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REPORT OF WORK PERFORMED

on

DIEPDAUME MINES LIMITED PROPERTY

Tisdale and Deloro Townships Porcupine Mining Division of Ontario January 1 - December 31, 1982



June 27, 1983

Revised December 9, 1983

H.A. PEARSON, P. Eng.



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DIEPDAUME MINES LIMITED

Work Performed during the Period

January 1 - December 31, 1982

1. SUMMARY

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A) THE PROPERTY

The property is comprised of the former Preston East Dome Mines Limited which produced gold from 1938 to 1968. During this period, the Preston East Dome mined 6,284,405 tons with an average grade of 0.24 ozs. gold per ton.

The property is located in the southeast quadrant of Tisdale Township in the Porcupine Mining Division of Ontario. It adjoins the south boundary of Dome Mines Limited which is in full production.

The mine was left in bad disorder, and in an unsafe condition. Total rehabilitation to safe production standards will be extensive.

Also included in this report is a group of claims in Deloro Township, adjoining the south side of the main mine property.

B) THE PROGRAM AND ITS OBJECTIVES

The Preston East Dome workings broke into the workings of the Paymaster Mine in the Midcamp Section of the Preston Mine.

The closing of the Paymaster Mine and its subsequent flooding ultimately forced the closing of the Preston East Dome which did not have the pumping capacity to handle the extra influx of water. Preston was faced with the problem of pumping 850 gallons of water per minute. This included 350 gallons per minute from the Paymaster and 90 gallons per minute from the Buffalo Ankerite Mine.

As a result, considerable tonnage of ore which would be viable at the current price of gold was left in place.

In the Midcamp Area of the Preston Mine there remain 350,000 tons of sulphide ore with an average grade of 0.15 ozs. gold per ton between the 18th level and the 10th level. The bulk of the Preston ore was free milling and 60 percent of the gold was recovered on the jigs. The remainder was recovered by cyanidation.

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However, there was no flotation circuit to handle the sulphide ore which caused flouring of the mercury and prevented amalgamation. In addition, the chlorite from the sulphide ore clogged the filters and the pyrrhotite consumed enormous quantities of cyanide.

The present mill being constructed on the Diepdaume Property has a flotation system and can handle the sulphide ore.

In addition, a minimum of 50,000 tons of ore with an average grade of approximately 0.5 ozs. gold per ton was developed on the Preston 14th level near the Dome boundary close to the Diepdaume Main (No. 2) Shaft. This was the highest grade ore ever encountered at the Preston East Dome. The rising water prevented it from being mined. It still remains in place.

Further, ore from the Dome Mines strikes and dips onto the Diepdaume on its 19th level (Dome, 20th level). This represents a considerable tonnage, on the Diepdaume property, which has been partially developed, but was not mined due to the rising water.

Finally considerable tonnage was left in the walls of the large stopes in the Preston Porphyry between the 9th level and surface. This would now be ore at current gold prices. Both Dome and Pamour (former McIntyre Mine) are now mining large tonnages of similar ore from the walls of their old stopes.

During 1982, dewatering of the 400,500 and 600 levels of the Diepdaume Mine was carried out. In addition, rehabilitation and sampling was carried out on the 250, 375 and 500 levels of the New York Porcupine Section of the Diepdaume Mine.

During this period, reconstruction of the mill continued and metallurgical tests were conducted on the Diepdaume ore (Appendix 2).

The sampling program both underground and on surface is outlined in Appendix 1.

Sampling, stripping and geological mapping was conducted on surface in an area approximately 400 feet south of the southeast corner of Simpson Lake.

And finally, a program of prospecting and geological mapping was completed in the vicinity of an electromagnetic conductor on the Deloro Township group of claims.

2) UNDERGROUND REHABILITATION

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A) MAIN SHAFT AREA (NO. 2 SHAFT)

Plans of all the levels de-watered to date to the 675 level are covered by Figures 1, 2, 2a, 3, 3a, 4, 4a, 5, 5a, 5b, 6 and 6a.

Due to the continuation of our 1981 de-watering and re-habilitation program, we were able to clear the 400, 500 and 600 levels.

As each level was de-watered new guides were installed in the cage and skip compartments. Landings and ladders were replaced in the manway compartment.

Shaft cables for the electrical installations were run at the time each level was washed, scaled and cleared of debris. Figure 7.

A fault on the fourth level was rockbolted and strapped and a fire door was installed.

Extremely unsafe ground conditions prevented any work from being done on the 4th level.

Due to the volume of water and depth of the 5th level a new pumping facility was installed. Figures 8 and 8a.

An one foot thick concrete dam was constructed with intake and outlet pipes at the entrance to a dead end drift.

The old charging station was slashed to facilitate the installation of a 100 hp. stationary pump. The pump station back and travelway were rockbolted.

A 140 hp. Flygt pump was installed behind the dam as a standby pump.

A 30 hp. Flygt pump was attached to a cross head and lowered down the shaft 160 feet; this pump is used to feed the 500 level dam.

The 550 loading pocket was re-habilitated. Old flooring and timber were replaced. The loading pocket chute was relined with abrasive plate. New control chains and air cylinders were installed.

Finally, the 600 level was cleaned and a bulk head built for conveyance safety.

B) NEW YORK PORCUPINE SHAFT AREA

The New York Porcupine shaft is located 2300 feet due west of the Diepdaume main shaft.

The N.Y.P. concrete shaft cap was removed to provide ventilation to the mine, and access to the N.Y.P. 250 and 375 levels. Manway, landings, and ladders were replaced from surface down to the 250 level.

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The shaft collar was housed to prevent unauthorized entry.

1200 feet due south of the N.Y.P. shaft an internal winze (250) was retimbered and new ladders installed in the manway compartment. This provided entry to the 375 N.Y.P. level.

Access from the 375 N.Y.P. level to the 500 level Diepdaume was provided by installing new ladders in the 375 access raise, a length of 225 feet.

The above work provided the mine with an emergency manway in case of fire, increased natural ventilation and provided access to partially developed areas.

The most difficult and time consuming aspects of working in this area were the long distances to travel and lack of mechanical transport to move material. All material needed was carried manually over considerable distances to the working areas.

A systematic sampling program was initiated for this area. The program included drift sampling, muck sampling, and stope sampling (see maps and assay reports). See Appendix 1.

The drift and muck sampling posed no problems. However, stope sampling proved much more difficult. Stope raises had to be timbered and stagings built to reach stope backs and faces.

3. SURFACE EXPLORATION

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A. AREA SOUTHEAST OF SIMPSON LAKE, FIGURE 14

This section lies about four-hundred feet south of the south-east end of Simpson Lake. It includes the area where a series of closely spaced drill holes were put down previously to test an area of quartz veins in porphyry in an effort to block out possible readily accessible surface ore for future early mill feed.

The area was prospected, light overburden was stripped and the whole geologically mapped in the fall of 1982.

This work uncovered a sizeable area of quartz veins and stringers in the porphyry north-east of the drill holes area. This zone of quartz and porphyry requires more stripping, rock trenching, sampling and drilling.

A number of grab samples were taken during the prospecting and mapping. The strong quartz vein which extends north-west of the raise area was chip sampled. (The raise is connected to the New York Porcupine underground workings of our property.) The areas east and west of the mapped area are heavily overburdened. The area to the north near Simpson Lake has some outcrops. 1997年1月1日には、1997年1月1日に、1997年1月1日には、1998年1月1日には、1997年1月1日には

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Assay results were disappointing but much stripping and sampling must be done to properly assess the economic potential of this part of the mine property.

B. AREA OF THE ELECTROMAGNETIC CONDUCTOR - DELORO TOWNSHIP, FIGURE 15

An electromagnetic survey was carried out in 1981 over a group of claims adjacent to the south side of the main property in Deloro Township. This work resulted in detecting several conductors. The strongest Conductor designated as "A" was selected as the most important. The area along the length of the conductor axis was prospected and then mapped in detail in an effort to ascertain the reason for the conductor in 1982.

A banded iron formation consisting of abundant quartz with ribbons of magnetite and red jasper was found to lie about 200 feet south of the conductor and p_{a} rallel to it for most of its length. Most of the conductor lies along a broad flat depression hosting a small watercourse and acting as a drainage basin with a south-west flow. The area is heavily overburdened with clay.

The north-east end of the conductor passes through an area of carbonatized volcanics and quartz prophyry with the Iron Formation on the south side. The conductor appears to be offset about 150 feet west side south along the porphyry.

The conductor appears to be caused in part by low wet clay soil conditions but the strong crossovers may preclude this. The conductor requires a drill test.

Low gold values were reported by previous operators in the iron formation. A program of stripping and sampling is planned to test the economic potential of this strong geological structure.

4. COSTS INCURRED

A total of \$635,873.80 was expended on the property during the period.

A breakdown of the apportioned costs accompanies the Application for the Ontario Mineral Exploration Program.Grant.

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December 9, 1983

APPENDIX 1

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THE SAMPLING PROGRAM

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In 1982, surface and underground sampling were conducted on the Diepdaume Mines property.

A total of 314 samples were taken. Of these, 20 were bulk or grab samples from surface; and 294 were underground channel, muck or chute samples.

Surface stockpiles were sampled to determine whether these would provide mill-feed. The stockpiles sampled were: Cincinatti stockpile east, Cincinatti stockpile west, New York Porcupine stockpile east and Preston East Dome stockpile south. All proved to be too low grade for the mill.

In the surface trenches, the area 400 feet south of the southeast end of Simpson Lake gave grab samples ranging from 0.005 ozs. gold per ton to 0.20 ozs. gold per ton.

In the Main Shaft area, chip samples near the stations on the 550 and 675 levels gave relatively high assays ranging up to 6.10 ozs. gold per ton. (Assay sheets 5 and 6) These are within the relatively high grade shaft ore pillar on the Main Shaft, which contains 42,000 tons with a grade of 0.35 ozs. gold per ton.

Sampling of the 550 level - 500 main drift west in the Main Shaft area gave only slight encouragement (Assay sheets 10, 11, and 12).

In the New York Porcupine Shaft area, drifts, cross-cuts and partially mined stopes were re-sampled on the 250 and 375 levels to see if the quartz veins would prove economic at the present price of gold (approximately \$400 per ounce); and some of the results of this sampling proved encouraging and merit further investigation. (Figures 9, 10, 11, 12 and 13).

Samples from 6 chutes in 260 stope proved to be exceptionally high grade ranging from 0.158 ozs. gold per ton to 0.956 ozs gold per ton - with samples from 4 of the 6 chutes assaying above 0.50 ozs. gold per ton. This material must have sloughed off the walls of the stope. The stope will be examined in detail (Assay sheet 14 - samples 1348 to 1353).

In this same area, 260A drift indicated 5 veins with good grade or high grade gold assays (0.473, 2.90, 0.119, 0.162 and 5.27 ozs.), Sheet 19.

Also quartz veins in 267 drift gave significant assays, indicating that the walls of this drift should be slashed and the extensions of the veins opened up. (Assay sheet 14 - Samples 1355 to 1366 and 1373), Figure 11.

Finally, on the 250 level, 203W cross-cut south west (Figure 9) returned significant assays in a series of channel samples (Samples 1379 to 1394 15). These channels were all across 5 foot widths. Further development of indicated for this area.

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A series of tests were conducted on Diepdaume's underground ore and old tailings, to study the amenability of these materials by the use of flotation.

- ii -

Tailings with a gold content in the range of 0.006 to 0.01 ozs. per ton yielded rough concentrates averaging 0.03 ozs. per ton, with recoveries ranging from 17 to 36 per cent.

Further testing is necessary and has been planned for these materials.

Underground ore was also subjected to flotation tests. Samples with a gold content in the range of 0.014 to 0.03 ozs./ton yielded rough concentrates averaging 0.25 ozs. per ton with recoveries up to 65 per cent.

Samples with a gold content in the range of 0.07 to 0.09 yielded concentrates averaging 1.5 ozs. per ton with recoveries up to 80 per cent.

Samples with a gold content of 0.2 ozs. per ton yielded rough concentrates assaying over 5 ozs. per ton gold, with recoveries up to 92 per cent.

Finally, high grade samples in the range of 0.4 to 0.6 ozs. per ton of gold, yielded concentrates in the 15 ozs. per ton range with recoveries up to 96 per cent.

No attempt was made at recovering elemental gold by gravity previous to flotation.

Further testing on these materials is presently being conducted.

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ASSAY REPORT

DATE _____ October 18, 1982.

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|---|---------------|---------------------------|--------------------------------|---|---|---|
| | SAMPLE NO. | DESCRIPTION | AU <u>% Nil</u> oz/m ton | % | % | 7o |
| | 1201 | Cincinatti Stockpile West | 0.031 | | | |
| Î | 12 02 | 11 | 0.040 | | | |
| | 1203 | 11 | 0.011 | | | |
| | 1204 | n |).015 | | | |
| | 1205 | n | .011 | | | |
| | 1206 | Cincinatti Stockpile East | 0.108 | | | |
| | 1207 | n | 0.020 | | | |
| | 1208 | n | 0.090 | | | |
| | 1209 | 11 | 0.007 | | | |
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DATE October 18, 1982.

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| SAMPLE NO. | DESCRIPTION | AU <u>% Ni]</u> oz/m ton | % | % | 5/0 |
| 1211 | N.Y.P. Stockpile East | 0,007 | | | |
| 1212 | 81 | 0.0571 | · · · · · · · · · · · · · · · · · · · | | |
| 1213 | 11 | 0.011 | | | |
| 1214 | 11 | 0.027 | | | |
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| | SAMPLE NO. | DESCRIPTION | AU % <u>Nil</u> oz/m ton | % | % | 51 10 |
| | 1215 | P.E.D. #1 Stockpile South | 0.145 | | | |
| | 1216 | 81 | 0.011 | | | |
| | 1217 | n | 0.020 | | | |
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| | | Certific | ate of Ana | lysis | 4 |
| Certificate No. | 53299 | | - | Date: | May 12 1982 |
| Received May 6 19 | 982 | 3 | Samples of | Ore | |
| Submitted byDiep | odaume Mines | Ltd., Tim | nins, Ontario | | |
| | | | | | |

| SAMPLE NO. | GOLD Oz./ton |
|------------|-----------------|
| GRAB-1 | 0.20 |
| -2 | 0.002 |
| -3 | 0.005 |

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G. Lebel - Manager

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|---|---------------|-------------|--|---|---|--|
| | SAMPLE NO. | DESCRIPTION | AU % N11 oz/m ton | % | % | <i>1</i> 0 |
| | 1 | Fifth Level | 6.10 | | | |
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| | 3 | n | 1.03 | | | |
| | 4 | lt | 0.12 | | | |
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ASSAY REPORT

DATE October 18, 1982.

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| SAMPLE NO. | DESCRIPTION | AU <u>%-N11</u> oz/m ton | % | % | <i>¶</i> 0 |
|---------------|---------------------------------------|--------------------------------|---|---|------------|
| 1 | Sixth Level | 0.08 | | | |
| 2 | 11 | 0.04 | | | |
| 5 | n | 0.206 | | | |
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|--|---|---|
| Űe | rtificate of Analysis | 7 |
| Certificate No. <u>52930</u> Received <u>Jan. 7/82</u> <u>2</u> Submitted by <u>Diepdaume Mines Ltd.</u> | Date: | January 7 1982 |
| SAMPLE NO. 1612 1613 | GOLD Oz./ton 0.09 203 S.DR 0.23 ``` | L.W. EAST Rw WEST |

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G. Lebel - Manager

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Certificate of Analysis

| Certificate No | 53193 | | | Date: | April 2 1982 | |
|----------------|-----------------|----------|-----------------|-------|--------------|---|
| Received Ma | r.26/82 | 3 | Samples of | Ore | | |
| Submitted by | Diepdaume Mines | Ltd., Ti | mmins, Ontario | | | |
| | <u></u> | | | | | |
| | | | | | | |
| | SAM | PLE NO. | GOLD Oz./ton | | | ĸ |

| 1614 | 2.38 | 555 D.A. | LW | 41 |
|------|------|-------------|-------|------|
| 1615 | 0.03 | N | RW | 2.5' |
| 1616 | 0.14 | 555 W. DR 4 | 555PR | 2' |

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G. Lebel - Manager

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| Submitted by <u>Diepdaume Mi</u> | nes Limited, Tin | <u>mmins, Ontari</u> GOLD | 0 | | | |
| Submitted by <u>Diepdaume Mi</u> | nes Limited, Tin SAMPLE NO. | GOLD GZ./ton | 0 | | | |
| Submitted by <u>Diepdaume Mi</u> | nes Limited, Tin SAMPLE NO. 1617 | GOLD 0z./ton 0.09 | 552 | DR 1 | R.W . | ج ۲ |
| Submitted by <u>Diepdaume Mi</u> | nes Limited, Tin SAMPLE NO. 1617 1618 | GOLD GOLD Oz./ton 0.09 0.04 | 0 5 5 2 1 | DR / | R.W . | 5 ¹ . 61 |
| Submitted by <u>Diepdaume Mi</u> | nes Limited, Tin SAMPLE NO. 1617 1618 1619 | GOLD 0z./ton 0.09 0.04 0.12 | 0 552 552DR | DR / | R.W . . W | 5 1. 61 3 1 |
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G. Lebel - Manager



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SHERIDAN GEOPHYSICS LTD. DIEPDAUMEMINE PROJECT

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ASSAY REPORT

DATE ____ DEC 10, 1982_

| r | RESTON | EAST DOME | · | | | |
|---|---------------|---------------------|------------------------|--------------|-------|----------|
| | SAMPLE NO. | DESCRIPTION | Au Dente oz/ton. | | ej, | 51 70 |
| | 2401 | 500DR MAIN DR. WEST | 0.005 | ow | | |
| | 2402 | | 0.009 | s W | | |
| | 2403 | | 0.061 | 10 W | | |
| | 2404 | | 0.038 | 15W | | |
| | 2405 | | 0.007 | 35.00 | | |
| | 2.406 | | 0.157 | 40W | | |
| | 2407 | | 0.173 | 450 | | |
| | 2408 | | 0.045 | <u>20 m</u> | | |
| | 2409 | | 0.089 | <u>55 w</u> | | |
| | 2410 | | 0.070 | 6 <u>0 m</u> | | |
| | 2411 | | 0.011 | - 115 W_ | | |
| | 2412 | | 0.001 | 120 W | | |
| | 2413 | | NI | 125W | | |
| | 2414 | | NIL | 130 W | | |
| | 2415 | | 0.002 | 13.5 W | | |
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Assayer <u>Jurk</u>

SHERIDAN GEOPHYSICS LTD. DIEPDAUME MINE PROJECT

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ASSAY REPORT

DATE _ DEC 11, 12, 13/8.

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|-----|---------------|------------------|--|----------|---|--------------|
| | SAMPLE NO. | DESCRIPTION | Au <u> <u> v</u> <u>v</u> <u>v</u> <u>v</u> <u>v</u> <u>v</u> <u>v</u> <u>v</u> <u>v</u> </u> | | % | <i>\$</i> /0 |
| | 2416 | 500 DR M. DR. W. | NIL | 1400 | | |
| | 2417 | | NIL | 145W | | |
| | 2418 | | 0.005 | 150W | | |
| | 2419 | | 0.017 | 155 W | | |
| | 2020 | | NIL | 160 W | | |
| | 2421 | | 0.016 | 165 W | | |
| | 21122 | | NIL | 180 W | | |
| | 2422 | | NIL | 185W | | |
| | 211211 | | NIL | 190 W | | |
| | 2:125 | | NIL | 195W | | |
| | <u> </u> | | NII_ | 200 W | | |
| | 2427 | | NIL | 2.05 W | | |
| | 21170 | | NIL | 2100 | | |
| | 2429 | | NIL | 215W | | |
| | | | | | | |
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Jurk Assayer _

SHERIDAN GEOPHYSICS LTD. DIEPDAVHE MINE PROJECT

12

ASSAY REPORT

PRESTON EAST DONE

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DATE DEC. 16, 1982

| <u> 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1</u> | (| | | | | |
|---|---|---|--|--|--|--|
| | DESCRIPT | NOIN | AU MII oz/ton | | % | <i>i</i> jo |
| P.E.D. | 500 DR | M.DR.W. | NIL | 220 W | | |
| P.E.D. | | | NIL | 225 ~ | | |
| PED | | | 0.002 | 2300 | | |
| PED | | | 0.014 | 235W | | |
| PED | | | NIL | 2400 | | |
| PED | | | NIL | 24500 | | |
| PED | | | NIL | 2500 | | |
| PED | | | 0.019 | 255W | | |
| PED | | | NIL | 2600 | ····· | ····· |
| PED. | | | NIL | 265W | | |
| P.E.D. | | | NIL | 2700 | | |
| PED | | | NIL | 2.75 W | | |
| PED | | | 0.002 | 2800 | | |
| PED | | | NIL | 2850 | | |
| PED | | | HIL | 290 W | | |
| PED | | | NIL | 295W | | |
| P.E.D. | | | NIL | 300 W | | |
| PED | | | 0.005 | 305 W | | |
| | 1 | | | | | |
| | | | | | | |
| | P.E.D. P.E.D. | DESCRIPT <i>P.E.D.</i> 500 D/R <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> <i>P.E.D.</i> | DESCRIPTION P.E.D. 500 D/R M. D.R. W. P.E.D. P.E.D. P.E.D. P.E.D. P.E.D. P.E.D. | DESCRIPTION Au PE.D. 500 D/R M.D.R.W. NIL PE.D. 500 D/R M.D.R.W. NIL PE.D. 0.002 PE.D. 0.002 PE.D. 0.002 PE.D. 0.014 PE.D. 0.014 PE.D. NIL PE.D. 0.019 NIL PE.D. PE.D. NIL PE.D. NIL PE.D. NIL PE.D. NIL | Au DESCRIPTION Description PED SOODR M.D.R.W. PED NIL 225 w PED 0.002 230 w PED NIL 240 w PED NIL 245 w PED NIL 240 w PED NIL 240 w PED NIL 240 w PED NIL 275 w PED NIL 275 w PED NIL 285 w PED NIL 280 w PED NIL 280 w PED NIL 290 w PED NIL 30 | Au Au % PED_SORIPTION PED_OZ/ton % PED_SOODR_M.DR.W. NIL 220 w PED_D NIL 225 w PED_D 0.002 230 w PED_D 0.002 230 w PED_D 0.002 230 w PED_D 0.014 235 w PED_N NIL 245 w PED_N NIL 245 w PED_N NIL 245 w PED_N NIL 245 w PED_N 0.019 255 w PED_N NIL 246 w PED_N NIL 246 w PED_N NIL 210 w PED_N NIL 210 w PED_N NIL 235 w PED_N NIL 245 w PED_N NIL 246 w PED_N NIL 235 w PED_N NIL 245 w PED_N NIL 280 w PED_N < |

buch Assayer

SAMPLE RECORD

| • | | | SAMPLE REC(| DRD | | |
|------------------|---------------|---|-----------------------------|---------------|---------------------------------------|-------------------|
| | | | | | 13 | |
| NE EA | SAMPLE NO. | WORKING PLACE | SAMPLE LOCATION | VIDTH FEET | DESCRIPTION | GRADE AU/OZ/TO |
| nc. | 1301 | 558 x/c | | | | 0.02 |
| | 13(12 | " | | | | 0.003 |
| ** | 1303 | n | | | Broken muck | 0.02 |
| | 1304 | 11 | 558x c & 579 x/c fork | | 11 | 0.036 |
| 11 | 1305 | 579 x/c | 579 x/c & 5798 x/c fork | | 11 | 0.016 |
| n | 1306 | 558 x/c | 5)' from 210 | | 50% quartz & 50% pyrite, | 0.016 |
| | | | | | left wall. | |
| v p | 1207 | x (a cast | refer to 250 level assav pl | | Broken muck | 0.09 |
| <u>عما</u> ۱۱ | 1200 | <u></u> | 51 from face off 906 wall. | | Selective | 0.028 |
| | 1_1320 | | right wall. | | | |
| 81 | 1309 | r.c.south | Face, old 900. | 4' | Quartz. tourmaline vein. | 0, 724 |
| 1 1 | 1310 | x/c east | Breast. | 2' | Quartz, tourmaline, string- | 0.79 |
| | | | | | er network. | |
| | 1311 | x o east | Face. | 31 | 60 quartz & tourmaline | 0,008 |
| 11 | 1312 | x/c north | •••••• | | Broken muck | NII |
| 11 | 1313 | 224 s. dr. | South free old sub | 31 | Quente & tournaling malling | 0.079 |
| | 1010 | | South face, oru soo | <u>_</u> | durte contect | 0.052 |
| | 3714 | | | | into contact. | 0.030 |
| | 1514 | | Right west corner to south | 5.5' | 60% quartz, tourmaline & | 0.016 |
| ** | 1715 | 1 | Drift most contamba by OFC | 1 2 5 1 | Volcanics. | |
| | 1313 | | UTIL MOST EASTERLY DY 250 | 1.5. | Pyrite, graphite, talc & | 0.713 |
| | 1216 | | | 4 01 | BILBU. | 0.027 |
| | 1310 | 250 Winze XC | neitwall, lace, north, | 4.0 | auartz & tourmaline | 0.005 |
| | 1317 | 075 274 64 | Right will. | 4.7 | Bushan mush | 0.072 |
| ····· | 1010 | | Aight pile lace south. | | broken muck. | 0.032 |
| | 1319 | | Left pile face south. | | n | 0.946 |
| <u>n</u> | 1320 | 267_drift | Right wall, 267 drift & 268 | 7.01 | Quartz & tourmaline. | 0.095 |
| | | 074 | drift y. | | | |
| | 1321 | $\frac{274 \text{ x/c}}{274 \text{ x/c}}$ | On vein face. | 0.5" | Quartz & tourmaline. | 0.048 |
| | 1322 | 260 A drift | Drift face upper left. | <u> </u> | | 0. 148 |
| <u>n</u> | 1323 | x/c | By 25) winze. | | Chute. | 0.72 |
| | 1324 | 375, #6 west | Drift, face. | 6.01 | Quartz, stringer. | 0.06 |
| 11 | 1325 | 11 | Right wall by y, 375 #6 wes | <u>t.1.0'</u> | | 0.06 |
| 11 | | | 375 #1 x c. | _ | | <u> </u> |
| 11 | 1326 | 36) west dr. | #3 chute, | | Grab. | <u>0.978</u> |
| 11 | 1327 | <u>375 4 x/c</u> | #1_chute. | | 11 | 0.02 |
| H | 1328 | <u>375 west x/c</u> | #2 chute. | | N | <u> </u> |
| 11 | 1329 | 375 4 w. x/c | Drift, face. | | | Nil |
| <u>n</u> | 1330 | 360 East dr. | #1 chute. | | Grab. | 0.08 |
| 11 | 1331 | 375 <u>#5_south</u> | Drift face, old 675. | | | 111 |
| 11 | 1332 | 11 | Right wall, old 676. | | | 0.073 |
| N | 1333 | 375 #5 north | Right wall, old 6.00. | 2.01 | Stringers. | 0.006 |
| 11 | 1334 | 375 #4 east | #1 chute. | | Grab. | 0.034 |
| 11 | 1335 | 375 #4 west | Stope, raise, far west, | 3.01 | 0.2' quartz and tourmaline. | 0.072 |
| | | btope. | right wall. | | · · · · · · · · · · · · · · · · · · · | ļ |
| <u>,</u> | | | | | | |
| | 1 | 1 | 1 | | · · | |

SAMPLE RECORD

| | | | SAMPLE REC | ORD | 1 | |
|-----------|-------------------|---------------------|-----------------------------|----------------|---------------------------------------|------------------|
| | | | | | 14 | , |
| | SAMPLE NO. | WORKING PLACE | SAMPLE LOCATION | V IDTH FEET | DESCRIPTION | GRAI AU/02 |
| Į | 1336 | 375 #4 w. st | St. rse., far w., left wall | 2.01 | J.2' quartz and tourmaline. | 0.0 |
| ļ | 1337 | 11 | St. rse., far w., footwall. | | 11 | 0.] |
| ┦ | 1338 | 561 A drift. | Drift, face, old 610. | 2.01 | Quartz and pyrite. | Nil |
| + | 1339 | 375 #3 east | Drift, face, old 979. | " | | Nil |
| ╀ | 1340 | n | Right wall, 31' from face. | 1.01 | On vein. | Nil |
| + | 1341 | 11 | Left wall, 21' from face. | 1.51 | | Nil |
| 4 | 1342 | 375 #4 stope | Left wall above opc., l'fr. | | Stringers. | 0.0 |
| + | | | face. | | · · · · · · · · · · · · · · · · · · · | |
| + | 1343 | 375 #4 store | 4' from left wall, 4' from | 6" | Vein ft. w. | 0.7 |
| ╉ | | | face. | | | |
| ╉ | 1344 | 375-4 E.ST. | 10' from left wall, 3.0' | 6" | On vein. | 0.0 |
| + | | | from face. | | | |
| + | 1345 | 11 | 15' from left wall, face. | 2.51 | Stringers | 0.0 |
| ┥ | 1346 | 11 | 12' fr. 375 #4 east, 2.5' | 2.01 | Stringers on back. | 0.0 |
| ┫ | | | from 375, 5 north. | | | |
| ╉ | 1347 | 375-4 W. ST. | lst. chute west. | | Grab. | 0.0 |
| ╉ | 1348 | 260 drift. | #6_chute. | | Grab. | 0.1 |
| ┥ | 1349 | 260 drift. | #5 chute. | | Grab. | 0.7 |
| \dagger | 1350 \ | | #4 chute. | | 11 | 0.8 |
| 1 | 1351 | 11 | #3 chute. | | | 0.9 |
| 1 | 1353 | 11 | #1 chute | | | Ú.] |
| 1 | 1754 | 875 5 couth | | | | 0.5 |
| 1 | 1355 | Corner 202 | 1800. | 3.5 | Quartz, stringer lower left | 0.0 |
| | | x/c_{2} , 267 Dr. | 014 AIR, 5.0 11011 393 6 50 | <u> </u> | 0.5' quartz, tourm, string. | 0.3 |
| | 1356 | 267 dr. r.w. | 121 west of 3996 | | | |
| | 1357 | 11 | II | 1.5 | Quartz stringers. | 0.7 |
| | 1358 | 11 . | 15' west of 3996 | 3.01 | Quartz, tourmaline, 0.4 | 0.1 |
| | 1359 ₁ | 267 Dr., 1W. | | 2 51 | Wall make statement | 0.1 |
| | 1360 | 267 Dr. RW. | 18' west of 3996 | 1.51 | Querta and tournalder. | 0.0 |
| | 1361 | 267 & 204 Dr | Back 27' west of 3996 | 3 (11 | | 0.0 |
| | 1362 | 267 dr. R.W1 | 301 west of 3996 | 1.51 | St ní ngo ng | 0.1 |
| | 1363 | 11 | 351 west of 3996 | 2 1 | | 0.0 |
| _ | 1364 | 267 Dr. L.W1 | 28' west of 3996 | 1.01 | 0.2 Seminan analy | 0.19 |
| | 1365 | 11 | 301 west of 3996 | 2.01 | " | <u> 0.</u> 01 |
| | 1366 | 267 Dr. back | 31 west of 3996 | 3.01 | 2 perellel stringens and | 0.0 |
| | | | | 10.0 | smeller incide | 0.1 |
| | 1367 | 202 xc. back | 9' north of 3996 | 1.51 | Stringer 0.91 August- | |
| | 1368 | 202 xc. R.W1 | 11' north of 3996 | 3.51 | Stringers | 0.00 |
| | 1369 | 267 E.Dr.RWL | 23' east of 3996 | 2.01 | U.5 quartz, noesible contest | 0.3 |
| | 1370 | 555 Stope | 10' far left wall. ton st. | 2.51 | Vein & stringens for and | 0.00 |
| • | 1371 | 11 | 5' far left wäll. top stone | 2:61 | Vein. face ebet | 0.00 |
| | 1372 | 11 | A+) = (+ | | | 0.98 |

| SAMPLE NO. 1373 1374 1375 1376 1377 1378 1379 1380 1381 1382 1383 1384 1385 1384 1385 1386 1387 1388 1389 1390 1391 1392 1393 1394 1395 1394 | LE . | WORKING PLACE 267 Dr. RWL. | SAMPLE LOCATION | VIDTH FEET | DESCRIPTION | GRADE |
|--|---------------|----------------------------------|---------------------------|---------------|---|--------------|
| 1373 1374 1375 1376 1377 1378 1379 1380 1381 1382 1383 1384 1385 1384 1385 1386 1387 1388 1387 1388 1389 1390 1391 1392 1393 1394 1395 | | 267 Dr. RWL. | Face east onnosite 170 m | 1 | | AU/OZ |
| 1374 1375 1376 1377 1378 1379 1380 1381 1382 1383 1384 1385 1384 1385 1386 1387 1388 1389 1390 1391 1392 1393 1394 1395 | | 11 | TUTE CODAL ANNOTAC ALA LO | 0.81 | Quartz and visible gold. | 1.36 |
| 1375 1376 1377 1378 1379 1380 1381 1382 1383 1384 1385 1386 1387 1386 1387 1388 1389 1390 1391 1392 1393 1394 1395 | | 1 | | 5.01 | Stringer. | 0.00 |
| 1376 1377 1378 1379 1380 1381 1382 1383 1384 1385 1386 1387 1388 1387 1388 1389 1390 1391 1392 1393 1394 1395 | | 1 | | 1.31 | Qtz. and tourm., conj. 1374 | Nil |
| 1377 1378 1379 1380 1380 1381 1382 1383 1384 1385 1386 1387 1388 1387 1388 1389 1390 1391 1392 1393 1394 1395 | | 11 | | 3.01 | Quartz stringers. | <u>ು.</u> :: |
| 1378 1379 1380 1380 1381 1382 1383 1384 1385 1386 1387 1388 1387 1388 1389 1390 1391 1392 1393 1394 1395 | | 11 | | Hort. 1.51 | Tourm-stringer, .255 spec | 0.00 |
| 1379 1380 1381 1382 1383 1383 1384 1385 1386 1387 1388 1387 1388 1387 1388 1390 1391 1392 1393 1394 1395 | | 203W.xc.SW: | 73.5! west of station | 5. 21 | Volcanics, old 785 | 0.02 |
| 1380 1381 1382 1383 1384 1385 1386 1387 1388 1387 1388 1389 1390 1391 1392 1393 1394 1395 | | 11 | 68.51 " | 11 | " old 784 | 1.35 |
| 1381 1382 1382 1383 1384 1385 1386 1387 1388 1387 1388 1389 1390 1391 1392 1393 1394 1395 | 1 1 | 11 - | 1-63.51 · · · · · · | - 11/ . | • " • • • • • • • • • • • • • • • • • • | 0.16 |
| 1382 1383 1384 1385 1386 1387 1388 1389 1390 1391 1392 1393 1394 1395 | \rightarrow | n | 58.51 " | 11 | " old 782 | 0.02 |
| 1383 1384 1385 1386 1387 1388 1389 1390 1391 1392 1393 1394 1395 | -/ | 11 | 53.51 11 | <u> </u> | " old 781 | 0.06 |
| 1384 1385 1386 1387 1388 1389 1390 1391 1392 1393 1394 1395 | | 11 | 48.51 " | 11 | " old 780 | 0.33 |
| 1385 1386 1387 1388 1389 1390 1391 1392 1393 1394 1395 | | n | 43.51 " | | " old 867 | 0.00 |
| 1386 1387 1388 1389 1390 1391 1392 1393 1394 1395 | | 1 11 | 38.51 11 | 1 | " old 866 | Nil |
| 1387 1388 1389 1390 1391 1392 1393 1394 1395 | / | ¥! | 33.51 " | 11 | "old_865 | 0.00 |
| 1388 1390 1391 1392 1393 1394 1395 | ·/- | ł1 | 28.51 11 | 11 | " old 864 Onstr. 3/ | 4"0.0' |
| 1389 1390 1391 1392 1393 1394 1395 | | 11 | 23.51 11 | H | " old 939 | 0.00 |
| 1390 1391 1392 1393 1394 1395 | <u> </u> | | 11 19 | | "old 938 | н |
| 1391 1392 1393 1394 1395 | | 11 | | 11 | " old 937 | II |
| 1392 1393 1394 1395 | | | | | " old 936 | " |
| 1393 | | 21.5 | | | old 935 | 0.0 |
| | l <u></u> | 203xc. S.W. | 18.5' from station | | 11 | <u>ο. χ</u> |
| | | <u>n</u> | 13.5' " | | 11 | 0.38 |
| | | | 8,51 " | | 11 | 0.)] |
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SAMPLE RECORD

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| રું સ | SAMPLE NO. | WORKING PLACE | SAMPLE LOCATION | V IDTH FEET | DESCRIPTION | GRADE AU/OZ/TON |
|----------|---------------|---|---------------------------------------|----------------|----------------------|--------------------|
| 9 | 2001 | 375#1RSK | 375 / RSF. AT 200 Level | 5 | E. woll ALL Chioped | 0.01 |
|) | 02 | ١ | <u>\</u> | 5.2 | REE. PK. with bommen | NIL |
| 1 | 50 |) | · · · · · · · · · · · · · · · · · · · | 5' | Vern Fr.WL. | 0.01 |
| 1- | <u>04</u> | N | 200 Level 5 | 044 | Vein Fr. W. | 0.03 |
| 1 | 05 |) | | 4.6 | WL E. | TR |
| <u>\</u> | <u> </u> |) | - 10 | 0.8 | VELNINFAUL | 0.04 |
| 1 | 57 | ١ |) | 43 | HW. R. | 0.01 |
| <u>`</u> | | 1 | -15 | 16 | FW. Vein | 0.05 |
| 1 | 02 |) |) | 34 | HW.R. | 0.01 |
| 1 | <u> </u> | | -20 | 20 | FW. VEIN | 0.02 |
|) | |) | .) | 3.1 | HW.R. | TR |
| 1 | |) | -25 | 22 | FWVEIN | 0.02 |
| 1 | 13 |) |) | 28 | HWR | TR |
| - | × | <u> </u> | - 30 | 20 | FW ULIN | 0.09 |
| 1 | 15 |) |) | 2.2 | HWR | TR |
|) | 16 | 1 | -35 | 1.0 | VEIN FW | 0.03 |
|) | 17 |) | ١ | 4.8 | HW.R | 001 |
|) | 18 |) | -40 | 1.4 | FULVEIN | 0.10 |
| 7 | 19 |) |) | 3.1 | HWR | 0.01 |
| - | 20 |) | -45 | 2.0 | FW VRIN | 0.29 |
| <u> </u> | 21 | · · · · · · · · · · · · · · · · · · · | ١ | 129 | HWR . | 001 |
| _ | 22 |) | -50 | 20 | FWUEIN | 0.04 |
| - | 23 |) | 1 | 2.8 | HWR | TR |
| 4[| 24 |) | - 55 | 1.3 | FW | 0.01 |
| ÷ | 25 |) |) | 20 | VEIN | 0.02 |
| - | 26 |) |) | 1.5 | HW | NIL |
| ; | 27 | <u> </u> | - 60 | 1.7 | FW . | ALL S |
| - | <u> </u> | · · · · · · · · · · · · · · · · · · · |) | 1.0 | VEIN | 0.18 |
| | 29 |) |) | 120 | HW et | TR |
| | 30 | 2360 ST | 36057 RK. SE OF 375 RS. | 1.5 | FW | 001 |
| _ | 31 | · · · · | <u>\</u> | 1.0 | VEIN | 0.10 |
| | 32 | · |) | 1.5' | HW | 0.01 |
| - | | · · · · · · · · · · · · · · · · · · · |) BK ID'E REE | 1.5 | FW | NIL |
| - | 34 | · · · · · · · · · · · · · · · · · · · |) | 10 | NEIN | 0.10 |
| - | 35 | · · | <u>ا</u> | 20 | HW | 0.01 |
| | 3.4 | <u>, </u> | AN 15'ERGE | 10 | T.W. | 001 |
| - | 3- | 1) | N | 10 | JENS | 0.0.4 |
| - | 3 1 | 3 > |) | 1.5 | - In W | TR |
| _ | 3 | 2 1 | BK 20E REE | 1.1 | FW . | NIL |
| - | 7 | <u> </u> | 1 | 10 | VEIN | 0.04 |
| - | 4 | 1 |) | 10 | kw | TR |
| - | 43 | 1 | BK25'ERSE | 10 | FW | 7.9 |
| - | | 1 |) | 08 | VIEIN | 0.04 |
| - | 4 | 7 . |) | 20 | | TR |
| | | <u> </u> | 31- 30'ERLE | 12 | FW | 0.01 |
| | | | | | | |

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| 2) -R | SAMPLE NO. | WORKING PLACE | SAMPLE LOCATION | VIDTH FEET | DESCRIPTION | GRADE AU/OZ/TON |
|---------------|---------------|---------------------------------------|--|---------------|--------------------|--------------------|
| 49 | 2046 | 36057 | BIS 30'E REE 375P1 | 1.5 | VEIN | 0.02 |
| | <u> </u> | 1 |) | 20 | HW | 0.67 |
| ; | 48 | ١ | BK35' NNN | 0.5 | FW | 0.03 |
| | 40 | 1 | ١ | 13 | VEIN | 0.13 |
| \downarrow | 50 | ١ |) | 27 | HW | 006 |
| | 51 | ١ | BK YO'ERE | 10 | FW | 0.02 |
| | |) | ١ | 2.1 | VEIN | 0 03 |
| | 53 |) |) | 10 | Hu | 0.01 |
| P | 2057 | 36057 | BK 45'E. OF 3757 REC | 32 | VEIN (VG) | 0.10 |
| | 55 | | BK 50 1 1 | 20 | FW VER (VG) | 0.02 |
| 1 | 36 | | | 1.6 | HW VEIN | 002 |
| | 57 | | BK55 11 | 2.3 | FW | 002 |
| 1 | 58 | | 1 1 1 | 0.8 | VEIN | 0.14 |
| - | 59 | ξ | | 08 | HW | 0.01 |
| | 60 | | 3/260 11 | 1.5 | FW | 0.01 |
| | 61 | | | 0.9 | VEIN | 014 |
| | 62 | | | 1.5 | HW | 0.01 |
| ••••• | · 65 | | 131×65 | 1.2 | FW | 0.01 |
| | <u> </u> | | | 0.5 | VEIN | 0.25 |
| | <u> </u> | | | 2.3 | HW | 001 |
| | <u> </u> | | | 08 | Vein | 0.20 |
| | | · · · · · · · · · · · · · · · · · · · | M. L. Q. E'r m | 30 | r/w | 0.01. |
| | | | MUCH ME DE Muy | | BRAB III VUR DI 12 | 0.29 |
| | 70 | |) M Equip | | <u> </u> | +1.17 |
| | 7/ | | 1 1 1 1 1 | | · · · · | 0.04 |
| | 72 |) | FAC 15 70' FAST P | <u> </u> | | 003 |
| - | 73 | | $\frac{1}{\sqrt{2}} \frac{1}{\sqrt{2}} \frac{1}{\sqrt{2}$ | 00 | FW | NIL |
| + | 74 | | 1 1 1 | 2 2 | Nui | 0.05 |
| _ | 75 | | 1 1-10'FR 1215 | | 1/12/04 | 1012 |
| | 76 | | | 25 | 17 4 | 004 |
| ii | | | <u>) 15'))</u> | | Ven | 001 |
| | 78 | | | 25 | It up | 006 |
| | 79 | · | 375 ST W.F. BROW | 10 | T.W. | 1/18 |
| 1 | 30 | | | | Vision | |
| 1 | 81 | | · · · · · · · · · · · · · · · · · · · | 15 | HW | |
| L | 82 | | FACE BAS | 0.5 | FW | |
| | 83 | | | P.0 | VEINI | 0.003 |
| | 34 | ¥ | | 2.0 | 14 MI | <u> </u> |
| . | 55 | - | WENTFACE | 5.0' | P.K.STR. | I DIL |
| 1 | 86 | | BROW 51 L. DACK | 3.6 | TR. | D Lung |
| + | 37 | | ID'E FRES | 3.5 | BIX .STR. | (n. 12.2 |
| L | 28 | 5 | RSE P.R. BK. IS'EFRO | 3.5 | S7R | 0.000 |
| [| 51 | | BR+5 W WALLRE | 06 | FW. STN | N/ND |
| (| 90 |) | BR+5 | 0.8 | VEIN | |
| _ | 1 | 1 | | | | 1 |

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|--------|--------------------------|-------------------|---------------------------------------|---------------|--|--------------------|
| | 2091 | | BR+5 | 3.3 | HULSTR | 0.002 |
| | 1 72 | | BR+5 | 0.8 | FW. STR. | 0.285 |
| | 93 | | BRTID | 1.5 | UEIN | 0.054 |
| | $\mathcal{F}\mathcal{P}$ | | BRTIC | 28 | H.W. STR | 0.007 |
| | 95 | | REF FACE BRIS | 25 | \$ 76 | 0.050 |
| | 95 | | $\lambda \lambda \beta R + 15$ | 2.5 | . 7n | 0.020 |
| | .97 | | EASTBR | 10 | IF W | 0.007 |
| | 1 25 | | T. RSIE RR | 00 | MEIN | 0.354 |
| | 99 | , . | | 2 5 | 17121 STR | |
| | | | | | | 0.007 |
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| 5) - 1 | SAMPLE NO. | WORKING PLACE | SAMPLE LOCATION | VIDTH FEET | DESCRIPTION | GRADE AU/OZ/TON |
| ſP | 1401 | 275 drift | 0+0) raise, brow. | | Quartz, tourmaline, muck. | Nil |
| 'I | 1402 | 11 | 6' north. | | II | 0.021 |
| " | 1403 | 11 | 13' north. | | 11 | 0.004 |
| It | 1404 | 275A drift | Center line of track, 48' | | 11 | 0.056 |
| | | | to face, U+UD start. | | | |
| 11 | 1405 | 11 | 10' west. | | 11 | 0.212 |
| 11 | 1406 | n | 221 west. | | Brown orogg styin abundant | NHI |
| | | | | | pyrite and quartz, 12" brown | |
| H | 1407 | 274 Dr. S. W | 58.51 from 5669 station, 71 | 3.21 | | 0.056 |
| | | | south center line of track | | | 0.000 |
| " | 1408 | 274 Dr. N. W | 158.51 from 5669 station, at | 2.51 | | 2.050 |
| | | | face. | ~ | | |
| " | 1409 | 268 raise | Below raise. | | Muck | 0.047 |
| | 1410 | 268 drift | 22.91 - 4711 for 5848 | ,, | Muck | 0.060 |
| | | | 22 (il in | | Muck. | 0.009 |
| " | 1411 | 260 A drift | 87' from 4014, stone 9' W1 | 0.01 | | |
| 11 | 1412 | 11 | 11 | 2.0. | Quartz, tourmaline vein, SW | |
| | 1413 | н | 14' west | 4.0 | Hanging wall porp., S.W. | 0.004 |
| 11 | 1414 | 11 | 11 | 7.61 | Quartz, tourmaline vein, SW. | 0.473 |
| ·1 | 1415 | 11 | 191 yest | 3.0 | hanging wall porp., S.W. | 0.008 |
| 1 | 1416 | 11 | 11 HO WESU. | 1.21 | Quartz, tourmaline vein, SW. | 2.90 |
| 1 | 1417 | 11 | 241 west | 5 01 | nanging wall porp., S.West | 0.721 |
| , | 1418 | . ti | 21 61 west to 241 west | 5.9 | | 0.021 |
| | | | £1.0 west to 24. west. | 2.4 H | rt. Special qtz. tourm. str. | 0,030 |
| 1 | 1419 | 11 | 291 upot | | south west. | |
| 1 | 1420 | 11 | 291 yest | 0.91 | Quartz, tourmaline vein, SW. | 0.014 |
| , | 1491 1 | el | 241 | 4.5 | Hanging wall porp. south w. | 0.004 |
| | 11492 | | 54' West. | 5.71 | | 0.021 |
| | 1423 | | Ja west. | 5.01 | I <u> </u> | 0.013 |
| 1 | n 424 | | 144 [•] West, | 0.51 | Quartz, tourmaline vein, SW. | Nil |
| , | 1 4 2 5 | · · · · · · · · · · · · · · · · · · · | 44' west. | 3.51 | Hanging wall porp., south w. | 0.706 |
| | 1460 | | 49' west. | 2.51 | Quartz, tourmaline, south w. | Nil |
| , | 1426 | n | 49' west. | 2.51 | Hanging wall porp., south w. | 0.039 |
| · | 1421 | | 54' west. | 2.81 | Quartz, tourmaline, south w. | Nil |
| | 1428 | 11 | 54' west. | 3.51 | Hanging wall porp., south w | 0.004 |
| - | 1429 | 1 | 59' west. | | | |
| | 1430 | 11 | 59' west. | | | |
| | 1431 | 11 | 64' west. | 2.)1 | Quartz, tourmaline, south w | 0.119 |
| | 1432 | 11 | 64' west. | 4.11 | Hanging wall porp., south w | 0.008 |
| | 1433 | | 69' west. | 1.01 | Quartz vein. south west. | 0.162 |
| | 1434 | 11 | 69' west. | 3.01 | Hanging wall porp., south w | 0.053 |
| | 1435 | | 74' west. | 1.61 | Quartz vein, south west. | 5.27 |
| | 1436 | 11 | 74' west. | 3.51 | Hanging wall porp., south w | 0.056 |
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DIEPDAUME MINES LIMITED GEOLOGICAL PLAN AREA SOUTHEAST OF SIMPSON LAKE

TISDALE TOWNSHIP PORCUPINE MINING DIVISION ONTARIO 007.31,1982. SCALE: //NCH=20FEET

Mapped and Drown By: C.F. DESSON, P.ENG.

63.4209 FIGURE 14.

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| Flooded 777 | SGE | |
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| Erren (flooded) | | |
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| 540242 | | · · · · |
| DIFPDALIME MINES LIMI | | |
| GEOLOGICAL PLAN H.E.M. CONDUCTOR ARE DELORO TOWNSHIP PORCUPINE MINING DIVISION ONTARIO SCALE: INCH = 200 FEET NOV.I Bedding or schust Navped and Brown By: C.F. DESSON, P.ENG | 2, 1982. | |
| LEGEND Swamp QP Quartz Forphyry CSS Chlorite Creek and flow direct IF Iron Formation CSSCB Chlorite: | sericite schist carbonatized | |
| - Claim lineani post T Tuff VCb Volconic 43 Claim number XT Crystal Tuff | Flow, Carbonatized 63.4209 FIGURE 15 | |