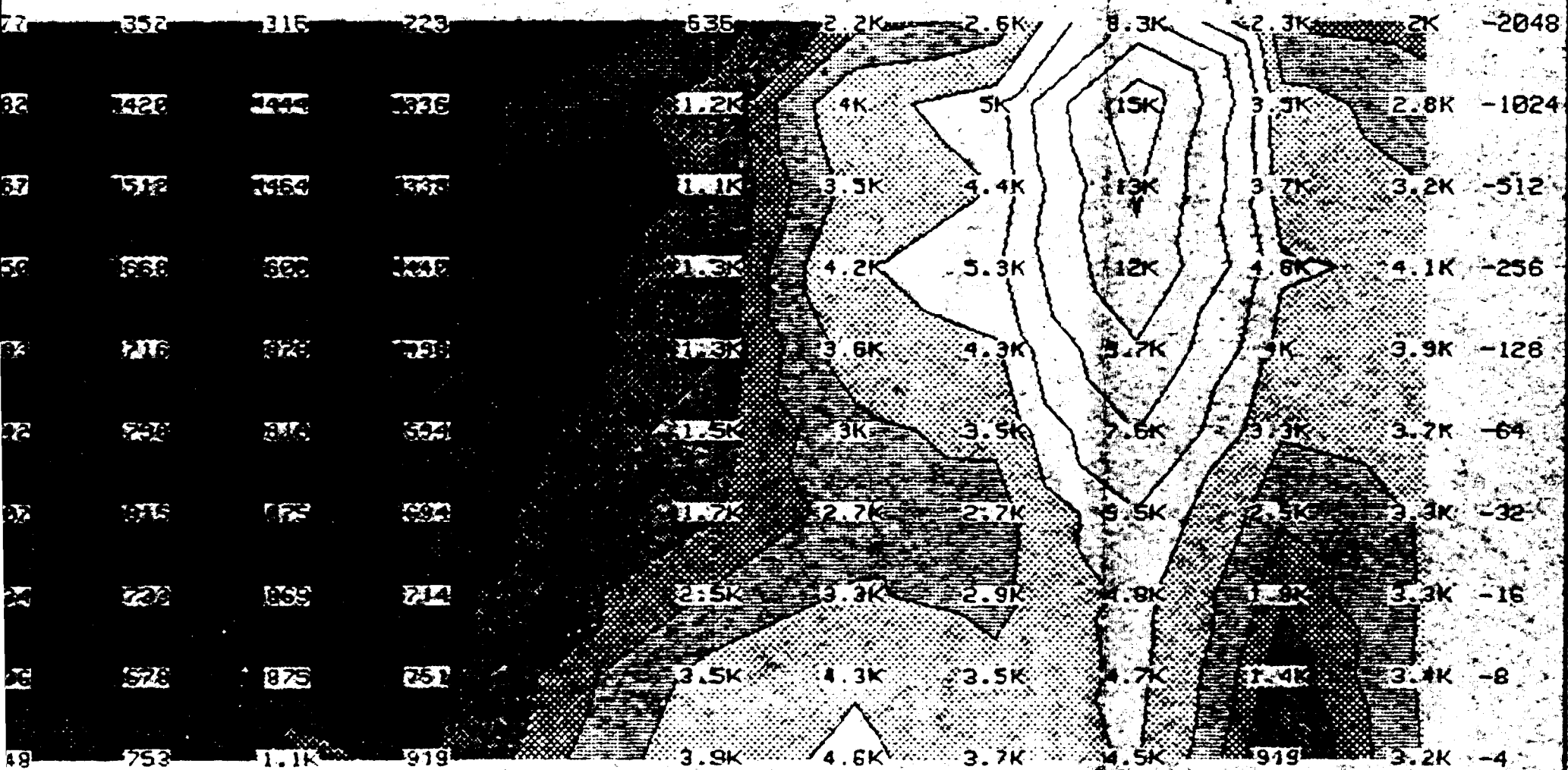
LAC MINERALS LTD. C14 LINE=1500E E-dipole=5000ft Tx-Rx=10km

775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N 1475N 15



Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV 1987

1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N  
 FREQ(hz)





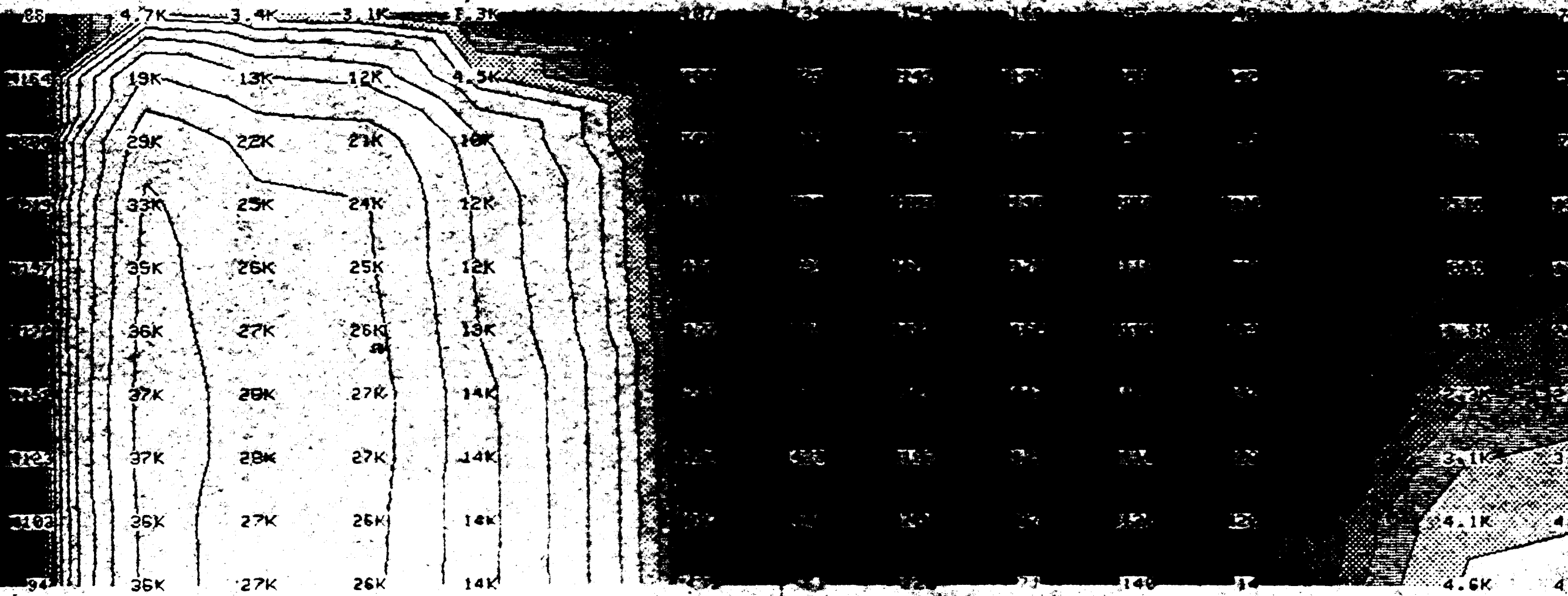


**CSAMT APPARENT RESISTIVITY (CORRECTED)**

LAC MINERALS LTD. C14 LINE=1625E

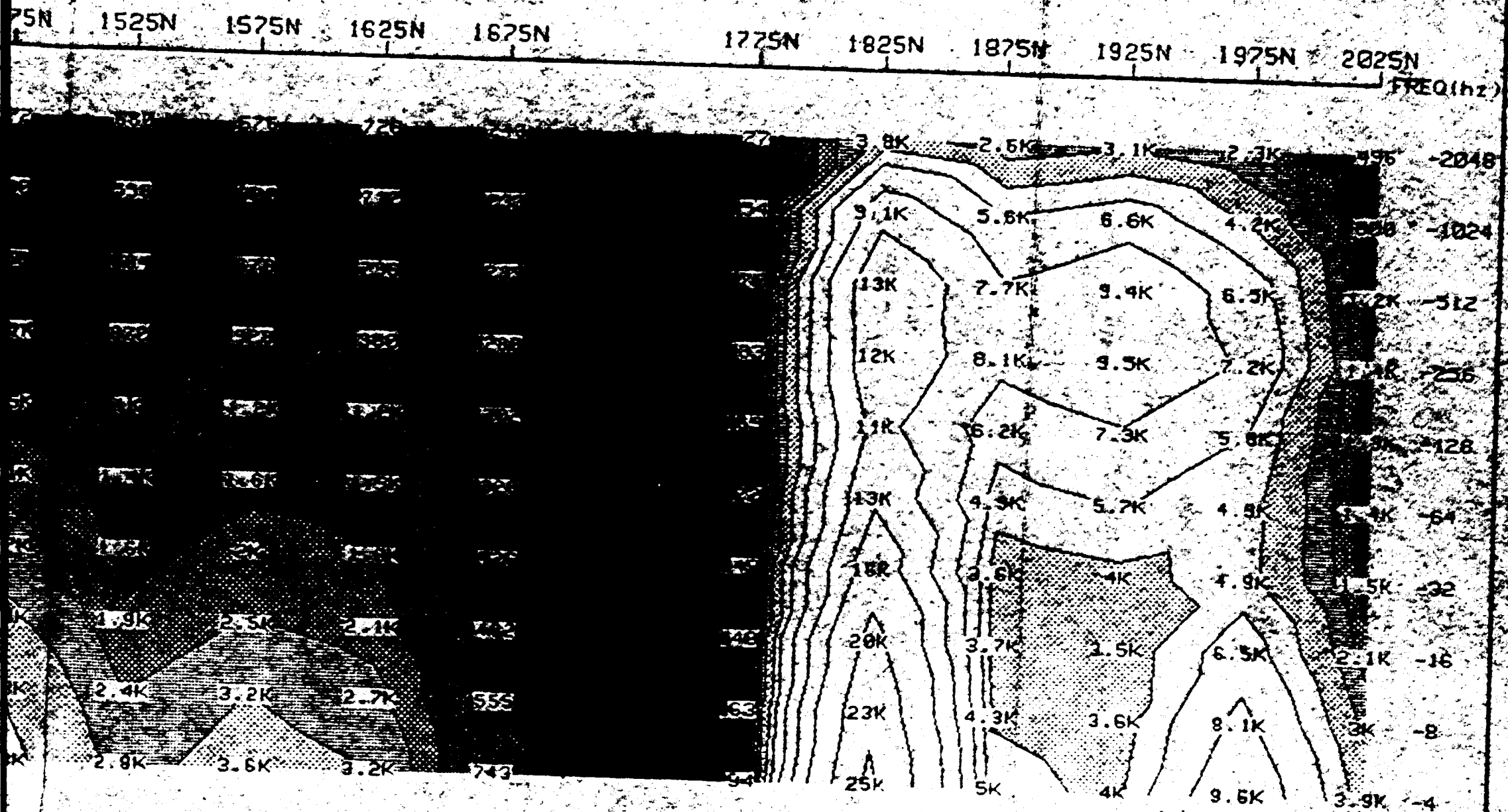
E-dipole=5000ft Tx-Rx=9.875km

775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N 1475N



Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC NOV 1987





### CSAMT APPARENT RESISTIVITY (CORRECTED)

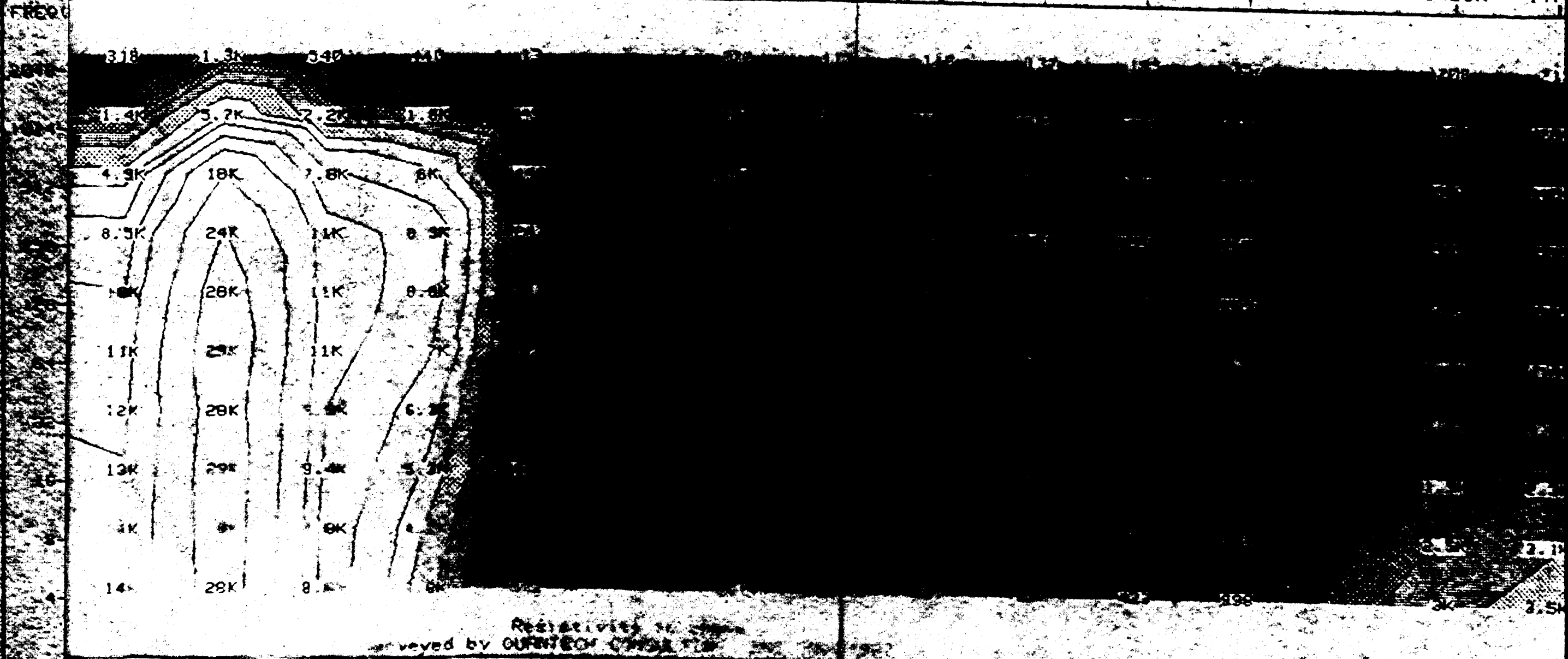
LAC MINERALS LTD. C14 LINE=1750E

E-dipole=5000ft Tx-Rx=9.75km

775N 825N 875N 925N 975N

1075N 1125N 1175N 1225N 1275N 1325N

1425N 1475N



**CSAMT APPARENT RESISTIVITY (CORRECTED)**

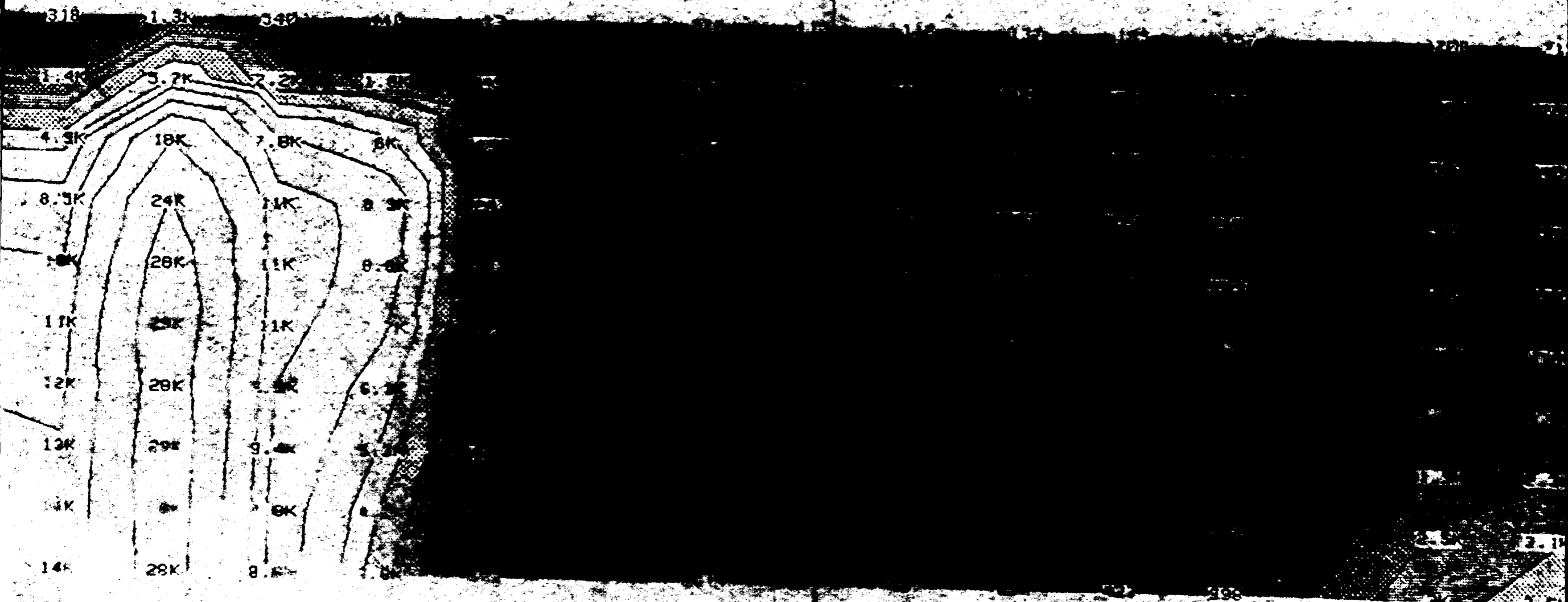
LRC MINERALS LTD. C14 LINE=1750E

E-dipole = 5000ft Tx-Rx=9.75km

775N 825N 875N 925N 975N

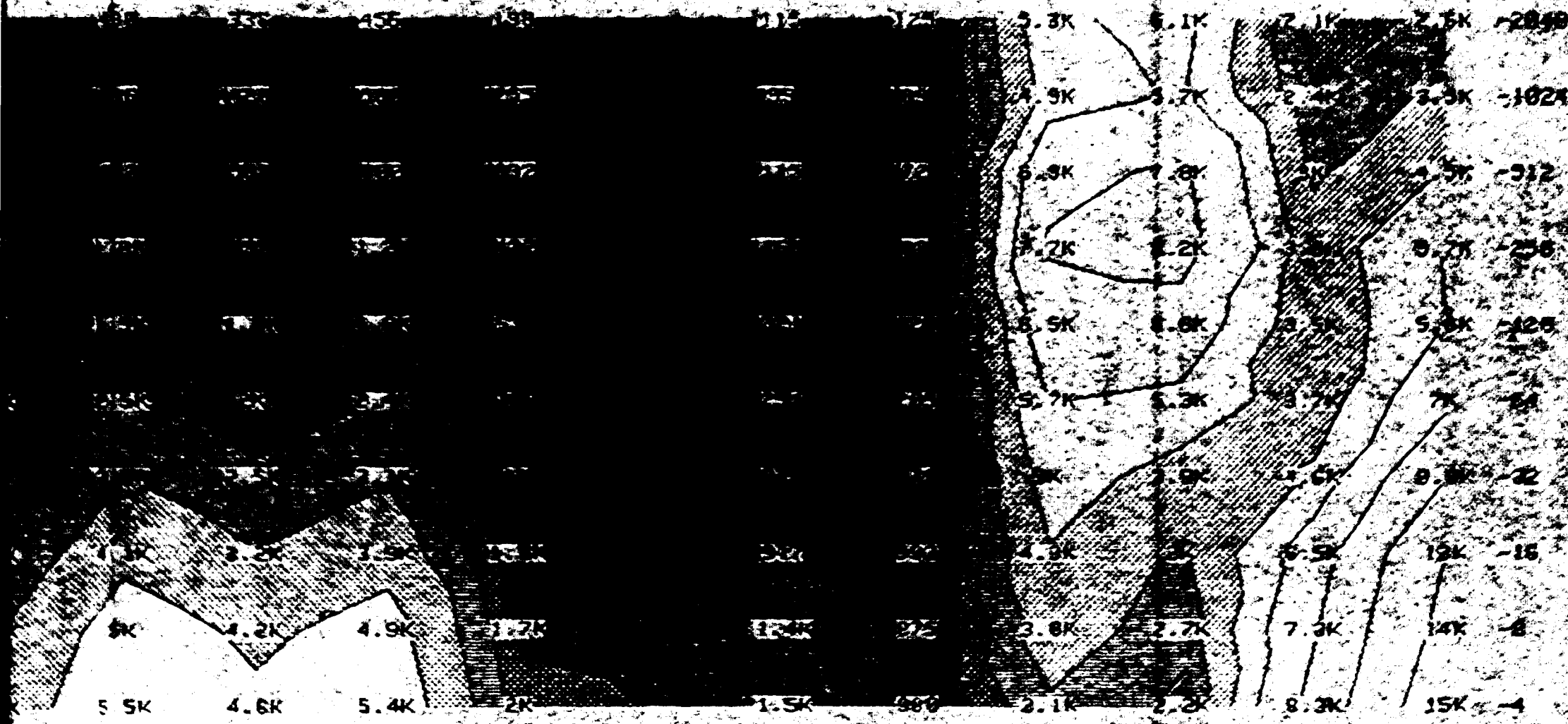
1075N 1125N 1175N 1225N 1275N 1325N

1425N 1475N



Resistivity  
measured by GURTECH

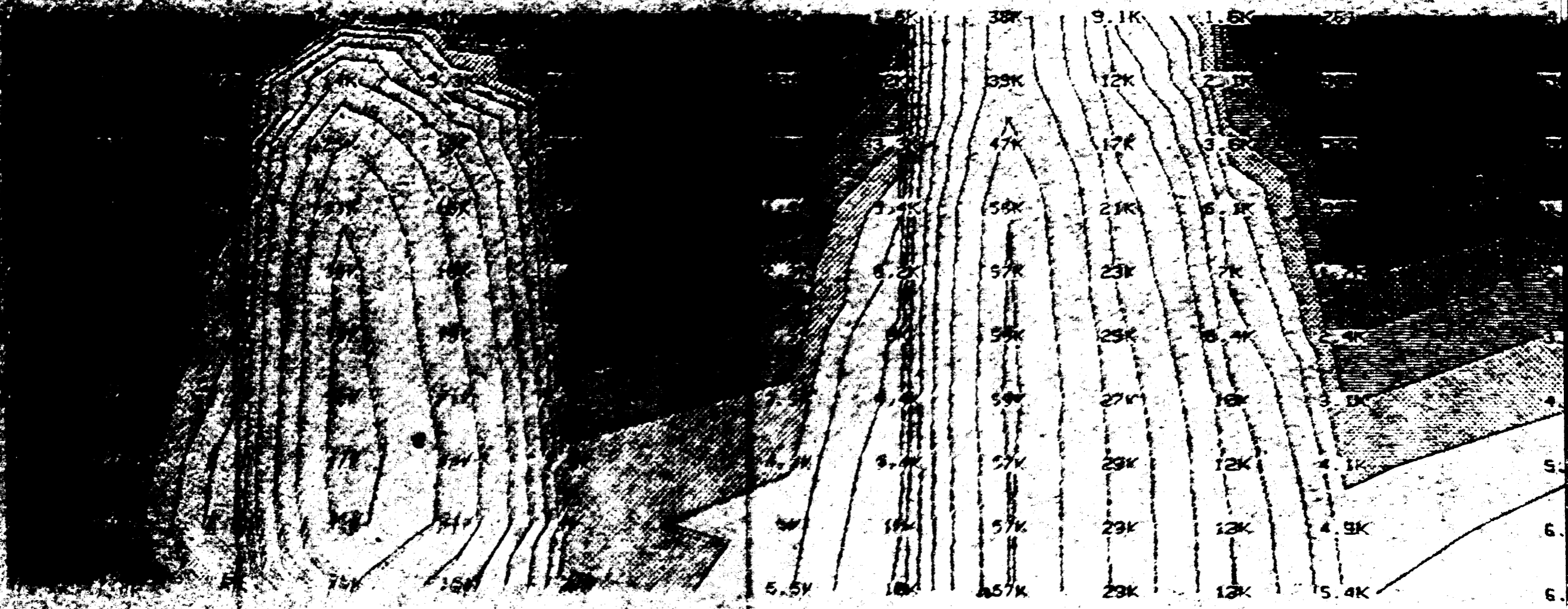
N 1525N 1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N  
FREO(147)





25N 75N 125N 175N 225N 275N 375N 425N 475N 525N 575N 625N 725

2048



**CSPT APPARENT RESISTIVITY (CONNECTED)**

LAC MINERALS LTD. C14 LINE-1875F

E-pole 525A, W-pole 525A

SN 775N 825N 875N 925N 975N 1025N 1075N 1125N 1175N 1225N 1275N 1325N 1375N 1425N



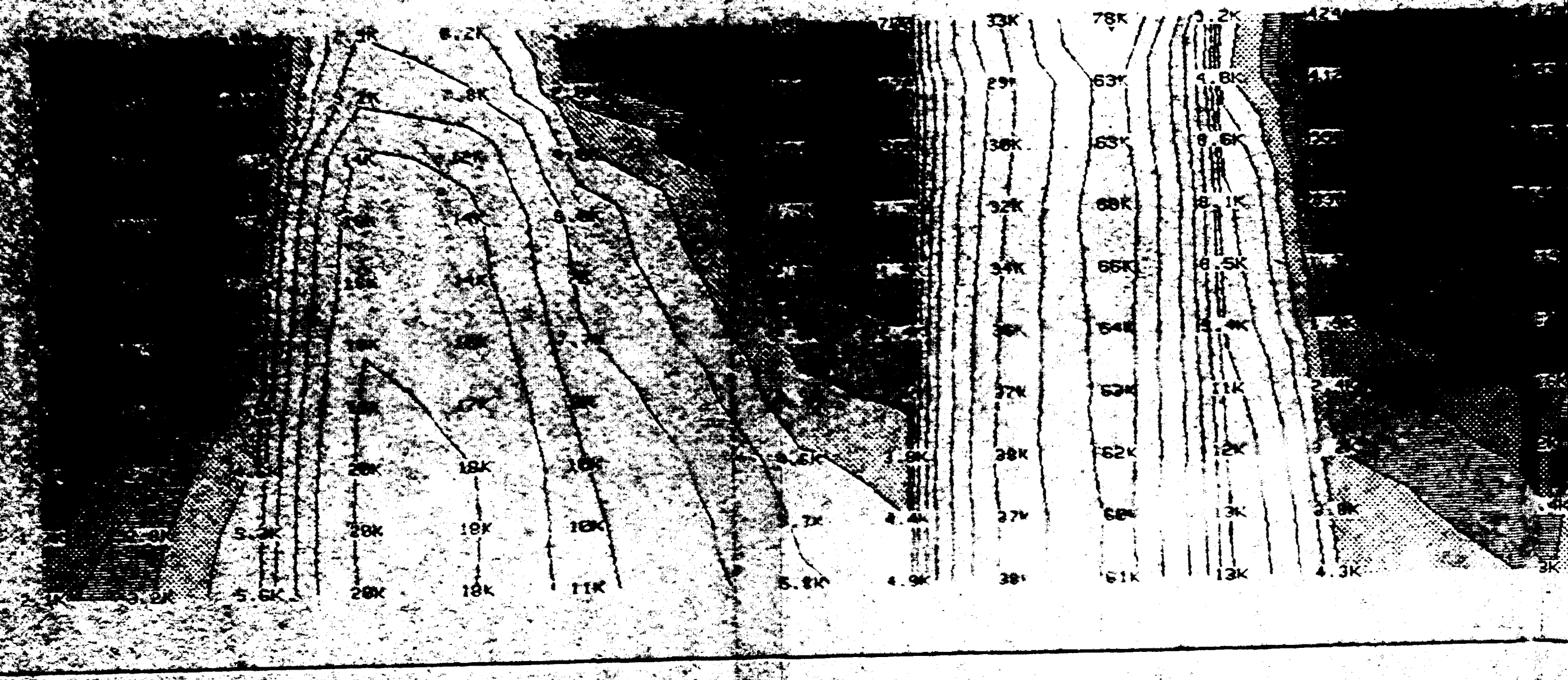
Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV 1987

1475N 1525N 1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N  
FRIGATE

2.7K  
4.2K  
2.9K  
2.1K  
2.5K  
2.5K



25N 75N 125N 175N 225N 275N 375N 425N 475N 525N 575N 625N 725N  
 FREQ (Hz)





CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 LINE=2000E

E-d pole=5000ft Tx-Rx=9.5km

775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N



1575N

1525N

1575N

1625N

1675N

1775N

1825N

1875N

1925N

1975N

2025N

FREDRICK



5.4K

5.6K

5.4K

5.6K

5.2K

5.4K

5.8K

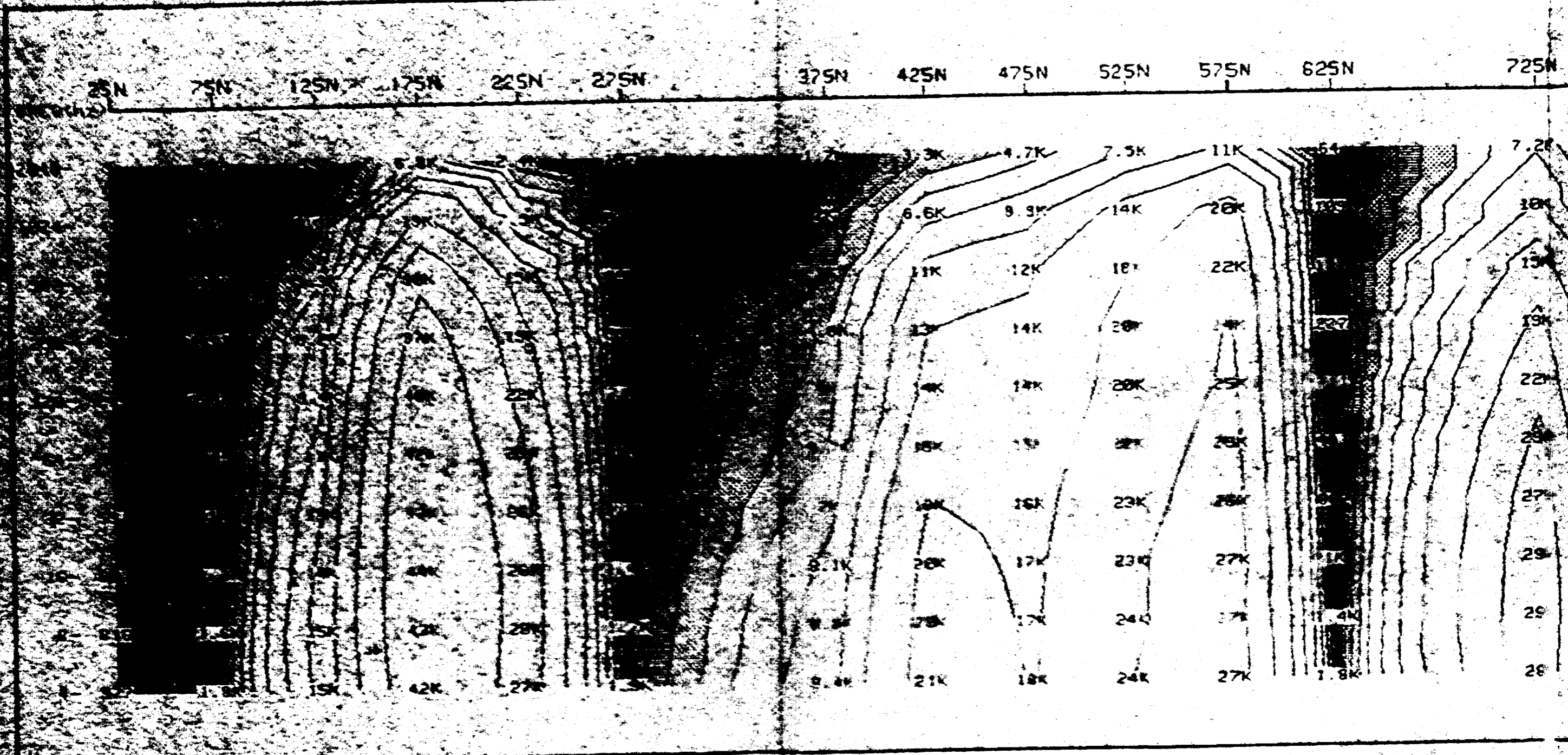
5.6K

5.4K

5.8K

5.8K

5.8K

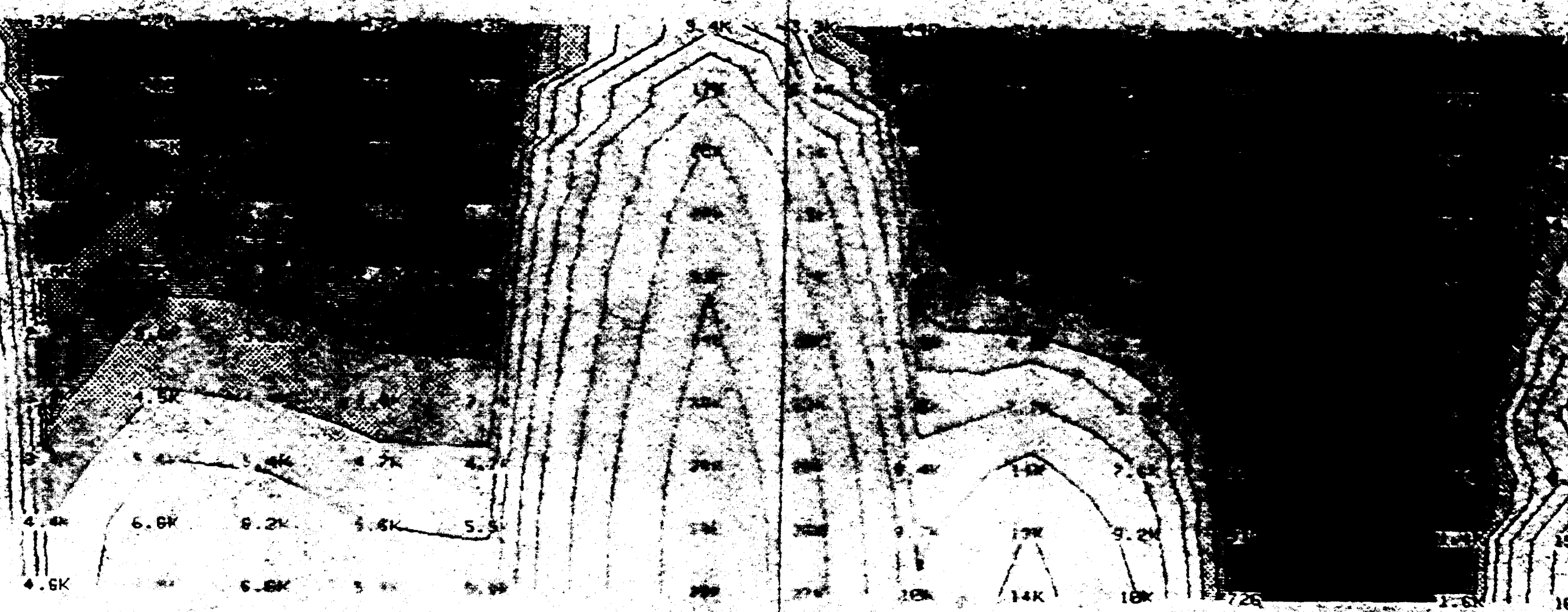




# CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 LINE=2125E E-dipole=5000ft Tx-Rx=9.375km

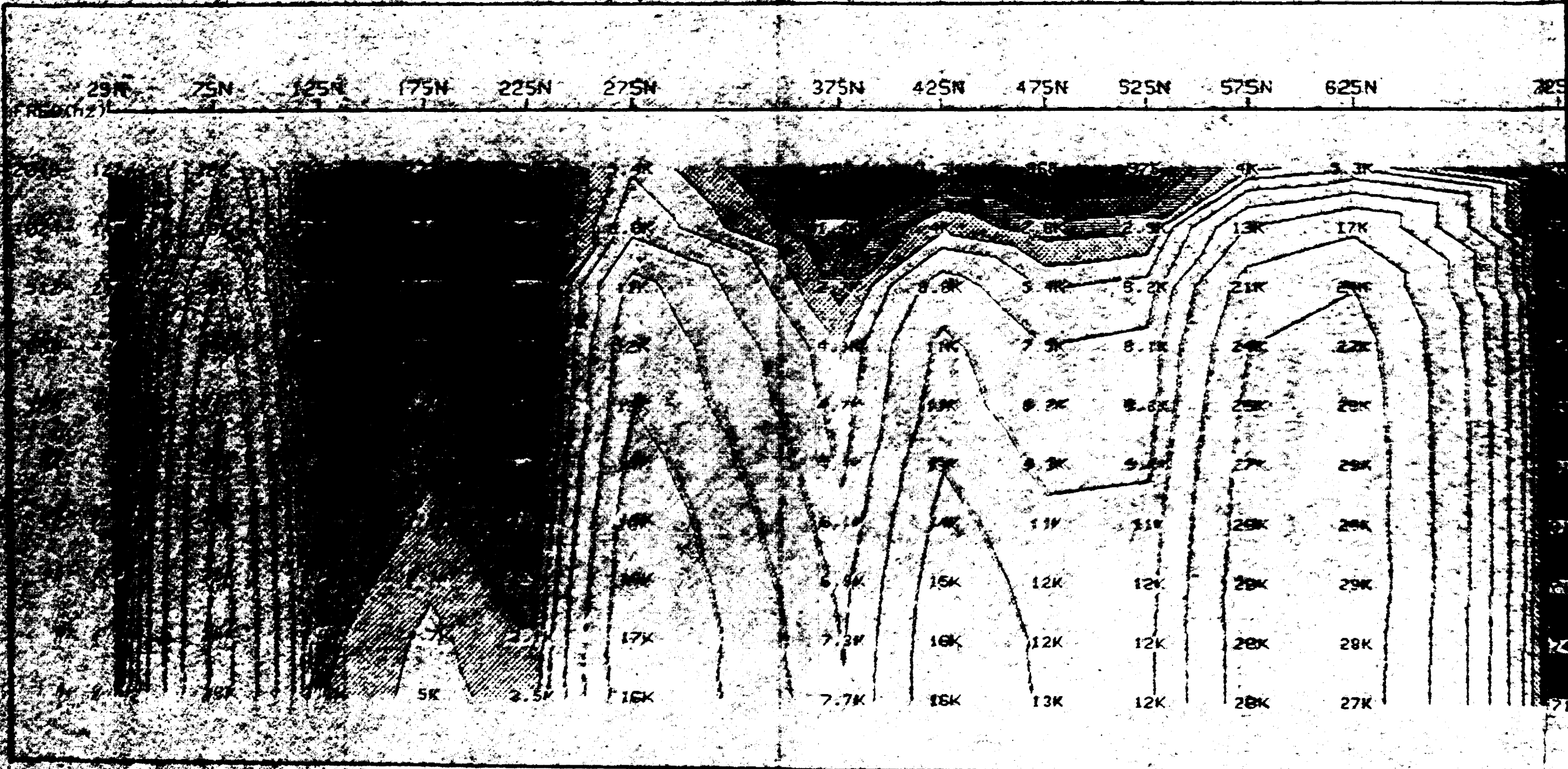
775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N 1475N



Resistivity in Ohm m  
 Surveyed by UNITED CONSULTING INC. 1987

1525N 1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N





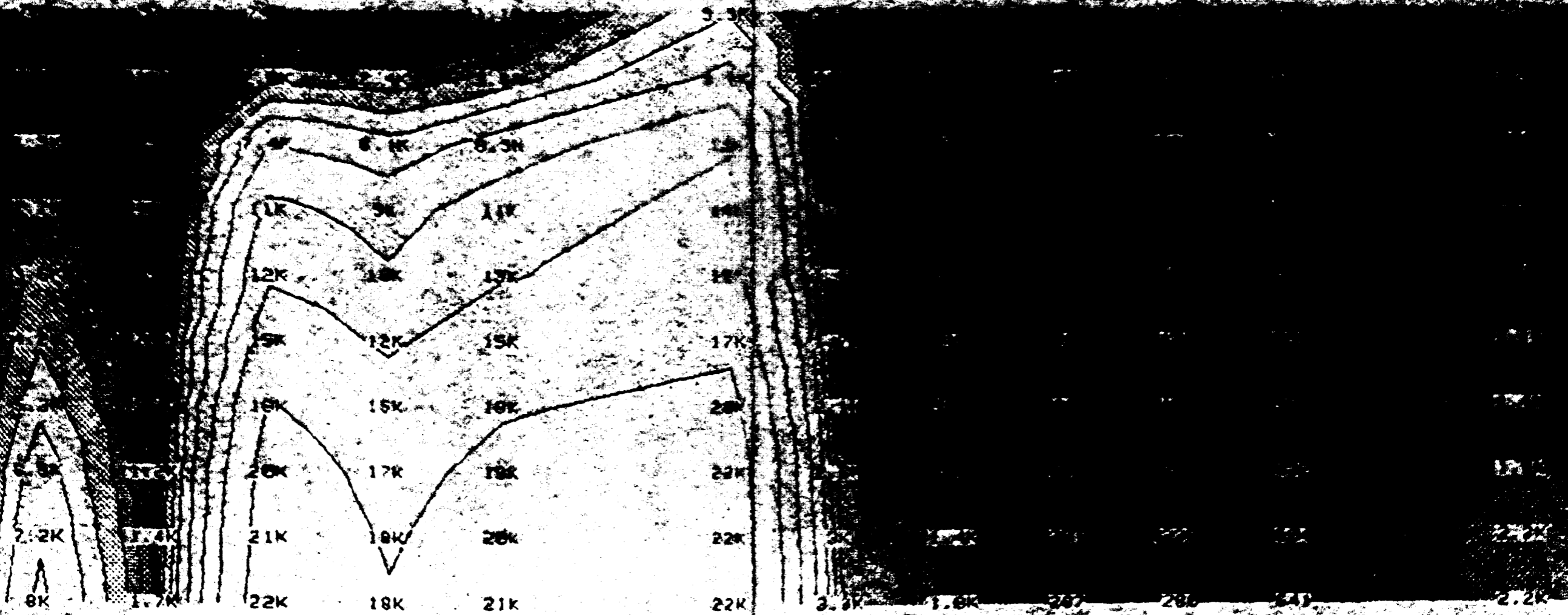


**CSAMT APPARENT RESISTIVITY (CORRECTED)**

LAC MINERALS LTD. C14 LINE-2375E

TX-PX=9.125km

775N 825N 875N 925N 975N 1025N 1075N 1125N 1175N 1225N 1275N 1325N 1425N



Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV/1987

1475N

1525N

1575N

1625N

1675N

1775N

1825N

1875N

1925N

1975N

2025N

FREQ (Hz)

-2048

-1024



2.812

2.812

2.812

3.49

3.49

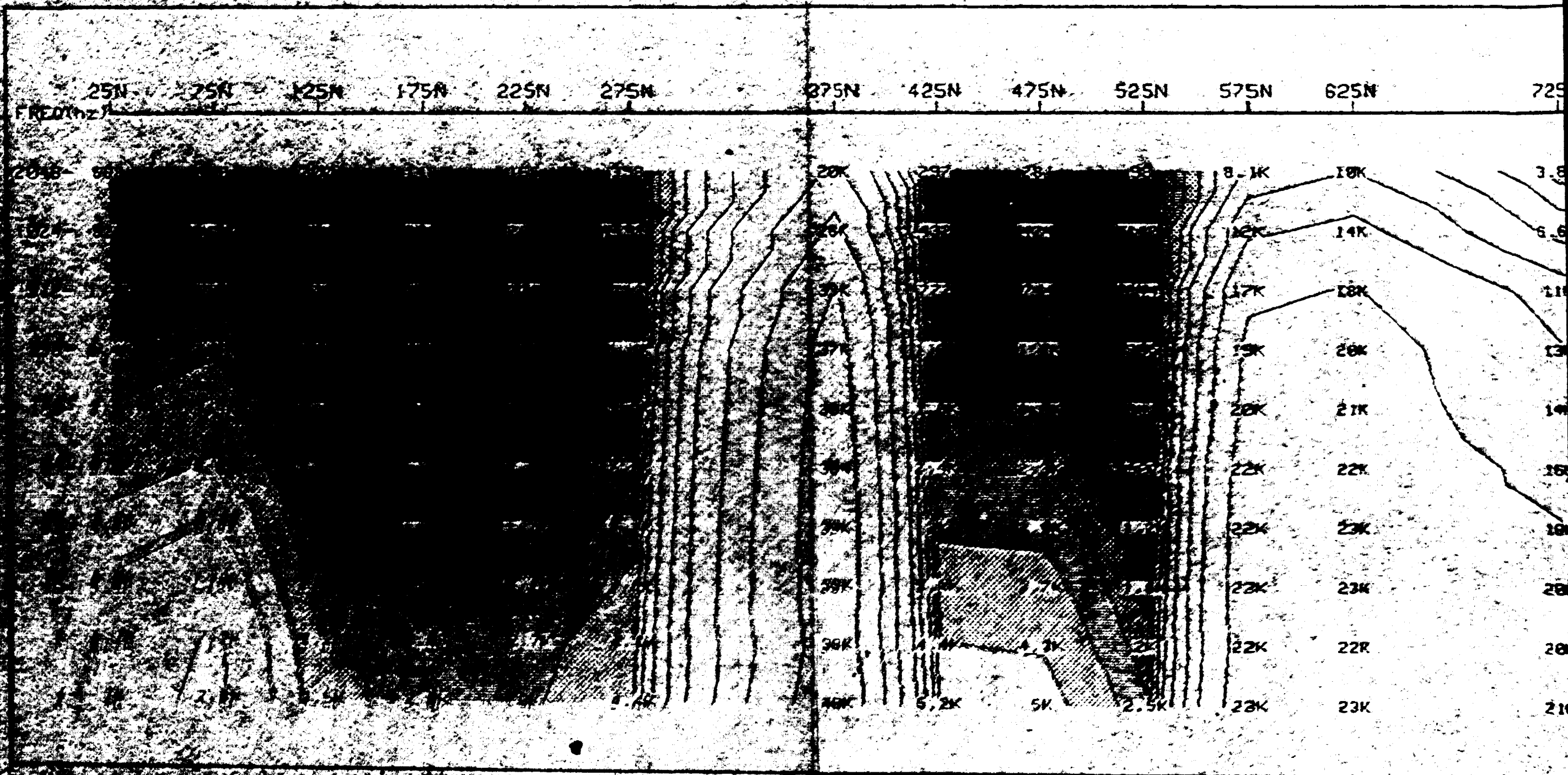
3.49

3.31

3.74

3.59







1475N 1525N 1575N 1625N 1675N 1725N 1825N 1875N 1925N 1975N 2025N  
FREQ (Hz)







CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 LINE=2625E E-dipole=5000ft Tx-Rx=8.875km

775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N



Resistivity in kΩm  
 Surveyed by QUANTECH CONSULTING INC.

1475N 1525N 1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N

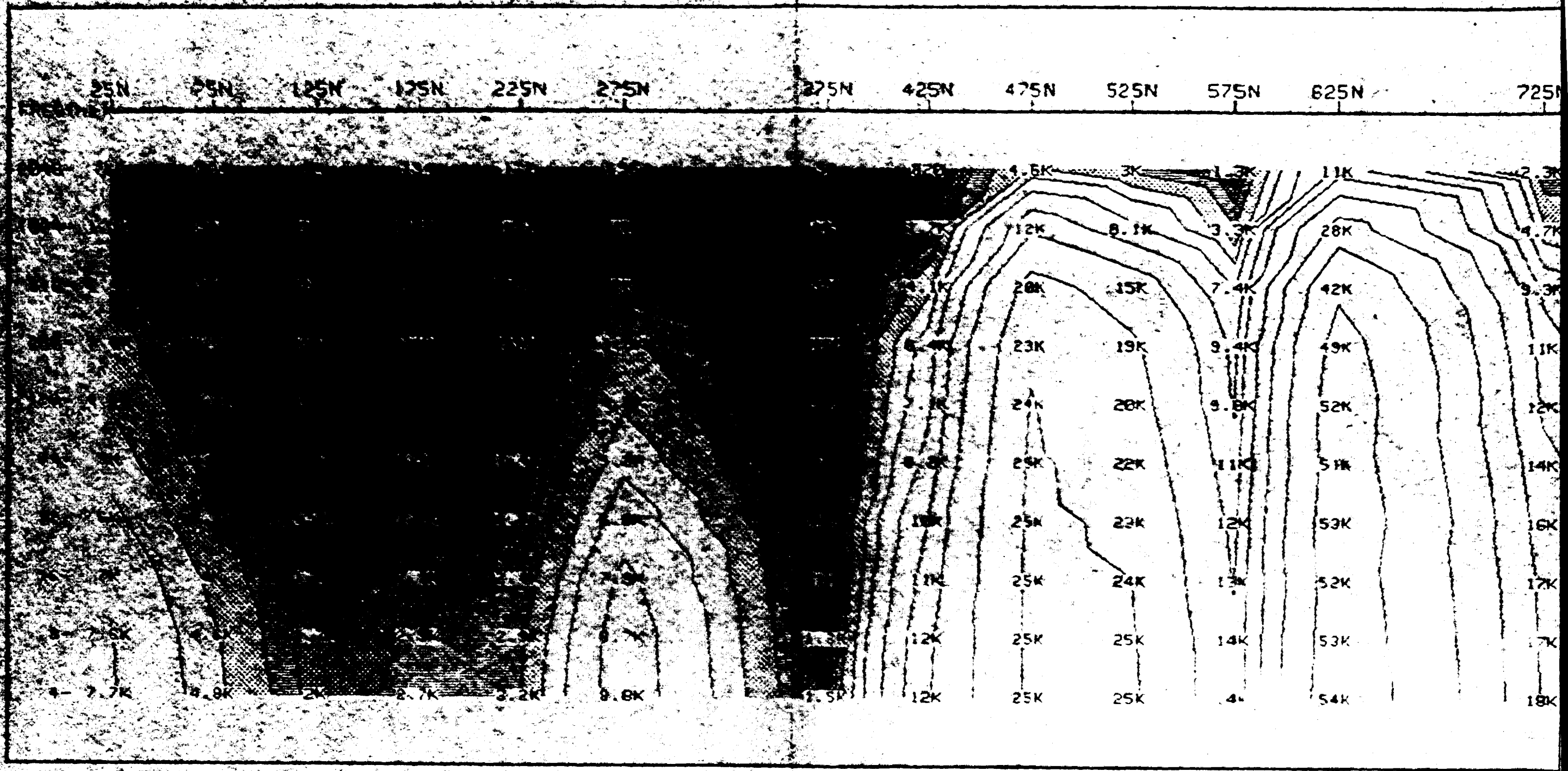
FREQ (Hz)

2040

1024

512

20 40 60 80 100 120 140 160 180 200





CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 LINE=2750E

E-dipole=5000ft Tx-Rx=8.75km

775N

825N

875N

925N

975N

1075N

1125N

1175N

1225N

1275N

1325N

1425N



Surveyed by [Name] Resistivity in ohm-m  
GENTECH CONSULTING INC. Nov 1987



1475N 1525N 1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N  
FREQUENCY



850 172 168 95 843 710 585 470 360 250 175





2925

1825N

1875N

1925N

1975N

2025N

FREQ (Hz)

2048

1024

512

256

128

64

32

16

8

4

828

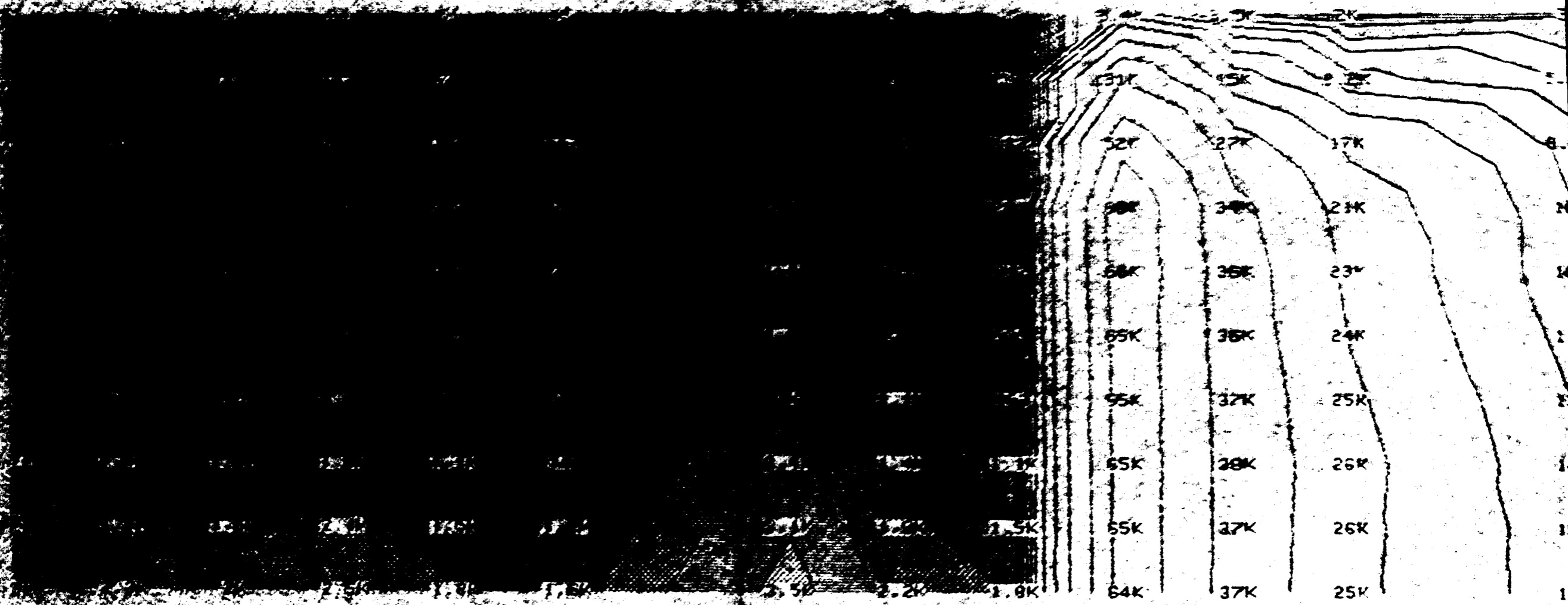
856

884

912

940

25K 75K 125K 175K 225K 275K 325K 375K 425K 475K 525K 575K 625K 675K 725K

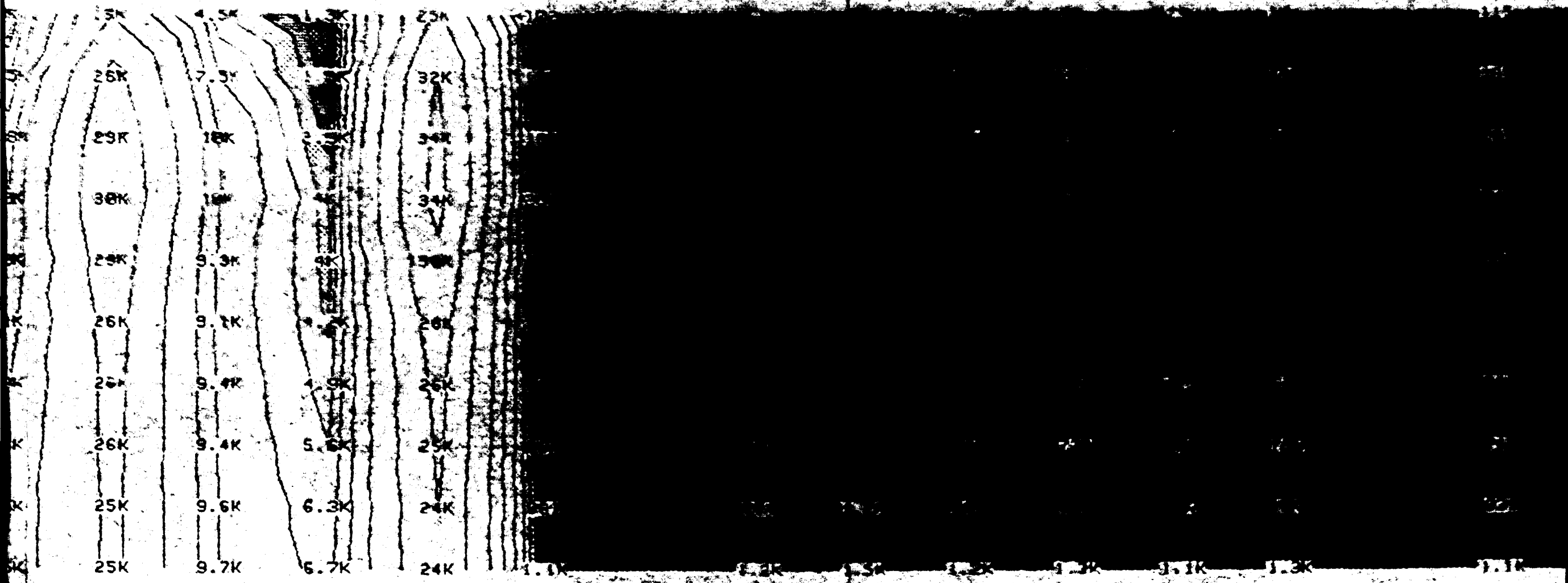


CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 LINE=3000E

E-dip = 90° S, A = 8.5km

775N 825N 875N 925N 975N 1075N 1175N 1225N 1275N 1325N 1425N



Resistivity in Ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV/1987



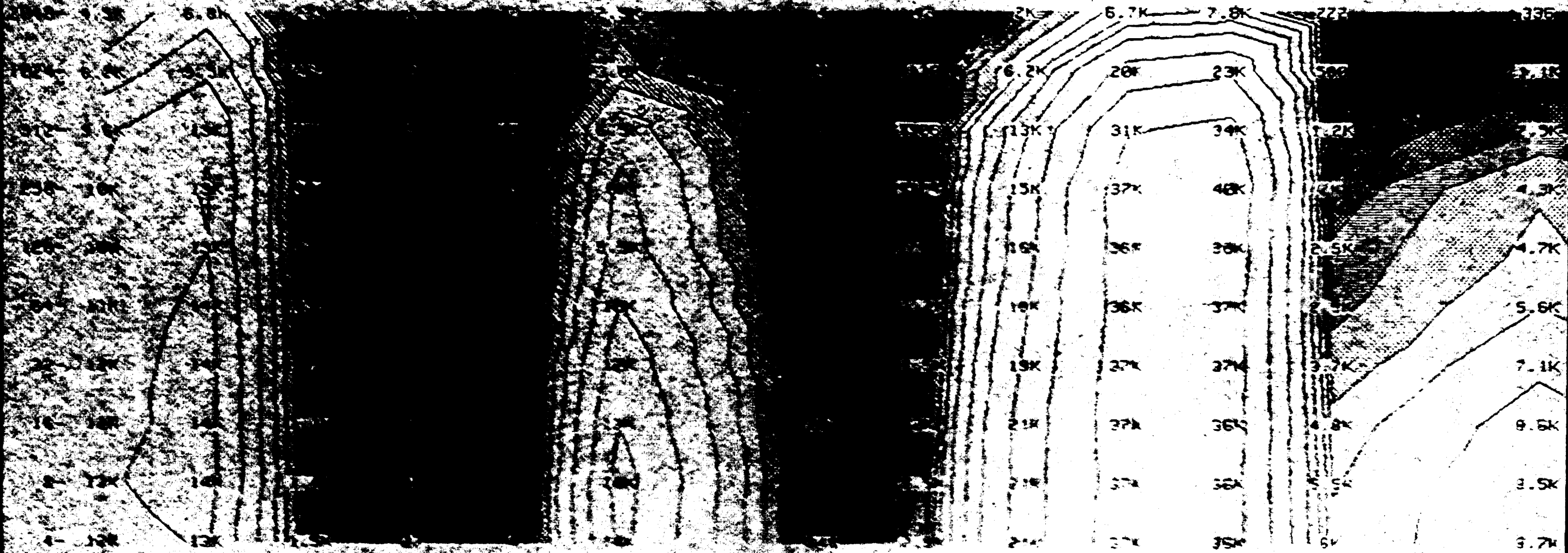
1475N 1525N 1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N

FREQ(hz)



1475 1525 1575 1625 1675 1775 1825 1875 1925 1975 2025

FREQ (Hz) 25N 75N 125N 175N 225N 275N 325N 425N 475N 525N 575N 625N 725N





# CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 LINE=3125E

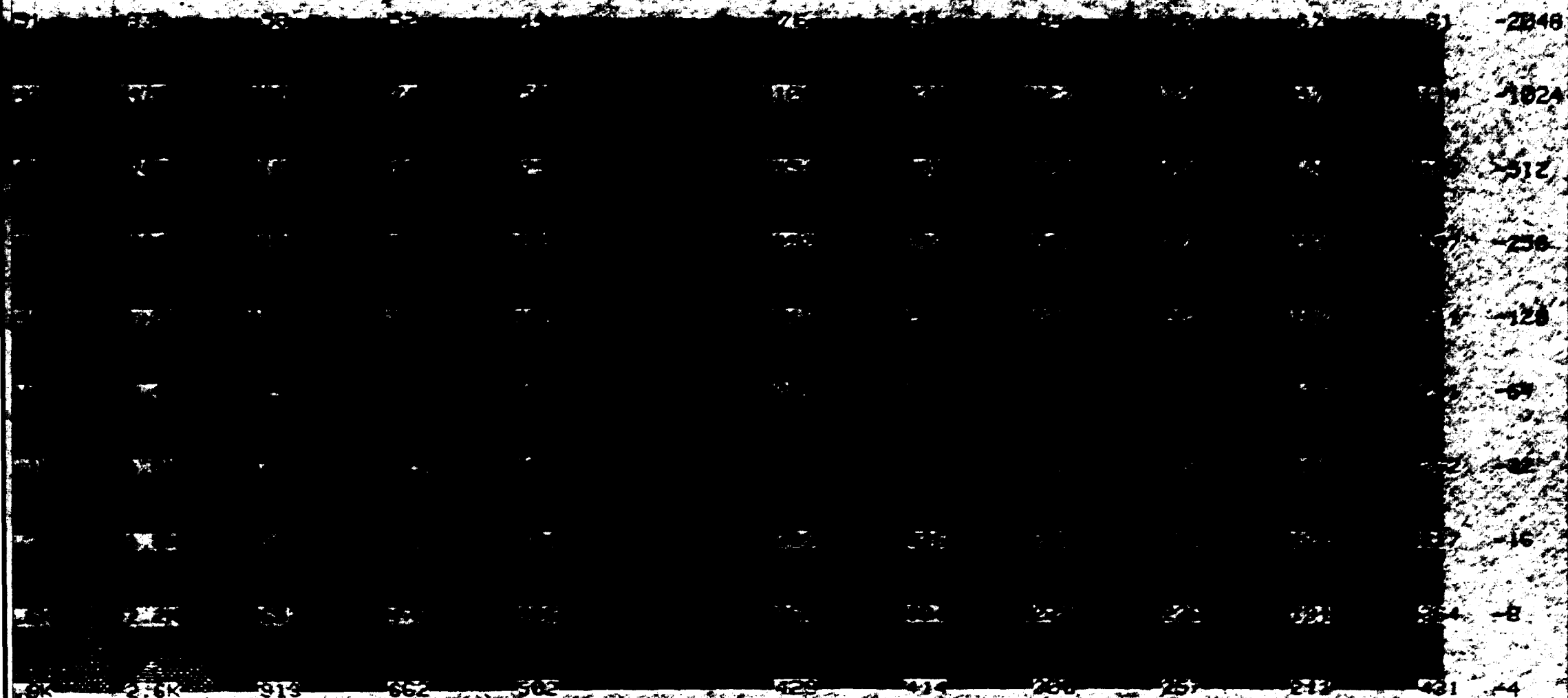
E-dipole=5000ft Tx-Rx=8.375km

775N 825N 875N 925N 975N 1075N 1125N 1175N 1225N 1275N 1325N 1425N 1475N



Resistivity contours  
 Surveyed by QUANTECH CONSULTING INC.

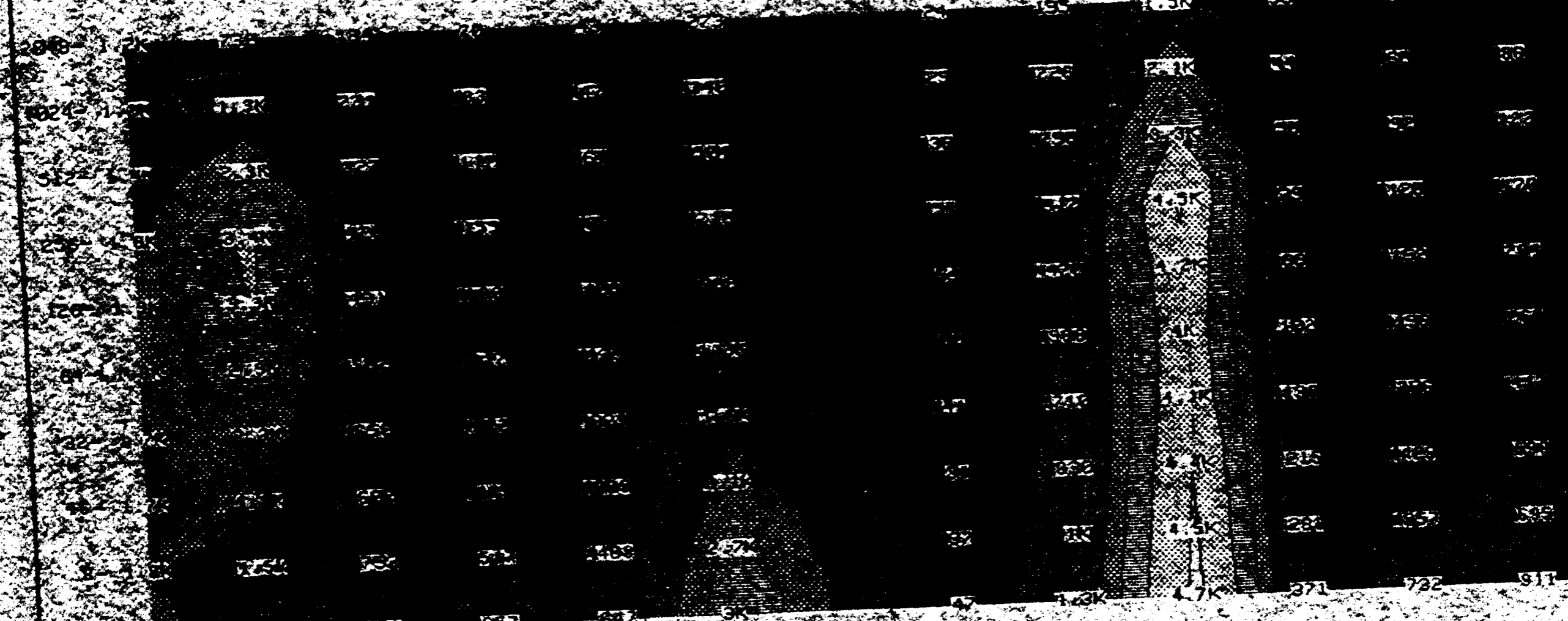
75N 1525N 1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N  
FREQ(hz)



CSAMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. - C14 LINE=3250E E-dipole=5000ft Tx-Rx=8.

FREQ (Hz) 1025N 1125N 1175N 1225N 1275N 1325N 1425N 1475N 1525N 1575N 1625N 1675N

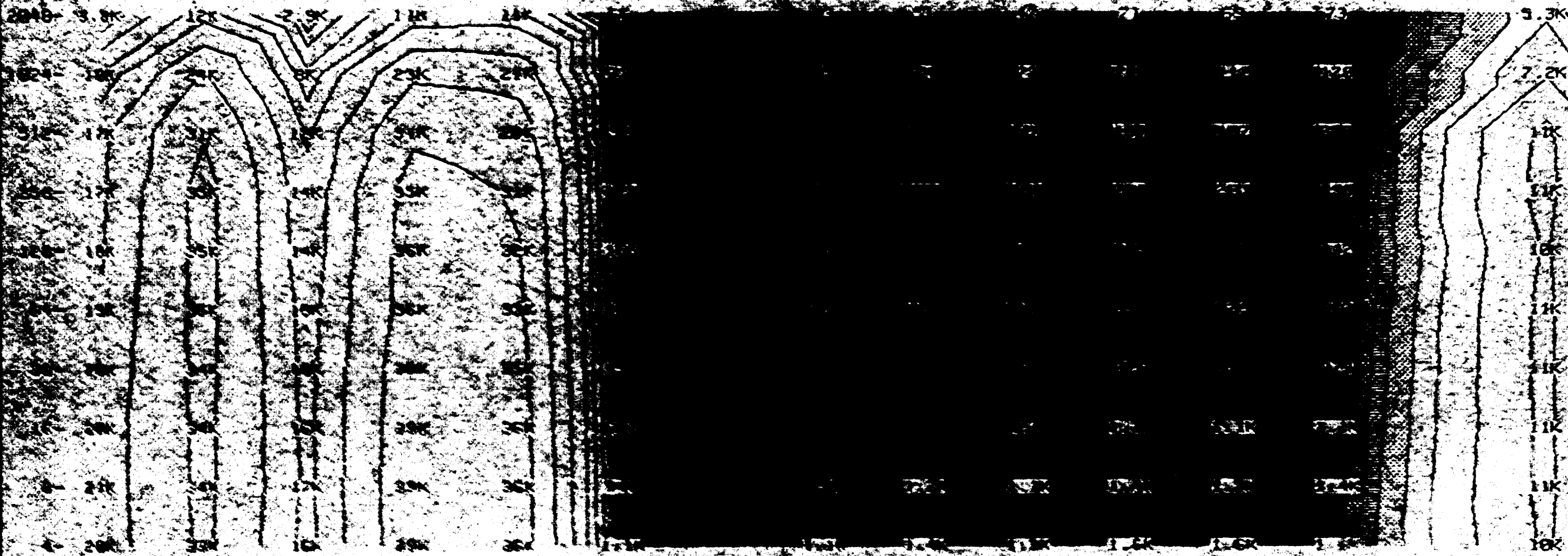


3250

25km  
1775N 1825N 1875N 1925N 1975N 2025N  
FREQ (hz)

1775N	1825N	1875N	1925N	1975N	2025N	FREQ (hz)
81	102	102	100	84	119	-2048
735	640	338	427	121	154	-1024
757	640	305	428	130	248	-512
675	624	247	428	122	264	-256
620	600	275	431	202	265	-128
628	620	428	424	102	247	-64
494	507	358	320	500	228	-32
578	574	278	445	126	198	-16
788	625	296	422	139	164	-8
991	816	334	183	78	161	-4

FREQ (Hz) 25N 75N 125N 175N 225N 275N 375N 425N 475N 525N 575N 625N 725N



# CSAMT APPARENT RESISTIVITY (CORRECTED)

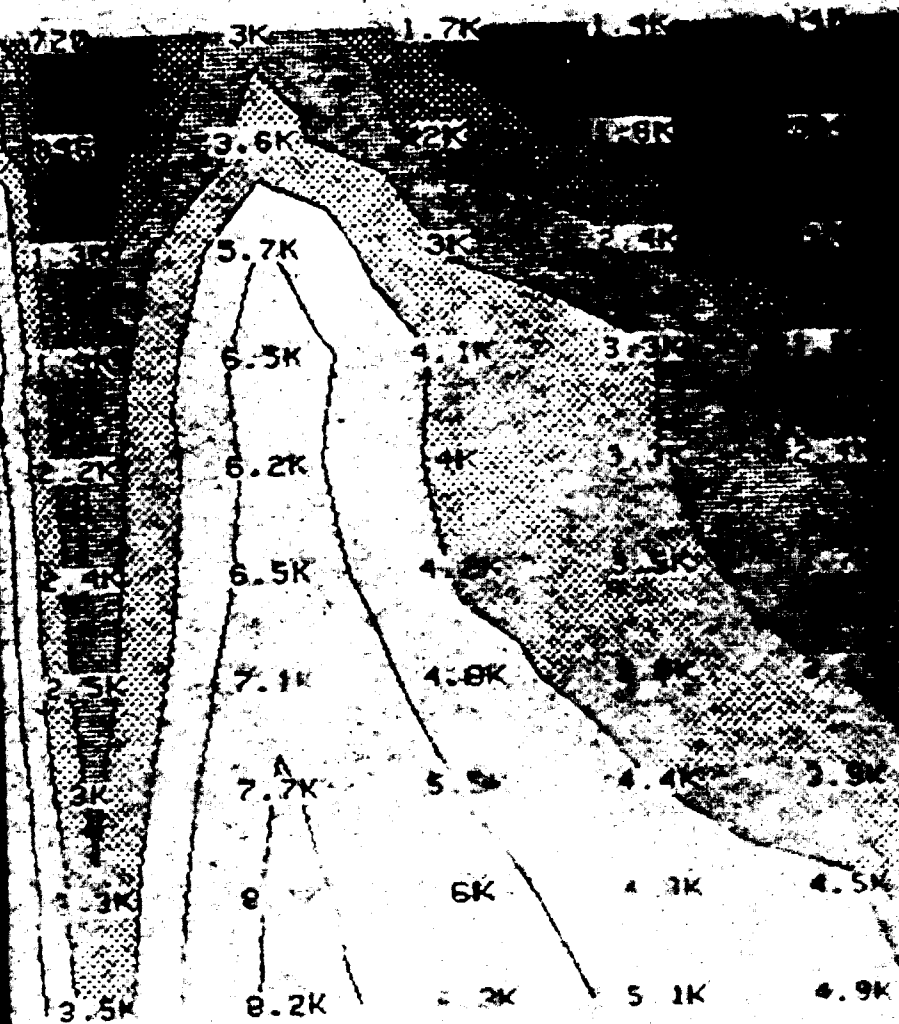
LAC MINERALS LTD. C14 LINE=3375E

E-dipole=5000ft Tx-Rx=8.125km

775N 825N 875N 925N 975N

1075N 1125N 1175N 1225N 1275N 1325N

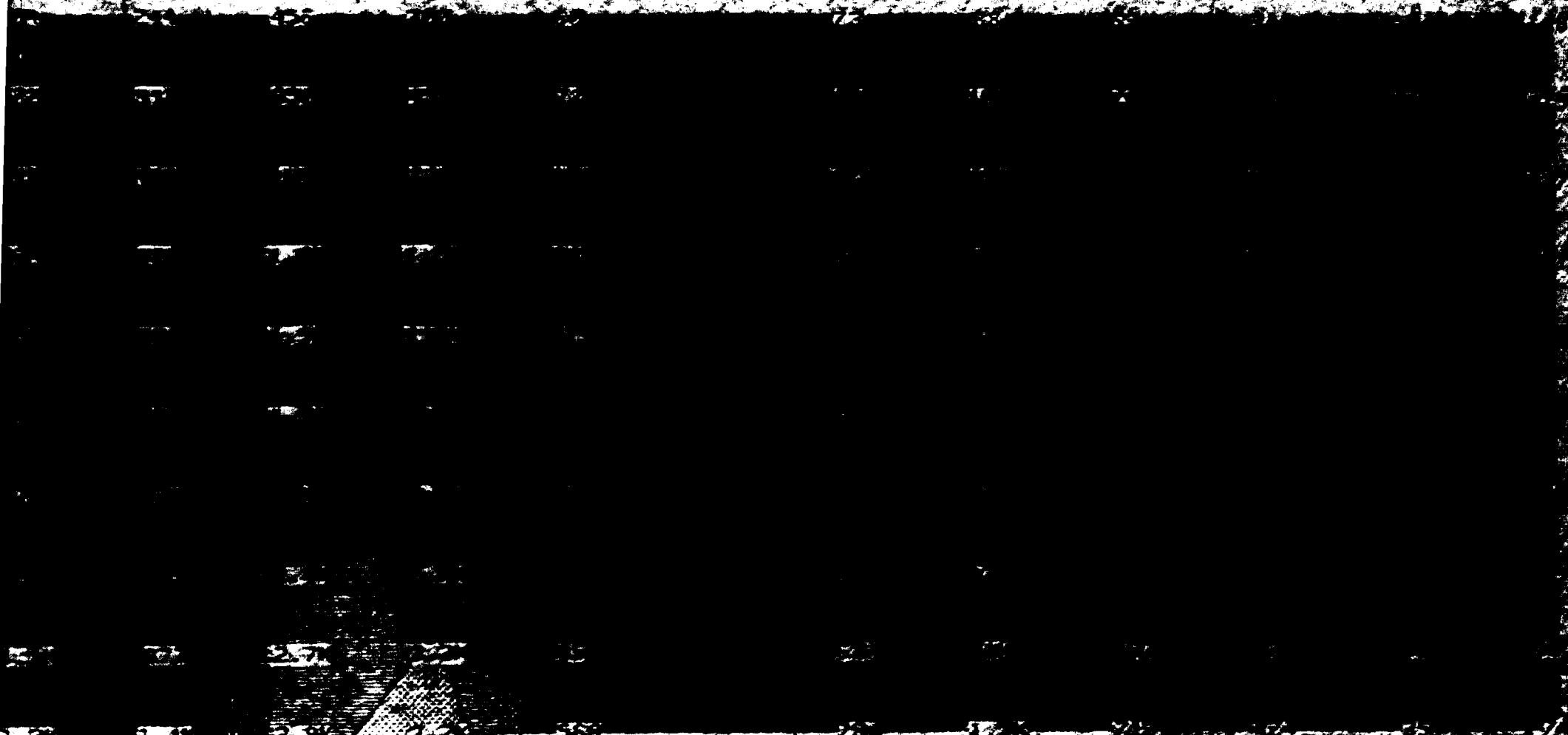
1425N 1475N



Resistivity in ohms  
 Surveyed by QUANTECH CONSULTING INC. 1995

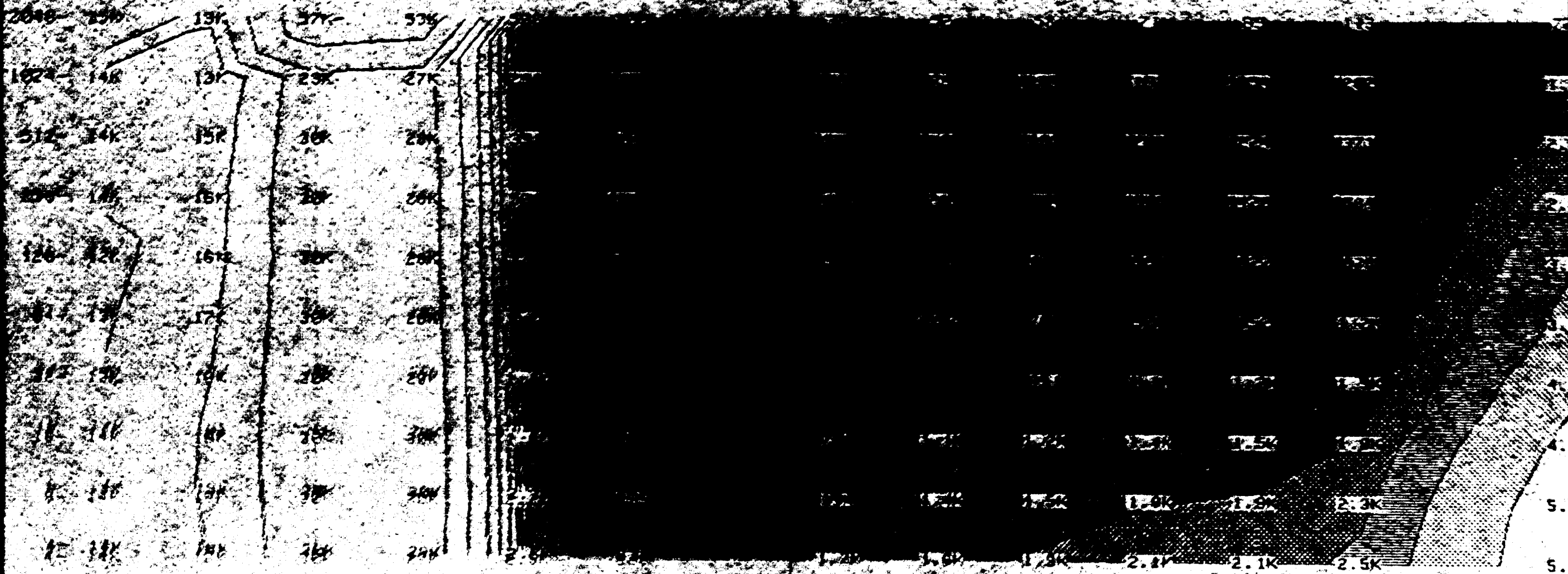


1525N 1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N



1.3K 1.4K 2.3K 2.4K 3.5K

FREQ (Hz)    25N    75N    125N    175N    225N    275N    375N    425N    475N    525N    575N    625N    725N



# CSMT APPARENT RESISTIVITY (CORRECTED)

LAC MINERALS LTD. C14 WINE-3500E

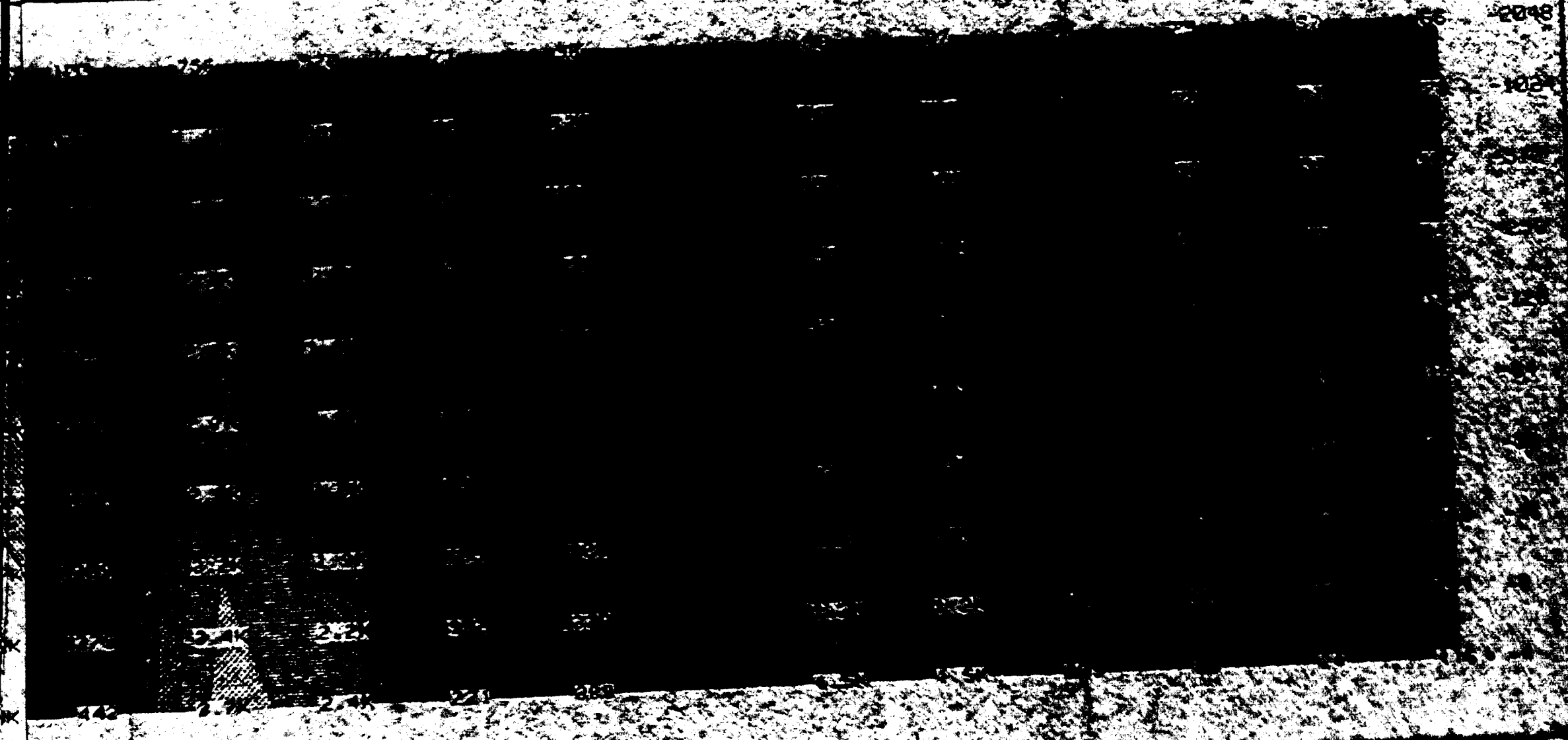
2-3 50000 Hz TV-R=8km

SN 775N 805N 875N 925N 975N 1025N 1075N 1175N 1225N 1275N 1325N 1425N



Resistivity in ohm-m  
 Surveyed by QUANTECH CONSULTING INC. NOV/1987

S 1475N 1525N 1575N 1625N 1675N 1775N 1825N 1875N 1925N 1975N 2025N FREQ (Hz)



2048

1024



**Report of Work**  
(Geophysical, Geological and Geochemical Surveys)

Mining Lands Section, Mineral Development and Lands Branch: **900**

**Mining Act**

Type of Survey(s) <b>CSAMT</b>	Mining Division <b>Larder Lake</b>	Township or Area <b>Clifford</b>
Recorded Holder(s) <b>LAC Minerals Ltd. 2.12955</b>	Prospector's Licence No. <b>T-664</b>	
Address <b>6 Al Wende Ave., P.O. Box 670, KIRKLAND LAKE, Ont. P2N 3K1</b>		Telephone No. <b>(705)-567-5656</b>
Survey Company <b>Quantech Consulting</b>		
Name and Address of Author (of Geo-Technical Report) <b>John Kovala, P.O. Box 334, KIRKLAND LAKE, Ontario P2N 3J1</b>		Date of Survey (from & to) <b>01 11 87 30 11 87</b> Day Mo. Yr. Day Mo. Yr.

Credits Requested per Each Claim in Columns at right

Mining Claims Traversed (List in numerical sequence)

Special Provisions	Geophysical	Days per Claim	Mining Claim		Mining Claim		Mining Claim	
			Prefix	Number	Prefix	Number	Prefix	Number
For first survey: Enter 40 days. (This includes line cutting)	• Electromagnetic	20	L	803325	L	918236	L	1014640
				803326		918237		1014648
				803327		918238		1014649
				803328		1014621		1014650
For each additional survey: using the same grid: Enter 20 days (for each)	• Magnetometer			803329		1014622		1014651
				803330		1014623		1014652
				803331		1014624		1014653
				803333		1014625		1014654
For each additional survey: using the same grid: Enter 20 days (for each)	• Other			803334		1014626		1014655
				803335		1014627		
				803336		1014635		
				803337		1014636		
Man Days Complete reverse side and enter total(s) here	Geological			803338		1014637		
				803339		1014638		
				803340		1014639		
				803341				
Airborne Credits Note: Special provisions credits do not apply to Airborne Surveys.	Geochemical			803342				
Total miles flown over claim(s)							Total number of mining claims covered by this report of work.	
Date <b>Oct 15 1989</b>	Recorded Holder or Agent (Signature) <i>[Signature]</i>						<b>41</b>	

**Certification Verifying Report of Work**

I hereby certify that I have a personal and intimate knowledge of the facts set forth in this Report of Work, having performed the work or witnessed same during and/or after its completion and annexed report is true.

Name and Address of Person Certifying  
**John Kovala, P.O. Box 334 KIRKLAND LAKE, Ontario**

P2N 3J1 Telephone No. (705)-567-5495 Date **October 5, 1989** Certified By (Signature) *[Signature]*

**For Office Use Only**

Total Days Cr. Recorded	Date Recorded	Mining Recorder
	Date Approved as Recorded	Provincial Manager, Mining Lands

Received Stamp

**LARDER LAKE MINING DIV.**

**RECEIVED**

**OCT 12 1989**

**AM 4:07 PM**

**7 18 10 10 11 11 12 15 11 10 5**

*[Signature]*



Ontario

Ministry of  
Northern Development  
and Mines

Ministère du  
Développement du Nord  
et des Mines

Mining Lands Section  
880 Bay Street, 3rd Floor  
Toronto, Ontario  
M5S 1Z8

Telephone: (416) 965-4888

April 10, 1990

Your File: W8908-336  
Our File: 2.12955

Mining Recorder  
Ministry of Northern Development and Mines  
4 Government Road East  
Kirkland Lake, Ontario  
P2N 1A2

Dear Sir:

Re: Notice of Intent dated February 23, 1990 for Geophysical  
(Electromagnetic) Survey submitted on Mining Claims:  
L 803326 et al in Clifford Township.

The assessment work credits, as listed with the above-mentioned Notice  
Intent have been approved as of the above date.

Please inform the recorded holder of these mining claims and so indicate  
on your records.

Yours sincerely,

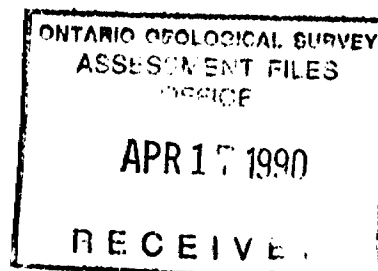
W.R. Cowan  
Provincial Manager, Mining Lands  
Mines & Minerals Division

LS:pt  
Enclosure

cc: Mr. G.H. Ferguson  
Mining and Lands Commissioner  
Toronto, Ontario

LAC Minerals Limited  
Kirkland Lake, Ontario

John Koval  
Kirkland Lake, Ontario



Resident Geologist  
Kirkland Lake, Ontario





File  
**2.12955**

Date  
**Feb 23/90**

Mining Recorder's Report of  
Work No.  
**W8908.336**

Recorded Holder  
**Lac Minerals Limited**

Township or Area  
**Clifford**

Type of survey and number of Assessment days credit per claim	Mining Claims Assessed
<b>Geophysical</b> Electromagnetic <u>20</u> days Magnetometer _____ days Radiometric _____ days Induced polarization _____ days Other _____ days Section 77 (19) See "Mining Claims Assessed" column Geological _____ days Geochemical _____ days Man days <input type="checkbox"/> Airborne <input type="checkbox"/> Special provision <input checked="" type="checkbox"/> Ground <input checked="" type="checkbox"/> <input type="checkbox"/> Credits have been reduced because of partial coverage of claims. <input type="checkbox"/> Credits have been reduced because of corrections to work dates and figures of applicant.	L 803326 to 331 incl. 803333 to 335 incl. 803337 to 342 incl. 918236 918238 1014621 1014623 to 627 incl. 1014635 to 637 incl. 1014639 1014648 to 655 incl.

Special credits under section 77 (16) for the following mining claims

15 days Electromagnetics L 1014638, 1014640

10 days Electromagnetics L 803325, 803336, 918237, 1014622

No credits have been allowed for the following mining claims

not sufficiently covered by the survey       insufficient technical data filed

Note: Credits were reduced because L 2250 E was not Surveyed and L3250 E was not surveyed from BLD to 1075N.

The Mining Recorder may reduce the above credits if necessary in order that the total number of approved assessment days recorded on each claim does not exceed the maximum allowed as follows: Geophysical - 80; Geological - 40; Geochemical - 40; Section 77(19) - 60.



Ministry of  
Northern Development  
and Mines

DOCUMENT No.  
**W8908-336**

Instructions

- Please type or print.
- Refer to Section 77, the Mining Act for assessment work requirements and maximum credits allowed per survey type.
- If number of mining claims traversed exceeds space on this form, attach a list.
- Technical Reports and maps in duplicate should be submitted to Mining Lands Section, Mineral Development and Lands Branch.

**Mining Act** Report of Work **2.12955**  
(Geophysical, Geological and Geochemical Surveys)

Type of Survey(s) <b>CSAMT</b>	Mining Division <b>Larder Lake</b>	Township or Area <b>Clifford</b>
Recorded Holder(s) <b>LAC Minerals Ltd.</b>	Prospector's Licence No. <b>T-664</b>	
Address <b>6 Al Wende Ave., P.O. Box 670, KIRKLAND LAKE, Ont. P2N 3K1</b>		Telephone No. <b>(705)-567-5656</b>
Survey Company <b>Quantech Consulting</b>		
Name and Address of Author (of Geo-Technical Report) <b>John Kovala, P.O. Box 334, KIRKLAND LAKE, Ontario P2N 3J1</b>		Date of Survey (from & to) 01 11 87 30 11 87 Day Mo Yr Day Mo Yr

Credits Requested per Each Claim in Columns at right

Mining Claims Traversed (List in numerical sequence)

Special Provisions	Geophysical	Days per Claim	Mining Claim		Mining Claim		Mining Claim	
			Prefix	Number	Prefix	Number	Prefix	Number
For first survey:  Enter 40 days. (This includes line cutting)	- Electromagnetic	<b>20</b>	<b>L</b>	<b>803325</b>	<b>L</b>	<b>918236</b>	<b>L</b>	<b>1014640</b>
	- Magnetometer			<b>803326</b>		<b>918237</b>		<b>1014648</b>
	- Other			<b>803327</b>		<b>918238</b>		<b>1014649</b>
For each additional survey using the same grid:  Enter 20 days (for each)	Geological			<b>803328</b>		<b>1014621</b>		<b>1014650</b>
	Geochemical			<b>803329</b>		<b>1014622</b>		<b>1014651</b>
				<b>803330</b>		<b>1014623</b>		<b>1014652</b>
				<b>803331</b>		<b>1014624</b>		<b>1014653</b>
				<b>803333</b>		<b>1014625</b>		<b>1014654</b>
				<b>803334</b>		<b>1014626</b>		<b>1014655</b>
				<b>803335</b>		<b>1014627</b>		
				<b>803336</b>		<b>1014635</b>		
				<b>803337</b>		<b>1014636</b>		
				<b>803338</b>		<b>1014637</b>		
				<b>803339</b>		<b>1014638</b>		
				<b>803340</b>		<b>1014639</b>		
				<b>803341</b>				
				<b>803342</b>				
Man Days			Total number of mining claims covered by this report of work.		<b>41</b>			
Complete reverse side and enter total(s) here	Geophysical	Days per Claim	<b>RECEIVED</b>					
	- Electromagnetic		<b>NOV 06 1989</b>					
	- Magnetometer		<b>MINING LANDS SECTION</b>					
	- Other							
	Geological							
	Geochemical							
Airborne Credits	Electromagnetic	Days per Claim						
Note: Special provisions credits do not apply to Airborne Surveys.	Magnetometer							
	Other							
Total miles flown over claim(s).	Date <b>Oct 5 1989</b>		Recorded Holder or Agent (Signature) <i>[Signature]</i>					

Mining Claim		Mining Claim		Mining Claim	
Prefix	Number	Prefix	Number	Prefix	Number
L	803325	L	918236	L	1014640
	803326		918237		1014648
	803327		918238		1014649
	803328		1014621		1014650
	803329		1014622		1014651
	803330		1014623		1014652
	803331		1014624		1014653
	803333		1014625		1014654
	803334		1014626		1014655
	803335		1014627		
	803336		1014635		
	803337		1014636		
	803338		1014637		
	803339		1014638		
	803340		1014639		
	803341				
	803342				

Certification Verifying Report of Work

I hereby certify that I have a personal and intimate knowledge of the facts set forth in this Report of Work, having performed the work or witnessed same during and/or after its completion and annexed report is true.

Name and Address of Person Certifying  
**John Kovala, P.O. Box 334 KIRKLAND LAKE, Ontario**

P2N 3J1 Telephone No. **(705)-567-5495** Date **October 5, 1989** Certified By (Signature) *[Signature]*

**For Office Use Only**

Total Days Cr. Recorded <b>820</b>	Date Recorded <b>Oct 12/89</b>	Mining Recorder <i>[Signature]</i>
	Date Approved as Recorded <b>See revised</b>	Provincial Manager, Mining Lands <i>[Signature]</i>

**work statement**

Received Stamp

**LARDER LAKE MINING DIV.**

**RECEIVED**

**OCT 12 1989**

AM **4:07** PM

7 18 19 10 11 12 13 14 15 16

*[Signature]*

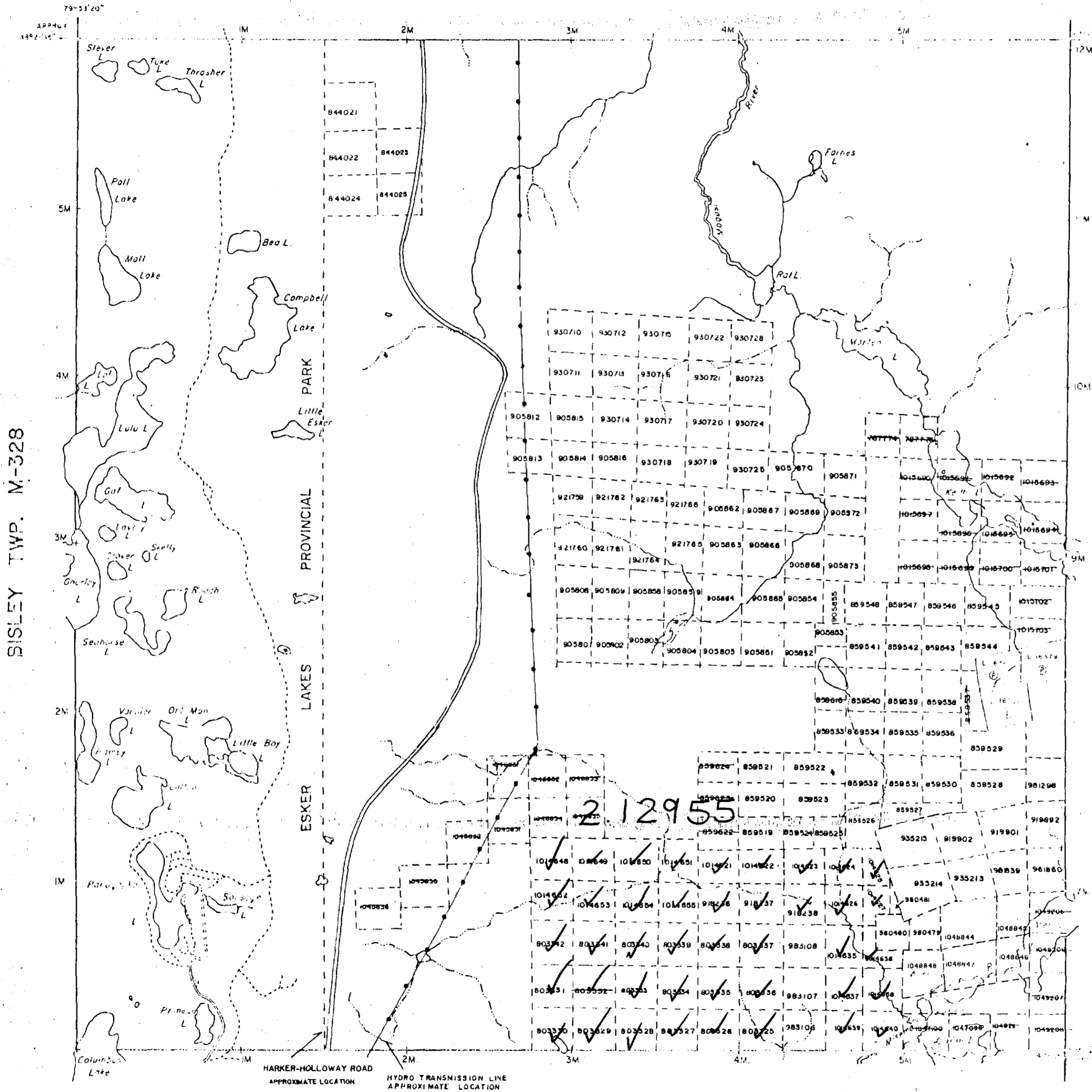
ELLIOTT TWP. M-347

NOTES

400' surface rights reservation along the shores of all lakes and rivers.

TOWNSHIP CLIFFORD  
 FORESTRY ACTIVITY

NOTICE OF FORESTRY ACTIVITY  
 THIS TOWNSHIP / AREA FALLS WITHIN THE  
 ABITIBI MANAGEMENT UNIT  
 AND MAY BE SUBJECT TO FORESTRY OPERATIONS  
 THE MNR UNIT FORESTER FOR THIS AREA CAN BE  
 CONTACTED AT: P.O. BOX 129  
 SWASTIKA, ONT.  
 POK 110  
 705-642-3222



SISLEY TWP. M-328

BEN NEVIS TWP. M-325

ARNOLD TWP. M-321

LEGEND

- PATENTED LAND
- PATENTED FOR SURFACE RIGHTS ONLY
- LEASE
- LICENSE OF OCCUPATION
- CROWN LAND SALES
- LOCATED LAND
- CANCELLED
- MINING RIGHTS ONLY
- SURFACE RIGHTS ONLY
- HIGHWAY & ROUTE NO.
- ROADS
- TRAILS
- RAILWAYS
- POWER LINES
- MINING CLAIM
- MINES
- Township Office

DATE OF ISSUE  
 6 6 1989  
 CLIFFORD  
 MINING & FORESTRY OFFICE

TOWNSHIP CLIFFORD  
 DISTRICT OF TIMISKAMING  
 LARDER LAKE  
 MINING DIVISION

SCALE: 1 INCH = 400 METERS (1:40000)

PLAN NO. M-338



MINISTRY OF  
 NORTHERN DEVELOPMENT  
 AND MINES



32055W002 2.12955 CLIFFORD



2.12955  
 Lac Minerals Ltd.  
 Grid C14  
 Clifford Twp. Ont.  
 Grid and Claim Plan  
 Nov 1989

