



42A07NW2012 2.18926 SHERATON 010

**GEOPHYSICS REPORT**

**ON THE**

**SHERATON-THOMAS TOWNSHIP**

**PROPERTY**

**FOR**

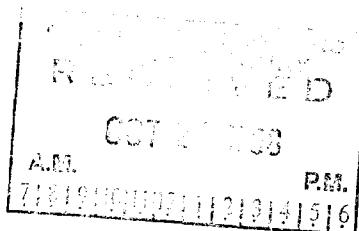
**MAPLE MINERALS INC.**

**TIMMINS AREA**

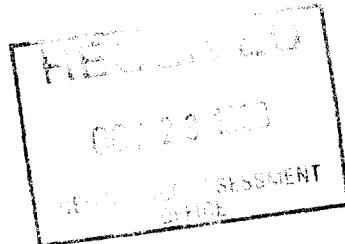
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**PORCUPINE MINING DIVISION**

**ONTARIO, CANADA**



Dan Patrie  
Dan Patrie Exploration Ltd.  
June 10, 1998



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## 1. **INTRODUCTION**

In December, 1997, Maple Minerals Inc., of Toronto, Ontario., commissioned Dan Patrie Exploration Ltd to do an exploration program on their property of 9 un-patented mining claims (120 units) situated in Thomas and Sheraton Townships, approximately 40 kilometers east of Timmins. The work was done from December 12, 1997 to February 28, 1998

## 2. **SUMMARY AND RECOMMENDATIONS**

The Maple property, acquired by Maple Minerals Inc., lies in south central Thomas Township, and the west side of Sheraton Township in Porcupine Mining Division. Thomas and Sheraton Townships lie approximately 40 km east of Timmins.

These claims are underlain by volcanic and sedimentary rocks of the Archean Abitibi subprovince of the Superior Province of the Canadian Shield. Earlier work has been primarily focused on gold, but not intensively. Thick, widespread cover of overburden has made cost effective exploration difficult in the past, so the Townships were poorly explored.

Cross Lake Minerals Ltd., recently discovered a polymetallic volcanic massive sulphide (VMS) deposit, east southeast of Timmins in Sheraton Township, in felsic volcanic rocks, has focused attention on the basemetal potential of the area. Of the Cross Lake Minerals Ltd., basemetal discovery, hole 16 intersected weighted average grades of 6.7% zinc, 1.86% lead, 0.16% copper, 106.95 g/tonne silver, 0.055 g/tonne gold over a core length of 33 meters.

This deposit was found using induced polarization surveys and diamond drilling, the methods of choice in basemetal deposit exploration.

Past airborne and ground magnetic surveys, VLF-EM, HLEM and induced polarization surveys have yielded inconclusive results about bedrock geology on the property. Prominent

pyroclastic rocks in the bedrock of Sheraton and Thomas Townships was also found.

A program of 84 Kilometers of line cutting, 84 kilometers of Magnetic, and 39.8 kilometers of induced polarization was done to explore the Maple Minerals Inc., property in Thomas and Sheraton townships for base metals and gold deposits.

Due to the lack of geological information, the following programs are recommended to complete the evaluation:

1. Completion of grid lines spaced at 100 meters over all of the claim group.
2. Magnetometer, HLEM and induced polarization on remaining lines.
3. Geochemical soil sampling of the property.
4. Diamond drilling anomalies as follows is recommended:

| Line | Station | Azimuth | Dip | Depth |
|------|---------|---------|-----|-------|
| 109E | 1450S   | 330     | -60 | 275M  |
| 109E | 1350s   | 330     | -50 | 400M  |
| 106E | 1950S   | 330     | -55 | 350M  |
| 104E | 400N    | 330     | -50 | 400M  |
| 104E | 775N    | 330     | -50 | 300M  |
| 102E | 550N    | 330     | -50 | 400M  |
| 102E | 175N    | 330     | -50 | 275M  |
| 105E | 1575S   | 330     | -55 | 400M  |
| 111E | 1110S   | 330     | -55 | 325M  |

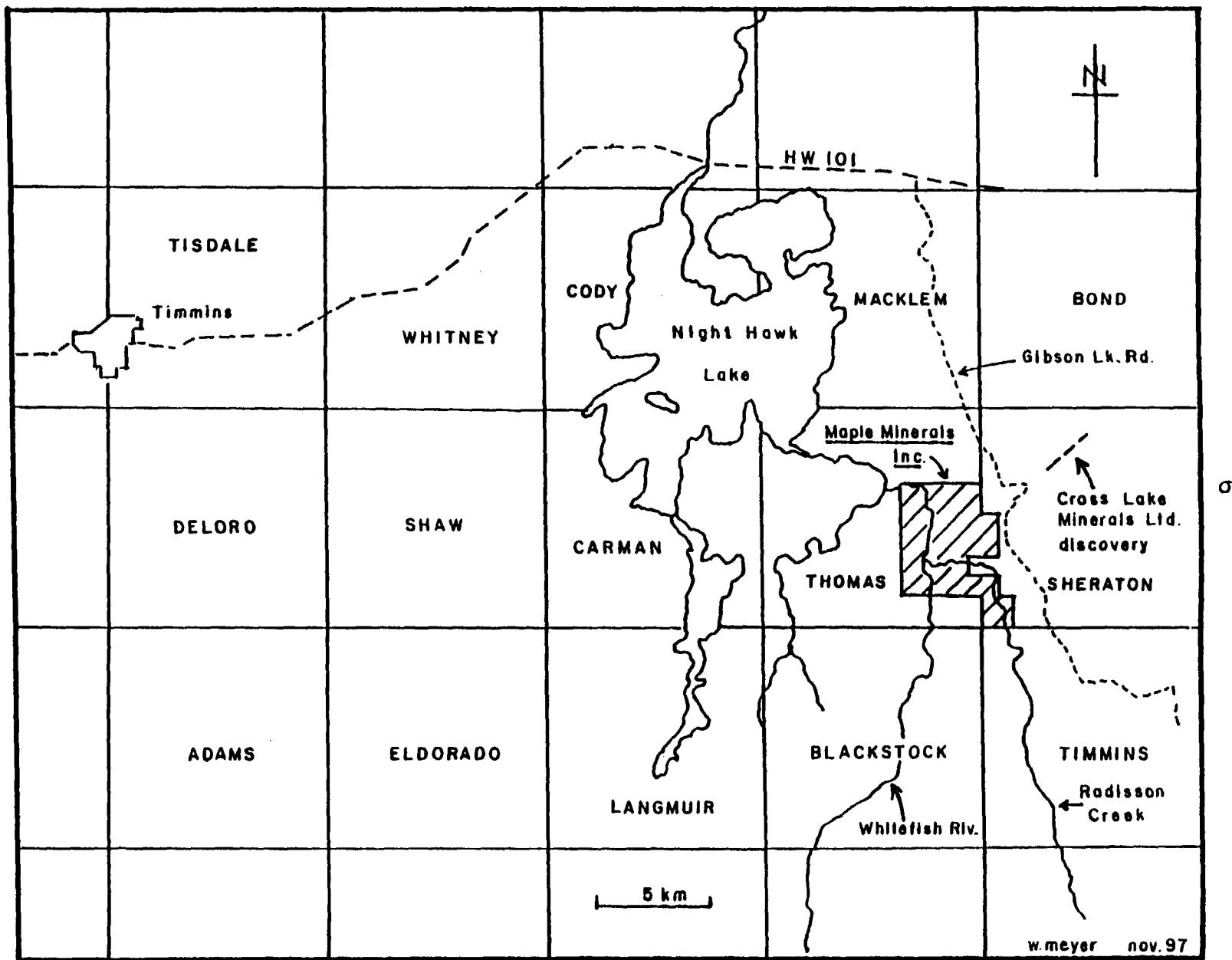
Following the completion of this work and contingent upon the results, additional work could be considered to further evaluate the property for gold and base metal mineralization.

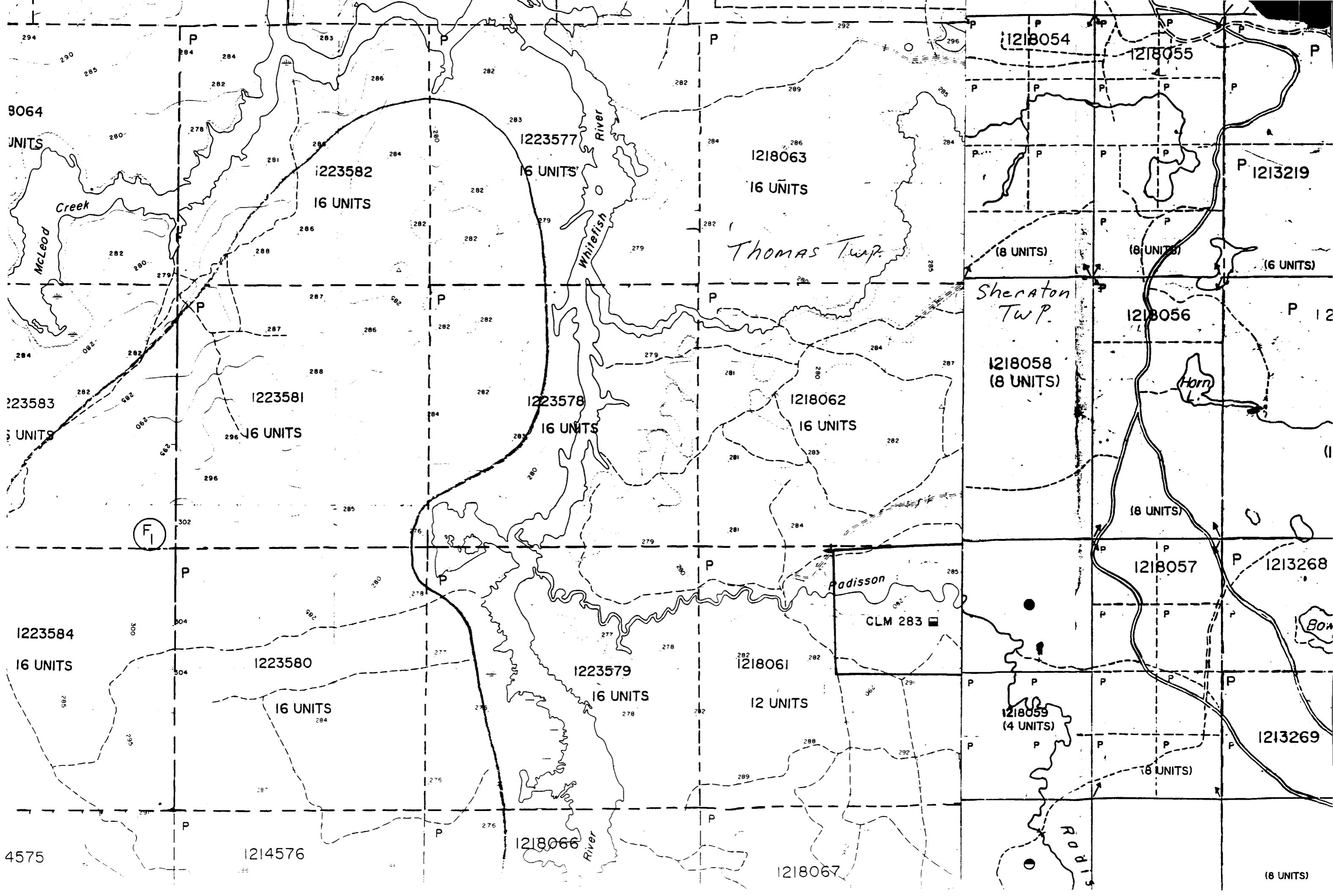
Daniel F. Patrie

Geology and Geophysics Technologist (Dipl.T)

June, 1998

**Figure 1.** The Maple Minerals Inc. property in Sheraton and Thomas Townships, 40 km east of Timmins, Ontario. Scale 1:253,440





3. **PROPERTY, LOCATION, AND ACCESS**

Timmins, a modern community of approximately 45,000 people, is the center for an area of active gold and basemetal mining and exploration. It includes all the amenities to discover and develop new mines, ie.; necessary infrastructure, material supplies and a stable professional work force. The city is located 700 kms north of Toronto in the heart of the Canadian Shield. Timmins is accessible by road, freight rail, and air from several directions, and is considered a service and supply center for the vast areas to the north.

Milling, concentrator and smelting capacity within a few kilometers from Timmins, are available through the Kidd Creek basemetal mine and several other large, long lived gold mines surrounding the area.

The property can be reached by traveling east from Timmins for 38 km on highway 101, then south on the gravel, Gibson Lake road for 20 km. The Gibson Lake road comes within a few hundred meters of the eastern boundary of the property. Numerous logging roads branch off the Gibson Lake road and crisscross the property. Also, by traveling by boat from Night Hawk Lake up Whitefish River, and along several tributary creeks.

The property is accessible by upgrading old logging roads, running from the Gibson Lake road South and west traveling into Thomas and Sheraton Townships.

The Maple property lies in an area of subdued relief, with elevations varying between approximately 276 and 292 meters above sea level (a difference of only 16 meters).

Located in the boreal forest, the property hosts stands of evergreen and deciduous trees and large animals such as moose, deer and bear. Seasonally, migratory birds and waterfowl use the marshes on either side of Whitefish River and the lower reaches of tributary creeks.

#### 4. GEOLOGY

The claims acquired by Maple Minerals Inc., in Thomas and Sheraton Townships, lie in a regionally mineral belt of Archean Age and in the Porcupine mining camp of northeastern Ontario, only 40 kilometers west of Timmins and its many mines. The Porcupine camp is one of the most productive mining camps in the world. It contains quartz vein-hosted gold deposits ultramafic intrusive hosted nickel-copper deposits and VMS-type nickel and zinc-lead-copper-silver-gold deposits. The property is in an important geological environment for hosting VMS-type nickel and ultramafic volcanic (komatiite) hosted nickel deposits. A VMS-type zinc-lead-copper-silver-gold zone is presently being outlined by Cross Lake Minerals in felsic rocks which adjoins the Maple Minerals Inc property to the west. About 50 to 60 meters of overburden cover the bedrock. The strike of the zone and enclosing felsic pyroclastic rock is southwest, with the zone dipping about 80 degrees to the southeast.

Minerals encountered in the drilling were pyrite, sphalerite, galena, chalcopyrite, silver and fluorite. Chalcopyrite occur with chlorite alteration and sphalerite and galena with sericite.

The high galena to chalcopyrite content for parts of the mineralized zone is unusual for this type of deposit, but is known from the Sudbury basin.

Leahy (1971) inferred that the bedrock in Thomas Township consists mostly of mafic flows intruded by a few diabase dykes and granitic rocks. The township is covered by 99% overburden. Of the little outcrops in thomas township the outcrops are carbonatized volcanic rocks with anomalous concentrations of gold which suggests that elevated gold values occur over a large area in Thomas Township and is good potential for a gold discovery in the area.

The world over, Archean greenstone belts have produced approximately 22 00 tonnes of gold and approximately 45 00 tonnes produced by Witswatersand. An estimated 135 000 tonnes total, of gold, has been mined throughout history, from all sources (Phillips and Law, 1997). This means that one half of all gold ever mined has come from the Archean age rocks, their potential as established gold producers cannot be overestimated.

VMS, or volcanic massive sulphide, deposits of copper, zinc, (gold, lead), are found near the top of volcanic piles in greenstone belts in felsic pyroclastic rocks. Common to the Canadian Shield. The property contains EM conductors, some of which have associated magnetic anomalies and induced polarization anomalies suggesting to be conformable to the bedding/foliation of the underlying bedrock, and may contain sulphide mineralization. The Maple Minerals Inc., property has very good potential for containing economic base and/or precious metals mineralization.

## 5 SURVEY PROCEDURE

### 5.1 MAGNETOMETER SURVEY

The magnetometer survey was carried out using an EDA Omni-Plus Mag/VLF unit with the total magnetic field being measured and an Omni-IV base station magnetometer for correcting magnetic drift. These are total field magnetometers which measure the magnetic field through the use of proton precessional effects caused by the interaction of a magnetic field with spin aligned, proton-rich fluid. An instrument accuracy, precision and resolution of 0.1 nt may be obtained with these instruments under ideal conditions. Microprocessors contained in these instruments allow for the collection of the readings, along with the time and its position, in

digital form suitable for downloading to a computer for data processing.

A total of 84 kilometers of mag was read and the readings were taken every 25 meters along the lines. The field measurements were corrected for diurnal variations of the earth's magnetic field by direct subtraction of the base station reading from the field readings taken at that same moment in time. The corrected magnetic data was then downloaded to a computer then plotted on the total field plot map. The magnetic survey picked up a high mag anomaly at the north ends of the lines running in an east west direction although with the lines spaced at 200 meters it is hard to get a good magnetic description of the magnetic contours.

## **5.2 INDUCED POLARIZATION SURVEY**

A total of 39.8 kilometers of induced polarization survey was done on the property with readings taken every 50 meters and 6 levels 1 to 6 read. The survey was a time domain pole dipole survey with a "a" spacing of 50 meters and was read with a Walcer MG-12 motor generator and a Huntex Tx Model 7500 transmitter and a Scintrex IPR-12 receiver. The motor generator and transmitter were stationary on the end of the line being read and current transmitted through a wire with an electrode driven down through the ground for a good contact and then transmitting current to that electrode from the transmitter by the transmitter man which is contact by radio to the receiver man. Ahead of the live current electrode is a crew of men driving electrodes in winter and using porous pots in summer at every station to be read and connected to the pots or electrode by length of wire from the receiver where the receiver operator picks up the readings in the receiver with the IPR-12. The data is then downloaded from the receiver at the end of the day to a computer where the resistivity and chargeability is calculated and plotted using Geosoft software for the earth sciences in pseudosection maps.

## 6. INTERPRETATION

The magnetic survey detected strong magnetic anomalies from line 102E to line 66E running east west across the north end of the lines which should be extended and a north south anomaly centered at line 94E. With the lines spaced 200 meters apart it is very hard to get a proper description of the magnetic contours.

The induced polarization survey picked up anomalous zones on line to the north running from line 100E to line 108E centered at approximately 700N.

Also, a high chargeability on lines 105E to line 111E at approximately 1000S to 1400S and running off the ends of the lines to the south on line 105E to 108E.

The induced polarization survey proved very successful in finding areas of high chargeability which merit more exploration such as drilling these high priority targets.

Most of the induced polarization anomalies were very strong, wide and long and deep which are identical to the Cross Lake Discovery induced polarization survey.

Also, most of the anomalies were on all six levels n=1 to 6.

The chargeability values for the anomalies are well above background and are consistent with metallic mineralization. The bulk resistivity values also, correspond to a mineralized target.

Background values between 2mV/V and 5mV/V are caused by electrolytic polarization as opposed to the combination of electrolytic and electrode polarization in the case of metallic mineralization. The resistivity plots show bulk resistivity corresponding to bedrock values. Also, for a better observation of data interpretation see maps in back of report.

7. **CONCLUSIONS**

With the presence of a favorable geological environment and the recent discovery of a polymetallic massive sulphide (VMS) deposit nearby by Cross Lake Minerals Limited in felsic volcanic rocks lends credence to the potential of the property hosting either a VMS or gold deposit. This considered, shows the Maple Minerals Inc., property to be very favorable geological environment for the localization of economic importance. To further evaluate the property's potential, with the encouraging results of the geophysics survey the writer recommends on going work consisting of line cutting and geophysical surveys over the balance of the property not covered and drilling the known targets outlined in this report.

Dan Patrie

June, 1998

## REFERENCES

- Atkinson, B. (1988): Ontario Geological Survey Resident Geologists Office, Timmins: Personal communications
- Burrows, A.G. (1911): The Porcupine gold area; Ont. Bureau Mines, Vol.20, pt. 2, 39 p
- Cross Lake Mines Ltd. (1997); news releases
- Dunbar, W.R. (1948) Structural Relations of the Porcupine Ore Deposits; in Structural Geology of Canadian Ore Deposits, C.I.M. Symposium, p. 442-456
- Bain, D. (1998). Economic Potential For Zn, Pb, Cu, Au and NI-CU Mineralization, Carman Property, Cochrane Mining District, N.E. Ontario
- Fyon, J.A., and Crockett, J.H. (1983): Gold Exploration in the Timmins Area Using Field and Lithogeochemical Characteristics of Carbonate Alteration Zones; Ontario Geological Survey Study 26
- Ginn, R.M., Savage, W.S., Thomson, R., Thomas, J.E., and Fenwick, K.G. (1964): Timmins-Kirkland Lake Sheet, Cochrane, Sudbury and Temiskaming Districts; Ont. Dept. Mines, Geol. Compilation Series, Map 2046, scale 1" =4 miles
- Hopkins, P.E. (1924) Night Hawk Lake gold area; Ont. Dept. Mines, Vol. 33, pt. 3, p. 27-36
- Kay, G.F. (1904): The Abitibi Region; Ont. Bureau Mines, Vol. 13 pt.1, p. 104-121
- Kindle, E.D. (1936) Gold Occurrences of Ontario East of Lake Superior; Geol. Survey Canada, Memoir 192, 162 p.
- Leahy, E.J. (1971): Geology of the Night Hawk Lake Area, District of Cochrane; Ontario Geological Survey Geol. Rpt. 96
- Miller, W.G. (1907): Lake Abitibi gold deposits; Ont. Bureau Mines, Vol. 16, pt. 1, p. 219-220
- Ontario Geological Survey (1973): Precambrian Geology, Timmins-Kirkland Lake; Ont. Dept. Mines Map 2205, Compilation Series, 1"=4 miles
- Pyke, D.R. (1970): Geology of Langmuir and Blackstone Townships; Ontario Dept. Mines Geol. Rpt. 86

**PERSONNEL**

Dan Patrie  
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POP 1P0

Charles Laundriault  
General Delivery  
Walford, Ontario  
POP2E0

Bruce McLeod  
Elliot Lake, Ontario

Tim Kelly  
General Delivery  
Spanish, Ontario

Micheal Burns  
General Delivery  
Massey, Ontario

Brent Patrie  
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POP 1P0

Julien Richer  
General Delivery  
Massey, Ontario  
POP 1P0

Henry Grimmerd  
Spanish, Ontario

Ron Bilton  
Massey, Ontario

Christopher Rivers  
General Delivery  
Walford, Ontario  
POP 2E0

## **CERTIFICATE OF QUALIFICATION**

I, Daniel Patrie do hereby certify:

1. That I am a Geology and Geophysics Technologist and I reside at Hwy. 17 West, P.O. Box 45, Massey, Ont., Canada, P0P 1P0,
2. I graduated from Cambrian College Of Applied Arts and Technology, Sudbury, Ontario, in 1987 with a diploma in Geological Technology with a one year certificate in Geophysics,
3. And I have practiced my profession continuously since graduation, as well as being an active prospector since 1972.
4. That my report on the Maple Minerals Property, Thomas and Sheraton Townships, Porcupine Mining Division, Ontario, is based on my personal knowledge of the geology of the area, and on a review of published and unpublished information on the property and surrounding area.

Daniel F. Patrie

Geology and Geophysics Technologist (Dipl. T)

June, 1998

**LETTER OF CONSENT**

I, Daniel F. Patrie, of the Town of Massey, Ontario, do hereby consent to Maple Minerals Inc., using in whole or in part my Geophysics report on the Maple Minerals Property in a prospectus or statement of material facts or for filing with government regulatory bodies as deemed necessary.

Dated at Massey, Ontario, this 22nd day of June, 1998, in the District of Sudbury.

**Daniel F. Patrie**

**Geology and Geophysics Technologist**



**Declaration of Assessment Work  
Performed on Mining Land**

Mining Act, Subsection 65(2) and 66(3), R.S.O. 1990

Transaction Number (office use)

129816 00819  
Assessment File Research Imaging



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ority of subsections 65(2) and 66(3) of the Mining Act. Under section 8 of the  
ed to review the assessment work and correspond with the mining land holder.  
ining Recorder, Ministry of Northern Development and Mines, 8th Floor,

PROVINCIAL RECORDING  
OFFICE - SUDBURY  
RECEIVED

OCT 26 1998  
6 A.M.  
10:40 AM  
7 8 9 10 11 12 1 2 3 4 5 6  
P.M.

**Instructions:** - For work performed on Crown Lands before recording a claim, use form 0240  
- Please type or print in ink.

**1. Recorded holder(s) (Attach a list if necessary)**

|  |                  |
|--|------------------|
| Name   | Client Number    |
| Maple Minerals INC.  | 137052           |
| Address  | Telephone Number |
| 2 First Canadian Place, The Exchange Tower<br>Suite 2810, P.O. Box 47, Toronto, Ont. M5K 1E9 | 416 941-8900     |
| Name   | Fax Number       |
|  | 416 941-9901     |
| Address  | Client Number    |
|  | Telephone Number |
|  | Fax Number       |

**2. Type of work performed: Check (✓) and report on only ONE of the following groups for this declaration.**

Geotechnical: prospecting, surveys, assays and work under section 18 (regs)       Physical: drilling, stripping, trenching and associated assays       Rehabilitation

|   |  |
|---|--|
| Work Type   | Office Use                               |
| Line Cutting, Mag & Induced Polarization  | Commodity                                |
|   | Total \$ Value of Work Claimed \$ 98,718 |
| Dates Work Performed From 12 Day   12 Month   97 Year To 28 Day   2 Month   98 Year | NTS Reference                            |
| Global Positioning System Data (if available)                                       | Mining Division Porcupine                |
|   | Resident Geologist District Timmins      |
| Township/Area Thomas & Sheraton   |  |
| M or G-Plan Number  |  |

Please remember to: - obtain a work permit from the Ministry of Natural Resources as required;

- provide proper notice to surface rights holders before starting work;
- complete and attach a Statement of Costs, form 0212;
- provide a map showing contiguous mining lands that are linked for assigning work;
- include two copies of your technical report.

**3. Person or companies who prepared the technical report (Attach a list if necessary)**

|                              |                                    |
|------------------------------|------------------------------------|
| Name                         | Telephone Number                   |
| Dan Patric Exploration Ltd   | 705 844-2113                       |
| Address                      | Fax Number                         |
| Box 45, Massey, Ont. P0P 1P0 | 705 844-2057                       |
| Name                         | Telephone Number                   |
|                              | Fax Number                         |
| Address                      | RECEIVED OCT 23 1998<br>ASSESSMENT |
| Name                         | Telephone Number                   |
| Address                      | Fax Number                         |

**4. Certification by Recorded Holder or Agent**

I, Daniel F. Patric, do hereby certify that I have personal knowledge of the facts set forth in this Declaration of Assessment Work having caused the work to be performed or witnessed the same during or after its completion and, to the best of my knowledge, the annexed report is true.

Signature of Recorded Holder or Agent

Deemed Deemed

Date

Oct 20/98

Agent's Address

Box 45 Massey P.O. Box 1001

Telephone Number

705 844-2113

Fax Number

705 844-2057

the mining land where work was performed, at the time work was performed. A map showing the contours and  
mining claims that are adjacent to claims that are eligible for assignment to contiguous claims must accompany this form.

W9860.00819.

| Mining Claim Number. Or if work was done on other eligible mining land, show in this column the location number indicated on the claim map. | Number of Claim Units. For other mining land, list hectares. | Value of work performed on this claim or other mining land. | Value of work applied to this claim. | Value of work assigned to other mining claims. | Bank. Value of work to be distributed at a future date. |
|---|--|---|--------------------------------------|--|---|
| eg TB 7827  | 16 ha  | \$26,825  | N/A                                  | \$24,000                                       | \$2,825   |
| eg 1234567  | 12   | 0   | \$24,000                             | 0  | 0   |
| eg 1234568  | 2  | \$ 8,892  | \$ 4,000                             | 0  | \$4,892   |
| 1 1223578 ✓   | 16   | 11,363'   | 6400                                 | 0  | 4963  |
| 2 1223577 ✓   | 16   | 2,040'  | 6400                                 | 0  | 2,040   |
| 3 1218063 ✓   | 16   | 17,322'   | 6400                                 | 0  | 10,922  |
| 4 1223579 ✓   | 16   | 8,977'  | 6400                                 | 0  | 2,577   |
| 5 1218062 ✓   | 16   | 22,024'   | 6400                                 | 0  | 15,624  |
| 6 1218061   | 12   | 620'  | 4800                                 | 0  | 620   |
| 7 1218058   | 8  | 36,372'   | 3200                                 | 19,200   | 13,972  |
| 8 1218060   | 16   | 0'  | 6400                                 | 0  | 0   |
| 9 1218059   | 4  | 0'  | 1600                                 | 0  | 0   |
| 10  |  |   |                                      |  |   |
| 11  |  |   |                                      |  |   |
| 12  |  |   |                                      |  |   |
| 13  |  |   |                                      | 2. 1 350 6                                     |   |
| 14  |  |   |                                      |  |   |
| 15  |  |   |                                      |  |   |
| Column Totals   |  | 98,718  | 48,000                               | 19,200   | 50,718  |

I, Daniel F. Patrie, do hereby certify that the above work credits are eligible under subsection 7 (1) of the Assessment Work Regulation 6/98 for assignment to contiguous claims or for application to the claim where the work was done.

Signature of Recorded Holder or Agent Authorized in Writing

CST 23 1033

Date

GEOSCIENCE ASSESSMENT OFFICE

OCT 20/88

#### 6. Instructions for cutting back credits that are not approved.

Some of the credits claimed in this declaration may be cut back. Please check (✓) in the boxes below to show how you wish to prioritize the deletion of credits:

- 1. Credits are to be cut back from the Bank first, followed by option 2 or 3 or 4 as indicated.
- 2. Credits are to be cut back starting with the claims listed last, working backwards; or
- 3. Credits are to be cut back equally over all claims listed in this declaration; or
- 4. Credits are to be cut back as prioritized on the attached appendix or as follows (describe):

1223577, 1223524, 1218061,

Note: If you have not indicated how your credits are to be deleted, credits will be cut back from the Bank first, followed by option number 2 if necessary.

#### For Office Use Only

Received Stamp

Deemed Approved Date

Date Notification Sent

Date Approved

Total Value of Credit Approved

Personal information collected on this form is obtained under the authority of subsection 6(1) of the Assessment Work Regulation 8/96. Under section 8 of the Mining Act, the information is a public record. This information will be used to review the assessment work and correspond with the mining land holder. Questions about this collection should be directed to the Chief Mining Recorder, Ministry of Northern Development and Mines, 6th Floor, 933 Ramsey Lake Road, Sudbury, Ontario, P3E 6B5.

| Work Type   | Units of Work<br>Depending on the type of work, list the number of hours/days worked, metres of drilling, kilo-metres of grid line, number of samples, etc. | Cost Per Unit of work        | Total Cost |
|---|---|------------------------------|------------|
| Line Cutting  | 83 kms  | \$ 348                       | \$ 28,884  |
| Mag   | 83 kms.   | \$ 118                       | \$ 9,794   |
| Induced Polarization  | 40 kms  | \$ 1391                      | \$ 55,640  |
| Report & Plotting   | 1   | \$ 2,400                     | \$ 2,400   |
| <b>Associated Costs (e.g. supplies, mobilization and demobilization).</b> |   |                              |            |
| Mob crews, Line Cutting, Mag & I.P.                                       |   | \$ 2,000                     | \$ 2,000   |
| <b>Transportation Costs</b>   |   |                              |            |
| <b>RECEIVED</b>   |   |                              |            |
| <b>Food and Lodging Costs</b>   |   | CST 23 1983                  |            |
|   |   | GEOLOGICAL ASSESSMENT OFFICE |            |
| <b>Total Value of Assessment Work</b>                                     |   |                              | \$ 98,718  |

**Calculations of Filing Discounts:**

1. Work filed within two years of performance is claimed at 100% of the above Total Value of Assessment Work.
2. If work is filed after two years and up to five years after performance, it can only be claimed at 50% of the Total Value of Assessment Work. If this situation applies to your claims, use the calculation below:

**TOTAL VALUE OF ASSESSMENT WORK****x 0.50 =****Total \$ value of worked claimed****Note:**

- Work older than 5 years is not eligible for credit.
- A recorded holder may be required to verify expenditures claimed in this statement of costs within 45 days of a request for verification and/or correction/clarification. If verification and/or correction/clarification is not made, the Minister may reject all or part of the assessment work submitted.

**Certification verifying costs:**

I, Daniel F. Patrice, do hereby certify, that the amounts shown are as accurate as may reasonably be determined and the costs were incurred while conducting assessment work on the lands indicated on the accompanying Declaration of Work form as Agent (recorded holder, agent, or state company position with signing authority) I am authorized to make this certification.

Signature

Date

Ministry of  
Northern Development  
and Mines

Ministère du  
Développement du Nord  
et des Mines

March 9, 1999

MAPLE MINERALS INC.  
2 First Canadian Place, Suite 2810  
P.O. Box 47, The Exchange Tower  
Toronto, ON  
M5K 1A9



Ontario

Geoscience Assessment Office  
933 Ramsey Lake Road  
6th Floor  
Sudbury, Ontario  
P3E 6B5

Telephone: (888) 415-9846  
Fax: (877) 670-1555

Visit our website at:  
[www.gov.on.ca/MNDM/MINES/LANDS/mlsmnpge.htm](http://www.gov.on.ca/MNDM/MINES/LANDS/mlsmnpge.htm)

Dear Sir or Madam:

**Submission Number:** 2.18926

**Status**

**Subject: Transaction Number(s):** W9860.00819 Approval After Notice

---

We have reviewed your Assessment Work submission with the above noted Transaction Number(s). The attached summary page(s) indicate the results of the review. WE RECOMMEND YOU READ THIS SUMMARY FOR THE DETAILS PERTAINING TO YOUR ASSESSMENT WORK.

If the status for a transaction is a 45 Day Notice, the summary will outline the reasons for the notice, and any steps you can take to remedy deficiencies. The 90-day deemed approval provision, subsection 6(7) of the Assessment Work Regulation, will no longer be in effect for assessment work which has received a 45 Day Notice. Allowable changes to your credit distribution can be made by contacting the Geoscience Assessment Office within this 45 Day period, otherwise assessment credit will be cut back and distributed as outlined in Section #6 of the Declaration of Assessment work form.

Please note any revisions must be submitted in DUPLICATE to the Geoscience Assessment Office, by the response date on the summary.

If you have any questions regarding this correspondence, please contact Bruce Gates by e-mail at [bruce.gates@ndm.gov.on.ca](mailto:bruce.gates@ndm.gov.on.ca) or by telephone at (705) 670-5856.

Yours sincerely,

A handwritten signature in black ink, appearing to read "Blair Kite".

ORIGINAL SIGNED BY

Blair Kite  
Supervisor, Geoscience Assessment Office  
Mining Lands Section

# **Work Report Assessment Results**

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**Submission Number:** 2.18926

**Date Correspondence Sent:** March 09, 1999

**Assessor:** Bruce Gates

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| <b>Transaction Number</b> | <b>First Claim Number</b> | <b>Township(s) / Area(s)</b> | <b>Status</b>         | <b>Approval Date</b> |
|---------------------------|---------------------------|------------------------------|-----------------------|----------------------|
| W9860.00819               | 1223578                   | THOMAS, SHERATON             | Approval After Notice | March 05, 1999       |

**Section:**

14 Geophysical IP

14 Geophysical MAG

The revisions outlined in the Notice dated January 19, 1999, have been corrected.

Assessment work credit has been approved as outlined on the attached Distribution of Assessment Work Credit sheet.

**Correspondence to:**

Resident Geologist  
South Porcupine, ON

Assessment Files Library  
Sudbury, ON

**Recorded Holder(s) and/or Agent(s):**

Daniel Patrie  
MASSEY, ONTARIO, CANADA

MAPLE MINERALS INC.  
TORONTO, ON

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## **Distribution of Assessment Work Credit**

The following credit distribution reflects the value of assessment work performed on the mining land(s).

**Date:** March 09, 1999

**Submission Number:** 2.18926

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**Transaction Number:** W9860.00819

| <b>Claim Number</b> | <b>Value Of Work Performed</b> |
|---------------------|--------------------------------|
| 1223577             | 2,735.00                       |
| 1223578             | 7,875.00                       |
| 1223579             | 2,500.00                       |
| 1218058             | 24,860.00                      |
| 1218061             | 0.00                           |
| 1218062             | 17,350.00                      |
| 1218063             | 23,538.00                      |
| <b>Total: \$</b>    | <b>78,858.00</b>               |

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## AREAS WITHDRAWN FROM DISPOSITION

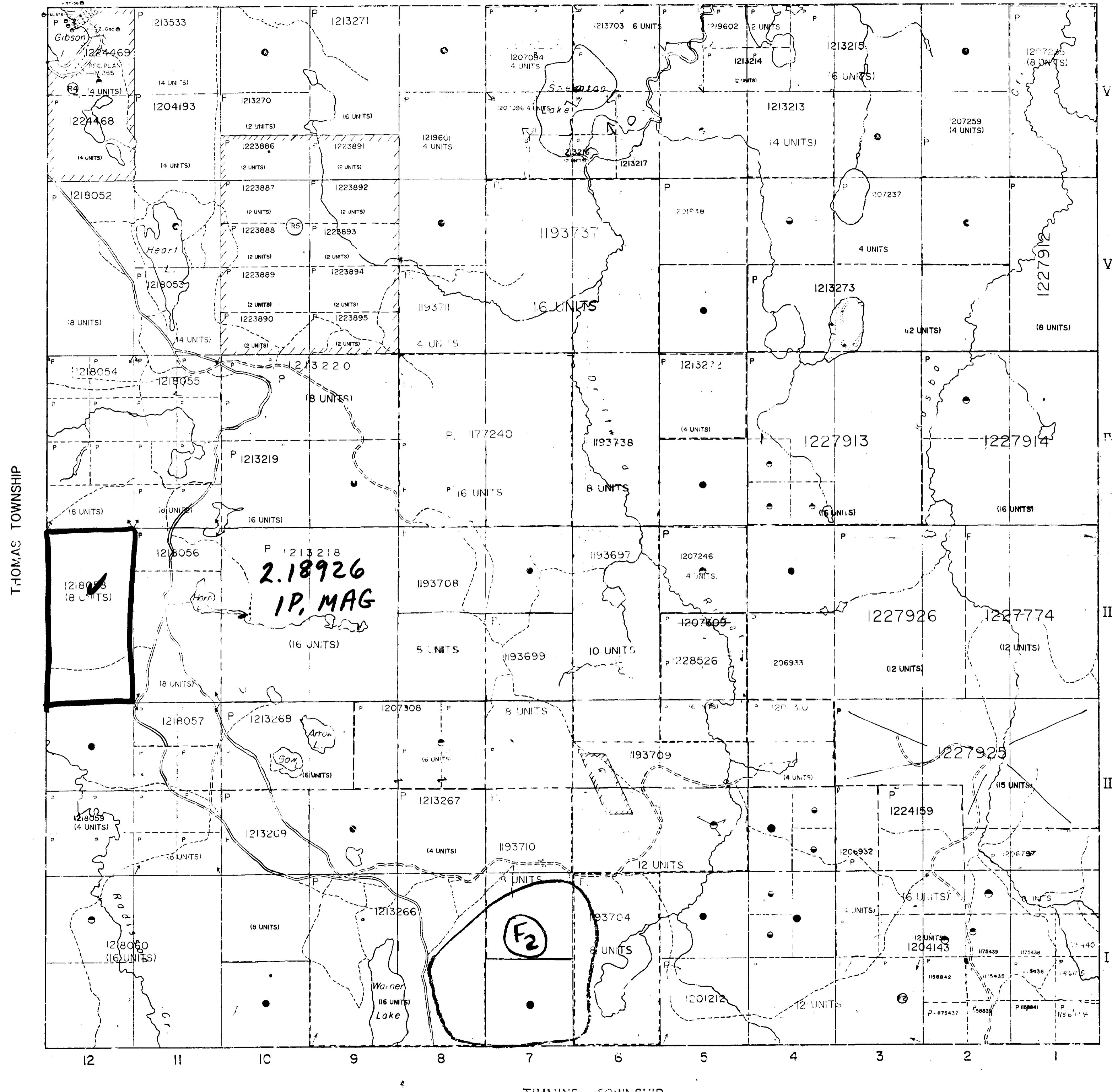
M.T.O. - MINING RIGHTS ONLY  
S.F.O. - SURFACE RIGHTS ONLY  
M+S - MINING AND SURFACE RIGHTS


| Description | Order No.  | Date    | Disposition | File No. |
|-------------|------------|---------|-------------|----------|
|             | W 56 77    | 4/6/77  | S.R.O.      | 17759    |
|             | N.W. 61 82 | 10/1/97 | S.R.O.      |          |
|             | N.W. 61 83 | 22/7/97 | S.R.O.      |          |

(R4) — MINING AND SURFACE RIGHTS RE-OPENED UNDER SECTION 35 OF THE MINING ACT, R.S.O. 1990 ORDER NO. O-P-13/97 NER DATED MAY 16/97, ORDER COMES INTO EFFECT AT 8AM STD TIME, JUNE 1, 1997.

(R5) — MINING AND SURFACE RIGHTS RE-OPENED UNDER SECTION 35 OF THE MINING ACT, R.S.O. 1990, ORDER NO. O-P-15/97 NER DATED MAY 26/97, ORDER COMES INTO EFFECT AT 8AM STD TIME, JUNE 1, 1997.

## BOND TOWNSHIP



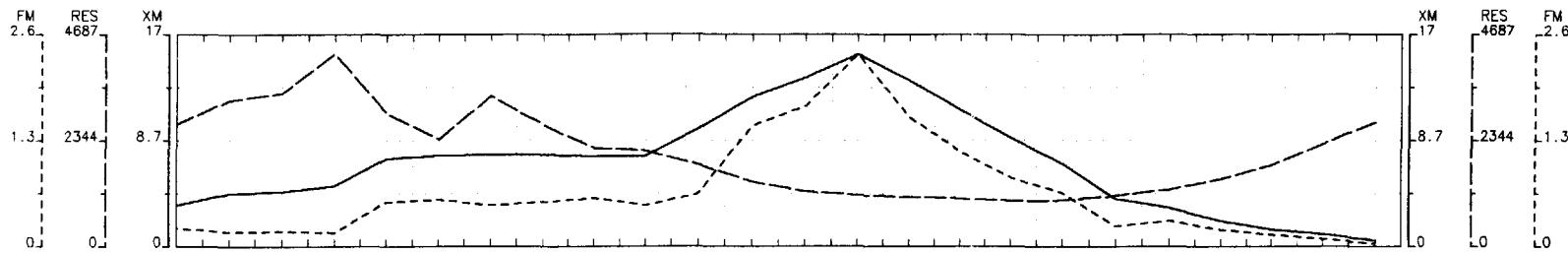




42A07NW2012

2.18926 SHERATON

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| Metal Factor | 0+00  | 1+00 N | 2+00 N | 3+00 N | 4+00 N | 5+00 N | 6+00 N | 7+00 N | 8+00 N | 9+00 N | 10+00 N | 11+00 N |
|--------------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|
| Filter       | 0.22  | 0.17   | 0.18   | 0.16   | 0.54   | 0.57   | 0.50   | 0.54   | 0.59   | 0.50   | 0.64    | 0.15    |
| n=1          | 0.36  | 0.14   | 0.10   | 0.080  | 0.59   | 0.33   | 0.10   | 0.34   | 0.38   | 0.32   | 0.91    | 4.8     |
| n=2          | 0.21  | 0.33   | 0.11   | 0.090  | 0.43   | 0.50   | 0.10   | 0.33   | 0.42   | 0.27   | 0.87    | 1.5     |
| n=3          | 0.090 | 0.28   | 0.38   | 0.11   | 0.54   | 0.37   | 0.16   | 0.33   | 0.52   | 0.43   | 0.66    | 1.1     |
| n=4          | 0.11  | 0.21   | 0.33   | 0.37   | 0.77   | 0.44   | 0.12   | 0.61   | 0.55   | 0.55   | 1.1     | 0.94    |
| n=5          | 0.060 | 0.13   | 0.060  | 0.37   | 3.8    | 0.55   | 0.14   | 0.31   | 0.73   | 0.44   | 1.2     | 1.2     |
| n=6          | 0.040 | 0.11   | 0.29   | 0.050  | 3.8    | 0.76   | 0.18   | 0.30   | 0.49   | 0.62   | 1.1     | 0.92    |

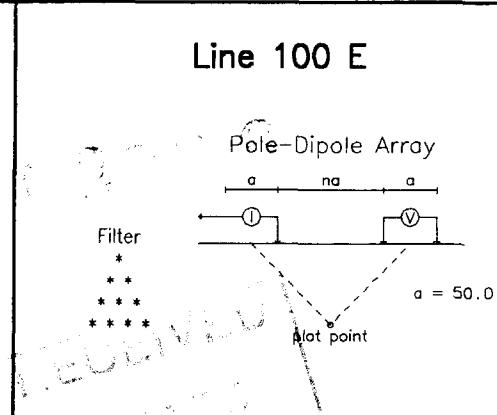
| Metal Factor | 0+00  | 1+00 N | 2+00 N | 3+00 N | 4+00 N | 5+00 N | 6+00 N | 7+00 N | 8+00 N | 9+00 N | 10+00 N | 11+00 N |
|--------------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|
| Filter       | 0.20  | 0.15   | 0.16   | 0.14   | 0.54   | 0.57   | 0.50   | 0.54   | 0.59   | 0.50   | 0.64    | 0.15    |
| n=1          | 0.36  | 0.14   | 0.10   | 0.080  | 0.59   | 0.33   | 0.10   | 0.34   | 0.38   | 0.32   | 0.91    | 4.8     |
| n=2          | 0.21  | 0.33   | 0.11   | 0.090  | 0.43   | 0.50   | 0.10   | 0.33   | 0.42   | 0.27   | 0.87    | 1.5     |
| n=3          | 0.090 | 0.28   | 0.38   | 0.11   | 0.54   | 0.37   | 0.16   | 0.33   | 0.52   | 0.43   | 0.66    | 1.1     |
| n=4          | 0.11  | 0.21   | 0.33   | 0.37   | 0.77   | 0.44   | 0.12   | 0.61   | 0.55   | 0.55   | 1.1     | 0.94    |
| n=5          | 0.060 | 0.13   | 0.060  | 0.37   | 3.8    | 0.55   | 0.14   | 0.31   | 0.73   | 0.44   | 1.2     | 1.2     |
| n=6          | 0.040 | 0.11   | 0.29   | 0.050  | 3.8    | 0.76   | 0.18   | 0.30   | 0.49   | 0.62   | 1.1     | 0.92    |

| Resistivity | 0+00 | 1+00 N | 2+00 N | 3+00 N | 4+00 N | 5+00 N | 6+00 N | 7+00 N | 8+00 N | 9+00 N | 10+00 N | 11+00 N |
|-------------|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|
| Filter      | 2701 | 3227   | 3389   | 4261   | 2931   | 2370   | 3322   | 2883   | 2171   | 2115   | 1806    | 1434    |
| n=1         | 914  | 3477   | 4023   | 6002   | 1157   | 1753   | 4927   | 1568   | 1781   | 1793   | 1080    | 259     |
| n=2         | 1490 | 1296   | 4575   | 6728   | 2165   | 1311   | 6456   | 1754   | 1469   | 2586   | 1526    | 224     |
| n=3         | 2746 | 1608   | 1348   | 6031   | 2165   | 2081   | 4510   | 1985   | 1340   | 1766   | 1887    | 238     |
| n=4         | 3757 | 2808   | 1494   | 1551   | 1778   | 2025   | 6690   | 1318   | 1466   | 1780   | 1588    | 152     |
| n=5         | 6327 | 3347   | 2298   | 1600   | 444    | 1652   | 6272   | 1945   | 959    | 2095   | 1534    | 1294    |
| n=6         | 11K  | 5398   | 2887   | 2169   | 451    | 410    | 5089   | 1756   | 1398   | 1480   | 1848    | 1477    |

| Resistivity | 0+00 | 1+00 N | 2+00 N | 3+00 N | 4+00 N | 5+00 N | 6+00 N | 7+00 N | 8+00 N | 9+00 N | 10+00 N | 11+00 N |
|-------------|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|
| Filter      | 2701 | 3227   | 3389   | 4261   | 2931   | 2370   | 3322   | 2883   | 2171   | 2115   | 1806    | 1434    |
| n=1         | 914  | 3477   | 4023   | 6002   | 1157   | 1753   | 4927   | 1568   | 1781   | 1793   | 1080    | 259     |
| n=2         | 1490 | 1296   | 4575   | 6728   | 2165   | 1311   | 6456   | 1754   | 1469   | 2586   | 1526    | 224     |
| n=3         | 2746 | 1608   | 1348   | 6031   | 2165   | 2081   | 4510   | 1985   | 1340   | 1766   | 1887    | 238     |
| n=4         | 3757 | 2808   | 1494   | 1551   | 1778   | 2025   | 6690   | 1318   | 1466   | 1780   | 1588    | 152     |
| n=5         | 6327 | 3347   | 2298   | 1600   | 444    | 1652   | 6272   | 1945   | 959    | 2095   | 1534    | 1294    |
| n=6         | 11K  | 5398   | 2887   | 2169   | 451    | 410    | 5089   | 1756   | 1398   | 1480   | 1848    | 1477    |

| Chareability | 0+00 | 1+00 N | 2+00 N | 3+00 N | 4+00 N | 5+00 N | 6+00 N | 7+00 N | 8+00 N | 9+00 N | 10+00 N | 11+00 N |
|--------------|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|
| Filter       | 3.4  | 4.3    | 4.5    | 4.9    | 7.2    | 7.4    | 7.5    | 7.4    | 9.6    | 12     | 14      | 16      |
| n=1          | 3.3  | 4.9    | 4.1    | 4.7    | 6.8    | 5.8    | 5      | 5.7    | 6.7    | 5.8    | 9.8     | 12      |
| n=2          | 3.2  | 4.3    | 5.1    | 5.8    | 9.3    | 6.5    | 6.2    | 5.9    | 6.3    | 6.9    | 13      | 16      |
| n=3          | 2.5  | 4.5    | 5.1    | 6.4    | 12     | 7.7    | 7.3    | 6.6    | 7      | 7.5    | 12      | 16      |
| n=4          | 4.1  | 5.6    | 4.9    | 5.8    | 14     | 8.9    | 8.3    | 8.1    | 8      | 9.8    | 15      | 17      |
| n=5          | 3.9  | 4.3    | 1.3    | 6      | 16     | 9.2    | 8.6    | 8      | 7      | 9.2    | 19      | 21      |
| n=6          | 4.8  | 6      | 8.4    | 1.1    | 17     | 3.1    | 9.4    | 5.3    | 6.8    | 9      | 20      | 14      |

| Chareability | 0+00 | 1+00 N | 2+00 N | 3+00 N | 4+00 N | 5+00 N | 6+00 N | 7+00 N | 8+00 N | 9+00 N | 10+00 N | 11+00 N |
|--------------|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|
| Filter       | 3.4  | 4.3    | 4.5    | 4.9    | 7.2    | 7.4    | 7.5    | 7.4    | 9.6    | 12     | 14      | 16      |
| n=1          | 3.3  | 4.9    | 4.1    | 4.7    | 6.8    | 5.8    | 5      | 5.7    | 6.7    | 5.8    | 9.8     | 12      |
| n=2          | 3.2  | 4.3    | 5.1    | 5.8    | 9.3    | 6.5    | 6.2    | 5.9    | 6.3    | 6.9    | 13      | 16      |
| n=3          | 2.5  | 4.5    | 5.1    | 6.4    | 12     | 7.7    | 7.3    | 6.6    | 7      | 7.5    | 12      | 16      |
| n=4          | 4.1  | 5.6    | 4.9    | 5.8    | 14     | 8.9    | 8.3    | 8.1    | 8      | 9.8    | 15      | 17      |
| n=5          | 3.9  | 4.3    | 1.3    | 6      | 16     | 9.2    | 8.6    | 8      | 7      | 9.2    | 19      | 21      |
| n=6          | 4.8  | 6      | 8.4    | 1.1    | 17     | 3.1    | 9.4    | 5.3    | 6.8    | 9      | 20      | 14      |



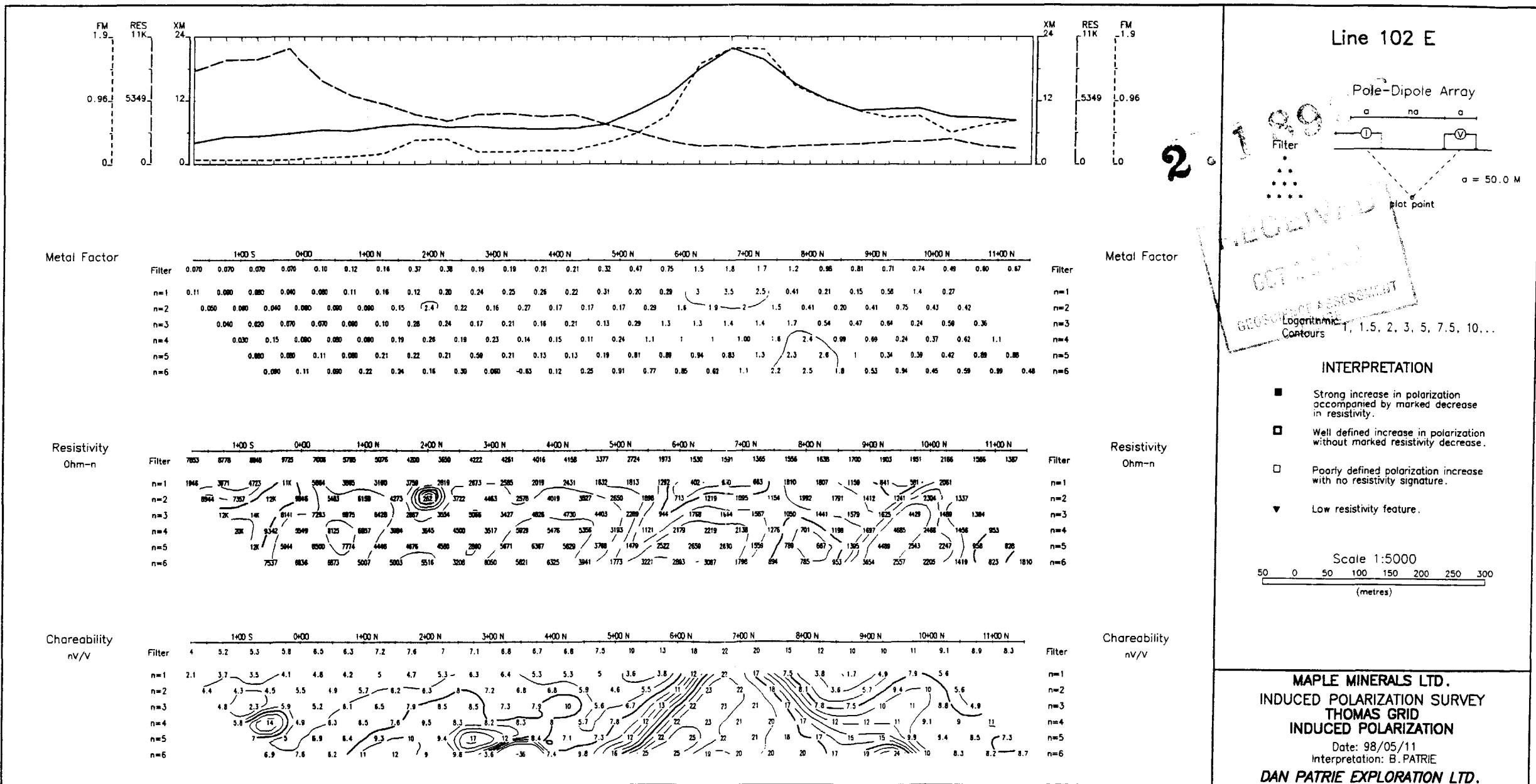
INTERPRETATION

- Strong increase in polarization accompanied by marked decrease in resistivity.
- Well defined increase in polarization without marked resistivity decrease.
- Poorly defined polarization increase with no resistivity signature.
- ▼ Low resistivity feature.

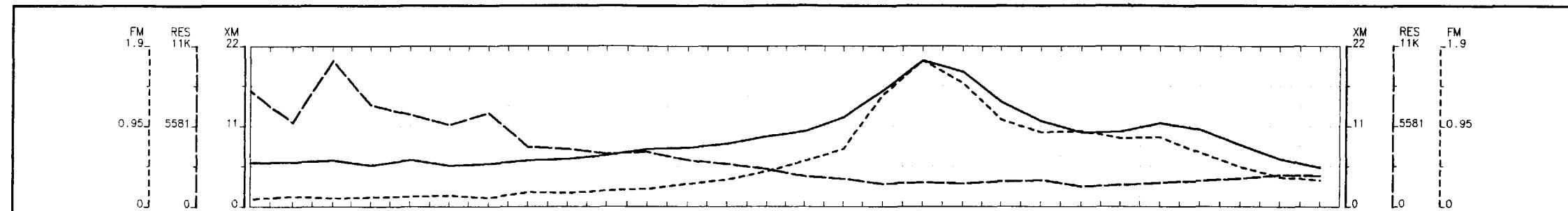
Scale 1:5000

50 0 50 100 150 200 250 300  
(metres)

MAPLE MINERALS LTD.  
INDUCED POLARIZATION SURVEY  
THOMAS GRID  
INDUCED POLARIZATION  
Date: 98/05/11  
Interpretation: B. PATRIE  
DAN PATRIE EXPLORATION LTD.



L-104E



Filter

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Metal Factor

|        | 3+00 S | 2+00 S | 1+00 S | 0+00  | 1+00 N | 2+00 N | 3+00 N | 4+00 N | 5+00 N | 6+00 N | 7+00 N | 8+00 N | 9+00 N | 10+00 N |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |     |
|--------|--------|--------|--------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|-----|
| Filter | 0.090  | 0.12   | 0.10   | 0.11  | 0.12   | 0.13   | 0.10   | 0.17   | 0.16   | 0.19   | 0.21   | 0.27   | 0.32   | 0.42    | 0.54 | 0.68 | 1.3  | 1.7  | 1.5  | 1    | 0.88 | 0.89 | 0.81 | 0.82 | 0.64 | 0.47 | 0.35 | 0.31 |      |     |
| n=1    | 0.050  | 0.12   | 0.030  | 0.050 | 0.070  | 0.20   | 0.070  | 0.23   | 0.11   | 0.17   | 0.25   | 0.32   | 0.28   | 0.45    | 0.46 | 0.38 | 2.5  | 4    | 2.1  | 0.38 | 0.18 | 0.24 | 0.32 | 1.2  | 0.79 | 0.24 | 0.14 | 0.13 |      |     |
| n=2    | 0.080  | 0.090  | 0.040  | 0.070 | 0.16   | 0.40   | 0.13   | 0.17   | 0.17   | 0.18   | 0.20   | 0.31   | 0.29   | 0.36    | 0.34 | 1.3  | 2.1  | 1.9  | 1.3  | 0.31 | 0.26 | 0.47 | 0.94 | 0.70 | 0.69 | 0.21 | 0.14 | 0.17 |      |     |
| n=3    | 0.060  | 0.10   | 0.070  | 0.19  | 0.040  | 0.10   | 0.13   | 0.27   | 0.16   | 0.21   | 0.23   | 0.29   | 0.28   | 0.29    | 1.1  | 1.1  | 1.3  | 1.2  | 0.86 | 0.56 | 0.63 | 1    | 0.56 | 0.63 | 0.53 | 0.23 | 0.17 | 0.17 |      |     |
| n=4    | -0.060 | 0.12   | 0.19   | 0.050 | 0.090  | 0.090  | 0.20   | 0.21   | 0.19   | 0.21   | 0.22   | 0.30   | 0.29   | 0.92    | 1    | 0.79 | 0.91 | 0.83 | 1.8  | 3    | 1.1  | 0.73 | 0.38 | 0.52 | 0.46 | 0.45 | 0.45 | 0.45 | 0.45 |     |
| n=5    | 0.51   | 0.30   | 0.050  | 0.12  | 0.10   | 0.15   | 0.17   | 0.23   | 0.21   | 0.20   | 0.24   | 0.31   | 0.86   | 0.86    | 0.82 | 0.60 | 0.67 | 2.1  | 3    | 1.5  | 0.69 | 0.68 | 0.42 | 0.41 | 1.2  | 2.5  | 2.5  | 2.5  | 2.5  | 2.5 |
| n=6    | 0.23   | 0.080  | 0.080  | 0.13  | 0.17   | 0.14   | 0.20   | 0.23   | 0.19   | 0.24   | 0.26   | 0.89   | 0.78   | 0.75    | 0.66 | 0.48 | 1.9  | 2.9  | 2    | 0.74 | 0.57 | 0.38 | 0.35 | 1.1  | 2.5  | 2.5  | 2.5  | 2.5  | 2.5  |     |

Metal Factor

Filter

n=1

n=2

n=3

n=4

n=5

n=6

Logarit Contou

CROSS SECTION ASSESSMENT

250

Resistivity

|        | 3+00 S | 2+00 S | 1+00 S | 0+00 | 1+00 N | 2+00 N | 3+00 N | 4+00 N | 5+00 N | 6+00 N | 7+00 N | 8+00 N | 9+00 N | 10+00 N |      |      |      |      |      |      |      |      |      |      |      |      |      |      |     |
|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|-----|
| Filter | 8025   | 5837   | 10K    | 7055 | 6375   | 5655   | 6495   | 4136   | 4002   | 3659   | 3796   | 3227   | 2967   | 2601    | 2094 | 1923 | 1579 | 1676 | 1609 | 1754 | 1839 | 1380 | 1505 | 1650 | 1794 | 1852 | 2211 | 2150 |     |
| n=1    | 3816   | 3902   | 22K    | 9325 | 7446   | 1823   | 4907   | 1670   | 2815   | 1790   | 2196   | ~1544  | 1716   | 1506    | 1008 | 1014 | 333  | 495  | 768  | 1651 | 2529 | 1421 | 1102 | 719  | 969  | 1771 | 2374 | 2718 | n=1 |
| n=2    | 7101   | 6950   | 11K    | 7055 | 2948   | 10K    | 3341   | 2789   | 2612   | 3645   | 3072   | 2321   | 2728   | 1872    | 1714 | 714  | 916  | 1056 | 1253 | 2786 | 1751 | 1125 | 1220 | 1566 | 1340 | 2254 | 3388 | 1030 | n=2 |
| n=3    | 12K    | 5320   | 7335   | 2513 | 1.3K   | 5379   | 4240   | 2391   | 4299   | 3937   | 3544   | 3062   | 2830   | 2447    | 871  | 1708 | 1533 | 1502 | 1916 | 1487 | 1118 | 1152 | 2189 | 2182 | 1895 | 2758 | 1221 | n=3  |     |
| n=4    | 7900   | 4385   | 2754   | 11K  | 7112   | 6419   | 3306   | 4176   | 4139   | 4332   | 4252   | 2862   | 3037   | 1181    | 1921 | 2580 | 2054 | 2237 | 932  | 938  | 1116 | 2163 | 2283 | 2215 | 882  | 2792 | 674  | n=4  |     |
| n=5    | 5442   | 1894   | 1K     | 5729 | 7304   | 4563   | 5145   | 3900   | 4356   | 4823   | 3644   | 2908   | 1399   | 2335    | 2607 | 3231 | 2820 | 912  | 570  | 1032 | 2250 | 2204 | 2649 | 2792 | 674  | 3175 | 618  | n=5  |     |
| n=6    | 2386   | 7755   | 6024   | 6079 | 5030   | 6830   | 4775   | 4227   | 4808   | 4014   | 3532   | 1366   | 2856   | 3023    | 3117 | 4077 | 1024 | 583  | 773  | 2205 | 2178 | 2528 | 3175 | 618  | 2178 | 2528 | 3175 | 618  | n=6 |

Resistivity

Filter

n=1

n=2

n=3

n=4

n=5

n=6

Chareability

|        | 3+00 S | 2+00 S | 1+00 S | 0+00 | 1+00 N | 2+00 N | 3+00 N | 4+00 N | 5+00 N | 6+00 N | 7+00 N | 8+00 N | 9+00 N | 10+00 N |     |    |    |     |     |     |     |     |     |     |     |     |     |     |     |     |
|--------|--------|--------|--------|------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|-----|----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Filter | 5.9    | 6      | 6.2    | 5.6  | 6.3    | 5.5    | 5.7    | 6.2    | 6.4    | 6.9    | 7.8    | 7.9    | 8.5    | 9.5     | 10  | 12 | 16 | 20  | 18  | 14  | 12  | 9.9 | 10  | 11  | 10  | 8.3 | 6.4 | 5.2 |     |     |
| n=1    | 4.2    | 4.6    | 6.3    | 4.3  | 4.9    | 3.7    | 3.3    | 3.9    | 3      | 5.4    | 4.9    | 4.8    | 6.7    | 4.6     | 3.9 | 20 | 18 | 6.3 | 4.8 | 3.4 | 3.6 | 8.7 | 7.7 | 4.2 | 3.3 | 3.5 | 1.8 | n=1 |     |     |
| n=2    | 5.3    | 6.3    | 5.1    | 4.8  | 4.8    | 4.4    | 4.4    | 4.8    | 4.4    | 6.3    | 7.3    | 7.8    | 6.8    | 5.8     | 3.9 | 20 | 19 | 16  | 11  | 11  | 11  | 9   | 9.5 | 4.7 | 4.9 | 2.1 | 2.1 | 2.1 | n=2 |     |
| n=3    | 7.2    | 5.4    | 5.3    | 4.7  | 5.7    | 5.3    | 5.3    | 6.4    | 7      | 8.2    | 8      | 8.8    | 7.3    | 7       | 9.8 | 20 | 19 | 16  | 16  | 12  | 12  | 10  | 8.1 | 8.3 | 12  | 10  | 9.9 | 9.3 | 4   | n=3 |
| n=4    | -4.7   | 5.5    | 5.2    | 5.7  | 6.5    | 6.1    | 5.5    | 8.7    | 7.8    | 9.1    | 9.5    | 8.7    | 9.1    | 9.6     | 9   | 12 | 21 | 23  | 20  | 19  | 19  | 19  | 17  | 15  | 16  | 15  | 11  | 12  | 8.1 | n=4 |
| n=5    | 28     | 5.6    | 5.8    | 6.8  | 7.6    | 6.9    | 6.7    | 8.8    | 8.8    | 9.1    | 9.6    | 9.7    | 9      | 9.6     | 9   | 12 | 21 | 23  | 20  | 19  | 19  | 19  | 17  | 15  | 16  | 15  | 11  | 12  | 8.1 | n=5 |
| n=6    | 5.4    | 6.1    | 5.3    | 7.6  | 8.4    | 9.7    | 9.5    | 9.7    | 9      | 9.6    | 9.5    | 9.6    | 9      | 9.6     | 9   | 12 | 21 | 23  | 20  | 19  | 19  | 19  | 17  | 15  | 16  | 15  | 11  | 12  | 9.3 | n=6 |

Chareability

Filter

n=1

n=2

n=3

n=4

n=5

n=6

MA

INDUCE

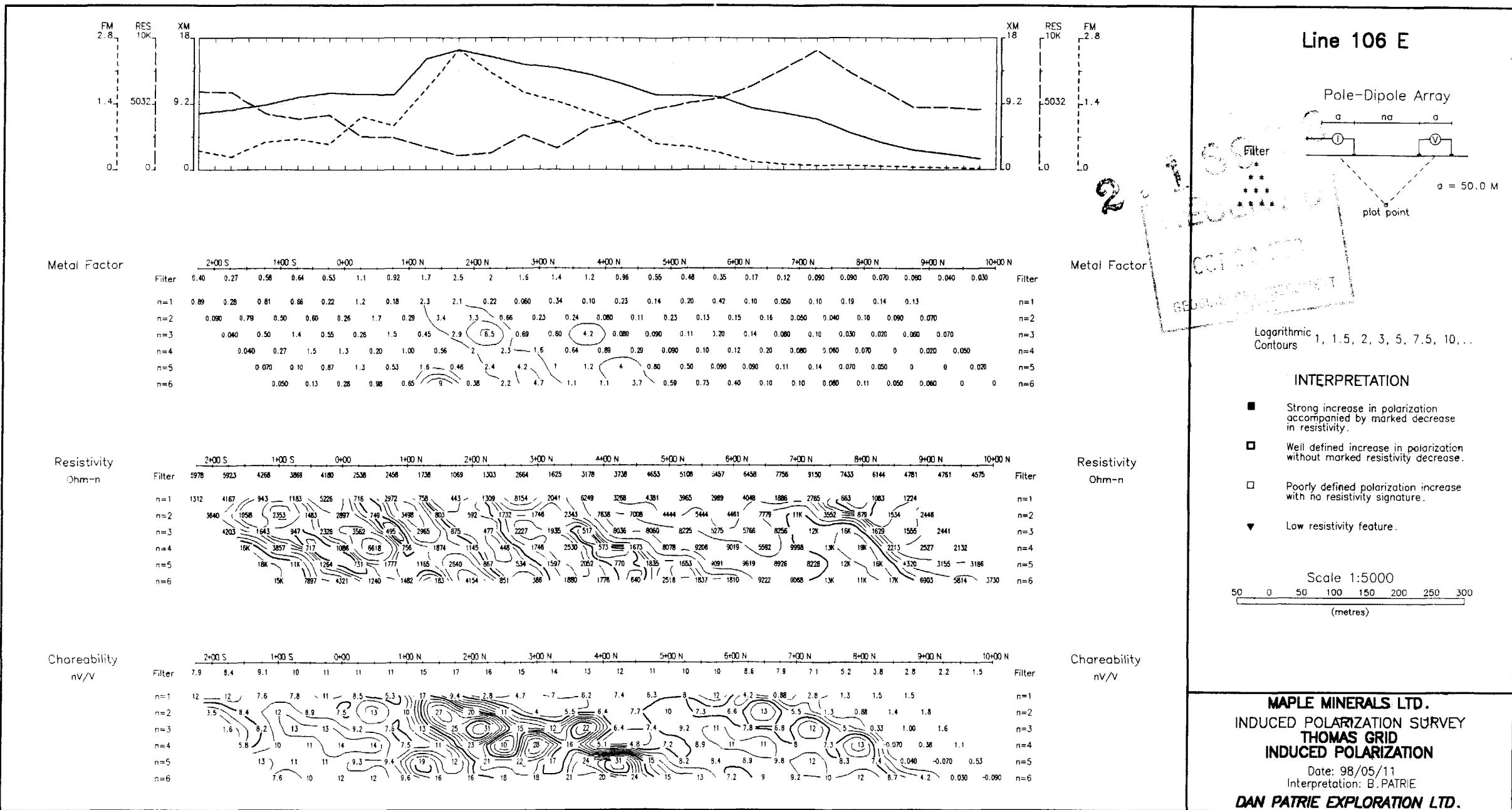
INC

DAN PA

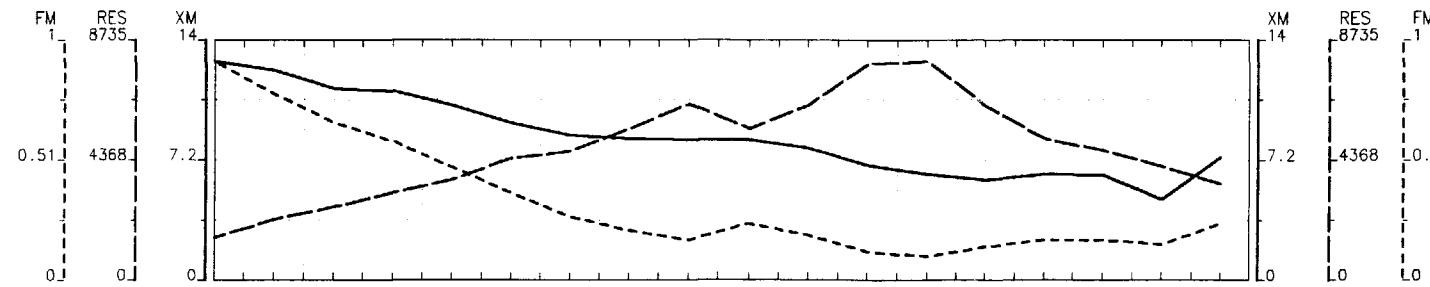


42A07NW2012 2.18926 SHERATON

260



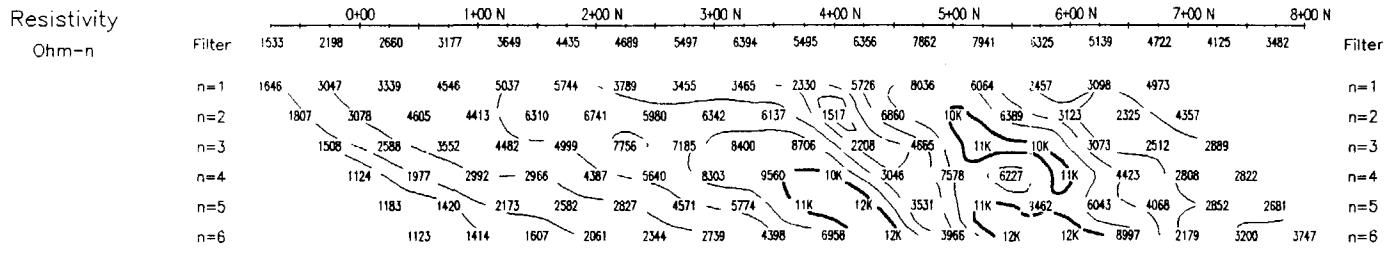
270 SHERATON 42A07NW2012 2.18926



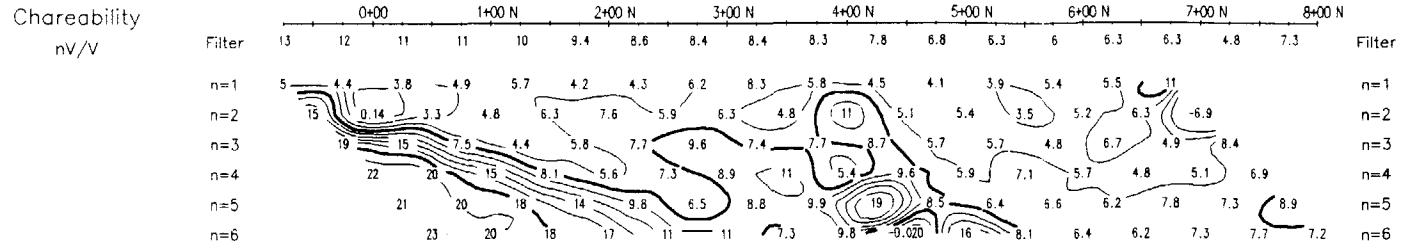
## Metal Factor

|     | 0+00 | 1+00 N | 2+00 N | 3+00 N | 4+00 N | 5+00 N | 6+00 N | 7+00 N | 8+00 N |       | Filter |       |       |      |      |       |
|-----|------|--------|--------|--------|--------|--------|--------|--------|--------|-------|--------|-------|-------|------|------|-------|
| n=1 | 0.30 | 0.14   | 0.11   | 0.11   | 0.070  | 0.11   | 0.18   | 0.24   | 0.25   | 0.080 | 0.050  | 0.060 | 0.22  | 0.18 | 0.22 |       |
| n=2 | 0.81 | 0      | 0.070  | 0.11   | 0.10   | 0.11   | 0.10   | 0.10   | 0.080  | 0.74  | 0.070  | 0.050 | 0.050 | 0.17 | 0.27 | -0.16 |
| n=3 | 1.2  | 0.57   | 0.21   | 0.10   | 0.12   | 0.10   | 0.13   | 0.090  | 0.090  | 0.39  | 0.12   | 0.050 | 0.050 | 0.22 | 0.20 | 0.29  |
| n=4 | 1.9  | 1      | 0.49   | 0.27   | 0.13   | 0.13   | 0.11   | 0.11   | 0.050  | 0.31  | 0.080  | 0.11  | 0.050 | 0.11 | 0.18 | 0.25  |
| n=5 | 1.8  | 1.4    | 0.85   | 0.54   | 0.35   | 0.14   | 0.15   | 0.090  | 0.16   | 0.24  | 0.060  | 0.070 | 0.10  | 0.19 | 0.25 | 0.33  |
| n=6 | 2    | 1.4    | 1.1    | 0.80   | 0.49   | 0.39   | 0.17   | 0.14   | 0      | 0.41  | 0.070  | 0.050 | 0.070 | 0.34 | 0.24 | 0.19  |

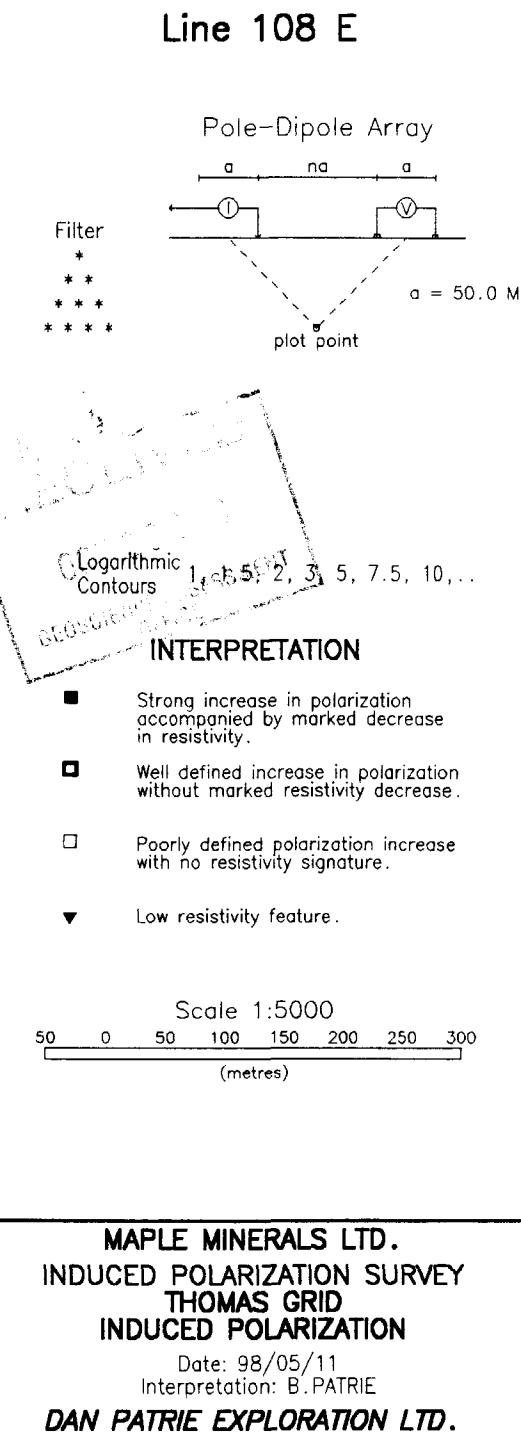
## Metal Factor

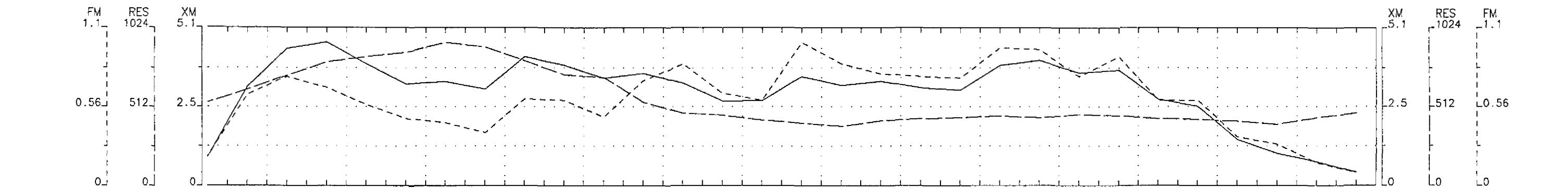


## Resistivity



## Chareability





42A07NW2012 2.18926 SHERATON

280

METAL FACTOR

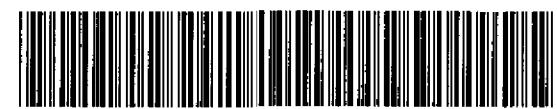
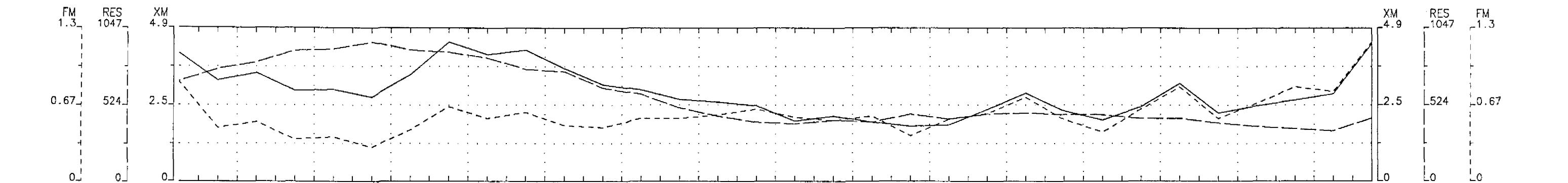
|        | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S |              |      |      |       |      |      |      |      |      |      |       |        |       |     |
|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------------|------|------|-------|------|------|------|------|------|------|-------|--------|-------|-----|
| Filter | 0.21    | 0.64    | 0.77    | 0.69    | 0.57    | 0.47    | 0.44    | 0.37    | 0.61    | 0.60    | 0.48   | 0.74   | 0.86   | 0.55   | 0.60   | METAL FACTOR |      |      |       |      |      |      |      |      |      |       |        |       |     |
| n=1    | 0.39    | 0.57    | 0.92    | 0.68    | 0.76    | 0.72    | 0.90    | 0.45    | 1.3     | 0.99    | 0.46   | 1.1    | 1.8    | 0.78   | 0.22   | 1.8          | 0.40 | 0.11 | 1     | 1.4  | 1.7  | 1.1  | 0.69 | 1.9  | 0.49 | 0.86  | 0.52   | 0.88  | n=1 |
| n=2    | 0       | 1.1     | 0.89    | 0.95    | 0.10    | 0.41    | 0.50    | 0.15    | 0.37    | 0.17    | 0.040  | 1.1    | 0.59   | 0.86   | 0.63   | 1.6          | 1.4  | 1.5  | 0.31  | 0.96 | 1.2  | 0.86 | 0.24 | 1.1  | 0.25 | 0.79  | -0.090 | 0.17  | n=2 |
| n=3    | -0.020  | 0.65    | 0.42    | 0.54    | 0.46    | 0.21    | 0.44    | 0.53    | 1       | 0.57    | 0.040  | 0.47   | 0.44   | 0.42   | 0.14   | 0.77         | 0.79 | 0.49 | 0.030 | 0.69 | 1.3  | 0.68 | 0.26 | 0.15 | 0.40 | 0.16  | -0.15  | 0.070 | n=3 |
| n=4    | 0.42    | 0.77    | 0.35    | 0.22    | 0.040   | 0.45    | 0.52    | 1.3     | 0.59    | 0.44    | 1.1    | 0.0100 | 0.34   | 1.1    | 1.7    | 0.37         | 0.63 | 0.52 | 0.75  | 1.3  | 0.47 | 0.22 | 0.35 | 0.49 | 0.62 | -0.28 | 0.37   | n=4   |     |
| n=5    | 2.4     | 0.42    | 0.35    | 0.22    | 0.24    | 0.19    | 0.63    | 1.1     | 0.47    | 0.45    | 0.87   | 0.29   | 0.56   | 0.90   | 1.1    | 0.52         | 0.69 | 0.86 | 0.62  | 1.4  | 2    | 0.45 | 0.40 | 0.21 | 0.69 | -0.39 | 0.040  | n=5   |     |
| n=6    | 0.38    | 0.44    | 0.45    | 0.31    | 0.060   | 0.44    | 0.80    | 0.62    | 0.31    | 0.79    | 2.3    | 1.5    | 0.12   | 1.4    | 0.75   | 0.52         | 0.24 | 0.75 | 0.96  | 1.3  | 1.2  | 0.69 | 0.83 | 0.24 | 0.59 | -0.68 | 0.27   | n=6   |     |

RESISTIVITY

|        | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S |     | Filter | Ohm-m | RESISTIVITY | Ohm-m |     |     |     |     |     |     |     |     |     |             |
|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|-----|--------|-------|-------------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------------|
| Filter | 539     | 623     | 717     | 803     | 839     | 887     | 931     | 900     | 813     | 722     | 705    | 540    | 459    | 454    | 423    | 383 | 418    | 431   | 438         | 449   | 437 | 459 | 450 | 432 | 426 | 415 | 395 | 438 | 457 | RESISTIVITY |
| n=1    | 443     | 296     | 291     | 324     | 278     | 307     | 326     | 389     | 358     | ~280    | 391    | 233    | 158    | 178    | 172    | 156 | 120    | 149   | 149         | 150   | 179 | 157 | 194 | 194 | 171 | 176 | 163 | 172 | n=1 |             |
| n=2    | 570     | 494     | 530     | 505     | 488     | 540     | 660     | 598     | 429     | 601     | 453    | 285    | 348    | 271    | 293    | 207 | 215    | 246   | 243         | 279   | 254 | 289 | 339 | 286 | 298 | 289 | 287 | 259 | n=2 |             |
| n=3    | 781     | 748     | 721     | 748     | 727     | 908     | 855     | 654     | 863     | 614     | 445    | 473    | 410    | 393    | 313    | 305 | 315    | 360   | 385         | 335   | 410 | 434 | 406 | 396 | 397 | 410 | 350 | 303 | n=3 |             |
| n=4    | 1454    | 946     | 1055    | 1118    | 1069    | 816     | 1081    | 757     | 581     | 637     | 532    | 395    | 443    | 453    | 449    | 621 | 438    | 512   | 530         | 480   | 500 | 488 | 517 | 458 | 383 | 401 | 513 | 518 | 539 | n=4         |
| n=5    | 313     | 1458    | 1546    | 1454    | 1454    | 855     | 973     | 737     | 786     | 711     | 659    | 546    | 545    | 626    | 591    | 679 | 519    | 672   | 633         | 465   | 519 | 629 | 581 | 513 | 518 | 539 | 513 | 518 | n=5 |             |
| n=6    | 1652    | 1538    | 1192    | 1717    | 1140    | 673     | 845     | 745     | 709     | 238     | 625    | 661    | 742    | 780    | 693    | 793 | 720    | 632   | 663         | 825   | 653 | 582 | 527 | 571 | 559 | 558 | 558 | n=6 |     |             |

CHARGEABILITY

|        | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S |     | Filter | mV/V | CHARGEABILITY | mV/V |      |     |      |     |       |       |      |      |               |
|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|-----|--------|------|---------------|------|------|-----|------|-----|-------|-------|------|------|---------------|
| Filter | 0.92    | 3.2     | 4.4     | 4.6     | 3.9     | 3.3     | 3.3     | 3.1     | 4.2     | 3.9     | 3.5    | 3.6    | 3.3    | 2.7    | 3.5    | 3.2 | 3.1    | 3.1  | 3.9           | 4    | 3.6  | 3.7 | 2.8  | 2.5 | 1.5   | 1     | 0.76 | 0.43 | CHARGEABILITY |
| n=1    | 1.7     | 2       | 2.7     | 2.2     | 2.1     | 2.2     | 3       | 1.7     | 4.5     | 2.8     | 1.8    | 2.5    | 2.8    | 1.4    | 0.37   | 2.9 | ~0.48  | 0.17 | 1.5           | 2.1  | 3    | 1.8 | 1.3  | 3.7 | 0.83  | 1.5   | 0.84 | 1.5  | n=1           |
| n=2    | 0       | 5.6     | 4.7     | 4.8     | 0.51    | 2.2     | 3.3     | 0.88    | 1.6     | 1       | 0.19   | 3.1    | 2.1    | 3.4    | 3      | 3.8 | 0.76   | 2.7  | 3             | 2.5  | 0.81 | 3.3 | 0.73 | 2.3 | -0.27 | 0.45  | n=2  |      |               |
| n=3    | -0.12   | 4.9     | 3.1     | 4       | 3.4     | 1.9     | 3.8     | 3.5     | 8.8     | 3.5     | 0.17   | 2.2    | 1.8    | 0.43   | 2.3    | 1.7 | 0.11   | 2.3  | 2.3           | 5.3  | 2.9  | 1.1 | 0.59 | 1.6 | 0.66  | -0.55 | 0.21 | n=3  |               |
| n=4    | 6.1     | 7.3     | 3.7     | 2.4     | 0.38    | 3.7     | 5.6     | 9.6     | 3.4     | 2.8     | 5.8    | 0.070  | 1.4    | 5      | 7.7    | 1.7 | 3.9    | 2.3  | 3.8           | 7    | 2.3  | 1.1 | 1.7  | 2.5 | 2.8   | -1.1  | 1.5  | n=4  |               |
| n=5    | 7.6     | 6.2     | 5.4     | 3.1     | 2.1     | 2.8     | 6.1     | 7.9     | 3.7     | 5.2     | 2.3    | 5.6    | 5.4    | 9.6    | 10     | 5.8 | 4.3    | 1.9  | 5.4           | 6.1  | 8.8  | 9.6 | 4.5  | 4.8 | 1.3   | 3.4   | -3.8 | 1.5  | n=5           |
| n=6    | 6.5     | 6.5     | 6.8     | 3.7     | 1.1     | 5       | 5.4     | 5.2     | 2.3     | 5.6     | 5.4    | 9.6    |        |        |        |     |        |      |               |      |      |     |      |     |       |       |      |      |               |



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SHERATON

**290**

### METAL FACTOR

|        | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S | Filter | METAL FACTOR |
|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|--------------|
| Filter | 0.86    | 0.47    | 0.52    | 0.37    | 0.39    | 0.30    | 0.45    | 0.65    | 0.55    | 0.60    | 0.49   | 0.47   | 0.55   | 0.58   | 0.63   | 0.60   | n=1          |
| n=1    | 1.5     | 0.54    | 0.76    | 0.44    | 0.66    | 0.35    | 0.76    | 1.5     | 0.83    | 0.87    | 0.51   | 0.34   | 1.1    | 0.91   | 0.63   | 0.64   | n=1          |
| n=2    | 0.42    | 0.52    | 0.60    | 0.34    | 0.32    | 0.28    | 0.68    | 0.49    | 0.55    | 0.52    | 0.60   | 0.50   | 0.080  | 0.69   | 0.95   | 0.98   | n=2          |
| n=3    | 0.58    | 0.68    | 0.73    | 0.15    | 0.75    | 0.11    | 0.29    | 1.1     | 0.25    | 0.40    | 0.12   | 0.48   | 0.37   | 0.25   | 0.66   | 1.1    | n=3          |
| n=4    | 0.37    | 0.38    | 0.29    | 0.16    | 0.29    | 0.12    | 0.81    | 0.77    | 0.57    | 0.24    | 0.41   | 0.68   | 0.62   | 0.41   | 0.26   | 0.81   | n=4          |
| n=5    | 0.28    | 0.32    | 0.20    | 0.20    | 0.32    | 0.54    | 0.48    | 0.62    | 0.17    | 0.72    | 0.49   | 0.57   | 0.70   | 0.32   | 0.38   | 0.29   | n=5          |
| n=6    | 0.20    | 0.30    | 0.13    | 0.11    | 0.51    | 0.41    | 0.74    | 0.42    | 0.15    | 0.80    | 1.1    | 0.57   | 0.47   | 0.28   | 0.72   | 0.15   | n=6          |

### RESISTIVITY

|        | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S | Filter | RESISTIVITY |
|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|-------------|
| Filter | 683     | 767     | 813     | 893     | 903     | 952     | 897     | 881     | 843     | 785     | 749    | 638    | 595    | 504    | 447    | 408    | Ohm-m       |
| n=1    | 333     | 351     | 321     | 412     | 296     | 387     | 325     | 360     | 391     | 304     | 340    | 216    | 284    | 202    | 197    | 162    | n=1         |
| n=2    | 654     | 587     | 591     | 572     | 544     | 599     | 571     | 627     | 476     | 578     | 484    | 446    | 437    | 323    | 273    | 220    | n=2         |
| n=3    | 770     | 771     | 680     | 915     | 754     | 822     | 823     | 605     | 803     | 633     | 655    | 541    | 451    | 365    | 376    | 339    | n=3         |
| n=4    | 1004    | 873     | 1111    | 1007    | —       | 1011    | —       | 1105    | 787     | 973     | 768    | 864    | 711    | 556    | 504    | 444    | n=4         |
| n=5    | 1138    | 1435    | 1237    | 1361    | 1420    | 1067    | 1237    | 1027    | 1100    | 919     | 765    | 618    | 494    | 356    | 462    | 487    | n=5         |
| n=6    | 1667    | 1469    | 1573    | 1876    | 1187    | 1505    | 1158    | 1196    | 1031    | 871     | 763    | 549    | 734    | 698    | 484    | 740    | n=6         |

### CHARGEABILITY

|        | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S | Filter | CHARGEABILITY |
|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|---------------|
| Filter | 4.1     | 3.2     | 3.5     | 2.9     | 2.9     | 2.7     | 3.4     | 4.5     | 4.1     | 4.2     | 3.6    | 3.1    | 2.9    | 2.6    | 2.5    | 2.4    | mV/V          |
| n=1    | 5       | 1.9     | 2.4     | 1.8     | 2       | 1.4     | 2.5     | 5.5     | 3.2     | 2.7     | 1.7    | 0.74   | 3      | 1.8    | 1.2    | 1      | n=1           |
| n=2    | 2.8     | 3       | 3.5     | 1.9     | 2       | 1.7     | 3.9     | 3       | 2.9     | 2.2     | 0.38   | 2.2    | 2.6    | 2.2    | 1.3    | 1      | n=2           |
| n=3    | 4.5     | 5.2     | 5       | 1.4     | 5.7     | 0.92    | 2.4     | 6.6     | 2.6     | 2.5     | 0.79   | 2.6    | 0.93   | 1.9    | 4      | 1.6    | n=3           |
| n=4    | 3.8     | 3.3     | 3.2     | 1.6     | 2.9     | 1.4     | 6.4     | 7.5     | 4.4     | 2.1     | 2.9    | 3.8    | 3.1    | 1.5    | 0.96   | 0.88   | n=4           |
| n=5    | 3.2     | 4.6     | 2.5     | 2.8     | 4.5     | 5.8     | 5.9     | 6.3     | 1.8     | 5.6     | 3.8    | 3.5    | 1.9    | 2.1    | 0.36   | 0.37   | n=5           |
| n=6    | 3.3     | 4.4     | 2.1     | 1.9     | 6       | 6.2     | 8.5     | 5.1     | 1.5     | 7       | 3.2    | 3.4    | 5      | 0.73   | 0.37   | 4.5    | n=6           |

Line 101 E

Pole-Dipole Array



Filter

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a = 50.0 M

plot point

**RECEIVED**  
OCT 23 1988  
Logarithmic  
Contours 1  
GEOSCIENCE ASSESSMENT  
OFFICE 2, 3, 5, 7.5, 10,..

### INTERPRETATION

- Strong increase in polarization accompanied by marked decrease in resistivity.
- Well defined increase in polarization without marked resistivity decrease.
- Poorly defined polarization increase with no resistivity signature.
- ▼ Low resistivity feature.

Scale 1:5000

50 0 50 100 150 200 250 300  
(metres)

MAPLE MINERALS INC.

INDUCED POLARIZATION SURVEY

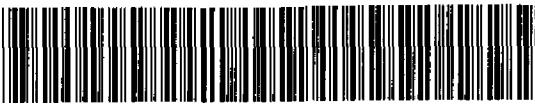
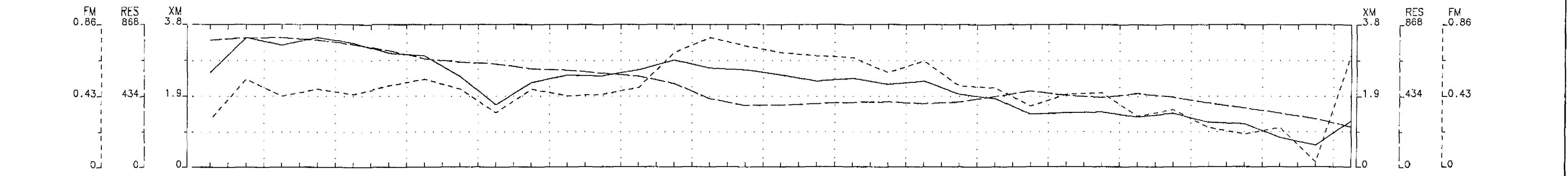
POLE-DIPOLE SURVEY

THOMAS SHERATON PROPERTY

Date: 98/06/08

Interpretation: B. PATRIE AND D. PATRIE

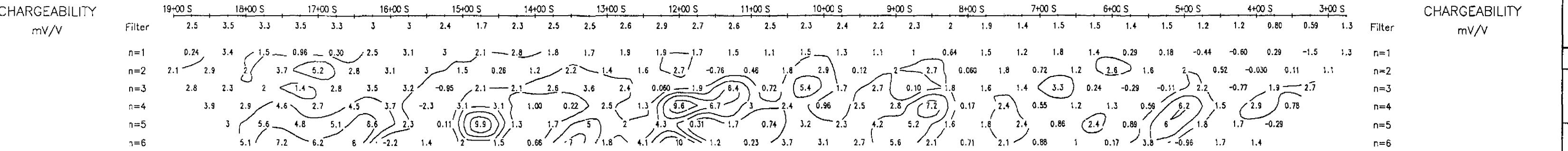
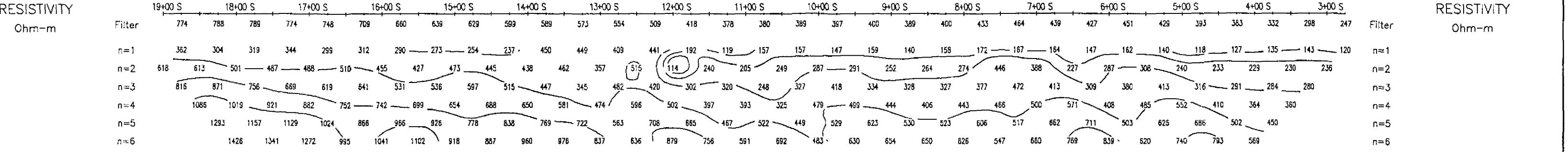
DAN PATRIE EXPLOSION LTD.



42A07NW2012 2.18926

SHERATON 300

| METAL FACTOR | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 M | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S | 4+00 S | 3+00 S | METAL FACTOR |     |
|--------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|--------|--------------|-----|
| Filter       | 0.29    | 0.53    | 0.43    | 0.47    | 0.44    | 0.49    | 0.53    | 0.47    | 0.33    | 0.47    | 0.44   | 0.48   | 0.69   | 0.78   | 0.73   | 0.69   | 0.67   | 0.68         |     |
| n=1          | 0.070   | 1.1     | 0.47    | 0.28    | 0.10    | 0.79    | 1.1     | 1.1     | 0.83    | 1.2     | 0.40   | 0.37   | 0.42   | 0.90   | 2.3    | -0.32  | 0.22   | 0.71         | n=1 |
| n=2          | 0.34    | 0.47    | 0.39    | 0.75    | 1.1     | 0.55    | 0.68    | 0.70    | 0.32    | 0.060   | 0.25   | 0.47   | 0.38   | 0.31   | 2.3    | -0.32  | 0.22   | 0.71         | n=2 |
| n=3          | 0.34    | 0.27    | 0.27    | 0.21    | 0.44    | 0.55    | 0.60    | -0.18   | 0.36    | 0.40    | 0.58   | 1      | 0.50   | 0.0100 | 0.62   | 2      | 0.29   | 1.6          | n=3 |
| n=4          | 0.36    | 0.28    | 0.50    | 0.31    | 0.60    | 0.50    | -0.33   | 0.48    | 0.45    | 0.15    | 0.040  | 0.52   | 0.22   | 1.9    | 1.7    | 0.76   | 0.73   | 0.20         | n=4 |
| n=5          | 0.23    | 0.48    | 0.43    | 0.50    | 0.76    | 0.24    | 0.0100  | 1.3     | 0.16    | 0.22    | 0.69   | 0.36   | 0.61   | 0.050  | 0.37   | 0.14   | 0.71   | 0.43         | n=5 |
| n=6          | 0.36    | 0.54    | 0.49    | 0.80    | -0.21   | 0.13    | 0.22    | 0.17    | 0.070   | 0.72    | 0.22   | 0.64   | 1.2    | 0.15   | 0.040  | 0.53   | 0.65   | 0.43         | n=6 |



## Line 102 E

Pole-Dipole Array



Filter

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a = 50.0 M

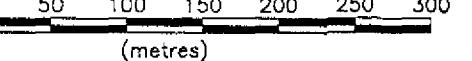
plot point

RECEIVED  
OCT 23 1988  
LOGARITHMIC ASSESSMENT  
GEOSCIENCE CONTOURS OFFICE, 2, 3, 5, 7.5, 10, ...

## INTERPRETATION

- Strong increase in polarization accompanied by marked decrease in resistivity.
- Well defined increase in polarization without marked resistivity decrease.
- Poorly defined polarization increase with no resistivity signature.
- ▼ Low resistivity feature.

Scale 1:5000



MAPLE MINERALS INC.

INDUCED POLARIZATION SURVEY

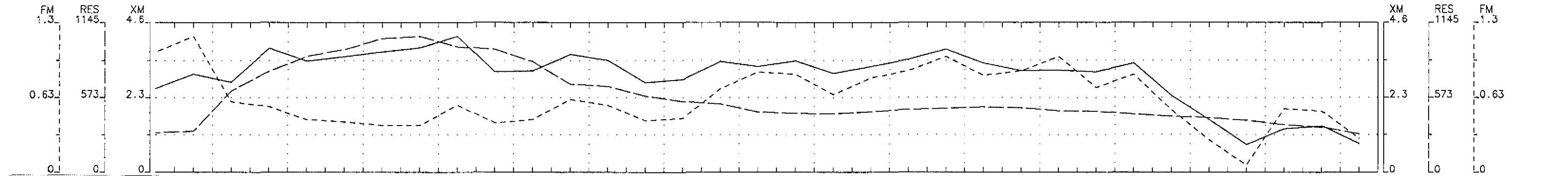
POLE-DIPOLE SURVEY

THOMAS SHERATON PROPERTY

Date: 98/06/08

Interpretation: B. PATRIE AND D. PATRIE

DAN PATRIE EXPLOSION LTD.

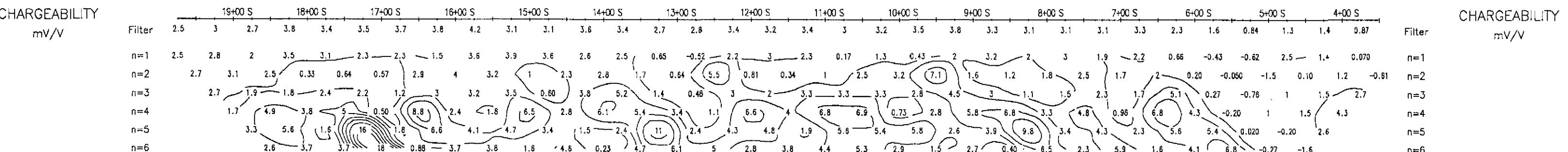
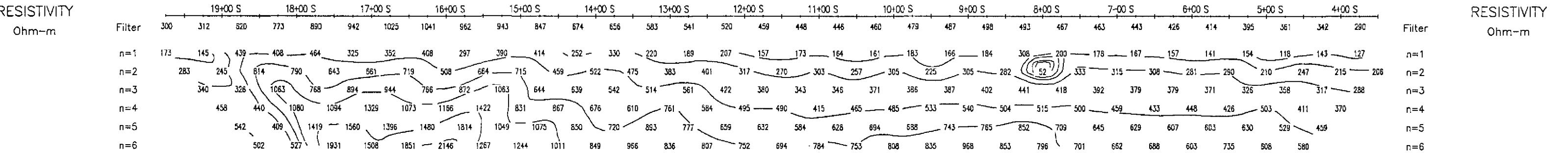


42A07NW2012 2.18926

SHERATON

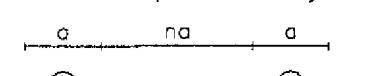
310

| METAL FACTOR | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 M | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S | 4+00 S | METAL FACTOR |     |
|--------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|--------------|-----|
| Filter       | 1       | 1.1     | 0.59    | 0.55    | 0.44    | 0.42    | 0.39    | 0.39    | 0.41    | 0.44    | 0.61   | 0.56   | 0.43   | 0.45   | 0.70   | 0.84   | Filter       |     |
| n=1          | 1.5     | 1.9     | 0.46    | 0.85    | 0.67    | 0.72    | 0.65    | 0.38    | 1.2     | 1.00    | 0.88   | 1      | 0.77   | 0.30   | -0.28  | 1.1    | 1.3          | n=1 |
| n=2          | 0.95    | 1.3     | 0.30    | 0.40    | 0.10    | 0.080   | 0.40    | 0.79    | 0.49    | 0.15    | 0.50   | 0.53   | 0.36   | 0.17   | 1.4    | 0.26   | 0.13         | n=2 |
| n=3          | 0.79    | 0.57    | 0.17    | 0.31    | 0.24    | 0.12    | 0.39    | 0.37    | 0.33    | 0.090   | 0.59   | 0.96   | 0.27   | 0.090  | 0.70   | 0.53   | 0.97         | n=3 |
| n=4          | 0.36    | 1.1     | 0.35    | 0.46    | 0.040   | 0.82    | 0.21    | 0.13    | 0.79    | 0.32    | 0.91   | 0.88   | 0.45   | 0.19   | 1.3    | 0.82   | 1.6          | n=4 |
| n=5          | 0.61    | 1.4     | 0.11    | 1       | 0.13    | 0.44    | 0.22    | 0.44    | 0.32    | 0.18    | 0.33   | 1.2    | 0.31   | 0.65   | 0.75   | 0.33   | 0.90         | n=5 |
| n=6          | 0.51    | 0.69    | 0.19    | 1.2     | 0.050   | 0.17    | 0.30    | 0.13    | 0.45    | 0.030   | 0.49   | 0.73   | 0.62   | 0.38   | 0.54   | 0.57   | 0.70         | n=6 |

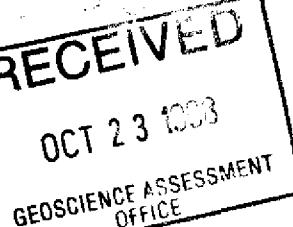


## Line 103 E

Pole-Dipole Array



Filter  
\* \* \* \* \*  
a = 50.0 M  
plot point

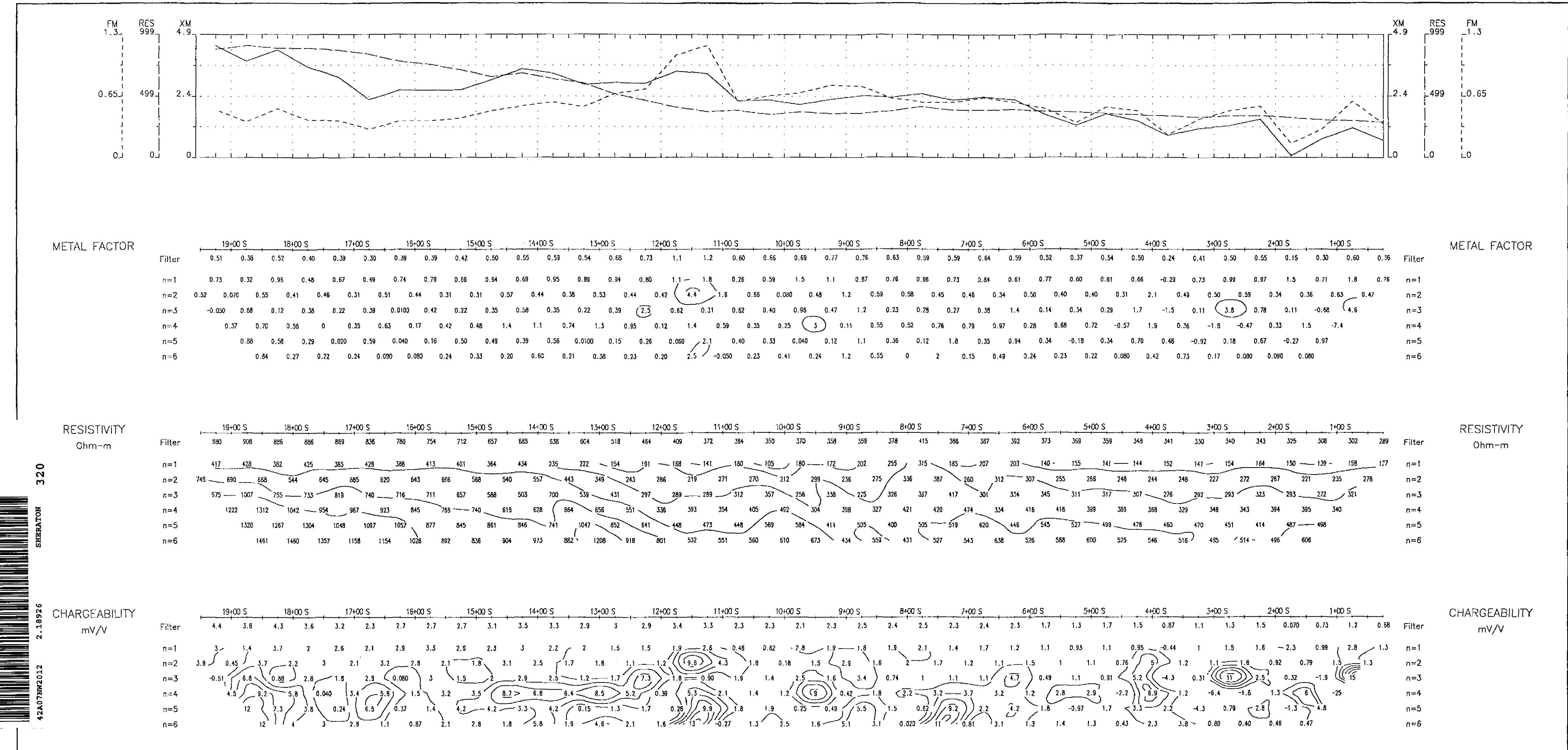


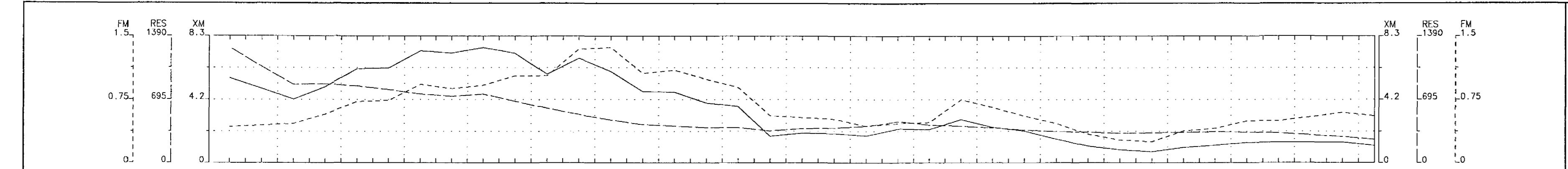
## INTERPRETATION

- Strong increase in polarization accompanied by marked decrease in resistivity.
- Well defined increase in polarization without marked resistivity decrease.
- Poorly defined polarization increase with no resistivity signature.
- ▼ Low resistivity feature.

Scale 1:5000  
50 0 50 100 150 200 250 300  
(metres)

MAPLE MINERALS INC.  
INDUCED POLARIZATION SURVEY  
POLE-DIPOLE SURVEY  
THOMAS SHERATON PROPERTY  
Date: 98/06/08  
Interpretation: B.PATRIE AND D.PATRIE  
DAN PATRIE EXPLOSION LTD.





Line 105 E

Pole-Dipole Array

$a$  na  $a$

Filter

\* \*

\* \* \*

\* \* \* \*

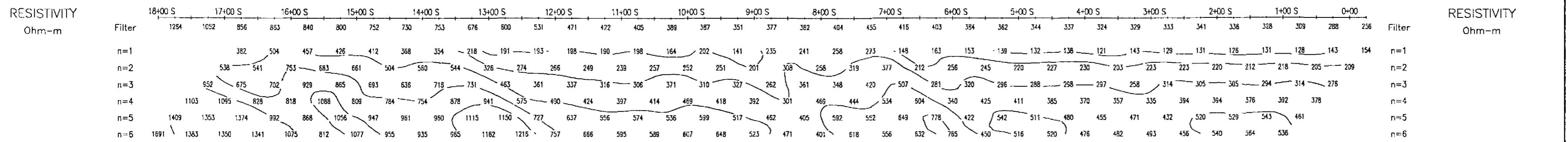
plot point

2

6

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OCT 23 1998  
LOGARITHMIC  
GEOSCIENCE ASSESSMENT  
OFFICE  
Contours 1, 1.5, 2, 3, 5, 7.5, 10,..

| METAL FACTOR | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S | 4+00 S | 3+00 S | 2+00 S | 1+00 S | 0+00 | METAL FACTOR |        |
|--------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------------|--------|
| Filter       | 0.43    | 0.45    | 0.47    | 0.58    | 0.73    | 0.74    | 0.93    | 0.88    | 0.92    | 1      | 1.4    | 1.1    | 0.99   | 0.89   | 0.56   | 0.54   | 0.52   | 0.44   | 0.47 | 0.42         | Filter |
| n=1          |         |         |         |         |         |         |         |         |         |        |        |        |        |        |        |        |        |        |      | n=1          |        |
| n=2          |         |         |         |         |         |         |         |         |         |        |        |        |        |        |        |        |        |        |      | n=2          |        |
| n=3          |         |         |         |         |         |         |         |         |         |        |        |        |        |        |        |        |        |        |      | n=3          |        |
| n=4          |         |         |         |         |         |         |         |         |         |        |        |        |        |        |        |        |        |        |      | n=4          |        |
| n=5          |         |         |         |         |         |         |         |         |         |        |        |        |        |        |        |        |        |        |      | n=5          |        |
| n=6          |         |         |         |         |         |         |         |         |         |        |        |        |        |        |        |        |        |        |      | n=6          |        |

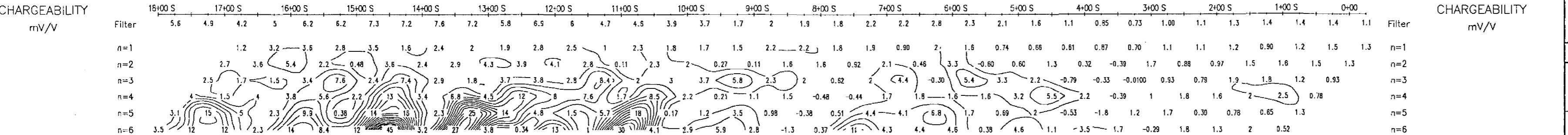


### INTERPRETATION

- Strong increase in polarization accompanied by marked decrease in resistivity.
- Well defined increase in polarization without marked resistivity decrease.
- Poorly defined polarization increase with no resistivity signature.
- ▼ Low resistivity feature.

Scale 1:5000

50 0 50 100 150 200 250 300  
(metres)



MAPLE MINERALS INC.

INDUCED POLARIZATION SURVEY

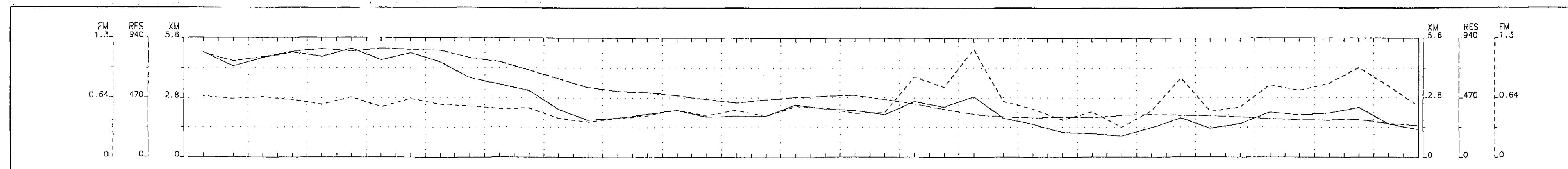
POLE-DIPOLE SURVEY

THOMAS\SHERATON PROPERTY

Date: 98/06/08

Interpretation: B. PATRIE AND D. PATRIE

DAN PATRIE EXPLOSION LTD.



| METAL FACTOR | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S | 4+00 S | 3+00 S | 2+00 S | 1+00 S | 0+00 | 1+00 N | METAL FACTOR |       |      |
|--------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|--------------|-------|------|
| Filter       | 0.66    | 0.63    | 0.65    | 0.62    | 0.57    | 0.65    | 0.54    | 0.63    | 0.57    | 0.55    | 0.52   | 0.42   | 0.39   | 0.42   | 0.45   | 0.51   | 0.44   | 0.53   | 0.68   | 0.71 | 0.75   | 1.1          | 0.65  |      |
| n=1          | 0.74    | 0.86    | 0.98    | 0.77    | 0.77    | 1.2     | 0.60    | 0.99    | 0.98    | 1.1     | 0.53   | 0.68   | 0.71   | 0.75   | 0.76   | 1.1    | 0.65   | 0.38   | 0.88   | 1.3  | 0.66   | 0.85         | ~2.5  | 0.84 |
| n=2          | 0.90    | 0.83    | 0.54    | 0.74    | 0.73    | 0.42    | 0.63    | 0.83    | 0.82    | 0.32    | 0.41   | 1.3    | 0.55   | 0.42   | 0.39   | 0.40   | 0.54   | 0.32   | 0.41   | 0.55 | 0.69   | 0.48         | 0.49  | 0.50 |
| n=3          | 0.41    | 0.57    | 0.50    | 0.63    | 0.47    | 0.31    | 0.46    | 0.72    | 0.53    | 0.52    | 0.84   | 0.72   | 0.080  | 0.58   | 0.35   | 0.65   | 0.44   | 0.40   | 0.74   | 0.61 | 0.53   | 1.1          | 0.070 | 0.71 |
| n=4          | 0.47    | 0.68    | 0.57    | 0.55    | 0.43    | 0.60    | 0.57    | 0.45    | 0.42    | 0.71    | 0.74   | 0.57   | 0.28   | 0.26   | 0.59   | 0.30   | 0.51   | 0.39   | 0.83   | 0.23 | 0.57   | 0.51         | 1.1   | 0.49 |
| n=5          | 0.21    | 0.17    | 0.67    | 0.54    | 0.47    | 0.24    | 0.67    | 0.28    | 0.38    | 0.41    | 0.17   | 0.23   | 0.27   | 0.15   | 0.40   | 0.35   | 0.58   | 0.18   | 0.060  | 0.15 | 0.42   | 0.52         | 0.69  | 0.34 |
| n=6          | 0.32    | 1.4     | 0.48    | 0.57    | 0.89    | 0.39    | 0.25    | 0.090   | 0.25    | 0.16    | 0.10   | -0.020 | 0.39   | 0.21   | 0.18   | 0.40   | 0.35   | 0.22   | -0.13  | 0.18 | 0.42   | 0.45         | 0.36  | 0.40 |

| RESISTIVITY | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S | 4+00 S | 3+00 S | 2+00 S | 1+00 S | 0+00 | 1+00 N | RESISTIVITY |     |     |
|-------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|-------------|-----|-----|
| Filter      | 821     | 756     | 789     | 832     | 853     | 834     | 855     | 847     | 840     | 783     | 753    | 688    | 522    | 554    | 523    | 513    | 488    | 458    | 475    | 484  | 455    | 420         | 378 | 338 |
| n=1         | 368     | ~269    | 379     | 475     | 476     | 453     | 525     | 456     | 503     | 379     | 357    | 272    | 257    | 276    | 296    | 221    | 226    | 325    | 355    | 297  | 251    | 178         | 156 | 153 |
| n=2         | 712     | 566     | 425     | 548     | 680     | 677     | 663     | 768     | 725     | 670     | 577    | 509    | 426    | 342    | 354    | 413    | 378    | 350    | 371    | 442  | 428    | 349         | 251 | 240 |
| n=3         | 973     | 809     | 542     | 759     | 771     | 823     | 762     | 885     | 739     | 694     | 644    | 633    | 476    | 412    | 403    | 441    | 476    | 425    | 377    | 326  | 455    | 445         | 425 | 352 |
| n=4         | 1231    | 1119    | 735     | 808     | 889     | 1003    | 893     | 754     | 847     | 842     | 796    | 752    | 603    | 507    | 501    | 528    | 582    | 498    | 451    | 379  | 539    | 542         | 565 | 557 |
| n=5         | 1444    | 1199    | 957     | 1131    | 1129    | 1197    | 1138    | 1045    | 1061    | 1229    | 1010   | 946    | 723    | 600    | 604    | 624    | 663    | 549    | 451    | 421  | 605    | 652         | 713 | 651 |
| n=6         | 1660    | 1250    | 917     | 1136    | 1146    | 1104    | 1007    | 1071    | 1157    | 1163    | 1096   | 1058   | 833    | 711    | 689    | 702    | 567    | 513    | 467    | 718  | 821    | 817         | 737 | 606 |

| CHARGEABILITY | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S | 4+00 S | 3+00 S | 2+00 S | 1+00 S | 0+00 | 1+00 N | CHARGEABILITY |      |       |
|---------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|---------------|------|-------|
| Filter        | 4.9     | 4.3     | 4.7     | 4.9     | 4.7     | 5.1     | 4.6     | 4.9     | 4.5     | 3.7     | 3.4    | 2.3    | 1.8    | 1.9    | 2      | 2.2    | 1.9    | 2.5    | 2.3    | 2.2  | 2.4    | 2.6           | 2.9  | 1.5   |
| n=1           | 2.7     | 2.3     | 3.7     | 3.7     | 3.7     | 5.3     | 3.2     | 4.5     | 4.9     | 4.2     | 1.9    | 1.8    | 2.1    | 2.3    | 1.4    | 2.2    | 1.3    | 3.1    | 3.7    | 1.6  | 1.3    | 3.9           | 1.2  | 1.2   |
| n=2           | 6.4     | 4.7     | 2.3     | 4.1     | 5       | 2.8     | 4.2     | 6.4     | 5.9     | 2.1     | 2.4    | 1.4    | 1.5    | 1.2    | 1.5    | 2      | 3      | 2.1    | 1.7    | 1    | 2.2    | 2.7           | 0.78 | 0.64  |
| n=3           | 4       | 4.6     | 2.7     | 4.8     | 3.6     | 2.6     | 3.5     | 6.3     | 3.9     | 3.6     | 5.4    | 4.6    | 0.39   | 2.4    | 1.4    | 2.9    | 2.8    | 2.8    | 2.3    | 1.7  | 1      | 2.1           | 1.7  | 1.3   |
| n=4           | 5.7     | 7.6     | 4.2     | 4.4     | 3.8     | 6       | 5.1     | 3.4     | 3.6     | 6       | 5.9    | 4.3    | 1.7    | 2.1    | 1.6    | 2      | 2.8    | 3.2    | 3.8    | 3.6  | 1.6    | 1.6           | 0.41 | 0.050 |
| n=5           | 3       | 2       | 5.4     | 6.1     | 5.3     | 2.9     | 9.9     | 2.9     | 4.1     | 5       | 2.4    | 1.7    | 2.2    | 1.9    | 1.5    | 2.3    | 3.2    | 3.3    | 2.7    | 2.8  | 1.7    | 1.3           | 1.6  | 0.47  |
| n=6           | 5.4     | 17      | 4.4     | 6.5     | 10      | 4.3     | 2.5     | 0.98    | 2.8     | 1.9     | 1.1    | -0.21  | 3.3    | 1.5    | 1.2    | 2.8    | 2.7    | 2.7    | 1.7    | 0.84 | 1.8    | 1.9           | 2.1  | 0.20  |

Line 106 E

Pole-Dipole Array

a na a

Filter

\* \*

\* \* \*

\* \* \* \*

plot point

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OCT 23 1998

GEOSCIENCE ASSESSMENT OFFICE

INTERPRETATION

Strong increase in polarization accompanied by marked decrease in resistivity.

Well defined increase in polarization without marked resistivity decrease.

Poorly defined polarization increase with no resistivity signature.

Low resistivity feature.

Scale 1:5000

50 0 50 100 150 200 250 300

(metres)

MAPLE MINERALS INC.

INDUCED POLARIZATION SURVEY

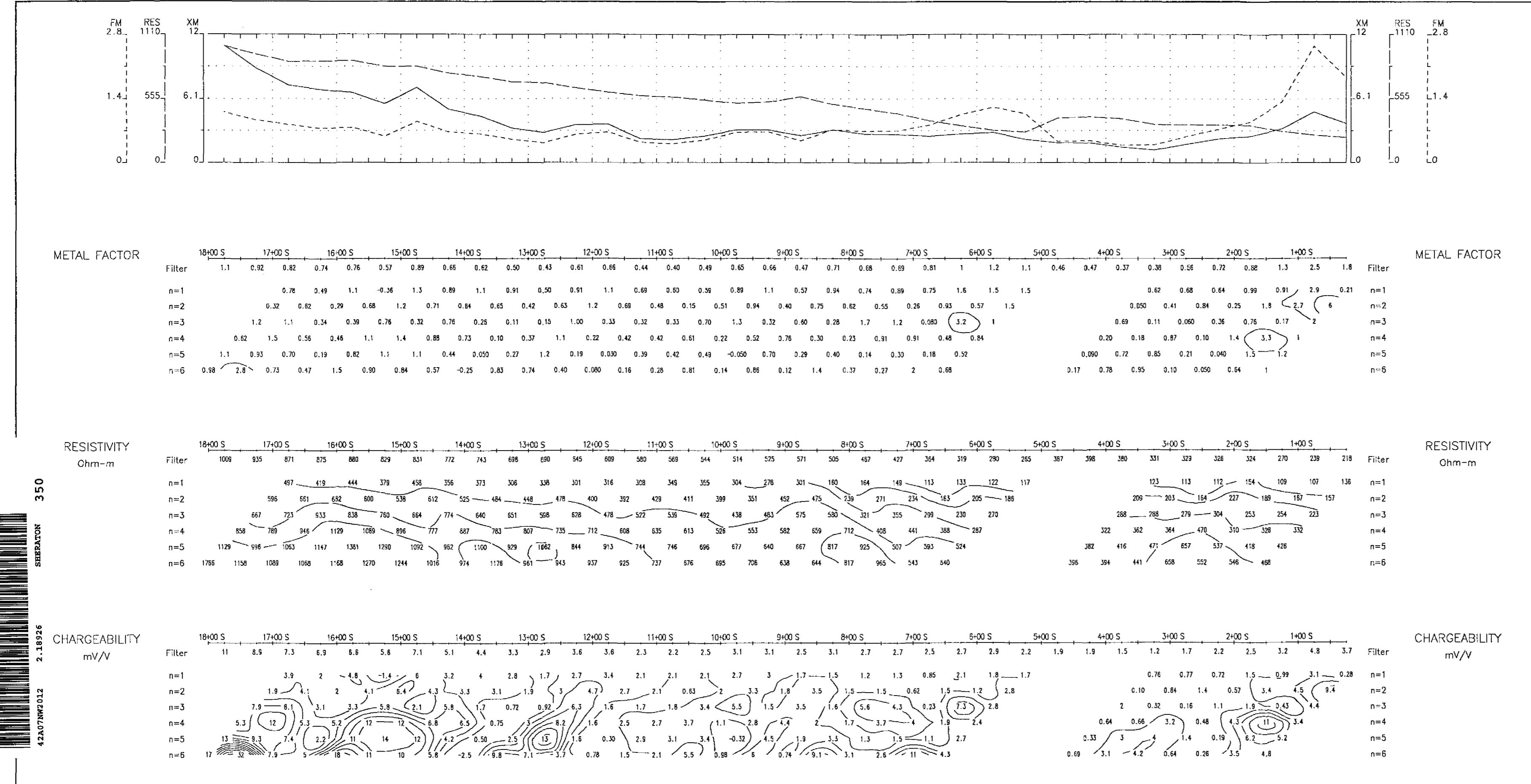
POLE-DIPOLE SURVEY

THOMAS-SHERATON PROPERTY

Date: 98/06/08

Interpretation: B.PATRIE AND D.PATRIE

DAN PATRIE EXPLOSION LTD.



**Pole-Dipole Array**  

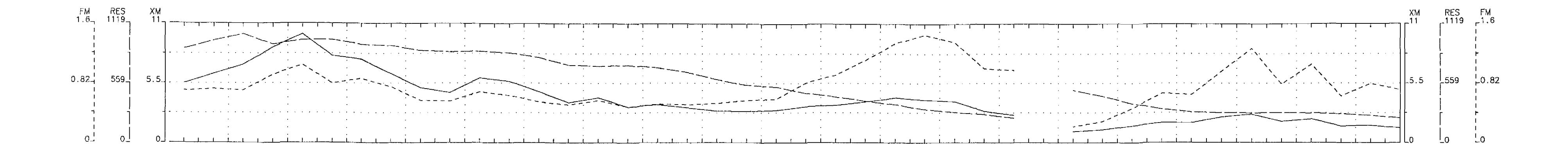
**RECEIVED**  
 OCT 23 1998  
 GEOSCIENCE ASSESSMENT  
 OFFICE

**INTERPRETATION**

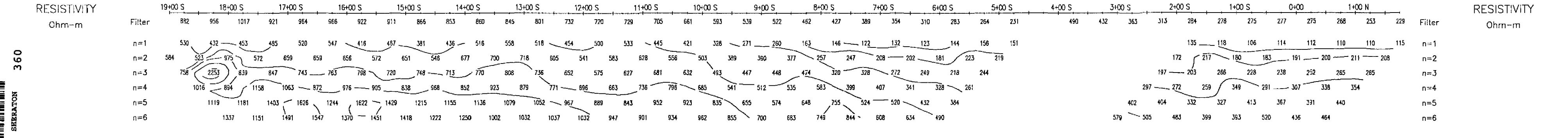
- Strong increase in polarization accompanied by marked decrease in resistivity.
- Well defined increase in polarization without marked resistivity decrease.
- Poorly defined polarization increase with no resistivity signature.
- ▼ Low resistivity feature.

Scale 1:5000  
 50 0 50 100 150 200 250 300 (metres)

**MAPLE MINERALS INC.**  
**INDUCED POLARIZATION SURVEY**  
**POLE-DIPOLE SURVEY**  
**THOMAS SHERATON PROPERTY**  
 Date: 98/06/08  
 Interpretation: B.PATRIE AND D.PATRIE  
**DAN PATRIE EXPLOSION LTD.**



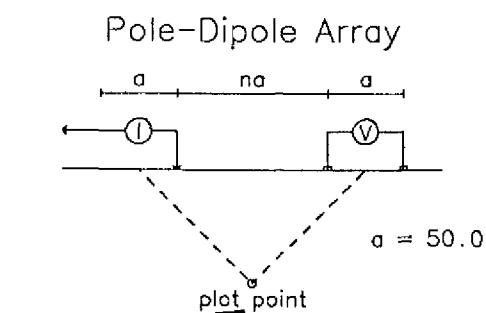
| METAL FACTOR | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S | 4+00 S | 3+00 S | 2+00 S | 1+00 S | 0+00 | 1+00 N | METAL FACTOR |      |      |      |      |        |      |      |      |       |      |       |      |      |      |      |      |      |                      |        |
|--------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|--------------|------|------|------|------|--------|------|------|------|-------|------|-------|------|------|------|------|------|------|----------------------|--------|
| Filter       | 0.72    | 0.74    | 0.72    | 0.94    | 1.1     | 0.82    | 0.89    | 0.77    | 0.58    | 0.57    | 0.70   | 0.65   | 0.56   | 0.62   | 0.58   | 0.49   | 0.53   | 0.52   | 0.54   | 0.58 | 0.60   | 0.53         | 0.94 | 1.1  | 1.4  | 1.5  | 1.4    | 1    | 0.22 | 0.29 | 0.47  | 0.68 | 0.66  | 0.99 | 1.3  | 0.81 | 1.1  | 0.64 | 0.82 | 0.73 <th>Filter</th> | Filter |
| n=1          | 1.1     | 1.2     | 0.57    | 0.71    | 1.1     | 0.64    | 1.2     | 1.3     | 0.56    | 1       | 0.72   | 0.50   | 0.62   | 0.80   | 0.77   | 0.63   | 0.68   | 0.57   | 0.70   | 0.66 | 0.57   | 1.2          | 1.2  | 1.4  | 1.7  | 1.7  | 1.1    | 0.71 | 0.79 | 0.58 | 1.7   | 3.9  | 1.5   | 3    | 0.94 | 1.5  | 1    | n=1  |      |                      |        |
| n=2          | 0.81    | 0.58    | 0.50    | 0.88    | 0.88    | 0.81    | 0.10    | 0.97    | 0.79    | 0.27    | 0.060  | 1.2    | 0.16   | 0.22   | 0.29   | 0.49   | 0.51   | 0.72   | 0.58   | 0.74 | 0.73   | 0.71         | 1.3  | 1.4  | 2.1  | 1.7  | 2.2    | 0.52 | 0.62 | 1.2  | 0.070 | 1.6  | 0.050 | 1.5  | 0.53 | 0.82 | 0.59 | n=2  |      |                      |        |
| n=3          | 0.30    | 0.26    | 0.38    | 1.3     | 0.32    | 1.4     | 0.070   | 0.46    | 0.89    | 0.72    | 0.45   | 1.4    | 0.25   | 0.52   | 0.53   | 0.66   | 0.35   | 0.76   | 0.56   | 0.44 | 0.72   | 0.71         | 1.1  | 1.4  | 0.83 | 2.6  | 2.1    | 1.2  | 0.10 | 0.54 | 1.00  | 1.7  | 0.48  | 0.40 | 1.3  | 0.61 | n=3  |      |      |                      |        |
| n=4          | 0.82    | 0.62    | 1.5     | 0.60    | 4       | 1.2     | 0.88    | 0.070   | 0.40    | 0.71    | 0.57   | 0.76   | 0.35   | 1.1    | 0.70   | 1.1    | 0.37   | 0.86   | 0.26   | 0.78 | 0.48   | 0.53         | 1.4  | 0.39 | 1.7  | 0.65 | 1.8    | 0.43 | 1.6  | 1.3  | 1.1   | 0.59 | 0.44  | 0.11 | 0.41 | n=4  |      |      |      |                      |        |
| n=5          | 0.020   | 0.93    | 0.61    | 1.2     | 1.3     | 0.72    | 0.27    | 0.34    | 0.73    | 1       | 0.13   | 1.8    | 0.25   | 0.020  | 0.58   | 0.040  | 0.090  | 0.40   | 0.49   | 0.58 | 0.63   | 0.94         | 0.41 | 1.1  | 1.8  | 1.9  | 0.38   | 0.17 | 0.89 | 0.94 | 1.2   | 0.87 | 0.15  | 0.42 | n=5  |      |      |      |      |                      |        |
| n=6          | 0.13    | 1.7     | 1.1     | 0.71    | 0.86    | 0.10    | 0.21    | 0.81    | 1.4     | 0.090   | 1.2    | 0.0100 | 0.53   | 0.030  | 0.27   | 0.54   | 0.23   | 0.43   | 0.54   | 0.38 | 0.62   | 0.54         | 0.59 | 0.88 | 0.92 | 0.25 | 0.0100 | 0.45 | 0.21 | 0.67 | 0.72  | 0.14 | 0.33  | n=6  |      |      |      |      |      |                      |        |



CHARGEABILITY

|      | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S | 4+00 S | 3+00 S | 2+00 S | 1+00 S | 0+00 | 1+00 N | CHARGEABILITY |     |     |     |     |     |       |      |      |     |      |      |      |     |      |     |     |     |     |        |      |
|------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|---------------|-----|-----|-----|-----|-----|-------|------|------|-----|------|------|------|-----|------|-----|-----|-----|-----|--------|------|
| mV/V | Filter  | 5.5     | 6.4     | 7.2     | 8.8     | 10      | 8.1     | 7.8     | 6.4     | 5.1     | 4.6    | 6      | 5.7    | 4.7    | 3.7    | 4.2    | 3.3    | 3.5    | 3.2    | 2.9  | 3      | 3.3           | 3.5 | 3.8 | 4.2 | 3.9 | 3.6 | 2.9   | 2.5  | 1    | 1.2 | 1.5  | 1.8  | 2.3  | 2.6 | 1.9  | 2.2 | 1.5 | 1.6 | 1.4 | Filter | mV/V |
| n=1  |         | 5.6     | 5.3     | 2.6     | 3.4     | 5.9     | 3.5     | 5.1     | 5.9     | 2.1     | 4.4    | 3.7    | 2.8    | 3.2    | 3.6    | 3.8    | 3.3    | 3      | 2.4    | 2.3  | 1.8    | 1.7           | 2   | 1.8 | 1.7 | 2.3 | 2.1 | ~1.6  | 1.1  | 1.2  |     | 0.78 | 2    | 4.1  | 1.7 | 3.3  | 1   | 1.7 | 1.2 | n=1 |        |      |
| n=2  |         | 4.8     | 3       | 4.9     | 5.1     | 5.8     | 5.3     | 0.67    | 5.5     | 5.2     | 1.5    | 0.39   | 8.2    | 1.2    | 1.4    | 1.6    | 2.9    | 3.2    | 4      | 2.9  | 2.8    | 2.7           | 3.3 | 3.4 | 4.3 | 3.5 | 3.9 | 1.1   | 1.4  |      | 2.1 | 0.15 | 2.8  | 0.10 | 2.9 | 1.1  | 1.7 | 1.2 | n=2 |     |        |      |
| n=3  |         | 2.3     | 5.9     | 3.2     | 11      | 2.4     | 10      | 0.57    | 3.3     | 6.7     | >5.2   | 3.5    | 11     | 3.4    | 3      | 4.1    | 2.3    | 4.8    | 2.8    | 2    | 3.2    | 3.4           | 3.6 | 4.7 | 2.3 | 6.6 | 4.5 | 2.8   |      | 0.20 | 1.1 | 2.7  | 3.8  | 1.1  | 1   | 3.4  | 1.6 | n=3 |     |     |        |      |
| n=4  |         | 8.3     | 5.5     | 17      | 6.4     | 35      | 11      | 7.9     | 0.58    | 3.8     | 6      | 5.3    | 6.7    | 2.7    | 7.3    | 1.83   | 3      | 1.4    | 5.9    | 4    | 2.6    | 3.1           | 5.4 | 1.6 | 5.7 | 5.9 | 2.2 | 4.8   |      | 1.3  | 4.4 | 3.4  | 3.9  | 1.7  | 1.4 | 0.37 | 1.5 | n=4 |     |     |        |      |
| n=5  |         | 0.25    | 11      | 8.5     | 20      | 16      | 12      | 3.9     | 4.1     | 8.4     | 12     | 1.4    | 19     | 2.4    | 0.18   | 4.9    | 0.39   | 0.79   | 3.3    | 3.2  | 4.1    | 7.1           | 2.2 | 5.6 | 7.9 | 7.4 |     | 1.5   | 0.88 | 3    | 3.1 | 5    | 3.2  | 0.60 | 1.9 |      | n=5 |     |     |     |        |      |
| n=6  |         | 1.8     | 20      | 16      | 11      | 12      | 1.5     | 3       | 9.9     | 12      | 0.89   | 0.15   | 5.5    | 0.27   | 2.4    | -5-    | 2.2    | 3.7    | 3.8    | 2.6  | 4.7    | 4.5           | 3.6 | 5.6 | 4.5 |     | 1.5 | 0.070 | 2.2  | 0.85 | 2.6 | 3.8  | 0.61 | 1.5  |     | n=6  |     |     |     |     |        |      |

Line 108 ■



RECEIVED

OCT 23 1998

**SCIENCE ASSESSMENT**

rithmic  
ours 1, 1.5, 2, 3, 5, 7.5, 10, ...

INTERPRETATIO

- Strong increase in polarization accompanied by marked decrease in resistivity.
  - Well defined increase in polarization without marked resistivity decrease.
  - Poorly defined polarization increase with no resistivity signature.
  - Low resistivity feature.

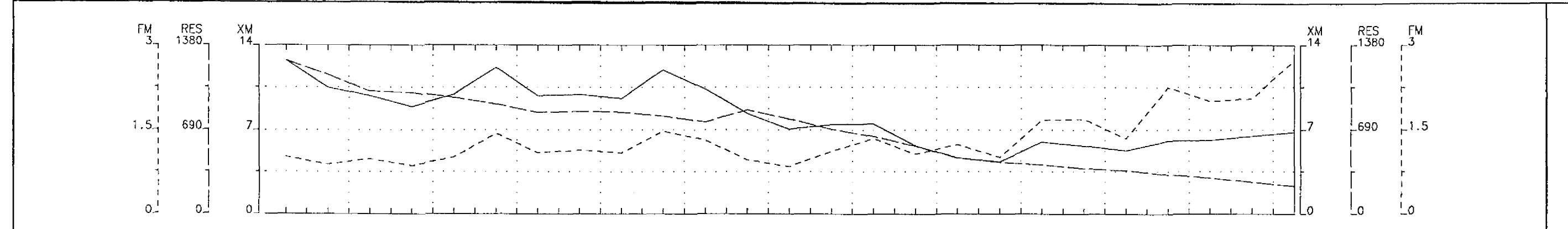
Scale 1:5000

(metres)

MAPLE MINERALS INC.  
CEDED POLARIZATION SURVEY  
POLE-DIPOLE SURVEY  
MASHERATON PROPERTY

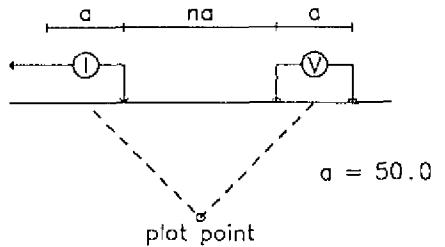
Date: 98/06/08

Interpretation: B. PATRIE AND D. PATRIE



Line 109 E

Pole-Dipole Array



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OCT 23 1993

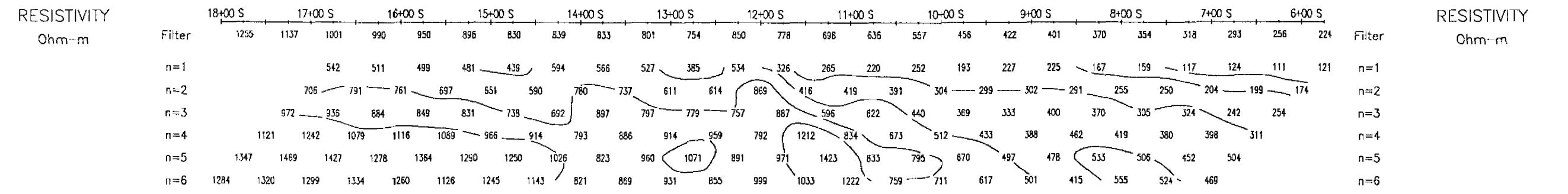
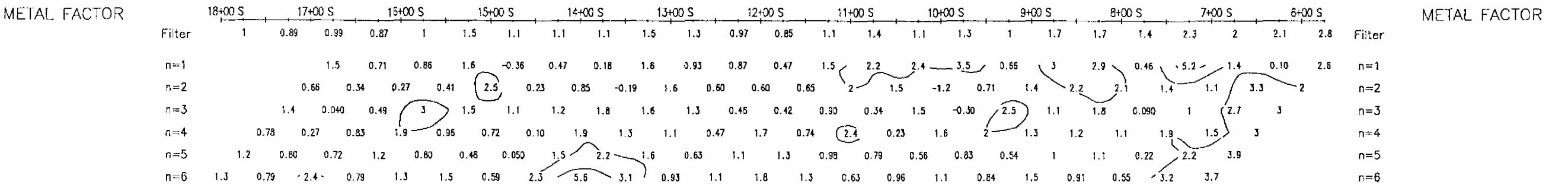
GEOSCIENCE ASSESSMENT  
OFFICE

Logarithmic  
Contours 1, 1.5, 2, 3, 5, 7.5, 10,..

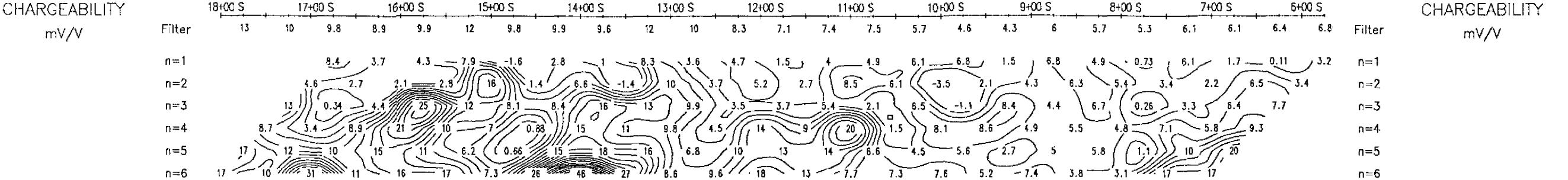
## 2 INTERPRETATION

- Strong increase in polarization accompanied by marked decrease in resistivity.
- Well defined increase in polarization without marked resistivity decrease.
- Poorly defined polarization increase with no resistivity signature.
- ▼ Low resistivity feature.

Scale 1:5000  
50 0 50 100 150 200 250 300  
(metres)



SHERATON



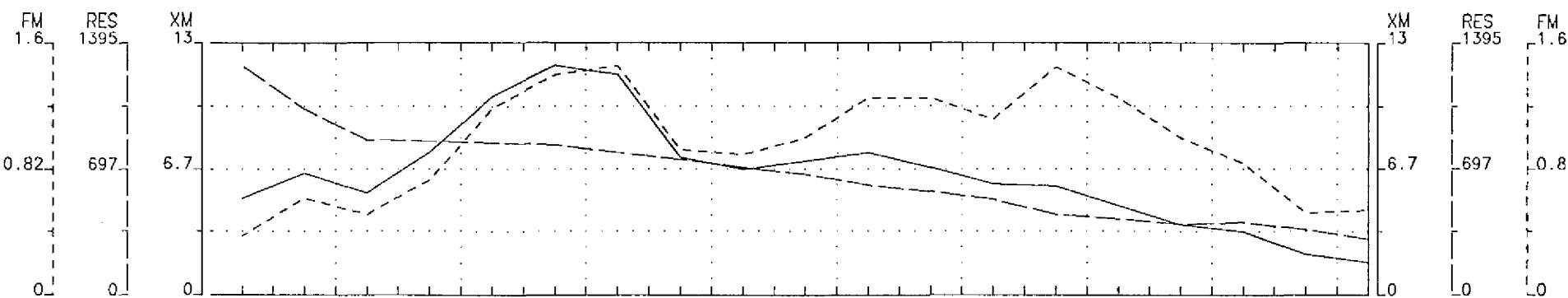
MAPLE MINERALS INC.

INDUCED POLARIZATION SURVEY  
POLE-DIPOLE SURVEY  
THOMAS\SHERATON PROPERTY

Date: 98/06/08

Interpretation: B. PATRIE AND D. PATRIE

DAN PATRIE EXPLOSION LTD.



42A07NW2012

2.18926

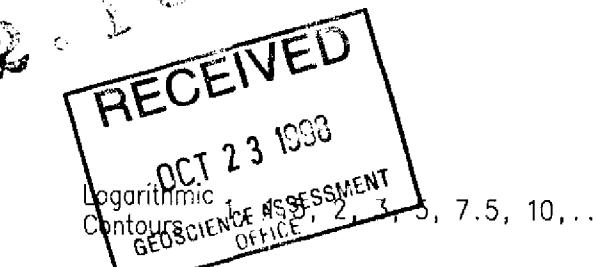
SHERATON

380

### METAL FACTOR

| Filter | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | Filter |
|--------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|
| n=1    | 0.38    | 0.63    | 0.52    | 0.75    | 1.2     | 1.4     | 1.5     | 0.95   | 0.92   | 1      | n=1    |
| n=2    | 0.85    | -0.31   | 1       | 1.1     | 1.8     | -0.13   | 0.91    | 0.040  | -0.43  | 2.5    | n=2    |
| n=3    | -0.030  | -1.1    | -0.43   | 0.50    | 1.9     | 0.60    | -0.46   | 0.77   | 2.7    | 0.95   | n=3    |
| n=4    | 0.39    | 0.83    | 1.1     | 1.2     | 3.2     | 1       | 0.61    | 0.88   | 0.79   | 0.44   | n=4    |
| n=5    | 0.19    | 0.66    | -0.17   | 1.6     | 2.2     | 2.7     | 0.41    | 1.2    | 0.030  | 1.3    | n=5    |
| n=6    | 0.46    | 0.52    | 0.33    | 0.83    | 4.8     | 1.9     | 1.2     | 1      | 1.6    | 0.95   | n=6    |

### METAL FACTOR



### RESISTIVITY

Ohm-m

| Filter | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | Filter |
|--------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|
| n=1    | 355     | 465     | 444     | 442     | 431     | 413     | 414     | 390    | 329    | 305    | n=1    |
| n=2    | 439     | 589     | 579     | 808     | 641     | 682     | 574     | 559    | 501    | 373    | n=2    |
| n=3    | 857     | 678     | 697     | 202     | 868     | 811     | 724     | 607    | 595    | 531    | n=3    |
| n=4    | 991     | 1185    | 760     | 939     | 795     | 969     | 798     | 671    | 716    | 665    | n=4    |
| n=5    | 1514    | 1365    | 1275    | 1028    | 1032    | 1132    | 1084    | 885    | 909    | 778    | n=5    |
| n=6    | 1390    | 1689    | 1367    | 1542    | 938     | 1079    | 954     | 1095   | 957    | 884    | n=6    |

### RESISTIVITY

Ohm-m

Scale 1:5000  
50 0 50 100 150 200 250 300  
(metres)

### CHARGEABILITY

mV/V

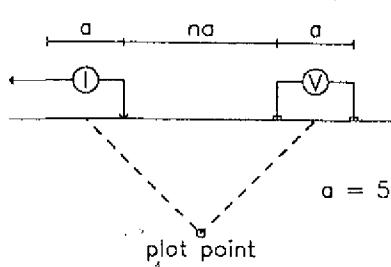
| Filter | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | Filter |
|--------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|
| n=1    | 5.1     | 6.5     | 5.4     | 7.6     | 11      | 12      | 7.3     | 6.7    | 7.1    | 7.6    | n=1    |
| n=2    | 0.53    | -0.29   | 4.2     | 5.3     | 9.8     | 5       | 4       | -5.4   | 5.6    | 3.7    | n=2    |
| n=3    | 3.7     | -1.8    | 6       | 9.1     | 12      | -0.89   | 5.2     | 0.21   | -2.2   | 9.1    | n=3    |
| n=4    | -0.25   | -7.4    | -3      | 4       | 11      | 4.9     | -3.3    | 4.7    | 5.6    | 3.3    | n=4    |
| n=5    | 3.9     | 9.9     | -8.4    | 11      | 25      | 10      | 4.9     | 6.9    | 5.3    | 7      | n=5    |
| n=6    | 2.8     | 9       | -2.2    | 16      | 23      | 30      | 4.4     | 10     | 19     | 0.25   | n=6    |

### CHARGEABILITY

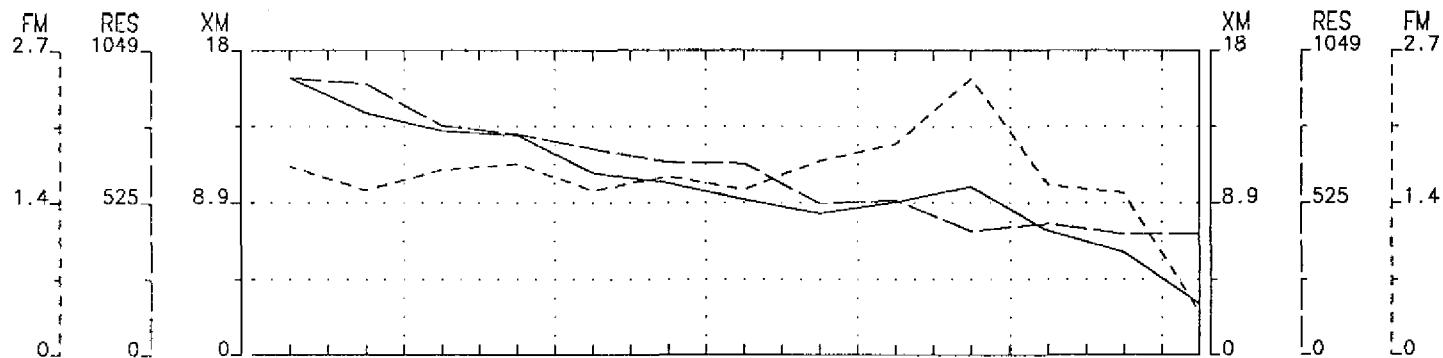
mV/V

Line 110 E

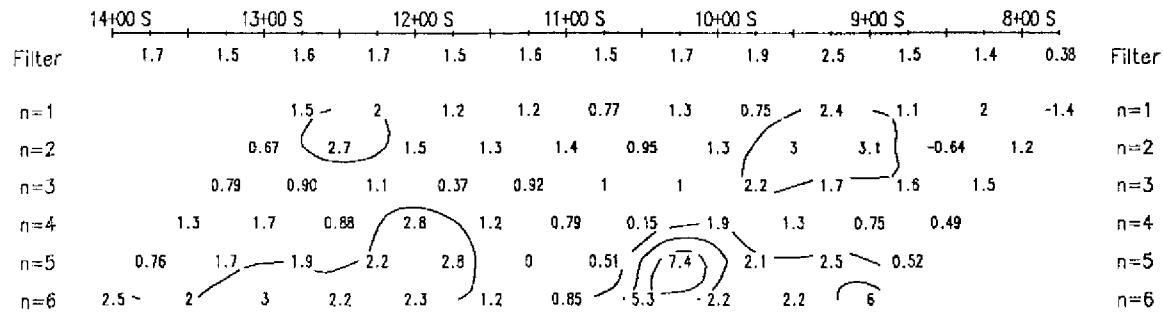
Pole-Dipole Array



MAPLE MINERALS INC.  
INDUCED POLARIZATION SURVEY  
POLE-DIPOLE SURVEY  
THOMAS\SHERATON PROPERTY  
Date: 98/06/08  
Interpretation: B.PATRIE AND D.PATRIE  
DAN PATRIE EXPLOSION LTD.



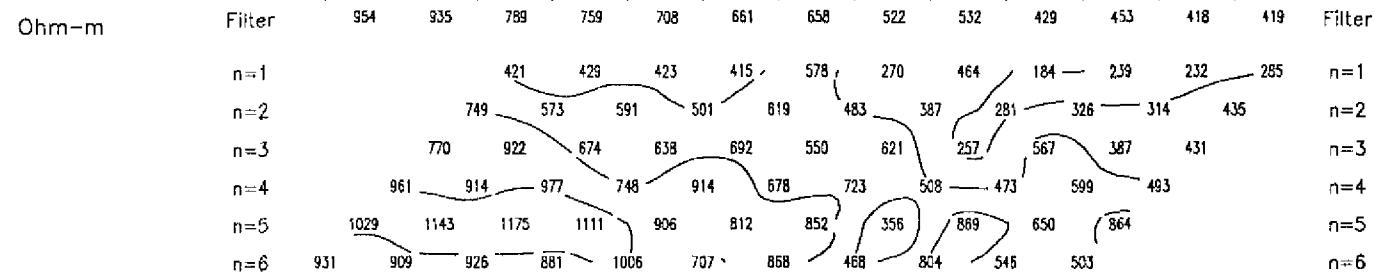
### METAL FACTOR



### METAL FACTOR

42107NMW2012 2.18926 SHERATON 390

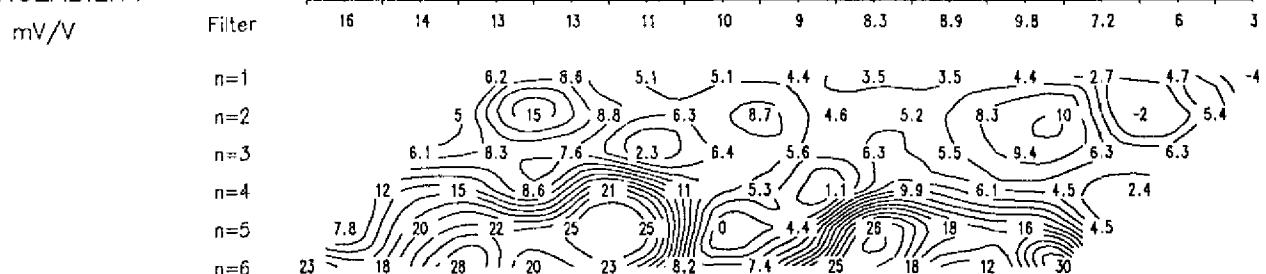
### RESISTIVITY



### RESISTIVITY

SHERATON 390

### CHARGEABILITY

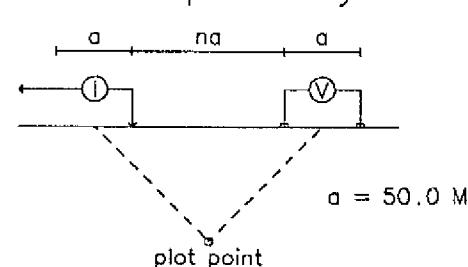


### CHARGEABILITY

mV/V

## Line 111 E

### Pole-Dipole Array



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OCT 23 1993  
1, GEOFISICS, 2, OFFICE

Logarithmic Contours 1, 5, 7.5, 10,..

### INTERPRETATION

- Strong increase in polarization accompanied by marked decrease in resistivity.
- Well defined increase in polarization without marked resistivity decrease.
- Poorly defined polarization increase with no resistivity signature.
- ▼ Low resistivity feature.

Scale 1:5000

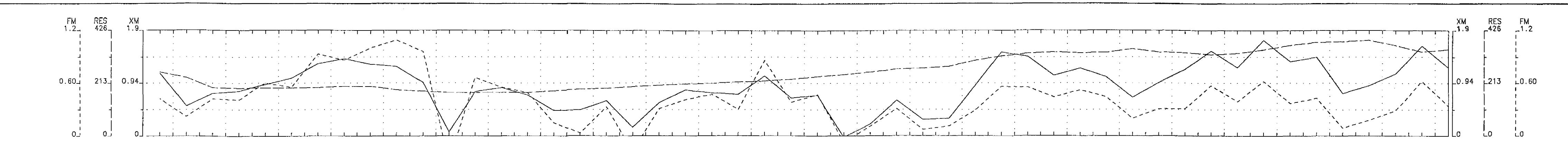
50 0 50 100 150 200 250 300  
(metres)

MAPLE MINERALS INC.

INDUCED POLARIZATION SURVEY  
POLE-DIPOLE SURVEY  
THOMAS SHERATON PROPERTY

Date: 98/06/08  
Interpretation: B. PATRIE AND D. PATRIE

DAN PATRIE EXPLOSION LTD.



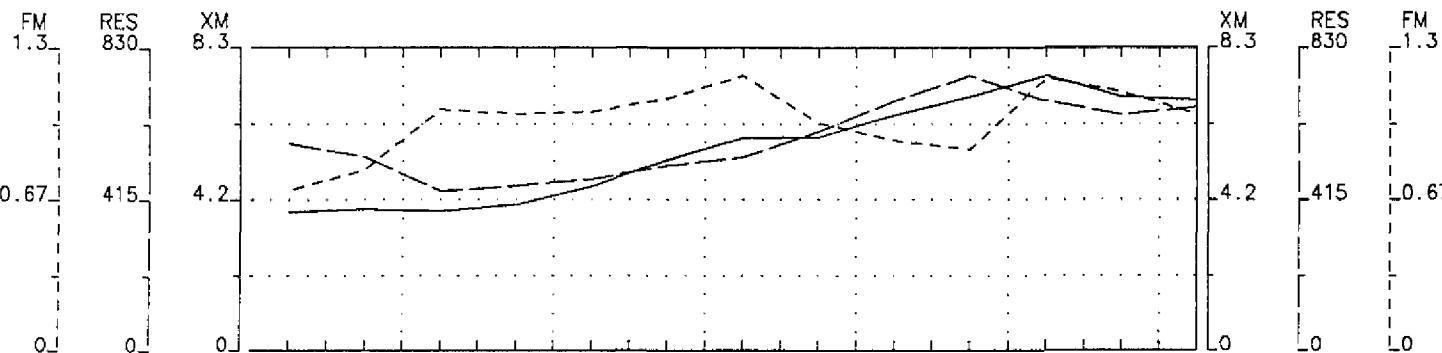
42A07NW2012 2.18926 SHERATON 400

| MATAL FACTOR | Filter  |         |         |         |         |         |         |         |         |         |         |         |         |         |         |        |        |         |        |        |        |        |        |        |        | Filter |       |       |       |       |      |      |       |       |      |       |       |      |      |       |        |      |      |      |       |       |      |        |
|--------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|---------|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|-------|-------|------|------|-------|-------|------|-------|-------|------|------|-------|--------|------|------|------|-------|-------|------|--------|
|              | 24+00 S | 23+00 S | 22+00 S | 21+00 S | 20+00 S | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S  | 6+00 S | 5+00 S | 4+00 S | 3+00 S | 2+00 S | 1+00 S | 0+00   |        |       |       |       |       |      |      |       |       |      |       |       |      |      |       |        |      |      |      |       |       |      |        |
| n=1          | 0.42    | 0.22    | 0.42    | 0.41    | 0.60    | 0.55    | 0.93    | 0.86    | 1.00    | 1.1     | 0.96    | 0.23    | 0.66    | 0.55    | 0.49    | 0.15   | 0.030  | 0.33    | 0.41   | 0.47   | 0.30   | 0.31   | 0.86   | 0.47   | -0.070 | 0.11   | 0.31  | 0.070 | 0.11  | 0.29  | 0.56 | 0.55 | 0.44  | 0.20  | 0.31 | 0.57  | 0.39  | 0.62 | 0.37 | 0.43  | -0.090 | 0.18 | 0.29 | 0.62 | 0.34  |       |      |        |
| n=2          | 0.16    | 0.68    | -0.59   | 0.48    | 1.1     | 1.1     | 1.3     | 0.79    | 3.3     | -0.030  | 1       | 1.8     | 0.99    | 0.19    | -0.26   | 0.65   | -0.28  | -0.38   | -0.27  | 0.93   | 0.73   | 3.1    | 0.70   | 0.88   | 0.95   | -0.46  | 1.8   | 0.49  | -0.17 | 0.40  | 0.54 | 1.1  | 0.52  | 0.70  | 0.99 | -0.45 | -0.70 | 0.61 | 1.1  | 0     | 0.74   | 0.75 | 0.65 | 0.57 | -0.35 | 0.23  | 1.1  | -0.030 |
| n=3          | 0.74    | 0.42    | 1.4     | 0.23    | -0.70   | 0.56    | 0.44    | 0.56    | 0.19    | 0.91    | -0.070  | 1       | 0       | 1.5     | 0.91    | 1.1    | 0.060  | -0.0100 | 0.53   | 1      | 0.13   | -1.6   | 1.5    | 0.20   | -0.090 | -0.34  | -0.21 | 0.45  | -0.16 | -0.45 | 0.57 | 0.91 | 0.19  | 0.71  | 0.83 | 0.59  | -0.45 | 0.52 | 0.90 | -0.17 | 1.3    | 0.35 | 0.51 | 0.59 | 0.45  | 0.17  | 0.71 | 0.22   |
| n=4          | 0.16    | 0.64    | -1.1    | 0.78    | -0.22   | 0.70    | 0.59    | 0.47    | 1.2     | -0.080  | 0.38    | 0.39    | 0.20    | 0.78    | -0.93   | 0.44   | -0.040 | 0.020   | 0.32   | 0.40   | 0.38   | 0.57   | -0.70  | 1      | 0.52   | -0.35  | 0.63  | 0.53  | -0.38 | -0.16 | 0.30 | 0.71 | 0.35  | 0.090 | 0.27 | 0.33  | 0.39  | 0.49 | 0.59 | 0.95  | 0.53   | 0.26 | 0.49 | 0.30 | 0.60  | 0.14  | 0.33 | 0.50   |
| n=5          | -0.49   | -0.050  | 0.54    | -0.23   | 0.69    | 0.58    | 0.92    | 0.75    | -0.18   | 0.22    | -0.050  | 1.5     | -0.36   | -0.62   | 1.1     | 1.5    | 0.52   | -0.10   | 0.020  | 0.71   | -0.030 | 0.73   | 0.31   | 0.16   | -0.65  | 1.4    | 0.25  | -0.35 | 0.070 | 0.42  | 0.68 | 0.32 | 0.22  | 0.25  | 0.22 | -0.10 | 0.33  | 0.27 | 0.14 | 0.57  | 0.0100 | 0.26 | 0.39 | 0.24 | 0.20  | 0.030 | 0.23 |        |
| n=6          | 0.82    | 0.34    | 1.5     | -0.080  | -0.040  | 0.85    | 1.8     | 0.020   | 1.3     | -0.20   | 0.040   | -0.030  | 1.2     | -1.4    | 0.78    | 0.030  | 0.59   | 0.16    | -0.14  | 0.77   | 0.040  | 0.57   | 0.31   | 0.44   | 0.32   | -0.29  | -0.67 | 0.20  | -0.33 | -0.76 | 0.60 | 0.50 | -0.54 | 0.20  | 0.17 | 0.21  | 0.36  | 0.34 | 0.25 | 0.41  | 0.43   | 0.24 | 0.18 | 0.21 | 0.12  | 0.33  | n=6  |        |

| RESISTIVITY | Filter  |         |         |         |         |         |         |         |         |         |         |         |         |         |         |        |        |        |        |        |        |        |        |        |      | Filter      |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
|-------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|-------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
|             | 24+00 S | 23+00 S | 22+00 S | 21+00 S | 20+00 S | 19+00 S | 18+00 S | 17+00 S | 16+00 S | 15+00 S | 14+00 S | 13+00 S | 12+00 S | 11+00 S | 10+00 S | 9+00 S | 8+00 S | 7+00 S | 6+00 S | 5+00 S | 4+00 S | 3+00 S | 2+00 S | 1+00 S | 0+00 | RESISTIVITY |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |     |
| n=1         | 258     | 235     | 194     | 192     | 193     | 193     | 194     | 198     | 198     | 185     | 179     | 174     | 174     | 175     | 174     | 181    | 187    | 191    | 197    | 203    | 209    | 212    | 217    | 221    | 228  | 240         | 248 | 258 | 269 | 280 | 273 | 280 | 305 | 323 | 334 | 339 | 336 | 337 | 352 | 339 | 349 | 367 | 379 | 381 | 387 | 368 | 340 | 350 |
| n=2         | 126     | 114     | 124     | 122     | 119     | 113     | 122     | 105     | 97      | 100     | 107     | 100     | 102     | 111     | 112     | 117    | 119    | 127    | 131    | 147    | 152    | 150    | 170    | 169    | 167  | 186         | 225 | 241 | 236 | 210 | 199 | 206 | 212 | 214 | 216 | 223 | 252 | 263 | 239 | 271 | 270 | 262 | 247 |     |     |     |     |     |
| n=3         | 171     | 179     | 168     | 168     | 164     | 162     | 176     | 177     | 158     | 122     | 142     | 152     | 141     | 145     | 158     | 160    | 161    | 167    | 177    | 186    | 187    | 196    | 207    | 214    | 238  | 238         | 231 | 239 | 260 | 322 | 310 | 312 | 283 | 277 | 287 | 300 | 317 | 368 | 333 | 358 | 371 | 386 | 366 |     |     |     |     |     |
| n=4         | 210     | 222     | 240     | 210     | 208     | 206     | 230     | 231     | 237     | 202     | 170     | 199     | 186     | 189     | 206     | 203    | 213    | 213    | 228    | 244    | 247    | 242    | 256    | 268    | 311  | 304         | 300 | 307 | 318 | 336 | 404 | 394 | 376 | 358 | 361 | 407 | 386 | 410 | 405 | 463 | 449 | 475 | 476 |     |     |     |     |     |
| n=5         | 251     | 255     | 283     | 280     | 247     | 248     | 275     | 284     | 291     | 289     | 227     | 253     | 253     | 259     | 250     | 266    | 274    | 275    | 286    | 307    | 314    | 311    | 308    | 363    | 373  | 361         | 376 | 389 | 391 | 403 | 484 | 489 | 492 | 488 | 443 | 475 | 458 | 556 | 573 | 589 | 548 |     |     |     |     |     |     |     |
| n=6         | 357     | 314     | 322     | 320     | 285     | 321     | 328     | 343     | 341     | 388     | 345     | 253     | 279     | 303     | 306     | 312    | 313    | 319    | 347    | 356    | 365    | 362    | 404    | 418    | 427  | 442         | 464 | 468 | 456 | 541 | 536 | 734 | 528 | 525 | 488 | 494 | 614 | 586 | 617 | 548 | 541 | 536 | 528 | 525 | 520 | 300 |     |     |

| CHARGEABILITY | Filter |  |
|---------------|--------|--|
|---------------|--------|--|





42A07NW2012

2.18926 SHERATON 420

## METAL FACTOR

|        | 30+00 W | 29+00 W | 28+00 W | 27+00 W | 26+00 W | 25+00 W | 24+00 W |        |
|--------|---------|---------|---------|---------|---------|---------|---------|--------|
| Filter | 0.71    | 0.80    | 1.1     | 1       | 1.1     | 1.2     | 1       | Filter |
| n=1    |         | 1.9     | 1.9     | 1.6     | 1.6     | 1.9     | 1.2     | 0.91   |
| n=2    |         | 1.3     | 1.5     | 0.87    | 1.1     | 1.2     | 1.3     | 0.57   |
| n=3    |         | 1.1     | 0.77    | 0.73    | 1.3     | 1.5     | 0.73    | 0.54   |
| n=4    |         | 0.87    | 0.65    | 0.40    | 0.83    | 0.96    | 0.67    | 0.86   |
| n=5    |         | 0.72    | 0.46    | 0.71    | 0.76    | 1.3     | 1.2     | 0.92   |
| n=6    |         | 0.63    | 0.44    | 0.58    | 0.60    | 0.98    | 1       | 0.79   |

## METAL FACTOR

n=1  
n=2  
n=3  
n=4  
n=5  
n=6

## RESISTIVITY

|        | 30+00 W | 29+00 W | 28+00 W | 27+00 W | 26+00 W | 25+00 W | 24+00 W |     |
|--------|---------|---------|---------|---------|---------|---------|---------|-----|
| Filter | 567     | 531     | 438     | 451     | 459     | 505     | 529     | 601 |
| n=1    |         | 138     | —       | 150     | 170     | 214     | 224     | 282 |
| n=2    |         | 288     | 249     | 268     | 326     | 345     | 286     | 458 |
| n=3    |         | 368     | 422     | 350     | 411     | 458     | 453     | 419 |
| n=4    |         | 477     | 497     | 566     | 526     | 543     | 545     | 579 |
| n=5    |         | 555     | 568     | 599     | 715     | 520     | 595     | 672 |
| n=6    |         | 591     | 762     | 687     | 851     | 741     | 651     | 795 |

## RESISTIVITY

ohm-m  
n=1  
n=2  
n=3  
n=4  
n=5  
n=6

## CHARGEABILITY

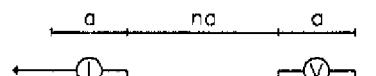
|        | 30+00 W | 29+00 W | 28+00 W | 27+00 W | 26+00 W | 25+00 W | 24+00 W |     |
|--------|---------|---------|---------|---------|---------|---------|---------|-----|
| Filter | 3.8     | 3.9     | 3.8     | 4       | 4.5     | 5.2     | 5.9     | 5.9 |
| n=1    |         |         | 2.7     | 2.8     | 2.8     | 3.5     | 4.2     | 3.3 |
| n=2    |         |         | 3.8     | 3.7     | 2.3     | 3.7     | 4.1     | 3.8 |
| n=3    |         |         | 4       | 3.3     | 2.5     | 5.5     | 6.7     | 3.3 |
| n=4    |         |         | 4.2     | 3.3     | 2.3     | 4.3     | 5.2     | 3.7 |
| n=5    |         |         | 4       | 2.6     | 4.2     | 5.4     | 8.1     | 7   |
| n=6    |         |         | 3.7     | 3.3     | 4       | 5.1     | 7.3     | 6.7 |

## CHARGEABILITY

mV/V  
n=1  
n=2  
n=3  
n=4  
n=5  
n=6Conc.  
3K4

Line 34 S

Pole-Dipole Array



Filter  
\*  
\*\*  
\*\*\*  
\*\*\*\*

plot points

 $a = 50.0 \text{ M}$ 

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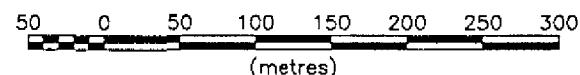
GEOSCIENCE ASSESSMENT OFFICE

Logarithmic Contours 1, 1.5, 2, 3, 5, 7.5, 10, ...

## INTERPRETATION

- Strong increase in polarization accompanied by marked decrease in resistivity.
- Well defined increase in polarization without marked resistivity decrease.
- Poorly defined polarization increase with no resistivity signature.
- ▼ Low resistivity feature.

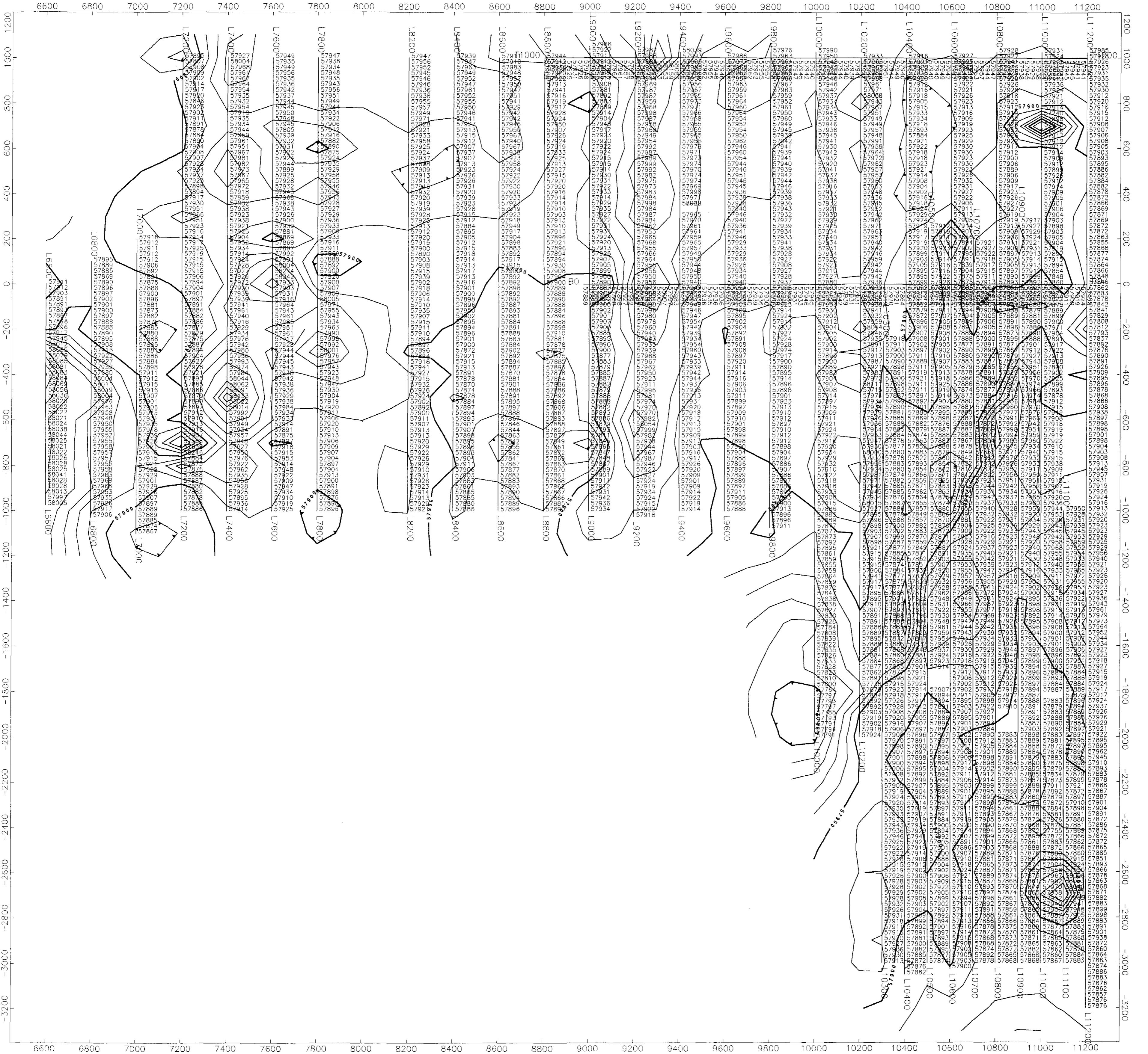
Scale 1:5000



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THOMAS\SHERATON TOWNSHIPDate: 98/06/08  
Interpretation: B.PATRIE AND D.PATRIE

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