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HIRBORNE GEOPHYSICAL SURVEY

FOR ASSESSMENT MORK CREDIT

ON THE

MEUNIER CLAIMS

FALLON TOWNSHIP, ONTARIO

PORCUPINE MINING DIVISION

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R.P. BOMEN, P.E.

With technical descriptions of equipment and interpretation of results by

Z. DVORAK Vice+President DIGHEM LIMITED

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This is to certify that the submitted airborne geophysical survey performed in Fallon Township on the Meunier claims has been done in a professional manner.

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R.P. Bowen, P.Eng.

JAN 1984

The list of the claims surveyed is this survey by Dighem of Toronto for Mr. David Meunier, License M-17157 in Fallon Township, Ontario follows this page.

MEUNIER CLAIMS IN FALLON TOWNSHIP

No.	Claim No.	Anniversare Date
1.	P. 65325 9	12 Sentember 1982
2.	P. 65326 0	12 Sentember 1982
3.	P. 653261	12 September 1982
4.	P. 653262	12 Sentember 1982
5.	P. 641742	27 September 1982
€.	P. 641743	27 Sentember 1982
7.	P. 653908	27 Sentember 1982
8.	P. 653909	27 Sentember 1982
9.	P. 641730	20 Sentember 1982
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DIGHEM^{III} SURVEY

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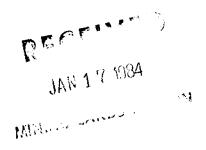
FALLON TOWNSHIP AREA, ONTARIO

FOR

DAVID J. MEUNIER

BY

DIGHEM LIMITED



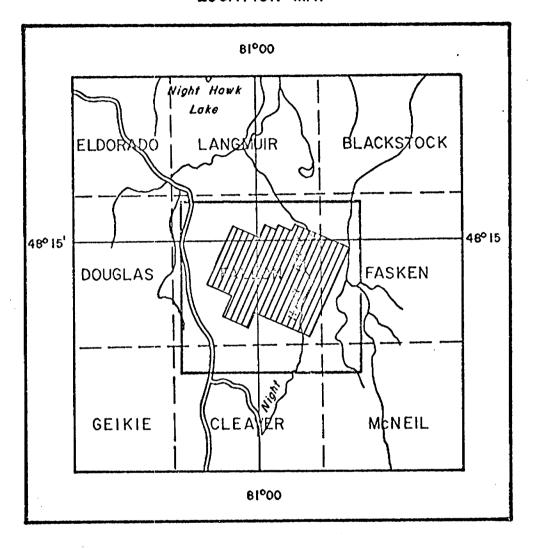
TORONTO, ONTARIO DECEMBER 6, 1983 Z. DVORAK VICE-PRESIDENT

SUMMARY AND RECOMMENDATIONS

A total of 249 km of electromagnetic/resistivity/magnetic/VLF survey was flown in October 1983, over a property held by David J. Meunier in the Fallon Township, Ontario.

The survey outlined several weak discrete bedrock conductors most of which were associated with areas of low resistivity. Most of these anomalies appear to warrant further investigation using appropriate surface exploration techniques. Areas of interest may be assigned priorities for follow-up work on the basis of supporting geological and/or geochemical information.

LOCATION MAP



Scale 1: 250,000

FIGURE 1
THE SURVEY AREA

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INTRODUCTION

A DIGHEM^{III} survey totalling 249 line-km was flown with a 200 m line-spacing for Mr. David J. Meunier, from October 25 to 29, 1983, in Fallon Township, Ontario (Figure 1).

The Astar CG-NSM turbine helicopter flew at an average airspeed of 131 km/h with an EM bird height of approximately Ancillary equipment consisted of a Sonotek PMH 5010 magnetometer with its bird at an average height of 46 m, a Sperry radio altimeter, a Geocam sequence camera, an RMS GR 33 analog recorder, a Sonotek SDS 1200 digital data acquisition system, a DigiData 1640 9-track 800-bpi magnetic Industries tape recorder. and а Herz VLF-electromagnetometer with its sensor towed at an average height of 54 m. The VLF-EM receivers were tuned to NAA, Cutler, Me., which operates at 17.8 kHz, and to NLK, Seattle, Wa., which operates at 24.8 kHz. The analog equipment recorded four channels of EM data at approximately 900 Hz, two channels of EM data at approximately 7200 Hz, two ambient EM noise channels (for the coaxial and coplanar receivers), two channels of magnetics (coarse and fine count), a channel of radio altitude, and four channels of VLF-EM (two total fields and two quadratures of the vertical component). The digital equipment recorded the EM data with a sensitivity of 0.20 ppm at 900 Hz, and 0.40 ppm at

7200 Hz, the magnetic field to one nT (i.e., one gamma), and the VLF-EM field to 0.10 percent.

Appendix A provides details on the data channels, their respective sensitivities, and the flight path recovery procedure. Noise levels of less than 2 ppm are generally maintained for wind speeds up to 35 km/h. Higher winds may cause the system to be grounded because excessive bird swinging produces difficulties in flving the helicopter. The swinging results from the 5 m² of which is presented by the bird to broadside qusts. The DIGHEM system nevertheless can be flown under wind conditions that seriously degrade other AEM systems.

It should be noted that the anomalies shown on the electromagnetic anomaly map are based on a near-vertical, half plane model. This model best reflects "discrete" bedrock conductors. Wide bedrock conductors or flat-lying conductive units, whether from surficial or bedrock sources, may give rise to very broad anomalous responses on the EM profiles. These may not appear on the electromagnetic anomaly map if they have a regional character rather than a locally anomalous character. These broad conductors, which more closely approximate a half space model, will be maximum coupled to the horizontal (coplanar) coil-pair and are clearly evident on the resistivity map. The resistivity

map, therefore, may be more valuable than the electromagnetic anomaly map, in areas where broad or flat-lying conductors are considered to be of importance.

In areas where magnetite causes the inphase components to become negative, the apparent conductance and depth of EM anomalies may be unreliable.

Areas, in which EM responses are evident only on the quadrature components, indicate zones of poor conductivity. Where these responses are coincident with strong magnetic inphase component it is possible that the anomalies, by the effects have been suppressed Most of these poorly-conductive magnetic of magnetite. features give rise to resistivity anomalies which only slightly below background. These weak features are evident on the resistivity map but may not be shown on the electromagnetic anomaly map. If it is expected that associated poorly-conductive sulphides may be with magnetite-rich units, some of these weakly anomalous features may be of interest.

SECTION I: SURVEY RESULTS

CONDUCTORS IN THE SURVEY AREA

The survey covered a single grid with 249 km of flying, the results of which are shown on one map sheet. Table I-1 summarizes the EM responses on this sheet with respect to conductance grade and interpretation.

The electromagnetic anomaly map shows the anomaly locations with the interpreted conductor shape, dip, conductance and depth being indicated by symbols. Direct magnetic correlation is also shown if it exists. The strike direction and length of the conductors are indicated when anomalies can be correlated from line to line. When studying the map sheets for follow-up planning, consult the anomaly listings appended to this report to ensure that none of the conductors are overlooked.

Resistivity of the geologic environment in the survey area varies over a broad range of values, from less than 200 ohm-m to in excess of 8,000 ohm-m, in an apparent agreement with topography. The low lying eastern half of the area displays low resistivities, whereas the high ground in the western half is characterized by resistivities

TABLE I-1

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CONDUCTOR		NUMBER OF
GRADE	CONDUCTANCE RANGE	RESPONSES
6	> 99 MHOS	,
5	50-99 MHOS	0
4	20-49 MHOS	0
3	10-19 MHOS	0
2	5- 9 MHOS	8
1	< 5 MHOS	281
X	INDETERMINATE	34
TOTAL	·	323

CONDUCTOR MODEL	MOST LIKELY SOURCE	NUMBER OF RESPONSES
В	DISCRETE BEDROCK CONDUCTOR	19
S	CONDUCTIVE COVER	175
H	ROCK UNIT OR THICK COVER	124
E	EDGE OF WIDE CONDUCTOR	3
L	CULTURE	2
TOTAL		323

(SEE EM MAP LEGEND FOR EXPLANATIONS)

generally higher than 1,000 ohm-m. This resistivity distribution is partly reflected by the VLF-EM patterns which suggest the presence of a number of northwesterly trends in the west half of the area, i.e., over the resistive ground. In comparison, the eastern, more conductive, half of the survey area contains only a small number of VLF-EM responses.

The division of the area into two distinct parts, so obvious from the resistivity and VLF-EM data, is only weakly apparent from the total magnetic field map. Much more pronounced is the presence of a highly magnetic unit (felsic intrusives?) in the north part of the grid. Also well defined is a 300 m to 500 m broad belt of high magnetic activity which extends approximately from 39E* toward the north end of lines 24 and 251. In addition, the enhanced magnetic map shows the presence of numerous northwesterly striking trends throughout the south half of the area, which roughly correlate with the VLF-EM trends.

The majority of the EM anomalies reflect near-surface conductive features (e.g., overburden) and broad, conductive rock units. There are only a few grade 1 EM anomalies which appear to reflect discrete conductors of bedrock origin. They are discussed below.

^{*} This denotes EM anomaly E on line 39.

Anomalies 1A, 1B

These grade 1 anomalies reflect weak conductors of possible bedrock origin. Anomaly 1A appears to be better defined than 1B. Note, that it is indicative of a conductor whose response is being masked by the presence of magnetite.

Anomalies 2B, 5B

Weak conductors of possible bedrock origin are indicated by these grade 1 anomalies. Similar to 1A, anomalies 2B and 5B are being masked by the presence of magnetite.

Anomaly 11D

This grade 1 anomaly is indicative of a very weak bedrock conductor.

Anomaly 12C

Although this grade 1 anomaly does not reflect a discrete bedrock conductor, it may be of some exploration interest. The anomaly is indicative of a weak conductive feature which appears

to occur as a buried, possibly flat lying, target. It should be investigated on the ground.

Anomalies 13A-15A, 17B-19C

These anomalies define a weak conductive feature which parallels the resistivity Conductor contours. 13A-15A correlates with a weak VLF-EM anomaly, whereas 17B-19C occurs on the flank of enhanced magnetic anomalies. Both conductors may have bedrock origin.

Anomalies 17A, 18A, 21A

These anomalies occur along a common strike paralleling 13A-15A and 17B-19C. While 17A and 18A appear to reflect broad targets, 21A may be indicative of a discrete bedrock conductor.

Anomalies 17E, 18P, 19L, 20H

These grade 1 anomalies are confined to the flanks of VLF-EM and enhanced magnetic localized trends. Anomaly 20H and possibly 19L may reflect discrete bedrock

conductors, whereas 17E and 18P are indicative of broader targets.

Anomaly 19J

The most attractive feature of this grade 1 anomaly is its magnetic association of 30nT. Note that 19J, which is of possible bedrock origin, occurs at the tip of a well defined localized enhanced magnetic anomaly.

Anomalies 23C, 24xA, 27B, 27E

These anomalies reflect weak conductive features which may occur in the bedrock. Anomaly 27E is suspected as being due to aerodynamic noise.

Anomaly 30K

This grade 1 anomaly reflects a weak conductor of possible bedrock origin, which occurs on the flank of the previously mentioned north-south magnetic feature.

SECTION II: BACKGROUND INFORMATION

ELECTROMAGNETICS

DIGHEM electromagnetic responses fall into two general classes, discrete and broad. The discrete class consists of sharp, well-defined anomalies from discrete conductors such as sulfide lenses and steeply dipping sheets of graphite and sulfides. The broad class consists of wide anomalies from conductors having a large horizontal surface such as flatly dipping graphite or sulfide sheets, saline water-saturated sedimentary formations, conductive overburden and rock, and geothermal zones. A vertical conductive slab with a width of 200 m would straddle these two classes.

The vertical sheet (half plane) is the most common model used for the analysis of discrete conductors. All anomalies plotted on the electromagnetic map are analyzed according to this model. The following section entitled Discrete conductor analysis describes this model in detail, including the effect of using it on anomalies caused by broad conductors such as conductive overburden.

The conductive earth (half space) model is suitable for broad conductors. Resistivity contour maps result from the

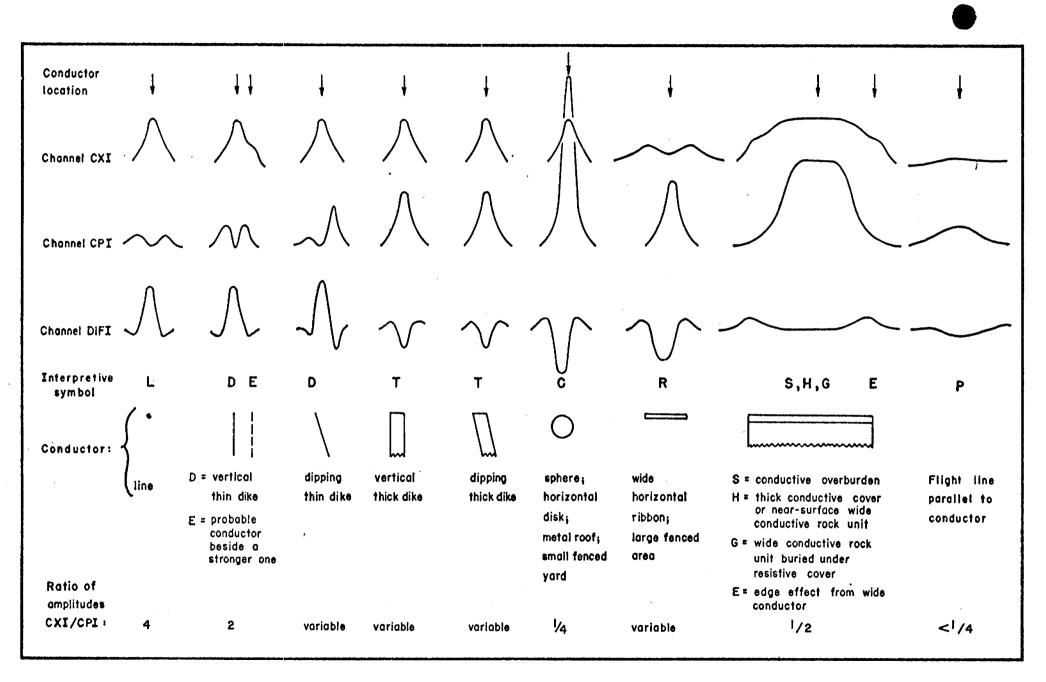
use of this model. A later section entitled Resistivity mapping describes the method further, including the effect of using it on anomalies caused by discrete conductors such as sulfide bodies.

Geometric interpretation

The geophysical interpreter attempts to determine the geometric shape and dip of the conductor. This qualitative interpretation of anomalies is indicated on the map by means of interpretive symbols (see EM map legend). Figure II-1 shows typical DIGHEM anomaly shapes and the interpretive symbols for a variety of conductors. These classic curve shapes are used to guide the geometric interpretation.

Discrete conductor analysis

The EM anomalies appearing on the electromagnetic map are analyzed by computer to give the conductance (i.e., conductivity-thickness product) in mhos of a vertical sheet model. This is done regardless of the interpreted geometric shape of the conductor. This is not an unreasonable procedure, because the computed conductance increases as the electrical quality of the conductor increases, regardless of its true shape. DIGHEM anomalies are divided into six



Typical DIGHEM anomaly shapes

grades of conductance, as shown in Table II-1. The conductance in mhos is the reciprocal of resistance in ohms.

Table II-1. EM Anomaly Grades

Anomaly Grade	Mho Range
6	> 99
5	50 - 99
4	20 - 49
3	10 - 19
2	5 - 9
`1	< 5

The conductance value is a geological parameter because it is a characteristic of the conductor alone; it generally is independent of frequency, and of flying height or depth of burial apart from the averaging over a greater portion of the conductor as height increases. Small anomalies from deeply buried strong conductors are not confused with small anomalies from shallow weak conductors because the former will have larger conductance values.

Conductive overburden generally produces broad EM responses which are not plotted on the EM maps. However, patchy conductive overburden in otherwise resistive areas

This statement is an approximation. DIGHEM, with its short coil separation, tends to yield larger and more accurate conductance values than airborne systems having a larger coil separation.

can yield discrete anomalies with a conductance grade (cf. Table II-1) of 1, or even of 2 for conducting clays which have resistivities as low as 50 ohm-m. In areas where ground resistivities can be below 10 ohm-m, anomalies caused by weathering variations and similar causes can have any conductance grade. The anomaly shapes from the multiple coils often allow such conductors to be recognized, and these are indicated by the letters S, H, G and sometimes E on the map (see EM legend).

bedrock conductors, the higher anomaly grades For indicate increasingly higher conductances. Examples: Insco copper discovery (Noranda, Canada) DIGHEM's New yielded a grade 4 anomaly, as did the neighbouring copper-zinc Magusi River ore body; Mattabi (copper-zinc, Lake, Canada) and Whistle (nickel, Sudbury, Sturgeon Canada) gave grade 5; and DIGHEM's Montcalm nickel-copper discovery (Timmins, Canada) yielded a grade 6 anomaly. Graphite and sulfides can span all grades but, in any particular survey area, field work may show that different grades indicate different types of conductors.

Strong conductors (i.e., grades 5 and 6) are characteristic of massive sulfides or graphite. Moderate conductors (grades 3 and 4) typically reflect sulfides of a less massive character or graphite, while weak bedrock conductors

(grades 1 and 2) can signify poorly connected graphite or heavily disseminated sulfides. Grade 1 conductors may not respond to ground EM equipment using frequencies less than 2000 Hz.

The presence of sphalerite or gangue can result in ore deposits having weak to moderate conductances. As an example, the three million ton lead-zinc deposit of Restigouche Mining Corporation near Bathurst, Canada, yielded a well defined grade 1 conductor. The 10 percent by volume of sphalerite occurs as a coating around the fine grained massive pyrite, thereby inhibiting electrical conduction.

Faults, fractures and shear zones may produce anomalies which typically have low conductances (e.g., grades 1 and 2). Conductive rock formations can yield anomalies of any conductance grade. The conductive materials in such rock formations can be salt water, weathered products such as clays, original depositional clays, and carbonaceous material.

On the electromagnetic map, a letter identifier and an interpretive symbol are plotted beside the EM grade symbol. The horizontal rows of dots, under the interpretive symbol, indicate the anomaly amplitude on the flight record. The

vertical column of dots, under the anomaly letter, gives the estimated depth. In areas where anomalies are crowded, the letter identifiers, interpretive symbols and dots may be obliterated. The EM grade symbols, however, will always be discernible, and the obliterated information can be obtained from the anomaly listing appended to this report.

The purpose of indicating the anomaly amplitude by dots is to provide an estimate of the reliability of the conductance calculation. Thus, a conductance value obtained from a large ppm anomaly (3 or 4 dots) will tend to be accurate whereas one obtained from a small ppm anomaly (no dots) could be quite inaccurate. The absence of amplitude dots indicates that the anomaly from the coaxial coil-pair is 5 ppm or less on both the inphase and quadrature channels. Such small anomalies could reflect a weak conductor at the surface or a stronger conductor at depth. The conductance grade and depth estimate illustrates which of these possibilities fits the recorded data best.

Flight line deviations occasionally yield cases where two anomalies, having similar conductance values but dramatically different depth estimates, occur close together on the same conductor. Such examples illustrate the reliability of the conductance measurement while showing that the depth estimate can be unreliable. There are a

number of factors which can produce an error in the depth estimate, including the averaging of topographic variations by the altimeter, overlying conductive overburden, and the location and attitude of the conductor relative to the flight line. Conductor location and attitude can provide an erroneous depth estimate because the stronger part of the conductor may be deeper or to one side of the flight line, or because it has a shallow dip. A heavy tree cover can also produce errors in depth estimates. This is because the depth estimate is computed as the distance of bird from conductor, minus the altimeter reading. The altimeter can lock onto the top of a dense forest canopy. This situation yields an erroneously large depth estimate but does not affect the conductance estimate.

Dip symbols are used to indicate the direction of dip of conductors. These symbols are used only when the anomaly shapes are unambiguous, which usually requires a fairly resistive environment.

A further interpretation is presented on the EM map by means of the line-to-line correlation of anomalies, which is based on a comparison of anomaly shapes on adjacent lines. This provides conductor axes which may define the geological structure over portions of the survey area. The absence of

conductor axes in an area implies that anomalies could not be correlated from line to line with reasonable confidence.

DIGHEM electromagnetic maps are designed to provide a correct impression of conductor quality by means of the The symbols can stand alone conductance grade symbols. with geology when planning a follow-up program. The actual conductance values are printed in the attached anomaly list for those who wish quantitative data. The anomaly ppm and depth are indicated by inconspicuous dots which should not distract from the conductor patterns, while being helpful to those who wish this information. The map provides an interpretation of conductors in terms of length, strike and dip, geometric shape, conductance, depth, and thickness (see The accuracy is comparable to an interpretation from a high quality ground EM survey having the same line spacing.

The attached EM anomaly list provides a tabulation of anomalies in ppm, conductance, and depth for the vertical sheet model. The EM anomaly list also shows the conductance and depth for a thin horizontal sheet (whole plane) model, but only the vertical sheet parameters appear on the EM map. The horizontal sheet model is suitable for a flatly dipping thin bedrock conductor such as a sulfide sheet having a thickness less than 10 m. The list also shows the

resistivity and depth for a conductive earth (half space) model, which is suitable for thicker slabs such as thick conductive overburden. In the EM anomaly list, a depth value of zero for the conductive earth model, in an area of thick cover, warns that the anomaly may be caused by conductive overburden.

Since discrete bodies normally are the targets of EM surveys, local base (or zero) levels are used to compute This contrasts with the use local anomaly amplitudes. of true zero levels which are used to compute true EM amplitudes. Local anomaly amplitudes are shown in the EM anomaly list and these are used to compute the vertical sheet parameters of conductance and depth. Not shown in the EM anomaly list are the true amplitudes which are used to horizontal sheet and conductive the earth compute parameters.

X-type electromagnetic responses

DIGHEM maps contain x-type EM responses in addition to EM anomalies. An x-type response is below the noise threshold of 3 ppm, and reflects one of the following: a weak conductor near the surface, a strong conductor at depth (e.g., 100 to 120 m below surface) or to one side of the flight line, or aerodynamic noise. Those responses that

have the appearance of valid bedrock anomalies on the flight profiles are indicated by appropriate interpretive symbols (see EM map legend). The others probably do not warrant further investigation unless their locations are of considerable geological interest.

The thickness parameter

DIGHEM can provide an indication of the thickness of a steeply dipping conductor. The amplitude of the coplanar anomaly (e.g., CPI) increases relative to the coaxial anomaly (e.g., CXI) as the apparent thickness increases, i.e., the thickness in the horizontal plane. (The thickness is equal to the conductor width if the conductor dips at 90 degrees and strikes at right angles to the flight line.) This report refers to a conductor as thin when the thickness is likely to be less than 3 m, and thick when in excess of Thin conductors are indicated on the EM map by the interpretive symbol "D", and thick conductors by "T". base metal exploration in steeply dipping geology, thick conductors can be high priority targets because many massive sulfide ore bodies are thick, whereas non-economic bedrock conductors are often thin. The system cannot sense the thickness when the strike of the conductor is subparallel to the flight line, when the conductor has a shallow dip, when

the anomaly amplitudes are small, or when the resistivity of the environment is below 100 ohm-m.

Resistivity mapping

widespread conductivity are commonly of Areas encountered during surveys. In such areas, anomalies can be generated by decreases of only 5 m in survey altitude as well as by increases in conductivity. The typical flight record in conductive areas is characterized by inphase and quadrature channels which are continuously active. Local EM peaks reflect either increases in conductivity of the earth or decreases in survey altitude. For such conductive areas, apparent resistivity profiles and contour maps are necessary for the correct interpretation of the airborne The advantage of the resistivity parameter data. that anomalies caused by altitude changes are virtually eliminated, so the resistivity data reflect only those anomalies caused by conductivity changes. The resistivity analysis also helps the interpreter to differentiate between conductive trends in the bedrock and those patterns typical of conductive overburden. For example, discrete conductors will generally appear as narrow lows on the contour map and broad conductors (e.g., overburden) will appear wide lows.

The resistivity profile (see table in Appendix A) and the resistivity contour map present the apparent resistivity using the so-called pseudo-layer (or buried) half space model defined in Fraser (1978)². This model consists of a resistive layer overlying a conductive half space. The depth channel (see Appendix A) gives the apparent depth below surface of the conductive material. The apparent depth is simply the apparent thickness of the overlying apparent depth (or thickness) resistive layer. The parameter will be positive when the upper layer is more resistive than the underlying material, in which case the apparent depth may be quite close to the true depth.

The apparent depth will be negative when the upper layer is more conductive than the underlying material, and will be zero when a homogeneous half space exists. The apparent depth parameter must be interpreted cautiously because it will contain any errors which may exist in the measured altitude of the EM bird (e.g., as caused by a dense tree cover). The inputs to the resistivity algorithm are the inphase and quadrature components of the coplanar coil-pair. The outputs are the apparent resistivity of the

Resistivity mapping with an airborne multicoil electromagnetic system: Geophysics, v. 43, p. 144-172.

conductive half space (the source) and the sensor-source distance. The flying height is not an input variable, and the output resistivity and sensor-source distance are independent of the flying height. The apparent depth, discussed above, is simply the sensor-source distance minus the measured altitude or flying height. Consequently, errors in the measured altitude will affect the apparent depth parameter but not the apparent resistivity parameter.

The apparent depth parameter is a useful indicator of simple layering in areas lacking a heavy tree cover. The DIGHEM system has been flown for purposes of permafrost mapping, where positive apparent depths were used as a measure of permafrost thickness. However, little quantitative use has been made of negative apparent depths because the absolute value of the negative depth is not a measure of the thickness of the conductive upper layer and, therefore, is not meaningful physically. Qualitatively, a negative apparent depth estimate usually shows that the EM anomaly is caused by conductive overburden. Consequently, the apparent depth channel can be of significant help in distinguishing between overburden and bedrock conductors.

The resistivity map often yields more useful information on conductivity distributions than the EM map. In

comparing the EM and resistivity maps, keep in mind the following:

- (a) The resistivity map portrays the absolute value
 of the earth's resistivity.
 (Resistivity = 1/conductivity.)
- (b) The EM map portrays anomalies in the earth's resistivity. An anomaly by definition is a change from the norm and so the EM map displays anomalies, (i) over narrow, conductive bodies and (ii) over the boundary zone between two wide formations of differing conductivity.

The resistivity map might be likened to a total field map and the EM map to a horizontal gradient in the direction of flight³. Because gradient maps are usually more sensitive than total field maps, the EM map therefore is to be preferred in resistive areas. However, in conductive areas, the absolute character of the resistivity map usually causes it to be more useful than the EM map.

³ The gradient analogy is only valid with regard to the identification of anomalous locations.

Interpretation in conductive environments

Environments having background resistivities below 30 ohm-m cause all airborne EM systems to yield very large responses from the conductive ground. This usually prohibits the recognition of discrete bedrock conductors. The processing of DIGHEM data, however, produces six channels which contribute significantly to the recognition of bedrock conductors. These are the inphase and quadrature difference channels (DIFI and DIFQ), and the resistivity and depth channels (RES and DP) for each coplanar frequency; see table in Appendix A.

The EM difference channels (DIFI and DIFQ) eliminate up to 99% of the response of conductive ground, leaving responses from bedrock conductors, cultural features (e.g., telephone lines, fences, etc.) and edge effects. An edge effect arises when the conductivity of the ground suddenly changes, and this is a source of geologic noise. While edge effects yield anomalies on the EM difference channels, they do not produce resistivity anomalies. Consequently, the resistivity channel aids in eliminating anomalies due to edge effects. On the other hand, resistivity anomalies will coincide with the most highly conductive sections of conductive ground, and this is another source of geologic

noise. The recognition of a bedrock conductor in a conductive environment therefore is based on the anomalous responses of the two difference channels (DIFI and DIFQ) and the two resistivity channels (RES). The most favourable situation is where anomalies coincide on all four channels.

The DP channels, which give the apparent depth to the conductive material, also help to determine whether a conductive response arises from surficial material or from a conductive zone in the bedrock. When these channels ride above the zero level on the electrostatic chart paper (i.e., depth is negative), it implies that the EM and resistivity profiles are responding primarily to a conductive upper layer, i.e., conductive overburden. If both DP channels are below the zero level, it indicates that a resistive upper layer exists, and this usually implies the existence of a bedrock conductor. If the low frequency DP channel is below the zero level and the high frequency DP is above, this suggests that a bedrock conductor occurs beneath conductive cover.

Channels REC1, REC2, REC3 and REC4 are the anomaly recognition functions. They are used to trigger the conductance channel CDT which identifies discrete conductors. In highly conductive environments, channel REC2

is deactivated because it is subject to corruption by highly conductive earth signals. Similarly, in moderately conductive environments, REC4 is deactivated. Some of the automatically selected anomalies (channel CDT) are discarded by the geophysicist. The automatic selection algorithm is intentionally oversensitive to assure that no meaningful responses are missed. The interpreter then classifies the anomalies according to their source and eliminates those that are not substantiated by the data, such as those arising from geologic or aerodynamic noise.

Reduction of geologic noise

Geologic noise refers unwanted to geophysical responses. For purposes of airborne EM surveying, geologic noise refers to EM responses caused by conductive overburden and magnetic permeability. It was mentioned above that the EM difference channels (i.e., channel DIFI for inphase and DIFQ for quadrature) tend to eliminate the response of conductive overburden. This marked a unique development in airborne EM technology, as DIGHEM is the only EM system which yields channels having an exceptionally high degree of immunity to conductive overburden.

Magnetite produces a form of geological noise on the inphase channels of all EM systems. Rocks containing less than 1% magnetite can yield negative inphase anomalies caused by magnetic permeability. When magnetite is widely distributed throughout a survey area, the inphase EM channels may continuously rise and fall reflecting variations in the magnetite percentage, flying height, and overburden thickness. This can lead to difficulties in recognizing deeply buried bedrock conductors, particularly if conductive overburden also exists. However, the response of broadly distributed magnetite generally vanishes on the inphase difference channel DIFI. This feature can be a significant aid in the recognition of conductors which occur in rocks containing accessory magnetite.

EM magnetite mapping

The information content of DIGHEM data consists of a combination of conductive eddy current response and magnetic permeability response. The secondary field resulting from conductive eddy current flow is frequency-dependent and consists of both inphase and quadrature components, which are positive in sign. On the other hand, the secondary field resulting from magnetic permeability is independent of frequency and consists of only an inphase component which

is negative in sign. When magnetic permeability manifests itself by decreasing the measured amount of positive inphase, its presence may be difficult to recognize. However, when it manifests itself by yielding a negative inphase anomaly (e.g., in the absence of eddy current flow), its presence is assured. In this latter case, the negative component can be used to estimate the percent magnetite content.

A magnetite mapping technique was developed for the coplanar coil-pair of DIGHEM. The technique yields channel "FEO" (see Appendix A) which displays apparent weight percent magnetite according to a homogeneous half space The method can be complementary to magnetometer mapping in certain cases. Compared to magnetometry, it is far less sensitive but is more able to resolve closely spaced magnetite zones, as well as providing an estimate of the amount of magnetite in the rock. The method is sensitive to 1/4% magnetite by weight when the EM sensor is at a height of 30 m above a magnetitic half space. individually resolve steeply dipping narrow magnetite-rich bands which are separated by 60 m. Unlike magnetometry, the EM magnetite method is unaffected by remanent magnetism or magnetic latitude.

Refer to Fraser, 1981, Magnetite mapping with a multicoil airborne electromagnetic system: Geophysics, v. 46, p. 1579-1594.

The EM magnetite mapping technique provides estimates of magnetite content which are usually correct within a factor of 2 when the magnetite is fairly uniformly distributed. EM magnetite maps can be generated when magnetic permeability is evident as indicated by anomalies in the magnetite channel FEO.

Like magnetometry, the EM magnetite method maps only bedrock features, provided that the overburden is characterized by a general lack of magnetite. This contrasts with resistivity mapping which portrays the combined effect of bedrock and overburden.

Recognition of culture

Cultural responses include all EM anomalies caused by man-made metallic objects. Such anomalies may be caused by inductive coupling or current gathering. The concern of the interpreter is to recognize when an EM response is due to culture. Points of consideration used by the interpreter, when coaxial and coplanar coil-pairs are operated at a common frequency, are as follows:

1. Channels CXS and CPS (see Appendix A) measure 50 and 60 Hz radiation. An anomaly on these channels shows

that the conductor is radiating cultural power. Such an indication is normally a guarantee that the conductor is cultural. However, care must be taken to ensure that the conductor is not a geologic body which strikes across a power line, carrying leakage currents.

- A flight which crosses a line (e.g., fence, telephone 2. line, etc.) yields a center-peaked coaxial anomaly and an m-shaped coplanar anomaly. 5 When the flight crosses the cultural line at a high angle of intersection, the amplitude ratio of coaxial/coplanar (e.g., CXI/CPI) is 4. Such an EM anomaly can only be caused by a line. The geologic body which yields anomalies most closely resembling a line is the vertically dipping thin dike. Such a body, however, an amplitude ratio of 2 rather than 4. yields Consequently, an m-shaped coplanar anomaly with a CXI/CPI amplitude ratio of 4 is virtually a guarantee that the source is a cultural line.
- 3. A flight which crosses a sphere or horizontal disk yields center-peaked coaxial and coplanar anomalies with a CXI/CPI amplitude ratio (i.e., coaxial/coplanar) of 1/4. In the absence of geologic bodies of this geometry, the most likely conductor is a metal roof or

⁵ See Figure II-1 presented earlier.

small fenced yard.⁴ Anomalies of this type are virtually certain to be cultural if they occur in an area of culture.

- 4. A flight which crosses a horizontal rectangular body or wide ribbon yields an m-shaped coaxial anomaly and a center-peaked coplanar anomaly. In the absence of geologic bodies of this geometry, the most likely conductor is a large fenced area. Anomalies of this type are virtually certain to be cultural if they occur in an area of culture.
- 5. EM anomalies which coincide with culture, as seen on the camera film, are usually caused by culture. However, care is taken with such coincidences because a geologic conductor could occur beneath a fence, for example. In this example, the fence would be expected to yield an m-shaped coplanar anomaly as in case #2 above. If, instead, a center-peaked coplanar anomaly occurred, there would be concern that a thick geologic conductor coincided with the cultural line.

⁴ It is a characteristic of EM that geometrically identical anomalies are obtained from: (1) a planar conductor, and (2) a wire which forms a loop having dimensions identical to the perimeter of the equivalent planar conductor.

The above description of anomaly shapes is valid 6. when the culture is not conductively coupled to the In this case, the anomalies arise from environment. inductive coupling to the EM transmitter. when the environment is quite conductive (e.g., less than 100 ohm-m at 900 Hz), the cultural conductor may be conductively coupled to the environment. In this latter case, the anomaly shapes tend to be governed by Current gathering can completely current gathering. distort the anomaly shapes, thereby complicating the identification of cultural anomalies. In such circumstances, the interpreter can only rely on the radiation channels CXS and CPS, and on the camera film.

MAGNETICS

The existence of a magnetic correlation with an EM anomaly is indicated directly on the EM map. An EM anomaly with magnetic correlation has a greater likelihood of being produced by sulfides than one that is non-magnetic. However, sulfide ore bodies may be non-magnetic (e.g., the Kidd Creek deposit near Timmins, Canada) as well as magnetic (e.g., the Mattabi deposit near Sturgeon Lake, Canada).

The magnetometer data are digitally recorded in the aircraft to an accuracy of one nT (i.e., one gamma). The digital tape is processed by computer to yield a total field magnetic contour map. When warranted, the magnetic data also may be treated mathematically to enhance the magnetic response of the near-surface geology, and an enhanced magnetic contour map is then produced. The response of the enhancement operator in the frequency domain is illustrated in Figure II-2. This figure shows that the passband components of the airborne data are amplified 20 times by the enhancement operator. This means, for example, that a 100 nT anomaly on the enhanced map reflects a 5 nT anomaly for the passband components of the airborne data.

The enhanced map, which bears a resemblance to a downward continuation map, is produced by the digital bandpass filtering of the total field data. The enhancement is equivalent to continuing the field downward to a level (above the source) which is 1/20th of the actual sensor-source distance.

Because the enhanced magnetic map bears a resemblance to a ground magnetic map, it simplifies the recognition of trends in the rock strata and the interpretation of

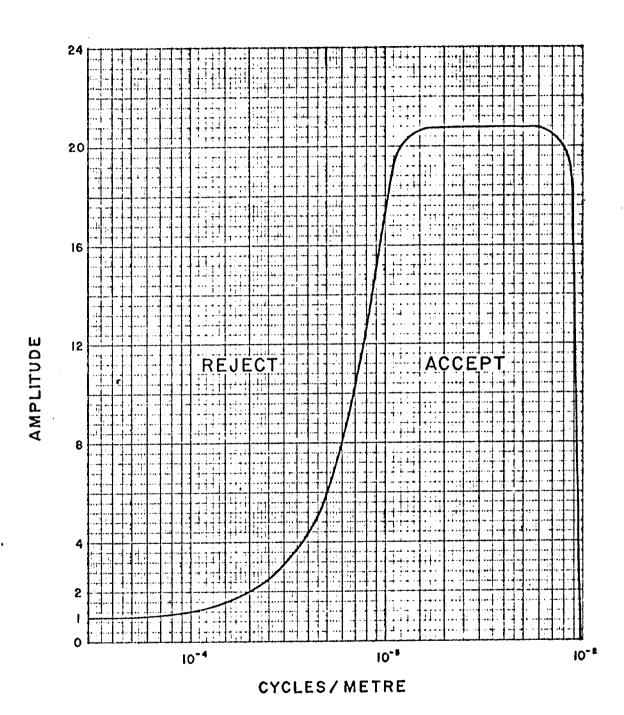


Figure 11-2 Frequency response of magnetic enhancement operator.

geological structure. It defines the near-surface local geology while de-emphasizing deep-seated regional features. It primarily has application when the magnetic rock units are steeply dipping and the earth's field dips in excess of 60 degrees.

VLF-EM

VLF-EM anomalies are not EM anomalies in conventional sense. EM anomalies primarily reflect eddy currents flowing in conductors which have been energized inductively by the primary field. In contrast, VLF-EM anomalies primarily reflect current gathering, which is a non-inductive phenomenon. The primary field sets currents which flow weakly in rock and overburden, and these tend to collect in low resistivity zones. Such zones may be due to massive sulfides, shears, river valleys and even unconformities.

The Herz Industries Ltd Totem VLF-electromagnetometer measures the total field and vertical quadrature components. Both these components are digitally recorded in the aircraft with a sensitivity of 0.1 percent. The total field yields peaks over VLF-EM current concentrations

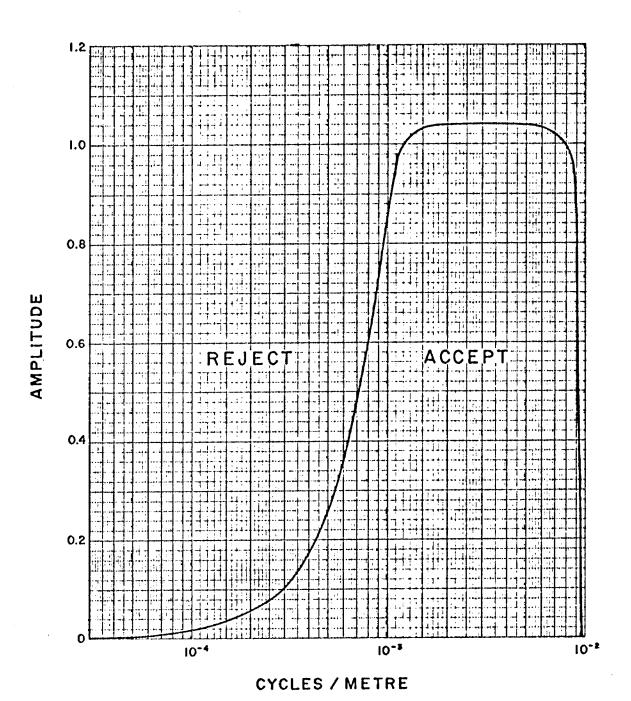


Figure II-3 Frequency response of VLF-EM operator.

whereas the quadrature component tends to yield crossovers. Both appear as traces on the profile records. The total field data also are filtered digitally and displayed on a contour map, to facilitate the recognition of trends in the rock strata and the interpretation of geologic structure.

The response of the VLF-EM total field filter operator in the frequency domain (Figure II-3) is basically similar to that used to produce the enhanced magnetic (Figure II-2). The two filters are identical along the abscissa but different along the ordinant. filter removes long wavelengths such as those which reflect regional and wave transmission variations. The filter sharpens short wavelength responses such as those which reflect local geological variations. The filtered total field VLF-EM contour map is produced with a contour interval of one percent.

MAPS ACCOMPANYING THIS REPORT

Five map sheets accompany this report:

Electromagnetic Anomalies	1	map	sheet
Resistivity	1	map	sheet
Magnetics	1	map	sheet
Enhanced Magnetics	1	map	sheet
Filtered Total VLF-EM Field	1	map	sheet

Respectfully submitted, DIGHEM LIMITED

Z. Scord

Z. Dvorak
Vice-President

APPENDIX A

THE FLIGHT RECORD AND PATH RECOVERY

Both analog and digital flight records were produced. The analog profiles were recorded on chart paper in the aircraft during the survey. The digital profiles were generated later by computer and plotted on electrostatic chart paper at a scale of 1:10,000. The digital profiles are listed in Table A-1.

In Table A-1, the log resistivity scale of 0.03 decade/mm means that the resistivity changes by an order of magnitude in 33 mm. The resistivities at 0, 33, 67, 100 and 133 mm up from the bottom of the digital flight record are respectively 1, 10, 100, 1,000 and 10,000 ohm-m.

The fiducial marks on the flight records represent points on the ground which were recovered from camera film. Continuous photographic coverage allowed accurate photo-path recovery locations for the fiducials, which were then plotted on the geophysical maps to provide the track of the aircraft.

The fiducial locations on both the flight records and flight path maps were examined by a computer for unusual helicopter speed changes. Such speed changes may denote

an error in flight path recovery. The resulting flight path locations therefore reflect a more stringent checking than is provided by standard flight path recovery techniques.

Table A-1. The Digital Profiles

Channel			Scale
Name (Fre		Observed parameters	units/mm
MAG		magnetics	10 nT
ALT		bird height	1 ppm
		vertical coaxial coil-pair inphase vertical coaxial coil-pair quadrature	1 ppm
			1 ppm
, , ,	0 Hz)	·	1 ppm
	00 Hz)		1 ppm
		horizontal coplanar coil-pair quadrature	1 ppm
	00 Hz)		1 ppm
•	0 Hz)		1 ppm
'	00 Hz)		1 ppm 1 %
VLFT		VLF-EM total field (primary station)	1 %
VLFQ		VLF-EM vertical quadrature (primary station)	1 %
VT2		VLF-EM total field (secondary station)	18
VQ2		VLF-EM vertical quadrature (secondary station)	1.0
		Computed Parameters	
DIFI (90	00 Hz)	difference function inphase from CXI and CPI	1 ppm
DIFQ (90	00 Hz)	difference function quadrature from CXQ and CPQ	1 ppm
REC1		first anomaly recognition function	1 ppm
REC2		second anomaly recognition function	1 ppm
REC3		third anomaly recognition function	1 ppm
REC4		fourth anomaly recognition function	1 ppm
CDT		conductance	1 grade
RES (9)	00 Ez)	log resistivity	.03 decade
RES (72)	00 Hz)		.03 decade
DP (90	00 Hz)		3 m
•	00 Hz)		3 m
FEO% (9	00 Hz)	apparent weight percent magnetite	0.25%

APPENDIX B

EM ANOMALY LIST

				AXIAL OO HZ		LANAR 00 HZ		LANAR 00 HZ			PICAL .		ZONTAL EET	CONDUCE EAR!	
	OMAL				REAL PPM	QUAD PPM	REAL PPM			COND MHOS	DEPTH*.	COND MHOS		RESIS OHM-M	DEPTH M
L	NE	1	(E	LIGHT	1)	1			•		•				
A	430		ò	9	3	6	6	62	•	1	0.	1	93	966	0
В	432	B?	0	0	3	5	3	57		2	57.		209	41	167
С	438	s	0	7	1	11	18	34		1	0.	. 1	46	741	0
D	442	S	0	9	0	14	31	36	•	1	9.	1	17	268	0
	· • • • • • • • • • • • • • • • • • • •		,-						•		•				
	NE 493	2	_	LIGHT			-	rn	•		•				_
A	493		0	5	0	8	5	57		1	0.		1	1925	0
B	464		0	8	0	14	22	105		1	0.		26	618	0
D	459		0	11 10	0	28	42	185		1	0.	•	7	419	0
υ 	439		U	10	U	20	21	140		1	0.	1	8	308	0
LI	NE	3	(F	LIGHT	1)				:		•				
A	600	S	Ö	6	o o	11	10	73		1	0.	1	3	979	0
В	632	S	0	8	0	14	19	100		1	0.	1	8	725	ō
D	640	S?	2	13	1	23	8	165		1	0.	1	20	555	0
E	645	S?	8	6	0	10	5	72		5	28 .	1	75	856	ŏ
F	655	S	0	8	0	15	40	97		1	0 .	1	8	382	Ö
									•		•				
	NE	4		LIGHT	•				٠		•				
A	716		0	12	0	23	20	163		1	0.	. 1	10	673	0
В	710		0	3	0	8	6	63		1	19.	1	63	792	0
D	692		0	5	0	13	17	88		1	0.	1	15	494	0
E	688		2	2	0	6	12	38		1	2.	1	20	376	0
F	676		0	19	0	37	79	221	•	1	0.	1	14	136	0
LT	NE	5	(F	LIGHT	1)				•		•				
A	811		o \-	6	0	13	18	93	•	1	0.	1	10	739	0
В	827		2	2	Õ	14	8	94	•	i	6.	i	29	683	0
С	830	S	0	13	Ō	25	54	161	•	1	0.	1	7	290	0
D	840	s	2	21	0	36	112	215		1	0.	1	1	379	Ö
E	845		0	6	0	20	56	110		1	0.	1	17	156	Õ
									•		•				
	NE			LIGHT	-				•		•				
	949		0	3	1	8	14	54		1	0.	1	10	927	0
В	945		1	4	1	7	13	59		1	0.	1	11	737	0
C	893		1	10	0	19	31	142		1	0.	1	9	475	0
D	879		5	13	0	35	81	218		1	0.	1	11	199	0
E	873		0	9	0	19	40	73		1	0.	1	17	514	0
F	859		0	19	0	33	82	194		1	0.	1	7	464	0
G	855	5	0	16	0	31	53	210	•	1	0.	1	9	209	0
T. T1	ne Ne	7	10	LIGHT	41				•		•				
	1041		0	3	1) 0	7	10	51	•	1	0.	1	72	900	^
	1		•	•	v	•	, 0	٠,	•	'	.	•	12	890	0

^{.*} ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

[.] OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

		XIAL O HZ		ANAR 00 HZ		LANAR 00 HZ			rical .		ZONTAL EET	CONDUC	
ANOMALY/ : FID/INTERP	REAL PPM	QUAD	REAL PPM	QUAD PPM	REAL PPM			COND MHOS		COND		RESIS OHM-M	DEPTH M
LINE 7	(F	LIGHT	1)				•		•				
B 1043 S	Ò	3	0	7	9	51	•	1	0.	1	13	1243	. 0
C 1055 S	2	11	0	23	26	148		1	1.	1	27	571	0
D 1063 H	13	9	0	15	41	97	•	6	18 .	1	33	695	0
200 and and and any pad any pad and							•		•				•
LINE 8	-	LIGHT			^	25	•		. •	_			_
А 1095 S С 1079 Н	0	2 11	0	3 21	0	35		1	4 .	1	12	3352	0
C 1079 n	U	1.1	U	21	28	136	•	1	0.	1	20	455	. 0
LINE 9	(F)	LIGHT	1)				•		•				
B 1230 S	-	3	o o	7	11	47		1	0.	1	16	986	0
C 1242 S	0	5	0	13	34	79		1	0.	1	22	273	3
										-			•
LINE 10	(F1	LIGHT	1)				•		•				
A 1271 H	0	6	0	13	29	69		1	0.	1	14	275	0
В 1268 Н	0	5	0	15	34	93		1	0.	1	23	272	4
C 1260 S	774	3	0	6	9	40	•	1	0.	1	19	382	0
LINE 11	/ P 1	LIGHT	1)				•		•				
A 1410 S	0	7	0	12	24	84	•	1	0.	1	8	468	•
B 1437 S	0	7	0	10	13	81		1	0.	1	7	859	0
C 1485 S	ŏ	8	Ŏ	18	53	90		1	0.	1	17	162	0
D 1492 B	0	7	0	8	28	54		1	Ŏ.	1	10	547	0
E 1501 S	0	2	1	7	37	19		4	11 .	1	23	94	6
F 1510 S	0	4	0	9	35	30		2	0 .	1	11	110	ŏ
							•		•				
LINE 12		LIGHT	1)				•						
A 1723 S	0	2	0	3	4	32		1	0.	1		2592	0
B 1713 S	0	2	0	8	5	50		1	0.	1	5	2115	0
C 1682 H	0	3	0	5	12	36		1	7.	1	34	596	8
D 1669 S E 1664 S	0	9 8	0	17 14	59 53	89 78		1	0.	1	12	135	0
F 1652 S	0	15	0	28	90	139		1	0.	1	9 12	138	0
	·	13	Ū	20	90	133	•	•	0.		12	110	0
LINE 13	(FI	LIGHT	2)						•				
A 533 B?	0	2	0	6	9	27		1	4 .	1	37	767	8
В 611 Н	1	1	0	2	7	19		1	0.	1	31	736	1
С 622 Н	0	9	1	17	51	103	•	1	2.	1	25	172	7
D 630 H	1	5	2	10	41	60		1	10 .	1	28	116	12
Е 638 Н	0	7	0	12	35	60		1	4.	1	19	203	1
F 641 H	1	8	0	20	45	96	•	1	0.	1	24	410	2
LINE 14	/151	TOUM	21				•		•				
A 759 B?	(F.T	JIGHT 2	2) 1	1	9	23	٠	4	•	4	4.0	500	^
1. 133 01	V	4	•	•	,	23	•	1	0.	1	40	598	8

^{.*} ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

				AXIAL 00 HZ		CANAR 00 HZ		LANAR 00 HZ		TICAL .	HORI:		CONDUC EAR	
A! FII	NOMAL D/INT	Y/ 1 ERP	REAL PPM	QUAD PPM	REAL PPM		REAL PPM		. COND . MHOS		MHOS		RESIS OHM-M	DEPTH M
L	INE	14	(E	LIGHT	2)	1			•	•				
В			1	6	2	10	36	57		0.	1	17	213	0
c -	666	s 	1	10	2	23	93	71	. 3	0.	1	17	78	3
L	INE	15	(F	LIGHT	2)	ı				•				
A	783	B?	0	3	0	4	12	39	. 1	1.	1	41	504	14
В	864		0	4	0	12	34	57	. 1	8.	1	33	371	10
С	870		1	7	0	12	38	91	. 1	0.	1	13	238	0
D	888		0	11	0	13	52	118		0.	1	10	118	0
E	900		1	9	0	15	66	82		0.	•	11	72	0
F			0	12	0	30	89	99		0.		21	74	7
G 	907		0	9	0	18	56	122	. 1	. 0.	1	22	167	4
L	INE	16	(F	LIGHT	2)				•	•				
A	1109	S?	0	2	0	6	27	36	. 1	0.	1	32	220	8
В	1027	S	1	7	0	17	49	94	. 1	0.	1	17	187	0
C	1004	s	0	3	0	9	14	60	. 1	0.	1	16	668	Ō
D	998	S	0	17	0	42	149	58	. 8	0.	1	13	71	0
E	996	S	0	8	0	18	73	73	. 2	0.	1	15	67	1
T.3	NE	17	/10	LIGHT	2)				•	•				
	1131		0	4	2,	10	29	46	. 1	6.		22	477	4.5
	1137		1	5	Õ	11	28	45		9.	1	33 38	177 234	13 16
	1218		1	8	2	37	61	180		0.	i	14	103	0
	1249		1	11	1	26	67	149		0.	1	10	199	0
	1254		2	12	2	27	101	128		0.	i	28	78	14
									•	•				
	NE	18		LIGHT	2)				•	•				
	1395		0	3	3	4	23	40		2.	1	44	352	17
	1393		0	2	4	9	16	52		20 .	1	108	154	60
C D	1388 1382		0	5 10	0	9	23	44		13.	1	35	249	15
	1373		0	2	0 1	17 2	50 17	98 10		0.	1	26	215	7
	1370		0	1	i	1	13	6	_	22 . 27 .	1	32 37	384 271	6
	1354		ŏ	3	o ·	6	11	53		0.	1	9	955	12 0
	1341		Ö	2	1	3	6	30		ŏ.	1	16	1305	0
	1313		1	16	3	32	91	77		2.	1	13	68	ŏ
K	1304	H	1	5	2	12	40	52		12 .	1	30	102	14
	1295		1	3	1	4	18	17	. 1	24 .	1	32	221	11
	1292		1	3	1	13	44	77		4.	1	30	341	8
	1274		1	17	3	33	112	172		0.	1	30	92	15
Q	1270	S	1	6	1	13	49	56	. 2	0.	1	30	61	15

^{.*} ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT . LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

				AXIAL OO HZ		ANAR 00 HZ		LANAR 00 HZ			rical .		ZONTAL EET	CONDUC EAR	
AN	IOMAL	Y/ 1	REAL	OUAD	REAL	OUAD	REAL	CAUO	•	COND	DEPTH*.	COND	איזים אַרו	PECTC	אייסימת
)/INT			PPM	PPM	PPM	PPM			MHOS		MHOS		OHM-M	M
-									•		•				
	NE	19		LIGHT					٠		•				
	1411		1	6	1	12	23	78		1	0.	1	19	371	0
	1416		0	2	1	4	9	42		1	2.	1	78	724	4
	1422 1436		0	3	0	4	12	30		1	6.	1	35	517	9
	1449		0	4 6	0	8 12	22 30	42 88		1	4.	1	31	250	9
	1460		0	4	0	7	11	57		1	0.	1	14 12	411 1015	0
	1473		1	9	0	21	57	124		1	0.	1	21	219	1
	1478		Ò	5	0	11	37	61		i	0.	i	19	164	1
	1493		1	9	1	18	58	84		1	0.	1	13	70	0
J	1506	B?	0	5	1	10	31	54		1	6.	1	28	169	10
	1514		0	5	0	11	28	42		1	11.	1	29	220	9
L	1535	E?	4	14	1	30	98	136	•	1	0.	1	29	605	0
 T T	ME	20	10	1 T (1) M	21				•		•				
	NE 1671	20	(£ 0	LIGHT	•		43	40	•		•		••		
	1652		0	4	0	4 11	13 37	40 66		1	0.	1	28	428	4
	1643		1	5	0	11	25	68		1	4.	1	28	186	9
	1642		1	7	1	20	45	133		1	0.	1	19 11	254 248	0 0
	1591		1	4	i	6	39	32		2	16.	1	29	126	12
	1552		2	5	6	31	134	133		2	6.	1	30	65	16
H	1550	B?	3	5	6	26	27	79		3	8.	1	19	203	0
									•		•				-
LI		21	(F	LIGHT	2)				•		•				
	1681		0	8	1	17	39	89		1	0.	1	21	234	0
	1705		1	13	1	28	81	155		1	0.	1		173	5
	1715		1	17	0	40	121	225		1	0.	1	9	112	0
	1744 1750		1	12 16	0	44	129	239		1	0.	1	9	112	0
	1753		1	16	0 1	26 45	80 134	150 227		1	0 . 0 .	1	9 10	90	0
	1796		1	5	Ó	11	37	63		1	4			93	0
	1818		1	12	2	43	158	198		1	0.	1	16 8	185 363	0
	1820		1	4	5	43	150	198		2	0.	i	18	50	5
	1832		3	12	5	21	64	82		1	4.	1	28	43	16
K	1836	H	3	12	7	27	104	100		2	0.	ì	30	49	15
									•		•				, ,
	NE		(F	LIGHT	2)				•		•				
	1977		0	6	0	15	18	108		1	0.	1	19	275	0
	1971		0	5	1	10	27	66		1	2.	1	23	230	4
	1966		1	9	0	26	80	113		1	0.	1	16	112	1
	1961 1927		1	18 6	1 2	34	104	93		3	0.	1	9	73	0
£	1741	5	1	О	2	35	134	196	•	2	0.	1	12	79	0

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[.] OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

[.] LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

NOMALY REAL QUAD REAL QUAD REAL QUAD COND DEPTH COND DEPTH RESIS DEPTH PID INTERP PPM PPM					AXIAL OO HZ		CANAR 00 HZ		LANAR 00 HZ			rical .		ZONTAL EET	CONDUC EAR	
FID/INTERP PPM PPM PPM PPM PPM PPM PPM Modes M Modes M Modes M OHM-M M Note	Α	NOMAL	Y/ 1	REAL	QUAD	REAL	OUAD	REAL	OUAD	•	COND	DEPTH*.	COND	שייים יוו	DECTO	משמשת
LINE 22 (FLIGHT 2) F 1898 H 0 5 5 0 12 42 67 1 0 1 15 122 0 G 1853 S 3 29 4 50 175 207 1 0 1 0 275 0 LINE 23 (FLIGHT 2) LINE 23 (FLIGHT 2) LINE 23 (FLIGHT 2) LOVER 1 16 1 29 84 61 3 7 1 16 114 1 B 2010 S 0 23 0 43 131 180 2 0 1 10 71 0 C 2017 B? 0 4 0 11 32 34 1 20 1 37 229 17 D 2044 S 1 21 1 40 160 127 3 0 1 12 63 0 E 2048 S 0 14 0 40 116 232 1 0 1 11 239 0 G 2063 H 1 7 1 17 47 99 1 0 1 11 339 0 G 2063 H 1 7 1 17 47 99 1 0 1 12 127 5 H 2074 H 0 7 1 14 41 66 1 1 1 1 1 20 141 3 I 2106 H 1 9 4 22 104 86 3 4 1 2 2 104 1 3 I 2106 H 1 9 4 22 104 86 3 4 1 2 1 1 1 5 20 K 2126 S 0 8 0 11 39 58 1 0 1 1 0 1 20 90 2 LINE 24 (FLIGHT 2) LINE 24 (FLIGHT 2) A 2257 S 0 3 0 5 5 13 28 1 0 0 1 20 90 2 LINE 24 (FLIGHT 2) A 2257 S 0 3 0 5 5 13 28 1 0 0 1 8 221 0 B 2248 S 0 9 0 15 33 81 1 0 1 6 396 0 B 2248 S 0 9 0 15 33 81 1 0 0 1 8 221 0 C 2141 H 1 8 1 15 58 62 2 5 1 21 105 5 H 2136 S 1 8 0 20 72 75 2 0 1 10 20 0 LINE 251 (FLIGHT 2) LINE 251 (FLIGHT 2) A 258 S 0 5 1 9 40 12 8 0 1 10 11 10 202 0 LINE 251 (FLIGHT 2) A 258 S 0 5 1 9 40 12 8 0 1 10 11 10 202 0 LINE 251 (FLIGHT 2) A 258 S 0 5 1 9 40 12 8 0 1 11 10 10 10 50 0 C 2569 S 1 9 1 14 31 86 1 0 1 1 10 202 0 LINE 251 (FLIGHT 2) A 258 S 0 5 1 9 40 12 8 0 1 22 127 3 B 2577 S 0 3 1 9 30 48 1 0 1 1 1 10 202 0 LINE 251 (FLIGHT 2) A 258 S 0 5 1 9 40 12 8 0 1 22 127 3 B 2577 S 0 3 1 9 30 48 1 0 1 1 11 160 0 C 2569 S 1 9 1 14 31 86 1 0 1 1 11 160 0 C 2569 S 1 9 1 14 31 86 1 0 1 1 11 20 11 30 0 C 2569 S 1 9 1 14 31 86 1 0 1 1 12 113 0 C 2569 S 1 9 1 14 31 86 1 0 0 1 12 21 127 85 11 LINE 26 (FLIGHT 3) A 619 S 1 2 1 5 21 20 1 0 1 24 119 1 B 629 H 2 10 2 17 58 92 1 0 0 1 24 119 1 B 629 H 2 10 2 17 58 92 1 0 0 1 21 125 4 C 658 S 0 6 0 15 58 80 1 1 0 1 1 1 388 0 E 678 S 0 6 0 1 2 0 17 37 111 1 1 0 1 1 23 304 304 3 D 665 S 0 4 0 11 24 72 1 1 0 1 1 1 388 0 E 678 S 0 6 0 6 0 15 58 80 1 1 0 1 1 1 1 388 0	FI	D/INT	ERP	PPM	PPM	PPM	PPM									
F 1898 H 0 5 0 12 42 67 1 0 1 15 122 0 G 1853 S 3 29 4 50 175 207 1 0 1 0 1 0 275 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1										•			14100	11	Onn-m	M,
G 1853 S 3 29 4 50 175 207 1 0 1 0 275 0 LINE 23 (FLIGHT 2) A 2004 S 1 16 1 29 84 61 3 7 1 16 114 1 B 2010 S 0 23 0 43 131 180 2 0 1 10 71 0 C 2017 BP 0 4 0 11 32 34 1 20 1 37 229 17 D 2044 S 1 21 1 40 160 127 3 0 1 12 63 0 E 2048 S 0 14 0 40 116 232 1 0 1 11 239 0 E 2048 S 0 14 0 40 116 232 1 0 1 11 239 0 G 2063 H 1 7 1 17 47 99 1 0 1 11 239 0 G 2063 H 1 7 1 17 47 99 1 0 1 11 20 141 3 I 2106 H 1 9 4 22 104 86 1 1 1 1 20 141 3 I 2106 H 1 9 4 22 104 86 3 4 1 29 56 16 X 2126 S 0 8 0 11 39 58 1 0 1 10 582 0 K 2126 S 0 8 0 11 39 58 1 0 1 10 582 0 E 2048 S 0 9 0 15 33 81 1 0 1 0 582 0 E 2048 S 0 0 4 0 11 14 59 1 0 1 8 221 0 E 2196 S 0 4 0 11 14 59 1 0 1 0 1 6 396 0 E 2141 H 1 8 1 15 58 62 2 5 1 21 105 5 H 2136 S 1 8 0 20 77 75 2 0 1 10 1 10 200 0 LINE 251 (FLIGHT 2) A 2586 S 0 5 1 9 40 12 8 0 1 10 20 0 LINE 251 (FLIGHT 2) A 2586 S 0 5 1 9 40 12 8 0 1 1 1 1 10 20 0 LINE 251 (FLIGHT 2) A 2586 S 0 5 1 9 40 12 8 0 1 1 22 127 3 B 2577 S 0 3 1 9 30 48 1 0 1 1 1 1 10 20 0 LINE 251 (FLIGHT 2) A 2586 S 0 5 1 9 40 12 8 0 1 1 22 127 3 B 2577 S 0 3 1 9 30 48 1 0 1 1 1 1 10 20 0 LINE 251 (FLIGHT 2) A 2586 S 0 5 1 9 40 12 8 0 1 1 22 127 3 B 2577 S 0 3 1 9 30 48 1 0 1 1 1 1 10 20 0 LINE 251 (FLIGHT 2) A 2586 S 0 5 1 9 40 12 8 0 1 1 22 127 3 B 2577 S 0 3 1 9 30 48 1 0 1 1 1 1 10 20 0 LINE 251 (FLIGHT 2) A 2586 S 0 5 1 9 40 12 8 0 1 1 22 127 3 B 2577 S 0 3 1 9 30 48 1 0 1 1 1 1 10 0 0 C 2569 S 1 9 1 1 1 14 31 86 1 0 1 1 1 1 1 10 0 E 2539 S 1 2 1 1 2 49 58 1 0 0 1 1 12 113 0 E 2539 S 1 2 1 1 2 49 58 1 0 0 1 1 12 113 0 E 2539 S 1 2 1 1 2 49 58 1 0 0 1 1 24 119 1 E 1NE 26 (FLIGHT 3) A 619 S 1 2 1 5 21 20 1 0 0 1 24 119 1 B 629 H 2 10 2 17 58 892 1 0 0 1 1 1 1 23 304 3 E 678 S 0 6 0 0 15 58 80 1 1 0 0 1 1 1 1 388 0 E 678 S 0 6 0 6 0 15 58 80 1 1 0 0 1 1 10 241 0	L	INE	22	(E	LIGHT	2)						•				
G 1853 S 3 29 4 50 175 207 . 1 0 . 1 0 275 0 LINE 23 (FLIGHT 2) A 2004 S 1 16 1 29 84 61 3 7 . 1 16 114 1 B 2010 S 0 23 0 43 131 180 . 2 0 . 1 10 71 0 C 2017 B? 0 4 0 11 32 34 . 1 20 . 1 37 229 17 D 2044 S 1 21 1 40 160 127 . 3 0 . 1 12 63 0 E 2048 S 0 14 0 40 116 232 . 1 0 . 1 11 239 0 G 2063 H 1 7 1 17 47 99 . 1 0 . 1 11 239 0 G 2063 H 1 7 1 17 47 99 . 1 0 . 1 11 20 141 3 I 2106 H 1 9 4 22 104 86 . 3 4 . 1 20 . 1 37 229 LINE 24 (FLIGHT 2) A 2257 S 0 3 0 5 13 28 . 1 0 . 1 10 582 0 B 2248 S 0 9 0 15 33 81 . 1 0 . 1 10 582 0 B 2248 S 0 9 0 15 33 81 . 1 0 . 1 0 . 582 0 B 2248 S 0 9 0 15 33 81 . 1 0 . 1 8 221 0 D 2218 S 0 7 0 20 72 76 . 2 0 . 1 8 172 0 E 2196 S 0 4 0 11 14 59 . 1 0 . 1 0 . 457 0 F 2188 H 0 6 0 9 57 21 . 6 9 . 1 2 11 105 5 F 2188 H 0 6 0 9 57 21 . 6 9 . 1 12 161 0 G 2141 H 1 8 1 15 58 62 . 2 5 . 1 21 105 5 H 2136 S 1 8 0 20 77 75 . 2 0 . 1 10 20 0 LINE 251 (FLIGHT 2) LINE 251 (FLIGHT 2) A 2586 S 0 5 1 9 1 14 3 186 . 1 0 . 1 16 0 0 C 2569 S 1 9 1 14 0 31 86 . 1 0 . 1 15 275 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 12 21 13 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 15 275 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 12 21 3 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 0 20 77 106 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 0 20 77 106 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 186 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 18 6 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 18 6 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 18 6 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 18 6 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 18 6 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 18 0 . 1 0 . 1 12 251 0 C 2569 S 1 9 1 14 3 18 0 . 1 0 . 1 12 251 0 C 2569 S 0 4 0 1 1 24 72 . 1 0 . 1 10 241 0				0	-	0	12	42	67		1	0.	1	15	122	0
LINE 23 (FLIGHT 2) A 2004 S 1 16 1 29 84 61 3 7 1 16 114 1 B 2010 S 0 23 0 43 131 180 2 0 1 10 71 0 C 2017 B7 0 4 0 11 32 34 1 20 1 37 229 17 D 2044 S 1 21 1 40 160 127 3 0 1 12 63 0 E 2048 S 0 14 0 40 116 232 1 0 1 11 239 0 F 2058 S 0 11 0 20 62 123 1 0 1 11 239 0 G 2063 H 1 7 1 17 47 99 1 0 1 10 359 0 G 2063 H 1 7 1 17 47 99 1 0 1 21 127 5 H 2074 H 0 7 1 14 41 66 1 1 1 1 20 141 3 I 2106 H 1 9 4 22 104 86 3 4 1 29 56 16 J 2121 S 2 10 2 7 28 36 1 0 1 10 582 0 K 2126 S 0 8 0 11 39 58 1 0 1 20 90 2 LINE 24 (FLIGHT 2) A 2257 S 0 3 0 5 13 28 1 0 1 20 90 2 LINE 24 (FLIGHT 2) A 2258 S 0 4 0 11 14 59 1 0 1 8 221 0 B 2248 S 0 9 0 15 33 81 1 0 1 8 821 0 D 2218 S 0 7 0 20 72 76 2 0 1 8 872 0 E 2196 S 0 4 0 11 14 59 1 0 1 0 457 0 F 2188 H 0 6 0 9 57 21 6 9 1 12 161 0 C 2141 H 1 8 1 15 58 62 2 5 5 1 21 10 20 0 LINE 251 (FLIGHT 2) A 2566 S 0 5 1 9 40 12 8 0 0 1 12 20 0 LINE 251 (FLIGHT 2) A 2586 S 0 5 1 9 40 12 8 0 0 1 12 12 13 0 E 2539 S 1 2 1 12 49 58 1 0 0 1 12 251 0 C 2569 S 1 9 1 1 4 3 86 1 0 1 1 15 275 0 D 2561 S 1 14 0 20 71 106 1 0 1 12 251 0 F 2533 S 0 5 2 10 42 77 58 92 1 0 1 10 11 27 85 11 LINE 26 (FLIGHT 3) A 619 S 1 2 1 5 21 20 1 0 1 0 1 24 119 1 B 629 H 2 10 2 17 58 92 1 0 0 1 23 304 3 E 678 S 0 6 0 4 0 11 24 72 1 0 1 1 2 2 113 304 3 E 678 S 0 6 0 6 0 15 58 80 1 0 0 1 1 2 2 11 3 304 3 E 678 S 0 6 0 6 0 15 58 80 1 0 0 1 1 11 13 88 0 E 678 S 0 6 6 0 15 58 80 1 1 0 1 1 1 1 1 1 388 0 E 678 S 0 6 6 0 15 58 80 1 1 0 1 1 1 1 1 1 388 0 E 678 S 0 6 6 0 15 58 80 1 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	G	1853	S	3	29	4	50	175	207		1	0.	'1			_
A 2004 S										•		•				
B 2010 S										•		•				
C 2017 B? 0 4 0 11 32 34 1 20 1 37 229 17 D 2044 S 1 21 1 40 160 127 3 0 1 12 63 0 E 2048 S 0 14 0 40 116 232 1 0 1 11 263 0 E 2048 S 0 11 0 20 62 123 1 0 1 11 239 0 G 2063 H 1 7 1 17 47 99 1 0 1 1 10 359 0 G 2063 H 1 7 1 17 47 99 1 0 1 21 127 5 H 2074 H 0 7 1 14 41 66 1 1 1 1 20 141 3 I 2106 H 1 9 4 22 104 86 3 4 1 29 56 16 J 2121 S 2 10 2 7 28 36 1 0 0 1 10 582 0 K 2126 S 0 8 0 11 39 58 1 0 1 10 1 20 90 2 LINE 24 (FLIGHT 2) A 2257 S 0 3 0 5 13 28 1 0 0 1 8 221 0 B 2248 S 0 9 0 15 33 81 1 0 0 1 8 221 0 E 2196 S 0 4 0 11 14 59 1 0 1 8 221 0 E 2196 S 0 4 0 11 14 59 1 0 1 0 457 0 F 2188 H 0 6 0 9 57 21 6 9 1 12 161 0 G 2141 H 1 8 1 15 58 62 2 5 1 21 10 2 0 F 2186 S 0 5 1 9 40 12 8 0 0 1 1 10 202 0 LINE 251 (FLIGHT 2) LINE 251 (FLIGHT 2) A 2569 S 1 9 1 14 31 86 1 0 1 1 1 1 160 0 C 2569 S 1 9 1 14 31 86 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				-						-					114	1
D 2044 S										-			•			0
E 2048 S				•						-		_				
F 2058 S				•									•			_
G 2063 H				-		_							-			
H 2074 H 0 7 1 14 41 66 1 1 1 1 20 141 3 I 2106 H 1 9 4 22 104 86 3 4 1 29 56 16 J 2121 S 2 10 2 7 28 36 1 0 1 10 582 0 K 2126 S 0 8 0 11 39 58 1 0 1 20 90 2 LINE 24 (FLIGHT 2) A 2257 S 0 3 0 5 13 28 1 0 1 6 396 0 B 2248 S 0 9 0 15 33 81 1 0 1 8 221 0 D 2218 S 0 7 0 20 72 76 2 0 1 8 172 0 E 2196 S 0 4 0 11 14 59 1 0 1 0 457 0 F 2188 H 0 6 0 9 57 21 6 9 1 12 161 0 G 2141 H 1 8 1 15 58 62 2 5 1 21 105 5 H 2136 S 1 8 0 20 72 75 2 0 1 10 20 0 LINE 251 (FLIGHT 2) A 2586 S 0 5 1 9 40 12 8 0 1 10 11 10 202 0 LINE 251 (FLIGHT 3) A 2586 S 1 2 1 12 49 58 1 0 1 1 1 12 113 0 E 2539 S 1 2 1 12 49 58 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				_							•					
I 2106 H				•									•			
J 2121 S				_									•			_
K 2126 S										-	_					
LINE 24 (FLIGHT 2) A 2257 S 0 3 0 5 13 28 1 0 1 8 221 0 B 2248 S 0 9 0 15 33 81 1 0 1 8 221 0 D 2218 S 0 7 0 20 72 76 2 0 1 8 172 0 E 2196 S 0 4 0 11 14 59 1 0 1 0 457 0 F 2188 H 0 6 0 9 57 21 6 9 1 12 161 0 G 2141 H 1 8 1 15 58 62 2 5 1 21 105 5 H 2136 S 1 8 0 20 72 75 2 0 1 10 202 0 LINE 251 (FLIGHT 2) A 2586 S 0 5 1 9 40 12 8 0 1 22 127 3 B 2577 S 0 3 1 9 30 48 1 0 1 11 160 0 C 2569 S 1 9 1 14 31 86 1 0 1 11 160 0 C 2569 S 1 9 1 14 31 86 1 0 1 1 15 275 0 D 2561 S 1 14 0 20 71 106 1 0 1 12 113 0 E 2533 S 0 5 2 10 42 34 2 0 1 1 1 12 251 0 F 2533 S 0 5 2 10 42 34 2 0 1 1 2 251 0 G 2527 H 0 4 0 6 39 25 3 10 1 27 85 11 LINE 26 (FLIGHT 3) A 619 S 1 2 1 5 21 20 1 0 1 24 119 1 B 629 H 2 10 2 17 58 92 1 0 1 21 125 4 C 654 H 0 12 0 17 37 111 1 0 1 1 23 304 3 D 665 S 0 4 0 11 24 72 1 0 1 10 21 1388 0 E 678 S 0 6 6 0 15 58 80 1 0 1 0 1 11 388 0				0							•	- •	•			
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^{.*} ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

				AXIAL OO HZ		LANAR 00 HZ		LANAR 00 HZ			FICAL .		ZONTAL EET	CONDUC EAR	
A FI	NOMAL D/INT	Y/ I	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	•	COND MHOS	DEPTH*. M .	COND MHOS		RESIS OHM-M	DEPTH M
 I.	INE	26	/16	LIGHT	. 3)				•		•				
G			1	4	0	9	40	24	٠	3	9.	4	20		
Н			Ô	3	0	12	37	49		1	^	1	28 31	51	14
I	723	Н	0	6	Ŏ	16	54	63	-	2	1.	1	31	45 50	17
J	741	H	0	5	0	10	24	55		1	0.	1	34	112	17 16
K	743	Н	0	6	0	10	49	74		1	0.	1	31	89	14
									٠		•				
_	INE	27	•	LIGHT	•				•		•				
A			0	6	1	13	35	85		1	0.	1	0	318	0
B C	863 849		1	13	0	16	48	95		1	0.	1	22	586	0
D			1	5	0	8	21	67	•	1	0.	1	0	708	0
E	837		0	8 0	0 2	7	16		٠	1	0.	1	3	625	0
F	813		0	7.		5 21	7	30		1	13 .	1	168	440	55
G	809		1	17	1	31	75 115		•	3	0.	1	5	131	0
Н	800		Ö	4	Ö	<i>3</i> 1	24	136 39	•	2	0.]	5	103	0
ī	792		2	7	5	15	57		•	1 6	5. 13.	1	11	279	0
J	772		1	6	2	12	43	34	-	2	11 .		20	68	6
K	765		Ö	2	0	4	18	25		1	0.	1	21	214	2
L	761		1	5	Ö	3	7	8	•	1	0.	• 1	0 28	311 741	0
M	757	Н	1	10	Ō	18	50	98	•	•	0.	. 1	15	181	0
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r:	INE	28	(F	LIGHT	3)						•				
A	883		1	12	1	25	76	117		1	0 .	1	7	104	0
В	890		1	5	1	18	55	63	•	2	3.	1	12	113	Õ
С	894		1	4	1	16	53	64	•	1	0.	1	6	116	Ŏ
D	897		0	10	1	18	58	89	•	1	0.	1	4	117	Ō
E	910		0	7	1	8	38	129	•	1	0.	1	13	160	0
F	926		0	6	0	12	47	62	•	1	0.	1	1	266	0
H	951		2	7	2	33	125	163		2	0.	1	16	84	2
	990		2	10	1	20	77	73		2	0.	1	3	116	0
J	996	Н	0	10	1	21	75	115	•	1	0.	1	17	140	1
T.T	NE	29	/101	r TOUM	21				•		•				
	1119		2	LIGHT 18	3).	26	105	124	•	•	•	_			
	1091		0	14	2	26	105	134		2	1.	1	21	49	9
	1084		0	18	0	27 34	60	83		1	2.	1	10	129	0
	1074		1	15	Ö	43	100	200		1	0.	1	9	91	0
	1072		Ó	15	0	43 27	129 77	226		1	0.	1	16	60	3
	1062		1	22	1	35	118	136 192		1	0.	1	18	63	5
	1045		4	13	4	33	125	72		1 2	0.	1	20	57	8
	1026		1	7	1	18	64	53		2	10.	1	15 27	185	0
				-	-		- •		•	-		•	41	73	12

^{.*} ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

[.] OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

[.] LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

NOMALY/ REAL QUAD REAL QUAD REAL QUAD COND DEPTH* COND DEPTH RESIS DEPTH FID/INTERP PPM PPM PPM PPM PPM PPM PPM NHOS M MHOS M OHM—M M M M M M M M M M					AXIAL 00 HZ		LANAR 00 HZ		LANAR 00 Hz			rical . ike .		ZONTAL EET	CONDUC EAR	
J 1019 S	A FI	NOMA: D/IN:	LY/ TERP	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	•	COND MHOS					
J 1019 S	L	INE	29	(F	LIGHT	31	ı			•		•				
K 1014 H 0 11 1 23 64 115				•		- ,		67	84	•	2	•	4	-		•
LINE 30 (FLIGHT 3) A 1445 S 0 4 0 2 10 11 1 1 13 1 30 208 7 B 1439 H 0 5 0 17 54 110 1 0 1 26 121 8 C 1427 H? 2 14 2 24 76 74 2 5 1 21 53 9 D 1414 S 0 11 0 13 61 50 2 6 1 10 101 0 E 1406 S 0 4 0 12 42 28 3 10 1 8 338 0 F 1399 H 0 21 0 37 108 212 1 0 1 8 159 0 H 1375 S 1 11 2 21 60 127 1 0 1 22 93 8 I 1371 H 1 6 4 13 69 67 2 10 1 26 70 13 J 1366 H 2 10 6 23 77 73 2 6 1 23 40 11 K 1361 B? 3 21 5 42 138 147 1 0 1 2 166 0 L 1342 H 1 8 1 18 85 74 2 6 1 25 92 10 M 1334 H 0 7 0 9 30 53 1 0 1 26 142 8 N 1329 H 1 5 1 13 56 39 3 8 1 29 80 14 LINE 31 (FLIGHT 3) A 1142 H 0 9 0 20 40 110 1 0 1 21 177 C 1147 H 0 17 2 30 81 170 1 0 1 22 8 10 E 1165 H 1 14 3 30 94 128 2 0 1 16 77 F 1174 H 0 9 2 2 20 55 105 1 1 1 1 9 95 G 1180 H 0 3 2 12 2 37 123 191 1 0 1 9 58 J 1245 S 1 11 0 20 65 24 1 0 1 1 9 74 LINE 32 (FLIGHT 3) LINE 32 (FLIGHT 3) B 1542 S 2 28 1 52 118 204 1 0 1 9 58 J 1245 S 1 11 3 30 92 145 1 0 1 9 58 LINE 33 (FLIGHT 3) B 1542 S 2 28 1 52 118 204 1 0 1 9 58 J 1245 S 1 11 3 30 92 145 1 0 1 8 36 LINE 33 (FLIGHT 3) B 1542 S 2 28 1 52 118 204 1 0 1 9 58 J 1245 S 1 11 3 30 92 145 1 0 1 8 36 LINE 33 (FLIGHT 3) B 1542 S 2 28 1 52 118 204 1 0 1 9 58 J 1245 S 1 11 3 30 92 145 1 0 1 1 0 1 25 155 B 1681 S 2 13 1 21 82 71 2 0 1 144 40 3	K	1014	H	0						-			-			_
A 1445 S 0 4 0 2 10 11 . 1 13 . 1 30 208 7 B 1439 H 0 5 0 17 54 110 . 1 0 . 1 26 121 8 C 1427 H? 2 14 2 24 76 74 2 5 . 1 21 53 9 D 1414 S 0 11 0 13 61 50 . 2 6 . 1 10 101 0 E 1406 S 0 4 0 12 42 28 . 3 10 . 1 8 338 0 F 1399 H 0 21 0 37 108 212 . 1 0 . 1 8 159 0 H 1375 S 1 11 2 21 60 127 . 1 0 . 1 22 93 8 I 1371 H 1 6 4 13 69 67 . 2 10 . 1 26 70 13 J 1366 H 2 10 6 23 77 73 . 2 6 . 1 23 40 11 K 1361 B? 3 21 5 42 138 147 . 1 0 . 1 2 166 0 L 1342 H 1 8 1 18 85 74 . 2 6 . 1 23 40 11 K 1362 H 1 8 1 18 85 74 . 2 6 . 1 23 40 11 K 1329 H 1 5 1 13 56 39 . 3 8 . 1 29 80 14 LINE 31 (FLIGHT 3) A 1134 S 1551 7 3 18 58 58 2 0 . 1 17 100 1 C 1147 H 0 17 2 30 81 170 . 1 0 . 1 21 177 C 1147 H 0 17 2 30 81 170 . 1 0 . 1 15 101 1 D 1153 H 2 9 1 20 67 78 2 8 . 1 26 73 12 E 1165 H 1 14 3 30 94 128 2 0 . 1 16 77 F 1174 H 0 9 2 2 20 55 105 1 1 1 1 1 9 95 G 1180 H 0 3 2 12 2 28 1 52 118 204 1 0 . 1 9 58 J 1245 S 1 11 3 30 92 145 1 0 . 1 8 36 D 1573 S 1 11 3 30 92 145 1 0 . 1 8 36 D 1573 S 1 11 3 30 92 145 1 0 . 1 8 36 D 1573 S 1 11 3 30 92 145 1 0 . 1 8 36 D 1573 S 1 11 3 30 92 145 1 0 . 1 8 36 D 1573 S 1 11 3 30 92 145 1 0 . 1 8 36 D 1573 S 1 11 3 30 92 145 1 0 . 1 8 36 D 1573 S 1 11 3 30 92 145 1 0 . 1 8 36 D 1570 S 0 15 0 34 86 161 1 0 . 1 16 76 2 D 1573 S 1 11 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	- L	INE	30	(F	יווינויי	31				•		•			• -	. •
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H 1375 S	F	1399	H	0	21							-	1	_		
I 1371 H	H	1375	s	1	11								1			
J 1366 H 2 10 6 23 77 73 . 2 6 . 1 23 40 11 K 1361 B? 3 21 5 42 138 147 . 1 0 . 1 2 166 0 L 1342 H 1 8 1 18 85 74 . 2 6 . 1 25 92 10 M 1334 H 0 7 0 9 30 53 . 1 0 . 1 26 142 8 N 1329 H 1 5 1 13 56 39 . 3 8 . 1 29 80 14 LINE 31 (FLIGHT 3) A 1134 S 1551 7 3 18 58 58 . 2 0 . 1 17 100 1 B 1142 H 0 9 9 0 20 40 110 . 1 0 . 1 21 177 4 C 1147 H 0 17 2 30 81 170 . 1 0 . 1 15 101 1 D 1153 H 2 9 1 20 67 78 . 2 8 . 1 26 73 12 E 1165 H 1 14 3 30 94 128 . 2 0 . 1 16 77 3 F 1174 H 0 9 2 20 55 105 . 1 1 . 1 19 95 5 G 1180 H 0 3 2 12 45 28 . 3 13 . 1 19 97 4 H 1230 S 2 21 2 37 123 191 . 1 0 . 1 9 58 0 I 1239 H 0 11 0 24 75 146 . 1 0 . 1 9 58 0 I 1239 H 0 11 0 24 75 146 . 1 0 . 1 25 155 8 J 1245 S 1 11 0 20 65 24 . 1 0 . 1 9 58 0 LINE 32 (FLIGHT 3) B 1542 S 2 28 1 52 118 204 . 1 0 . 1 9 58 0 LINE 32 (FLIGHT 3) B 1576 S 1 6 2 26 98 104 . 2 0 . 1 6 36 0 LINE 33 (FLIGHT 3) LINE 34 (FLIGHT 3) LINE 35 (FLIGHT 3) LINE 36 (FLIGHT 3) LINE 37 (FLIGHT 3) LINE 38 (FLIGHT 3) LINE 39 (FLIGHT 3) LINE 39 (FLIGHT 3) LINE 30 (FLIGHT 3) LI	I	1371	H	1									1			
K 1361 B? 3 21 5 42 138 147 . 1 0 . 1 2 166 0 L 1342 H 1 8 1 18 85 74 . 2 6 . 1 25 92 10 M 1334 H 0 7 0 9 30 53 . 1 0 . 1 26 142 8 N 1329 H 1 5 1 13 56 39 . 3 8 . 1 29 80 14 LINE 31 (FLIGHT 3) A 1134 S 1551 7 3 18 58 58 . 2 0 . 1 17 100 1 B 1142 H 0 9 0 20 40 110 . 1 0 . 1 21 177 4 C 1147 H 0 17 2 30 81 170 . 1 0 . 1 15 101 1 D 1153 H 2 9 1 20 67 78 . 2 8 . 1 26 73 12 E 1165 H 1 14 3 30 94 128 . 2 0 . 1 16 77 3 F 1174 H 0 9 2 20 55 105 . 1 1 1 19 95 5 G 1180 H 0 3 2 12 45 28 . 3 13 . 1 19 97 4 H 1230 S 2 21 2 37 123 191 . 1 0 . 1 9 58 0 I 1239 H 0 11 0 24 75 146 . 1 0 . 1 25 155 8 J 1245 S 1 11 0 20 65 24 . 1 0 . 1 0 571 LINE 32 (FLIGHT 3) B 1542 S 2 28 1 52 118 204 . 1 0 . 1 9 58 0 L 1245 S 1 11 3 30 92 145 . 1 0 . 1 9 42 0 C 1559 S 1 27 1 46 149 202 . 1 0 . 1 0 302 0 D 1573 S 1 11 3 30 92 145 . 1 0 . 1 8 36 0 E 1576 S 1 6 2 26 98 104 . 2 0 . 1 6 36	J	1366	H	2	10							-	1			
L 1342 H	K	1361	B?	3	21	5						-	•			
M 1334 H 0 7 0 9 30 53 1 0 1 26 142 8 N 1329 H 1 5 1 13 56 39 3 8 1 29 80 14 LINE 31 (FLIGHT 3) A 1134 S 1551 7 3 18 58 58 2 0 1 17 100 1 B 1142 H 0 9 0 20 40 110 1 0 1 21 177 4 C 1147 H 0 17 2 30 81 170 1 1 0 1 15 101 1 D 1153 H 2 9 1 20 67 78 2 8 1 26 73 12 E 1165 H 1 14 3 30 94 128 2 0 1 16 77 3 F 1174 H 0 9 2 2 20 55 105 1 1 1 1 19 95 5 G 1180 H 0 3 2 12 45 28 3 13 1 1 19 97 4 H 1230 S 2 21 2 37 123 191 1 0 1 9 58 0 I 1239 H 0 11 0 24 75 146 1 0 1 25 155 8 J 1245 S 1 11 0 20 65 24 1 0 1 25 155 8 J 1245 S 1 11 0 20 65 24 1 0 1 0 1 0 302 0 D 1573 S 1 11 3 30 92 145 1 0 1 9 42 0 C 1559 S 1 27 1 46 149 202 1 0 1 8 36 0 E 1576 S 1 6 2 26 98 104 2 0 1 16 76 2 B 1681 S 2 13 1 21 82 71 2 0 1 14 40 3	L	1342	H	1	8					•	•		-			
N 1329 H 1 5 1 13 56 39 3 8 1 29 80 14 LINE 31 (FLIGHT 3) A 1134 S 1551 7 3 18 58 58 2 0 1 1 17 100 1 B 1142 H 0 9 0 20 40 110 1 0 1 21 177 4 C 1147 H 0 17 2 30 81 170 1 0 1 15 101 1 D 1153 H 2 9 1 20 67 78 2 8 1 26 73 12 E 1165 H 1 14 3 30 94 128 2 0 1 16 77 3 F 1174 H 0 9 2 20 55 105 1 1 1 1 19 95 5 G 1180 H 0 3 2 12 45 28 3 13 1 19 97 4 H 1230 S 2 21 2 37 123 191 1 0 1 9 58 0 I 1239 H 0 11 0 24 75 146 1 0 1 9 58 0 I 1239 H 0 11 0 24 75 146 1 0 1 9 58 0 LINE 32 (FLIGHT 3) B 1542 S 2 28 1 52 118 204 1 0 1 9 42 0 C 1559 S 1 27 1 46 149 202 1 0 1 9 302 0 D 1573 S 1 11 3 30 92 145 1 0 1 8 36 0 E 1576 S 1 6 2 26 98 104 2 0 1 6 36 0	M	1334	H	0	7	0				•			1			
LINE 31 (FLIGHT 3) A 1134 S 1551 7 3 18 58 58 2 0 1 17 100 1 B 1142 H 0 9 0 20 40 110 1 0 1 21 177 4 C 1147 H 0 17 2 30 81 170 1 0 1 15 101 1 D 1153 H 2 9 1 20 67 78 2 8 1 26 73 12 E 1165 H 1 14 3 30 94 128 2 0 1 16 77 3 F 1174 H 0 9 2 20 55 105 1 1 1 19 95 5 G 1180 H 0 3 2 12 45 28 3 13 1 19 97 4 H 1230 S 2 21 2 37 123 191 1 0 1 9 58 0 I 1239 H 0 11 0 24 75 146 1 0 1 9 58 0 I 1245 S 1 11 0 20 65 24 1 0 1 10 571 0 LINE 32 (FLIGHT 3) B 1542 S 2 28 1 52 118 204 1 0 1 9 42 0 C 1559 S 1 27 1 46 149 202 1 0 1 9 302 0 D 1573 S 1 11 3 30 92 145 1 0 1 8 36 0 E 1576 S 1 6 2 26 98 104 2 0 1 6 36 0	N	1329	H	1	5	1	13			•			-			
A 1134 S 1551 7 3 18 58 58 2 0 1 1 17 100 1 B 1142 H 0 9 0 20 40 110 1 0 1 21 177 4 C 1147 H 0 17 2 30 81 170 1 0 1 15 101 1 D 1153 H 2 9 1 20 67 78 2 8 1 26 73 12 E 1165 H 1 14 3 30 94 128 2 0 1 16 77 3 F 1174 H 0 9 2 2 20 55 105 1 1 1 1 1 19 95 5 G 1180 H 0 3 2 12 45 28 3 13 1 1 19 97 4 H 1230 S 2 21 2 37 123 191 1 0 1 9 58 0 I 1239 H 0 11 0 24 75 146 1 0 1 9 58 J 1245 S 1 11 0 20 65 24 1 0 1 10 571 LINE 32 (FLIGHT 3) B 1542 S 2 28 1 52 118 204 1 0 1 9 42 0 C 1559 S 1 27 1 46 149 202 1 0 1 9 42 0 C 1559 S 1 27 1 46 149 202 1 0 1 9 42 0 D 1573 S 1 11 3 30 92 145 1 0 1 8 36 0 E 1576 S 1 6 2 26 98 104 2 0 1 6 36 0 LINE 33 (FLIGHT 3) A 1709 S 0 15 0 34 86 161 1 0 1 16 76 2 B 1681 S 2 13 1 21 82 71 2 0 1 14 40 3	T.1		21	/1P ⁻	T TCUM	21				•		•				• •
B 1142 H 0 9 0 20 40 110 1 0 1 21 177 4 C 1147 H 0 17 2 30 81 170 1 0 1 15 101 1 D 1153 H 2 9 1 20 67 78 2 8 1 26 73 12 E 1165 H 1 14 3 30 94 128 2 0 1 16 77 3 F 1174 H 0 9 2 20 55 105 1 1 1 1 19 95 5 G 1180 H 0 3 2 12 45 28 3 13 1 1 9 97 4 H 1230 S 2 21 2 37 123 191 1 0 1 9 58 0 I 1239 H 0 11 0 24 75 146 1 0 1 9 58 J 1245 S 1 11 0 20 65 24 1 0 1 10 571 LINE 32 (FLIGHT 3) B 1542 S 2 28 1 52 118 204 1 0 1 9 42 0 C 1559 S 1 27 1 46 149 202 1 0 1 9 302 0 D 1573 S 1 11 3 30 92 145 1 0 1 9 36 0 E 1576 S 1 6 2 26 98 104 2 0 1 6 36 LINE 33 (FLIGHT 3) A 1709 S 0 15 0 34 86 161 1 0 1 16 76 2 B 1681 S 2 13 1 21 82 71 2 0 1 14 40 3						•	10			•	_	•				
C 1147 H 0 17 2 30 81 170 1 0 1 15 101 1 D 1153 H 2 9 1 20 67 78 2 8 1 26 73 12 E 1165 H 1 14 3 30 94 128 2 0 1 16 77 3 F 1174 H 0 9 2 20 55 105 1 1 1 1 19 95 5 G 1180 H 0 3 2 12 45 28 3 13 1 19 97 4 H 1230 S 2 21 2 37 123 191 1 0 1 9 58 0 I 1239 H 0 11 0 24 75 146 1 0 1 9 58 J 1245 S 1 11 0 20 65 24 1 0 1 25 155 8 J 1245 S 1 11 0 20 65 24 1 0 1 0 571 LINE 32 (FLIGHT 3) B 1542 S 2 28 1 52 118 204 1 0 1 9 42 0 C 1559 S 1 27 1 46 149 202 1 0 1 9 302 0 D 1573 S 1 11 3 30 92 145 1 0 1 8 36 0 E 1576 S 1 6 2 26 98 104 2 0 1 6 36 LINE 33 (FLIGHT 3) A 1709 S 0 15 0 34 86 161 1 0 1 16 76 2 B 1681 S 2 13 1 21 82 71 2 0 1 14 40 3													1		100	. 1
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E 1165 H											•	- •	•			•
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J 1245 S											•]			
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B 1542 S 2 28 1 52 118 204 1 0 1 9 42 0 C 1559 S 1 27 1 46 149 202 1 0 1 0 302 0 D 1573 S 1 11 3 30 92 145 1 0 1 8 36 0 E 1576 S 1 6 2 26 98 104 2 0 1 6 36 0 LINE 33 (FLIGHT 3) A 1709 S 0 15 0 34 86 161 1 0 1 16 76 2 B 1681 S 2 13 1 21 82 71 2 0 1 14 40 3		~		•	• •	•	20	0,5	24	•	•	υ.	1	10	571	0
B 1542 S 2 28 1 52 118 204 1 0 1 9 42 0 C 1559 S 1 27 1 46 149 202 1 0 1 0 302 0 D 1573 S 1 11 3 30 92 145 1 0 1 8 36 0 E 1576 S 1 6 2 26 98 104 2 0 1 6 36 0 LINE 33 (FLIGHT 3) A 1709 S 0 15 0 34 86 161 1 0 1 16 76 2 B 1681 S 2 13 1 21 82 71 2 0 1 14 40 3	LI	NE	32	(FI	LIGHT	3)				•		•				
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D 1573 S 1 11 3 30 92 145 . 1 0 . 1 8 36 0 E 1576 S 1 6 2 26 98 104 . 2 0 . 1 6 36 0 LINE 33 (FLIGHT 3) A 1709 S 0 15 0 34 86 161 . 1 0 . 1 16 76 2 B 1681 S 2 13 1 21 82 71 . 2 0 . 1 14 40 3											-					
E 1576 S 1 6 2 26 98 104 . 2 0 . 1 6 36 0 LINE 33 (FLIGHT 3) A 1709 S 0 15 0 34 86 161 . 1 0 . 1 16 76 2 B 1681 S 2 13 1 21 82 71 . 2 0 . 1 14 40 3	D	1573	S			•					-					
LINE 33 (FLIGHT 3) A 1709 S 0 15 0 34 86 161 1 0 1 16 76 2 B 1681 S 2 13 1 21 82 71 2 0 1 14 40 3	E	1576	s	1							-		•			
A 1709 S 0 15 0 34 86 161 . 1 0 . 1 16 76 2 B 1681 S 2 13 1 21 82 71 . 2 0 . 1 14 40 3				•	•	-	20	70	104	•	2	٠.	1	6	36	Ð
B 1681 S 2 13 1 21 82 71 . 2 0 . 1 14 40 3				(FI	IGHT	3)				•		•				
B 1681 S 2 13 1 21 82 71 . 2 0 . 1 14 40 3				0	15		34	86	161		1	0.	1	16	76	2
D 4000 0						1	21									
D = 1 + 0 + 0 + 23 + 91 + 48 + 5 + 2 + 1 + 19 + 50 + 7				1	6	0	23	91			5		·=			
F 1603 H 1 13 4 31 95 110 . 2 6 . 1 25 39 13	F	1603	H	1	13	4	31									

^{.*} ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

[.] OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

[.] LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

			AXIAL OO HZ		LANAR 00 Hz		LANAR 00 Hz	•		FICAL .		ZONTAL EET	CONDUC EAR	
ANOMALY FID/INTE	/ R RP	EAL PPM	QUAD PPM	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	•	COND MHOS	DEPTH*.	COND MHOS		RESIS OHM-M	DEPTH M
LINE 3	41	/ F	LIGHT	3)				•		•				
A 1941 8		0	3	0	5	23	20	•	2	•				
B 1932	H	0	9	0	14	67	76		2 2	0.	1	19	330	0
C 1891 I	H	2	12	2	21	76	58			0.	1	24	74	10
D 1857 8		2	17	2	31	94	110		3 2	3. 0.	1	25	45	12
E 1848 S	S	2	10	3	23	90		•	2	0.	1	12	44	0
F 1834 S	S	2	9	2	22	59	36	-	3	0.		17	68	4
G 1830 I	[·}	5	16	3	17	52	78		2	0.	1	14	51	1
Н 1814 Р	H	2	12	2	22	77	96		2	0.	1	•	227	. 0
							•	:	•	•	,	21	48	8
	35	(F	LIGHT	3)						•				
A 1957 H		2	20	4	41	78	89		1	0.	1	5	338	0
B 1961 H		1	4	4	10	31	38		1	13 .	1	12	316	0
С 1964 Н		1	9	0	18	59	72		2	4 .	i	11	274	0
D 1970 S		0	1	1	4	12	19		1	7.	1	0	939	0
E 1974 S		0	2	0	2	11	13		1	24 .	1	1	745	0
F 1978 S		0	3	0	7	21	35		1	5.	1	3	457	0
G 1985 H		1	8	1	13	45	46	•	1	2.	1	19	260	0
H 1989 S		1	6	1	12	42	42	•	2	2.	1	3	387	Ŏ
I 1996 S		1	3	2	5	18	43	•	1	0.	1	Ō	869	Õ
J 2002 S		1	5	2	11	37		•	1	0.	· 1	0	349	Ô
K 2009 S L 2023 S		1	6	1	11	38	57	•	1	0.	1	0	255	Ō
и 2023 в м 2031 н		0	1	1	2	11		•	1	11 .	1	0	481	0
N 2041 S	-	0	11	1	20	70	85	•	2	3.	1	14	172	0
0 2072 S		1	14	3	27	78	111 .	•	1	0.	1	7	161	0
P 2078 S		1	16 15	1	29	90	126		1	0.	1 .	2	142	0
Q 2081 S		0	15	4	8	26	25 .		1	10 .	1	4	359	0
S 2086 S		0	2	3 0	34 13	47	25 .	•	4	7.	1	0	799	0
	_	Ū	L	U	13	0	21 .	•	1	0.	1	0	1783	0
LINE 3	6	(FI	IGHT	3)			•	•		•				
A 2212 S	•	0	7	0	14	44	71 .	•	4	•				
В 2101 Н		Ō	16	Ö	31	86	141 .		1	0.	1	11	98	0
C 2098 S		1	39	Ö	68	204	321 .		•	2.	1	23	43	11
D 2093 H		1	7	5	14	41	39 .		1 2	0.	1	0	241	0
	_		•		• •	* '	33 .		2	3.	1	35	39	21
LINE 37	7	(FL	IGHT	3)			•			•				
A 2245 S		3	10	4	38	142	138 .		3	ο:	1	22	60	•
В 2259 Н		1	6	3	21	75	80 .		2	0.	1	22	68	8
С 2262 Н		1	6	4	19	61	46.		3	0.	1	29 22	52	15
D 2267 H		8	11	3		149	86.		3	4.	1	32 15	50	18
F 2276 S		0	15	1	30	82	117.		1	0.	i	12	316	0
•						=			•	•	'	14	76	0

^{.*} ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .

LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.

				AXIAL OO HZ		LANAR 00 HZ		CANAR OO HZ			TICAL IKE		ZONTAL EET	CONDU	
Al FI	NOMAL D/INT	Y/ : ERP	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	REAL PPM	QUAD PPM	•	COND MHOS		COND MHOS		RESIS OHM-M	DEPTH M
L	INE	37	15	LIGHT	3)				٠			•			
	2286		1	12	0	16	53	83	•	1	0	•	27	670	^
H	2292	H	1	8	1	13	39	57		1	4 0	. 1	37	678 109	0
I	2296	s	2	13	1	19	77	75		2	_	. 1	13	60	21
J	2304	S	1	4	1	9	33	20	-	3	_	. 1	13	105	0
K	2317	H	2	8	3	20	68	44	-	3	9	. 1	24	45	12
L	2332	S	2	20	2	36	125	154		2	Ó	. 1	21	43	9
									•	_		• '	21	. 43	,
L	INE	38	(F	LIGHT	3)										
A	2450	S	0	5	0	12	47	55		1	0	. 1	11	363	0
В	2443	H	0	4	0	9	23	61		i	_	. 1	14	620	0
C	2438	H	0	10	0	18	47	40		2		. 1	19	156	2
D	2421	H	1	10	0	18	66	104		1	0	. 1	13	181	0
E	2408	H	1	15 -	0	21	73	113	-	i	Ŏ	. 1	31	675	0
F	2404	H	1	7	1	6	35	37		1	10	. i	36	116	19
G	2399	S	1	4	0	6	22	33		1	3	. 1	27	197	6
H	2385	H	1	7	1	22	65	94	-	1	2	. i	32	146	14
I	2380	H	2	6	4	11	51	17		7	20	. 1	32	53	18
J	2370	S	0	20	0	36	98	203		1	0	. 1	14	49	3
K	2352	S	2	15	2	32	102	108		2	0	. 1	14	41	3
												•	• •	• •	•
	NE	39	(F	LIGHT	3)							•			
	2512		0	6	0	17	53	83		1	0	. 1	9	344	0
	2525		3	10	2	16	49	100		1	0	. 1	28	673	Ŏ
	2544		0	4	1	7	25	43		1	3	. 1	25	221	4
	2551		0	3	0	6	13	35		1		. 1	30	360	7
	2561		0	3	0	5	3	28	•	1	0	. 1	39	421	13
	2583		2	5	1	13	43	27		3	11	. 1	26	75	11
	2603		1	11	2	19	63	65	•	2	0 .	. 1	13	41	1
K	2612	S	1	10	1	26	78	80	•	2	0	. 1	15	49	1

^{*} ESTIMATED DEPTH MAY BE UNRELIABLE BECAUSE THE STRONGER PART .

OF THE CONDUCTOR MAY BE DEEPER OR TO ONE SIDE OF THE FLIGHT .
LINE, OR BECAUSE OF A SHALLOW DIP OR OVERBURDEN EFFECTS.



1984 05 28

Your File: 416/83 Our File: 2.6274

Mr. Bruce Hanley Mining Recorder Ministry of Natural Resources 60 Wilson Avenue Timmins, Ontario P4N 287

Dear Sir:

RE: Notice of Intent dated May 3, 1984 Airborne Geophysical (Electromagnetic,
Magnetometer, VhF & Resistivity) Survey
submitted on Mining Claims P 641730 et
al in the Township of Fallon

#FOR SIGNER AND SIGNER AND SIGNER SECTION OF THE PROPERTY OF THE PROPERTY OF THE SECTION OF THE

The assessment work credits as listed with the above mentioned Notice of Intent, have been approved as of the above date.

Please inform the recorded holder of these mining claims and so indicate on your records.

Yours sincerely,

S.E. Yundt Director Land Management Branch

Whitney Block, Room 6643 Queen's Park Toronto, Ontario M7A 1W3 Phone: (416) 965-69

D. Kinvig:sc

ec: Mr. David Meunier
403 Dome Street
P.O. Box 1624
South Porcupine, Ontario



Technical Assessment: Work Credits

			2.6274
1984	05	03	Mining Recorder's Report of Work No. 415,416,
		41	7. 418. 419.

File

VID MEUNIER	
LLON	
nber of per claim	Mining Claims Assessed
	0
days	
days	
days	See attached list
	days

Magnetometer <u>16</u> days				
Raction of the VLF 16 days	See attached list			
Induced polarization days				
Other days	·			
Section 77 (19) See "Mining Claims Assessed" column	,			
Geological days				
Geochemical days				
Man days ☐ Airborne ☑				
Special provision Ground				
Credits have been reduced because of partial coverage of claims.	1			
Credits have been reduced because of corrections to work dates and figures of applicant.				
Special credits under section 77 (16) for the following	mining claims			
No credits have been allowed for the following mining claims				
not sufficiently covered by the survey				
No credit can be given for the Resistivity Survey, as it is a direct calculated derivative of the Airborne Electromagnetic Survey.				

The Mining Recorder may reduce the above credits if necessary in order that the total number of approved assessment days recorded on each claim does not exceed the maximum allowed as follows: Geophysical — 80; Geological — 40; Geochemical — 40; Section 77 (19)—60:

MEUNIER CLAIMS IN FALLON TOWNSHIP

		•
No.	Claim No.	Anniversary Date
1.	P. 653259	12 Sentember 1982
2.	P. 653260	12 Sentember 1982
3.	P. 653261	12 Sentember 1982
4.	P. 653262/	12 Sentember 1982
<u>.</u>	P. 641742	
6.		
	P. 641743/	27 Sentember 1982
?.	P. 653908	27 Sentember 1982
8.	P. 653909	27 Sentember 1982
9.	P. 641730	20 Sentember 1982
10.	P. 641731	20 Sentember 1982
11.	P. 641732	20 Sentember 1982
12.	P. 641733	20 Sentember 1982
13.	P. 641794	20 Sentember 1982
14.	P. 661936	20 Sentember 1982
15.	P. 654191	28 September 1982
16.	P. 654192	28 Sentember 1982
17.	P. 654193	28 Sentember 198 2
18.	P. 654194	- 28 Sentember 1982
19.	P. 654195	28 Sentember 1982
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194.	P. 758819	17 May 1983
195.	P. 758820	17 May 1983
196.	P. 758851	17 May 1983

1984 05 03

Your File: 416/83 Our File: 2.6274

Mr. Bruce W. Hanley Mining Recorder Ministry of Natural Resources 60 Wilson Avenue Timmins, Ontario P&N 287

Dear Sir:

RE:

Airborne Geophysical (Electromagnetic, Magnetometer, V.L.F. & Resistivity) Survey submitted on Mining Claims P641730 et al in the Township of Fallon.

Please disregard the approval for assessment work credits for the above mentioned survey. It was approved on April 3, 1984 in error. No credits may be allowed for the Resistivity Survey when credits have been requested for the Electromagnetic survey, as an airborne Resistivity survey is a direct calculated derivative of an airborne Electromagnetic survey.

Enclosed is a Notice of Intent. I sincerely apologise for any inconvenience this error may have caused. Yours sincerely,

S.E. Yundt Director Land Management Branch

Whitney Block, Room 6643 Queen's Park Toronto, Ontario M7A 1W3 Phone: (416)965-6918

D. Kinvig:sc

cc: Mr. David Meunier
403 Dome Street
P.O. Box 1624
South Porcupine, Ontario



Your file: 416/83

.1984 05 03

Our file: 2.6274

Mr. Bruce W. Hanley Mining Recorder Ministry of Natural Resources 60 Wilson Avenue Timmins, Ontario P4N 2S7

Dear Sir:

Enclosed are two copies of a Notice of Intent with statements listing a reduced rate of assessment work credits to be allowed for a technical survey. Please forward one copy to the recorded holder of the claims and retain the other. In approximately fifteen days from the above date, a final letter of approval of these credits will be sent to you. On receipt of the approval letter, you may then change the work entries on the claim record sheets.

For further information, if required, please contact Mr. F.W. Matthews at 416/965-6918.

Yours very truly,

S.E. Yundt

Director

Land Management Branch

Whitney Block, Room 6643 Queen's Park Toronto, Ontario M7A 1W3

Phone: 416/965-1316

D. Kinvig:sc Encls.

cc: Mr. David Meunier
403 Dome Street
P.O. Box 1624
South Porcupine, Ontario

cc: Mr. G.H. Ferguson
Mining & Lands Commissioner
Toronto, Ontario



Notice of Intent for Technical Reports

1984 05 03

Your File: 416/83

Our File: 2.6274

An examination of your survey report indicates that the requirements of The Ontario Mining Act have not been fully met to warrant maximum assessment work credits. This notice is merely a warning that you will not be allowed the number of assessment work days credits that you expected and also that in approximately 15 days from the above date, the mining recorder will be authorized to change the entries on his record sheets to agree with the enclosed statement. Please note that until such time as the recorder actually changes the entry on the record sheet, the status of the claim remains unchanged.

If you are of the opinion that these changes by the mining recorder will jeopardize your claims, you may during the next fifteen days apply to the Mining and Lands Commissioner for an extension of time. Abstracts should be sent with your application.

If the reduced rate of credits does not jeopardize the status of the claims then you need not seek relief from the Mining and Lands Commissioner and this Notice of Intent may be disregarded.

If your survey was submitted and assessed under the "Special Provision-Performance and Coverage" method and you are of the opinion that a re-appraisal under the "Man-days" method would result in the approval of a greater number of days credit per claim, you may, within the said fifteen day period, submit assessment work breakdowns listing the employees names, addresses and the dates and hours they worked. The new work breakdowns should be submitted direct to the Land Management Branch, Toronto. The report will be re-assessed and a new statement of credits based on actual days worked will be issued.

Natural (Geo	ort of Work ophysical, Geological, chemical and Expendit	-	6274 1-4/0 The Mining	1/83.	Note: -	exceeds space only days "Expendituring the "Expendituring the "Expenditure space spa	or print. of mining claim the on this form, a credits calcular res" section may the control of the control the con	attach a list. ted ,in the be entered " columns.
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Name and Address of Author to	Suite 70	10, [vs+			10. Yr.	ronto O	N
Credits Requested per Each (<u>/</u>			laims Traversed (L	List in nume	ical sequen	ice)	
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	- Survey	<u>"</u>	المرا	184/	7/		1 /D	2
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or witnessed same during and	d/or after its completion a	and the anr	nexed report is	s true.				
R.F. Sowey				Date Certified		Certified	(Skinature)	
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Certification Verifying Res	port of Work		ــــــــا د	***	<u> </u>		V
I hereby certify that I have	a personal and intimate ki	nowledge c	of the facts se	t forth in the Report	of Work and	nexed hereto, having perfo	ormed the work
or witnessed same during a	nd/or after its completion	and the an	nexed report	is true.			
Name and Postal Address of P	erson Certifying						
		611 D		Date Certified	1.1	Certified by (Signatur	re) Pal
P.U. R. 5010 PMS	South Farending	ON (1) <i>ルバの</i>	13 lan	E4-	(Jest 200	way

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Cleim Holder(s) Dayid J. M	lunier			t			Prospecto —	17157	
403 Dome St, P.O. Box 1624 South Parcupine, ON									
Survey Company Dichem					Date of Survey	(from & to)	0 E3	Total Miles of lin	ne Cut
Name and Address of Author to	Sulfe 701	O.F	>	-5+0				ronto,	ON
Credits Requested per Each (laims Traversed (L				
Special Provisions	Geophysical	Days per	 		lining Claim	Expend, Days Cr.		Mining Claim Number	Expend. Days Cr.
For first survey:		Claim		Prefix	Number 750016	Days Cr.	97.	75841	
Enter 40 days. (This	- Electromagnetic	<u> </u>		 	758818		72475		
includes line cutting)	- Magnetometer				758819		a sibate	75941	
For each additional survey:	- Radiometric				758820	<u> </u>	AND SHAP	75841	9
using the same grid:	- Other	!			758821			75912	O
Enter 20 days (for each)	Geological		1 1	المعالم الماري المعالم الماري الماري الماري	764414		Jakarka say	75842	1
				1000	- 4			75842	5
Man Days	Geochemical	D			+64415	 	301	<u> </u>	
	Geophysical	Days per Claim		in in shirth	769 416		79 1.2 S	75842	3
Complete reverse (ide	Electromagnetic				764 417		A Calendaria	75842	4
and enter (\$\text{pta}(\frac{1}{3})\text{ here}	- Magnetometer		1		758402		建筑	758421	
EFB ,	5.54		1 1		758403	 		758120	
	- Radiometric			1	· · · · · · · · · · · · · · · · · · ·		175 **		
WHING TW	- Other			30.9	758404			75842	7
W.W.	Geological				758405			75842	8
	Geochemical		1		758406		14	75842	9
Airborne Credits		Days per	1					75843	
		Claim			758407			<u> </u>	
Note: Special provisions credits do not apply	Electromagnetic	-16	1]	. 1	758408	1		75843	
to Airborne Surveys.	Magnetometer	16	179	4 075	758409			75843	34
	Redismotric	16.	מ'ל[198	758410			75843	3
Expenditures (excludes pow	ver stripping)	<u> </u>	VC	em:	758411	 		75843	
Type of Work Performed]	*****		 	ે જેવાનું ક		
	CCRDEI)		No. Se	758412	ļ		758 4	
Performed on Claim(s					758413			75843	6
	1:07-1-1:1983		1		758414	1	100	75843	7
		1			758415	1 00	1	75443	8
Calculation of Expenditure Day		Total	1	4 () 2 () 2 () () ()		1 . or C		25613	>0
Total Expenditures	Day	s Credits		TANKETS.	758416	وللإنبا	J. Non	75045	21
\$	+ 15 = _				9	2 1 X	Total nu claims co report of	ember of mining overed by this f work.	46
Instructions Total Days Credits may be a	pportioned at the claim	holder's				<u>ν"</u>	7	()	<u> </u>
choice. Enter number of day	ys credits per claim select	ed		Total Da	For Office Use C		Minghage	regulater /	1 2
in columns at right.	-3CD		J	Recorde		41831	100	conley	1
13 Jan 94 R	edorated Hotor or Agent	A . " /]	294	Dete Dete	1000000		A CONTROL OF THE CONT	
Certification Verifying Rep	ert of Work	J	J	<u> </u>	V T	~ (/ (37	1/2/	
I hereby certify that I have	a personal and intimate l	nowledge	of th	e facts set	forth in the Report	of Work anne	xed hereto	, having performe	ed the work
or witnessed same during an	id/or after its completion	and the ar	nexe	ed report	is true.				
Name and Postal Address of Pe	rson Certifying						10-1	DP.	
P.O. Box 5010,	PMS, South	Porcup	21 N	~ ON	Date Certified /S Jan	94	Certified	Sov (Slowerure)	erj

				,		le	vised	
Motural	ort of Work			1/1つ Ins	tructions: —		e or print. of mining claims	travers
Resources (Geo	physical, Geological, chemical and Expendito	ures) بنہر	:411	1/83		exceeds sp	ace on this form, at a credits calculate	ttach a li
Ontario O			$-i\omega_{I}$	Act WRH.	322/2	"Expendit in the "E	ures" section may Expend. Days Cr."	be enter colum
(ype of Survey(s)			The Mining	Act WK .	Township		shaded areas below	
Airborne magneti	c, VLF EM, H	where	ty, el	ectromagnet	he Fal	lon		
Claim Holder(s)	e.mie C					Prospecto	Licence No.	
Address	Do P	100 1	0	AL D.		n N	PONINO	
403 Dome St.	P.O. DOY	1624	, Sou	In roman	pine,		Total Miles of line (
Survey Company Dishem				Date of Survey (3 29 /	10 E3	10(01,000000000000000000000000000000000	,,,,
Name and Address of Author (o Z. Dvoval, Su	Geo-Technical report)	-ct Ca	, <u>, , , , , , , , , , , , , , , , , , </u>	an Place			T1)	•
Credits Requested per Each (laims Traversed (L				
Special Provisions	, , , , , , , , , , , , , , , , , , , 	Days per Claim		lining Claim	Expend. Days Cr.		ining Claim Number	Expen Days C
For first survey:	• Electromagnetic	Claim	Pretix	72 5 23 6	Days Ci.	1>	725199	Day. C
Enter 40 days. (This includes line cutting)	- Magnetometer		'-'	725236				
· •	- Radiometric		ayan Sebesa en ayên azerî en ayên azerî	720770		and the second	725200	
For each additional survey: using the same grid:	-		والمتحديما	725738		To a given so ye	725202	ļ
Enter 20 days (for each)	- Other			725239			725203	
	Geological		130.Va	7252AO			725204	
	Geochemical		Part of the Control	725241		7	725205	ļ
Man Days	Geophysical	Days per Claim	oga i sporpredavi	725 242		. Topsoil	725206	
Complete reverse side and enter total(s) here	- Electromagnetic		13 1 - •	725243		والمحجود في	725207	<u> </u>
OF	Magnetometer		a min makesha	725244		a second	725208	1
CEB .	Radiometric Cother Geological Geochemical		1.772	725-245			725209	,
	Phother Other		7.073	725246			725210	
OHIO	Geological		11.00	725247			725211	
Wile	Geochemical		2013	775744			725212	
Airborne Credits		Days per	387	475749			72/2/3	
Note: Special provisions	Electromagnetic	Claim 6	1 logs	775000			7207 14	
credits do not apply	VLF EM Magnetometer	11/1	44	12525			725215	
to Airborne Surveys.	Resistinty	76 76	yam	F65 651			1252 11	
Expenditures (excludes pow				77/4-2	 		725016	
Type of Work Performed				725 953		100 m	725217	-
Performed on Claim(s)	NO / 14 1983			725 254	 		763210	<u>'</u>
Performed on Claim(s)	ń Na			725 255	 		765 217	
	And the same of th			275256	$\alpha \vdash \vdash$	C. 104	+45220	-
Calculation of Expenditure Day	s Credits	Otal		725 197	1 .pp v	And the second	122661	
Total Expenditures		otal Credits		725 198		\$200°	758817	
\$	+ 15 =			G	CX CX		mber of mining vered by this	46
Instructions Total Days Credits may be a	poortioned at the claim h	older's	<i>-</i>		T 19	report of	work.	/ ~
Total Days Credits may be a choice. Enter number of day in columns at right.			Total Day	For Office Use O	only	Mining N	CONTRACTOR OF THE PARTY OF THE	
in columns at fight.	78		Recorded		1/83	10	Marley	10
Date Jan 84 Re	do ded Holder of Agent (S	ignature)	2,9+	Date Dopoved	A RECOLUED		Approvided /	1
Certification Verifying Repe	THE WAR	70		N. C.				X
I hereby certify that I have a	personal and intimate kn	owledge of	the facts set	forth in the Report	of Work anne:	ced hereto,	beving performed to	he work
or witnessed same during and Name and Poetal Address of Per		ind the anne	exed report i	s true.				
ICT. Bowen								
P.O. Box 50/01	3M S. South Parcy	Dine Of	N PONI	KO Date Certified	g4	Certificat	By (Signature)	21



Geotechnical Report Approval

File			
2	62	7	4

lining Lands Co			
- 7	maps require dain mumbans		
	1		
	<u> </u>		
,			
y Goophysias	Mr. R. Barlow.		
omments	LIL. K. BAIDA!		
Approved	Wish to see again with corrections	Date /3/2/84	Signature
Approved		Date /3/2/84	Signature
o: Geology - Ex		Date /3/2/84	Signature
o: Geology - Ex		Date /3/2/84	Signature
o: Geology - Ex		Date /3/2/84	Signature
o: Geology - Ex		Date /3/2/84	Signature
o: Geology - Ex		Dete /3/2/84	Signature
o: Geology - Ex			
o: Geology - Ex		Date /3/2/84	Signature
Capelogy - Example 1	Wish to see again with corrections		
Approved	Wish to see again with corrections		
Approved	Wish to see again with corrections		Signature
D: Geology - Experiments Approved D: Geochemistr	Wish to see again with corrections		Signature
o: Geology - Exomments Approved o: Geochemistr	Wish to see again with corrections		Signature
o: Geology - Experiments Approved o: Geochemistr	Wish to see again with corrections		Signature
o: Geology - Ex	Wish to see again with corrections		Signature

1984 01 19

Your File: 329, 330, 331,

332, 333.

Our File: 2.6274

Mining Recorder
Ministry of Natural Resources
60 Wilson Avenue
Timmins, Ontario
P4N 257

Dear Sir:

We have received reports and maps for an Airborne Geophysical (Electromagnetic & Magnetometer) Survey submitted on Mining Claims P 663010 et al in the Township of Fallon.

This material will be examined and assessed and a statement of assessment work credits will be issued.

Yours very truly,

J.R. Morton Acting Director Land Management Branch

Whitney Block, Room 6643 Queen's Park Toronto, Ontario M7A 1W3

A. Barr:sc

cc: David J. Heunier
403 Dome Street
P.O. Box 1624
South Porcupine, Ontario
PON 180

cc: R.P. Bowen
P.O. Box 5010
South Porcupine, Ontario
PON 1H0

Assessed	
Approved Reports of Work	*.
sent out	i
Notice of Intent filed	•
,	
Approval after Notice of Intent sent out	
Duplicate sent to Resident	
Conlamict	

Duplicate sent to A.F.R.O.

The second of th

Ontario

Ministry of Natural Resources

GEOPHYSICAL – GEOLOGICAL – GEOCHEMICAL TECHNICAL DATA STATEMENT

TO BE ATTACHED AS AN APPENDIX TO TECHNICAL REPORT FACTS SHOWN HERE NEED NOT BE REPEATED IN REPORT TECHNICAL REPORT MUST CONTAIN INTERPRETATION, CONCLUSIONS ETC.

TECHNICAL REPO	RT MUST CONTAIN INTERPRETATION	N, CONCLUSIONS ETC.
Airborne magr	netic, electromagnetic,	L
Type of Survey(s) VIT electro		y
Township or Area <u>Pallor</u> Claim Holder(s) <u>David Meunice</u>	ar	MINING CLAIMS TRAVERSED
Claim Holder(s)		List numerically
Survey Company Dighem	,	See attached list
Author of Report Z. Dvoral	k & R.P. Bowen	(prefix) (number)
Address of Author P.O. Box 50	10, S. Porcupine, ON	
Covering Dates of Survey 25 Oct.	. 83 - 29 Oct. 83	
Total Miles of Line Cut	(linecutting to office)	
TOTAL WILLS OF TALE ON A LANGUAGE VANA DEPOSIT OF THE PROPERTY		
SPECIAL PROVISIONS	DAYS	
CREDITS REQUESTED	Geophysical per claim	
DAMOND AO Jose /in the Jac	Electromagnetic	
ENTER 40 days (includes line cutting) for first	Magnetometer	
survey.	–Radiometric	
ENTER 20 days for each	Other	
additional survey using same grid.	Geological	
は、 一般のない はいままり かいかい かいかい かいまい かいまい かいまい かいまい かいまい 	Geochemical_	
AIRBORNE CREDITS (Special provisio		
Magnetometer 140 Electromagne	rtic 4() Radiometric	
40 Resistivity DATE: 13 Jan. 84 SIGNAT	18/1× 1.1	
DATE: 20 Group V. SIGNAT	Author of Report or Agent	
		Page 10 and 10 a
Res. Geol. Qualific	. 9.2257	
Previous Surveys	ations (A)(A)(A)	JAS. ₹ * ***
File No. Type Date	Claim Holder	
		TOTAL CLAIMS 196

GEOPHYSICAL TECHNICAL DATA

GROUND SURVEYS - If more than one survey, specify data for each type of survey

Number of Stations	**** * *******************************	Number o	f Readings	
Station interval		Line spaci	ng	
Profile scale				
Contour interval				
Instrument				
Accuracy — Scale constant Diurnal correction method				
Diurnal correction method			- SAIRLES - 1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	
Base Station check-in interval (hou	ars)			
Base Station location and value				
Instrument				
Coil configuration				
Coil separation				
Accuracy				
	d transmitter		☐ In line	☐ Parallel line
Frequency		(specify V.L.F. station)		
Parameters measured				
Instrument	ALCANAMA CONTRACTOR CONTRAC			
Scale constant		······································		
Corrections made				
				· · · · · · · · · · · · · · · · · · ·
Base station value and location				
Elevation accuracy				
·				
Instrument				
Method Time Domain		☐ Fr	equency Domain	
Parameters – On time		Fr	equency	
Off time		Ra	inge	
– Delay time				
 Integration time 				
— Delay time — Integration time Power				
Electrode array				
Electrode spacing				
Type of electrode				

INDUCED POLARIZATION

SELF POTENTIAL	
Instrument	Range
Survey Method	
Corrections made	
RADIOMETRIC Instrument	
Values measured	
Energy windows (levels)	
Height of instrument	Background Count
Overburden	
(type, depth –	include outcrop map)
OTHERS (SEISMIC, DRILL WELL LOGGING ETC.) Type of survey	
Instrument	
Accuracy	
Parameters measured	
Additional information (for understanding results)	
AIRBORNE SURVEYS Type of survey(s) Dighem III electromagnet Sonotek PEH 5010 magneton Instrument(s) order for PM resistivity	tic, magnetic, mesistivity & VLF EM neter; Totem-2RVL* EM RCVR; GR-33 analog
Accuracy EN: 0.2 ppm at 900 Hz & 0.4 pr	calculated in type of survey by Acvn; Gh-55 and log on type of survey by at 7200 Hz; Mag: 1 gamma; VLF EM: 0.2%
Aircraft used Astar CG-NSM turbine heli	
Sensor altitude Eil: 31m; Nag: 46m; VIP Eil:	54m
Navigation and flight path recovery methodSperry	radio altimeter. Geocam sequence camera
analog and digital profiles	
Aircraft altitude 60m	Line Spacing 200m
Miles flown over total area155	Over claims only 79

GEOCHEMICAL SURVEY - PROCEDURE RECORD

Numbers of claims from which samples taken						
Table 1 of Co. 1						
Total Number of Samples						
Type of Sample(Nature of Material) Average Sample Weight	n n m					
Method of Collection						
Soil Horizon Sampled	Others					
Horizon Development	Field Analysis (tests)					
Sample Depth						
Terrain						
Drainage Development	· · · · · · · · · · · · · · · · · · ·					
Estimated Range of Overburden Thickness	· · · · · · · · · · · · · · · · · · ·					
	A 1 / 134 / 1					
	Reagents Used					
SAMPLE PREPARATION	Commercial Laboratory (tests)					
(Includes drying, screening, crushing, ashing)	Name of Laboratory					
Mesh size of fraction used for analysis	Name of Laboratory					
	Extraction Method					
	Analytical Method Reagents Used					
General	General					

7.8,9,10,11,12,1,12,8,4,5 M.278 ONTARIO MINISTRY OF NATURAL RESOURCES MINISTRY OF NAT
SURVEYS AND **RESOURCES** SURVEYS AND MAPPING BRANCH PORCUPINE MINING DIVISION DISTRICT OF TIMISKAMING Scale: 40 Chans-Ilnch 24274 LANGMUIR DOUGLAS 764410 758277 758278 750429 750436 750621 758432 758433 758474 - P 754414 714652 758821 758620 758819 758618 586987 P 636079 636075 636078 636074 P 636077 |636073 586998 5863999 | 594506 P | P 10 63 6076 63 60 72 3.M LEGEND 400' Surface rights reservation around all lakes & rivers. CLEAVER CANCELLED PATENTED LAND CROWN LAND SALE

MEUNIER CLAIMS



MINING RIGHTS ONLY

SURFACE RIGHTS ONLY

LO. MRO

MINISTRY OF NATURAL RESOURCES SURVEYS AND MAPPING BRANCH

M.278

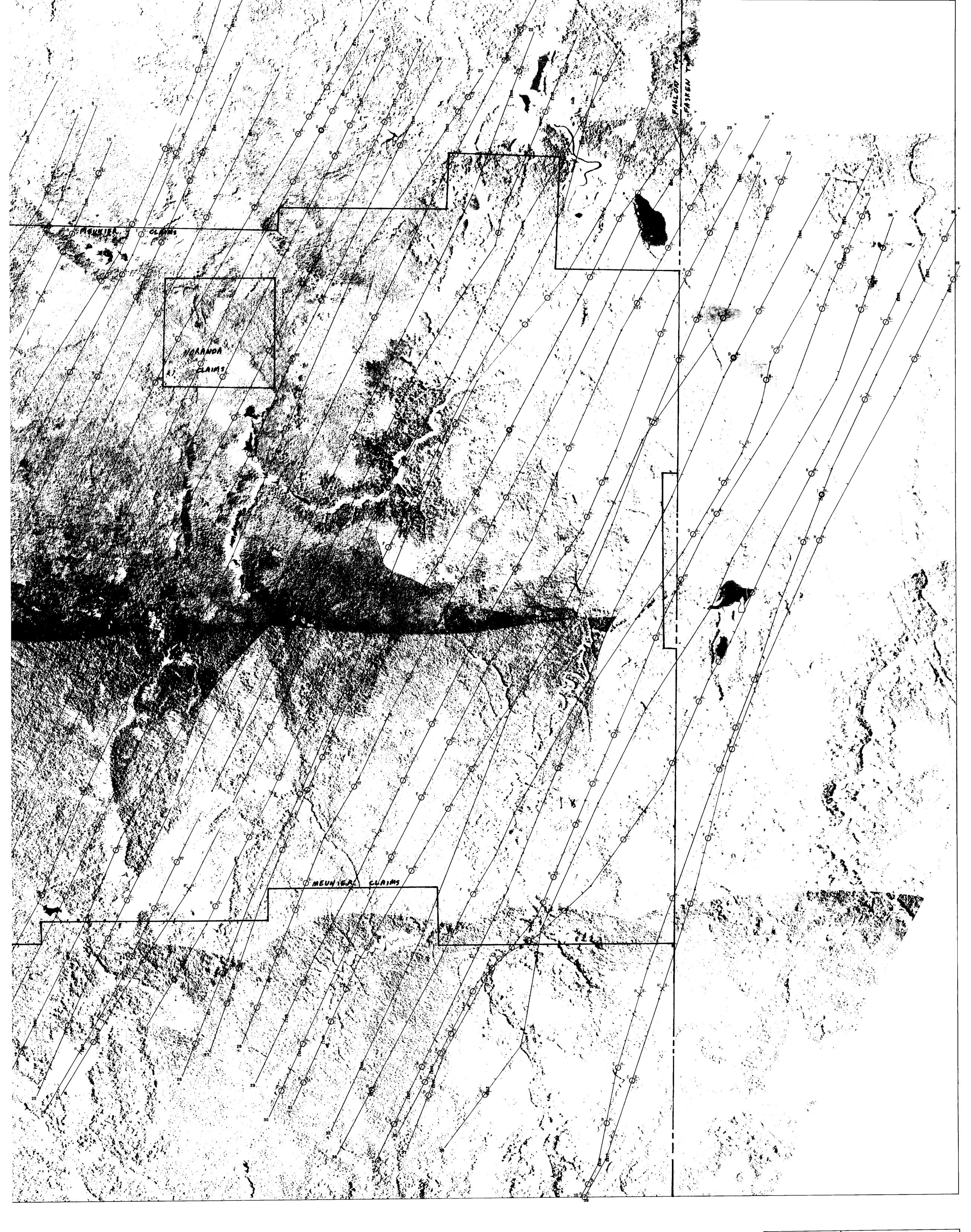
RESO'JRCES'

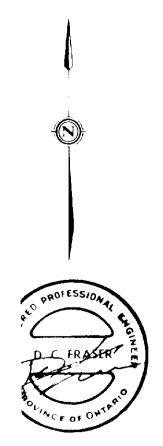
I ORCUPINE MININGDIVISION DISTRICT OF TMISKAMING

Scale - 40 Chams-tinch

LANGMUIR

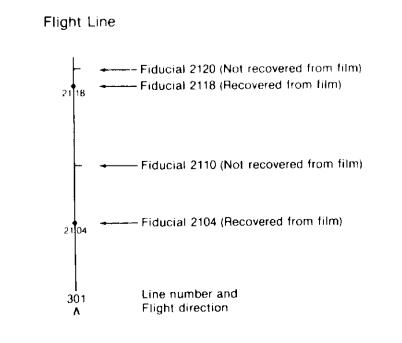
LEGEND





FALLON TWP. ONTARIO ELECTROMAGNETIC ANOMALIES FOR DAVID J. MEUNIER

1 Kilometres



6	ONDUCTANCE (MHOS) 99 50—99 20—49 10—19 5— 9 ndeterminate	conductivit	nomalies are divided into six grades of ly-thickness product. This product in measure of conductance.
"name" Inp	interpretive symbol phase and paxial Coil greater than 5 ppm 10 ppm 15 ppm 20 ppm	Interpretive symbol B. S. H.	Conductor ("model") Bedrock conductor Conductive cover ("horizontal thin sheet") Broad conductive rock unit, deep conductive weathering, thick conductive cover ("half space") Edge of broad conductor ("edge of half space") Culture, e.g. power line, building, fence
arcs indicate the conductor has a thick- ness → 10 m	E B. 288		dip direction magnetic correlation in nT (gammas) conductor axis flight line

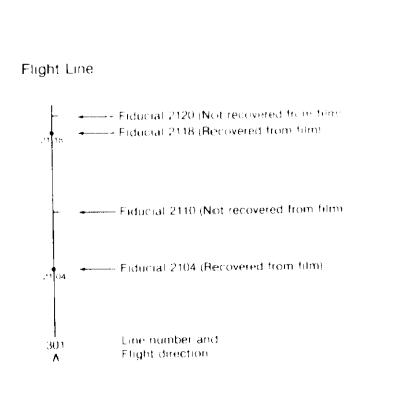
JOB 190	DATE DEC./83	DRAWN BY	CHECKED BY
------------	-----------------	----------	------------





FALLON TWP. ONTARIO
RESISTIVITY
FOR

DAVID J. MEUNIER



LEGEND
Contours in ohm — m at ten intervals per decade
1000
800
600
500
400
300
250
200
150
125
100
Note
The numbers face in the direction of increasing value.

JOB 1 9 0	DATE DEC./83	DRAWN BY	CHECKED BY 3.
---------------------	-----------------	----------	---------------



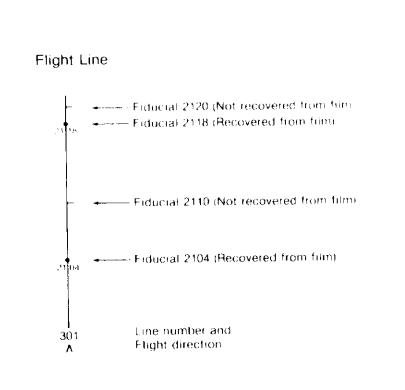
FALLON TWP. ONTARIO
TOTAL FIELD MAGNETICS
FOR

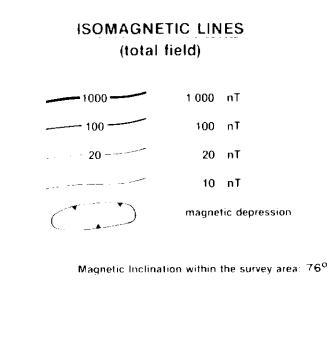
ROFESSIONAL PLANTS OF CHICAGO

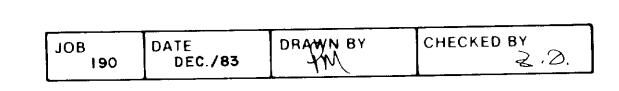
DAVID J. MEUNIER

Scale 1:10,000

0 12 1 Kilometres
1 4 0 14 12 Miles









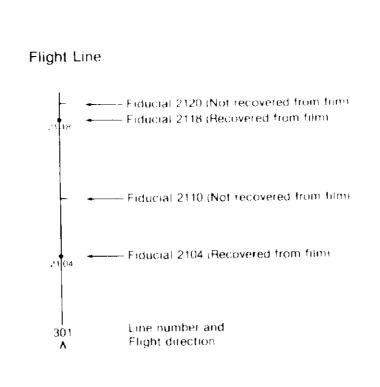


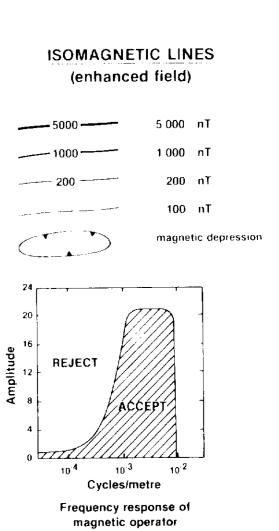
FALLON TWP. ONTARIO **ENHANCED MAGNETICS** FOR

DAVID J. MEUNIER

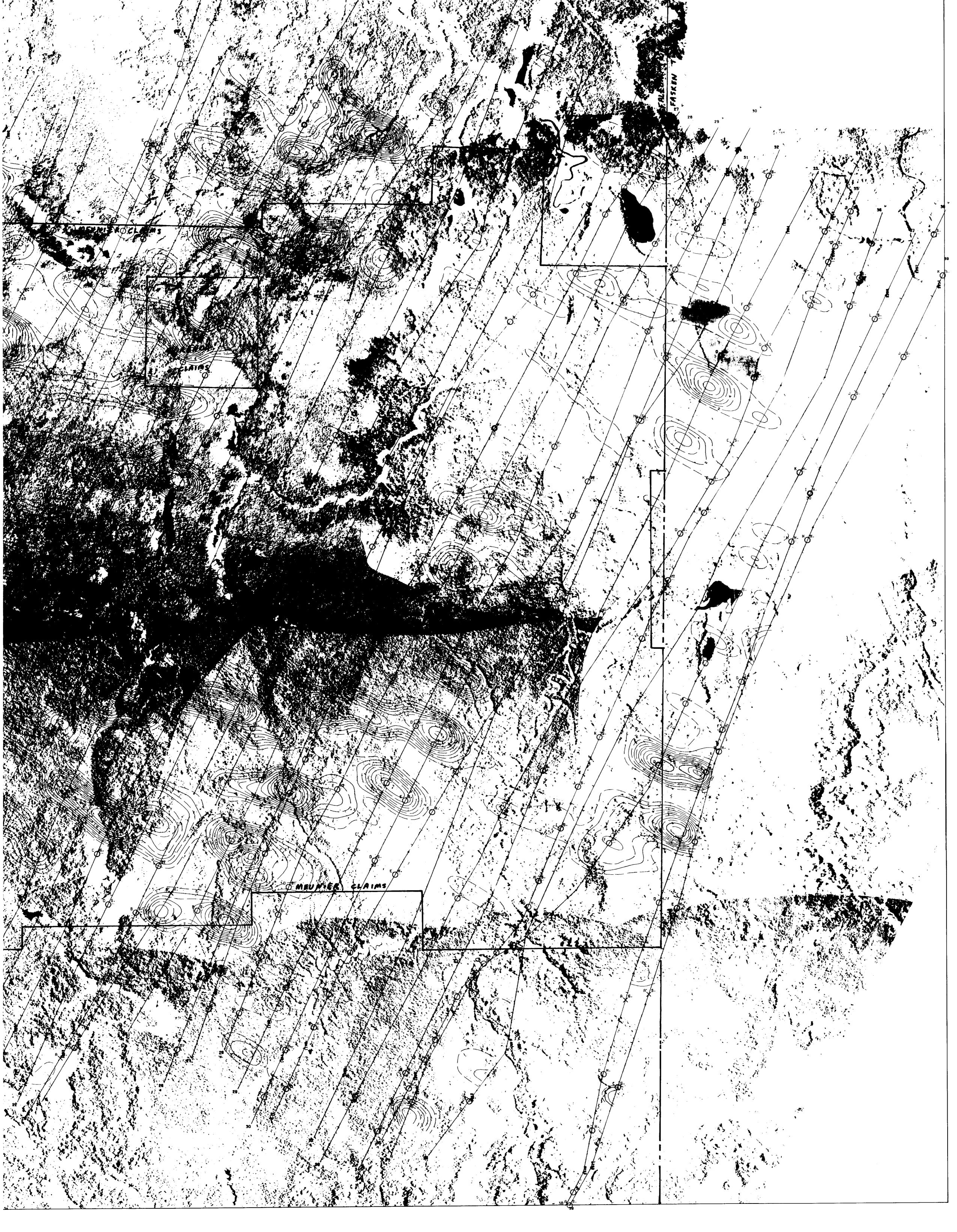


1 2 Miles





	<u> </u>		Tauranian By
JOB 190	DATE DEC./83	DRAWN BY	CHECKED BY

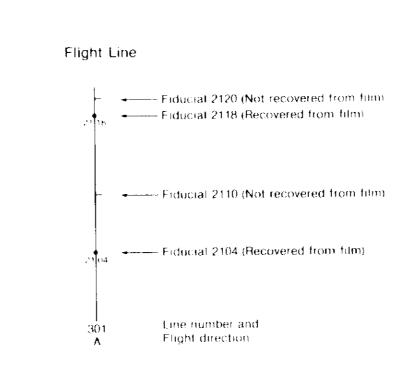


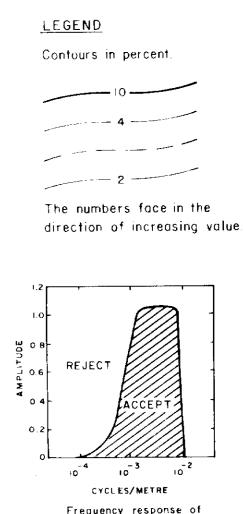


FALLON TWP. ONTARIO FILTERED TOTAL VLF EM FIELD FOR DAVID J. MEUNIER

Scale 1:10,000 1 Kilometres 1 2 Miles

27271



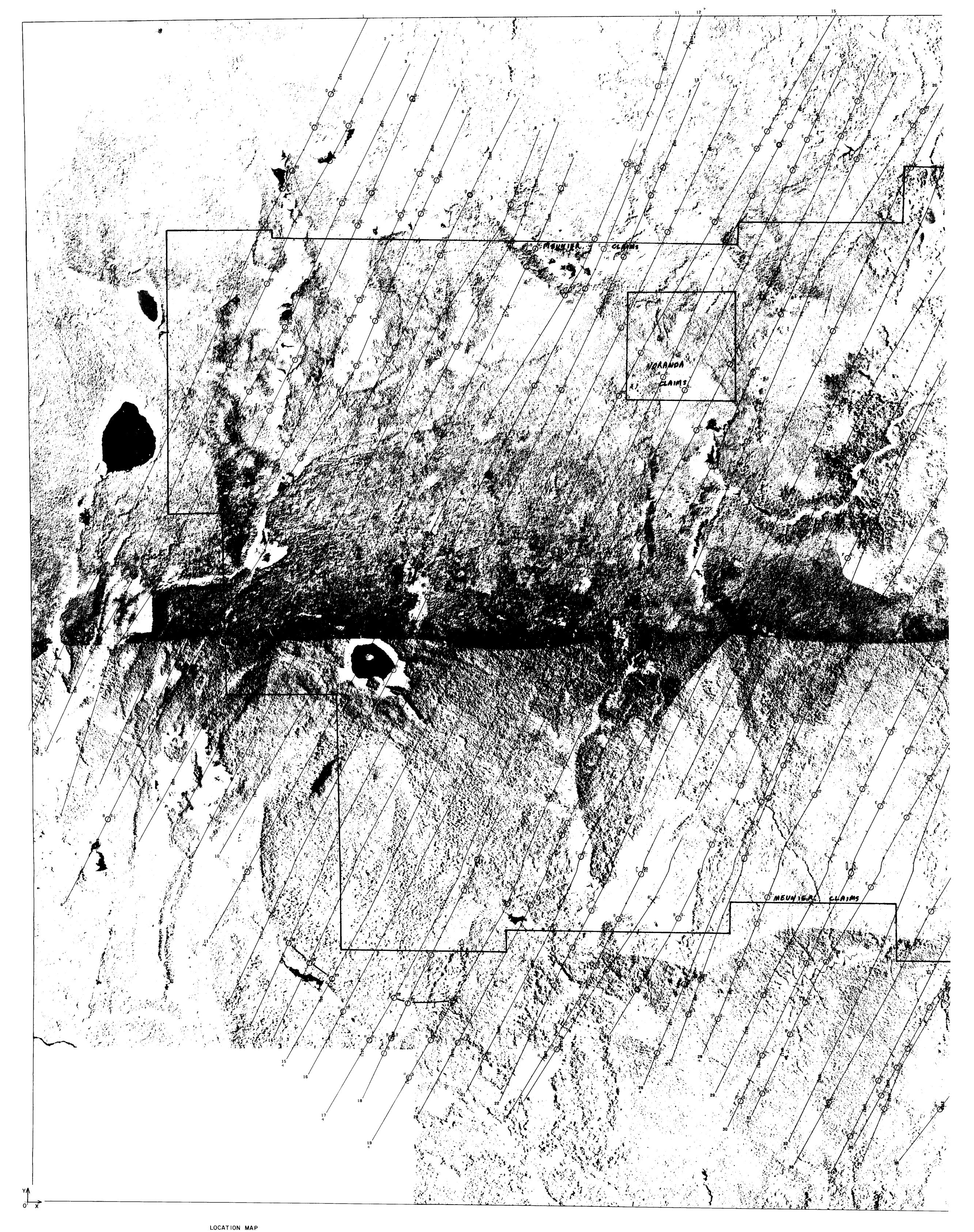


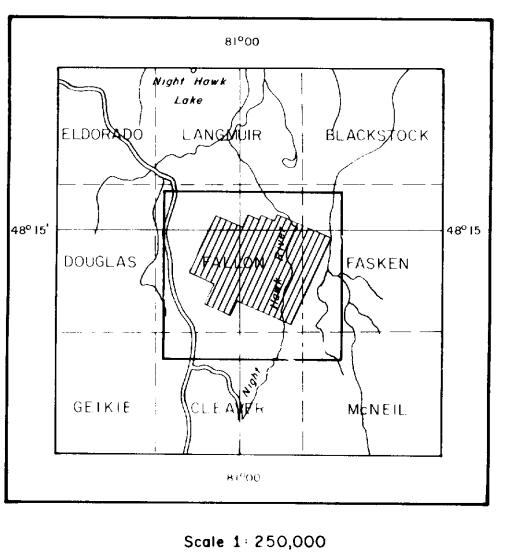
0.6	REJECT
04	ACCEPT
0.2	
	10 10 10
	CYCL ES/METRE
	Frequency response of
	VLF — EM filter

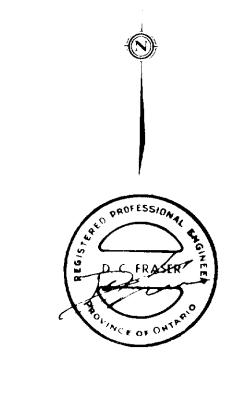
Tx NAA CUTLER, MAINE

f = 178 kHz

I JOB 190 1 DRAWN BY CHECKED BY DATE DEC./83 30.





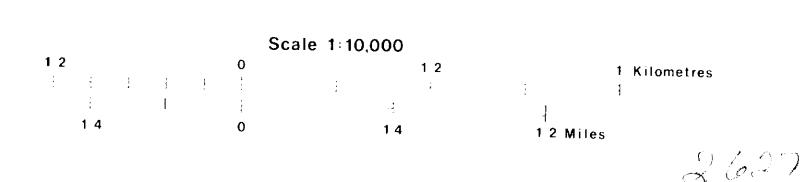


FALLON TWP. ONTARIO

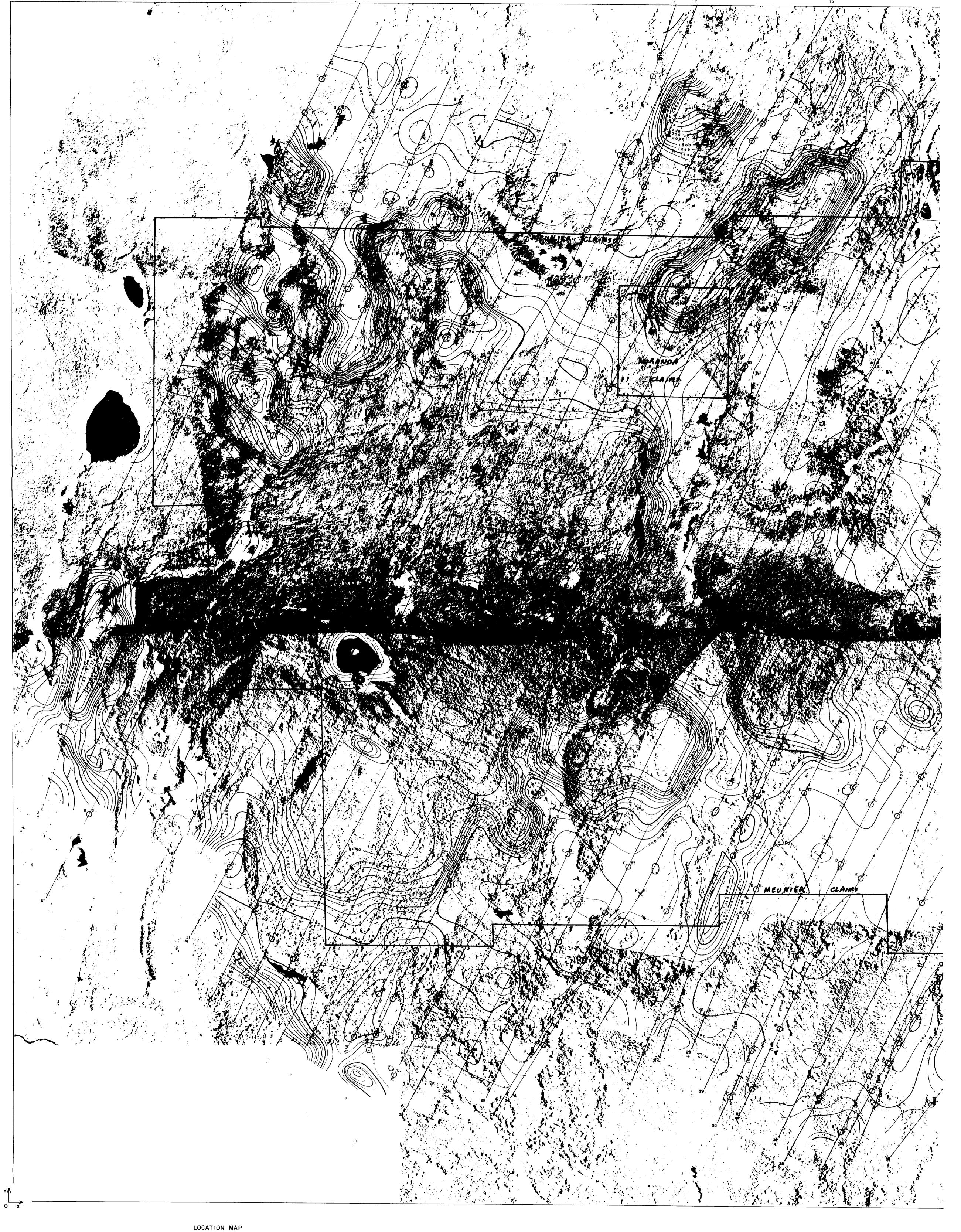
ELECTROMAGNETIC ANOMALIES

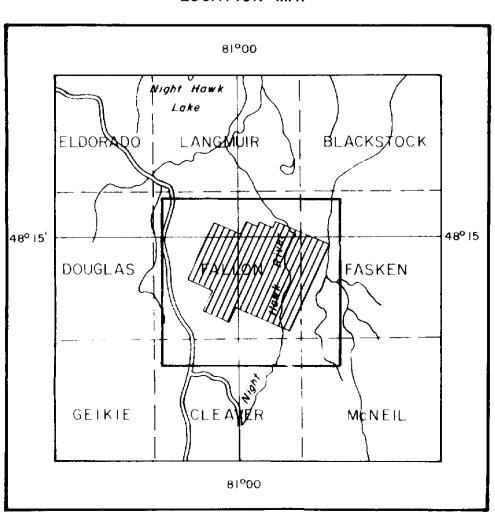
FOR

DAVID J. MEUNIER

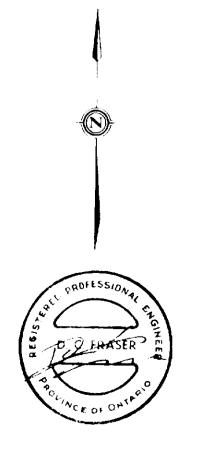








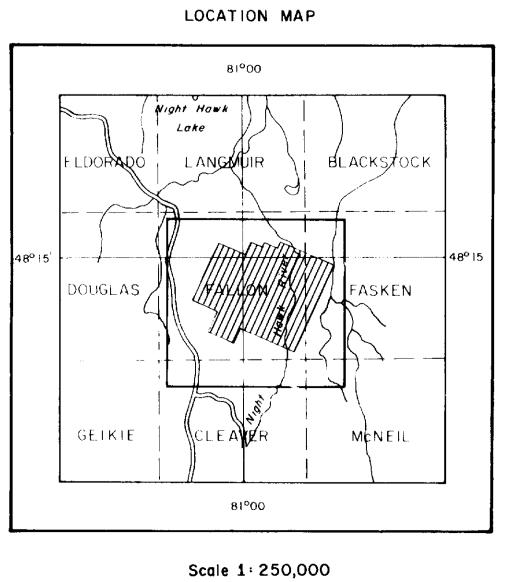
Scale 1: 250,000

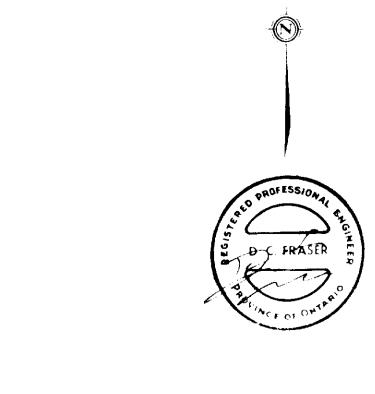


DIGHEM^{III} SURVEY

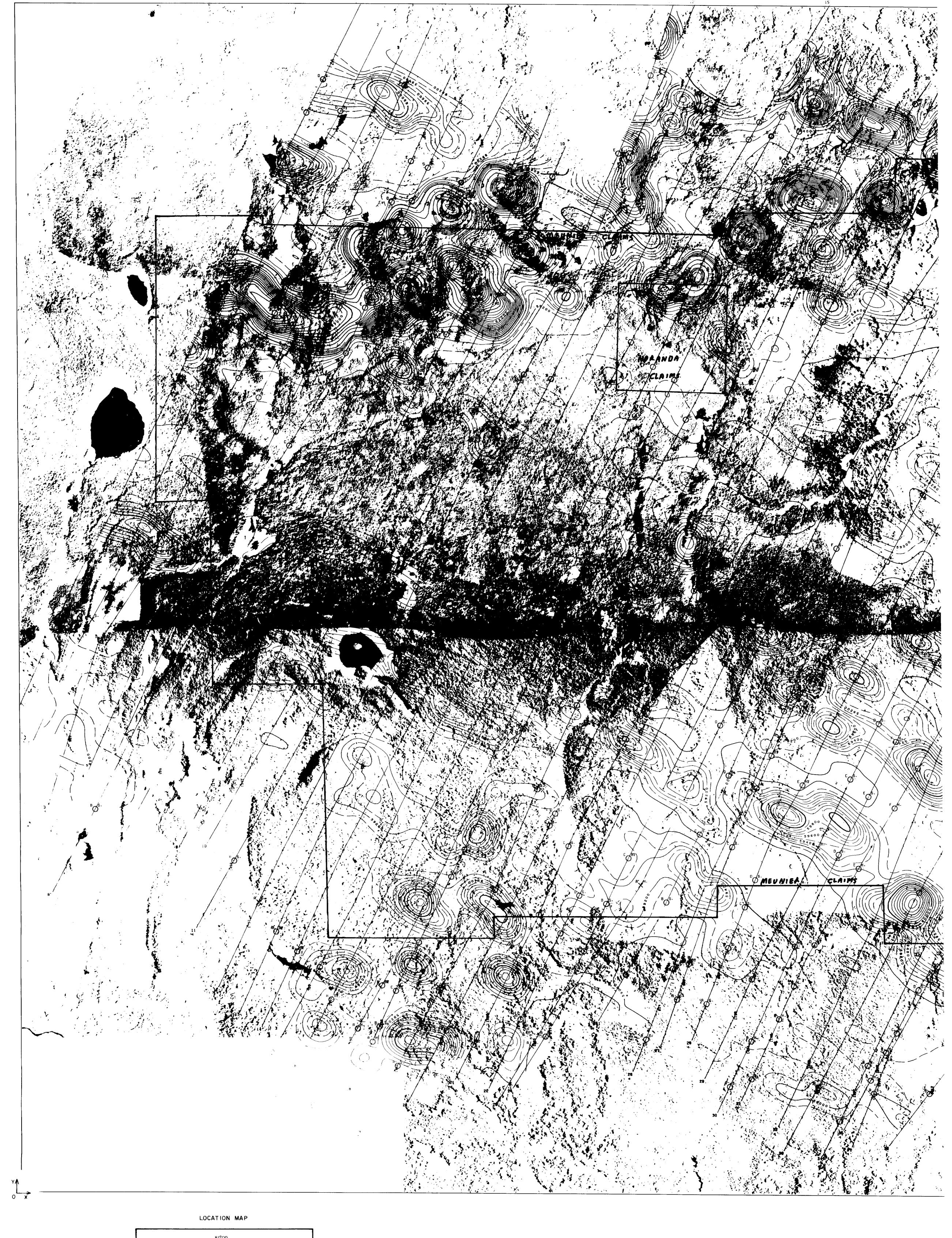
FALLON TWP. ONTARIO RESISTIVITY FOR DAVID J. MEUNIER

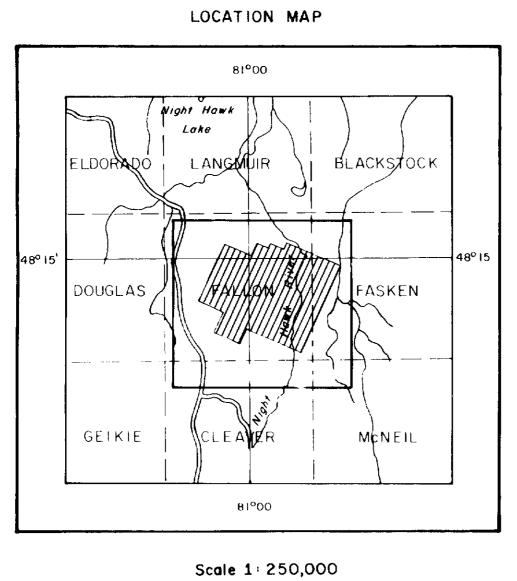


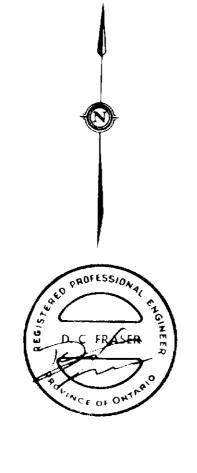




FALLON TWP. ONTARIO
TOTAL FIELD MAGNETICS
FOR
DAVID J. MEUNIER



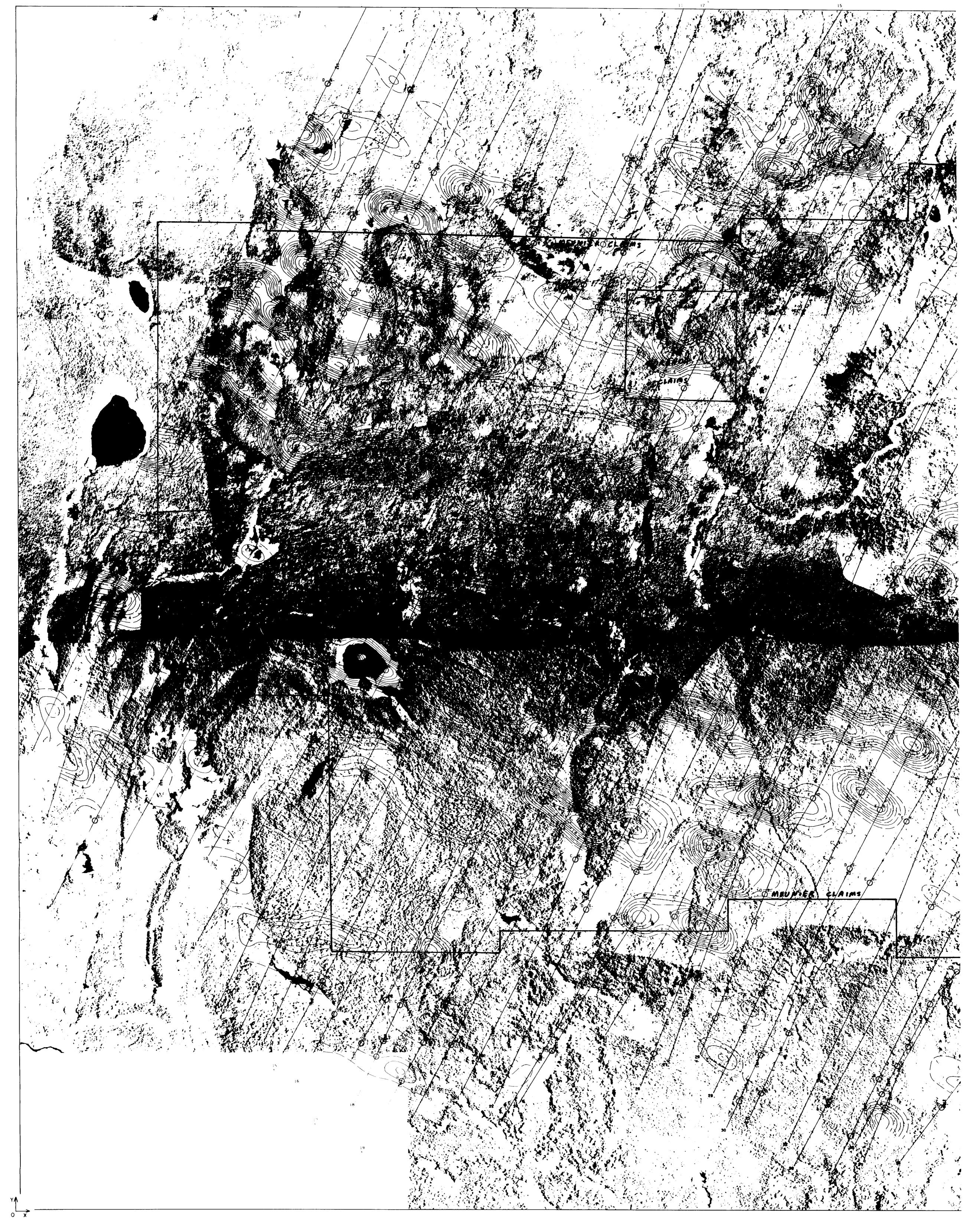


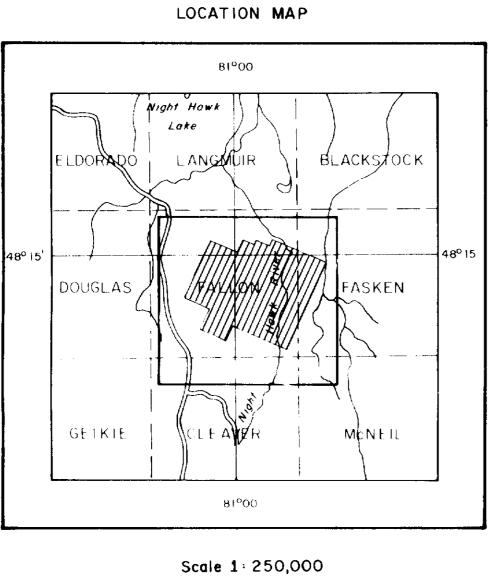


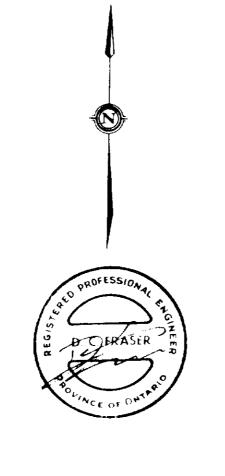
FALLON TWP. ONTARIO **ENHANCED MAGNETICS** FOR DAVID J. MEUNIER

1 Kilometres 1 2 Miles









FALLON TWP. ONTARIO

FILTERED TOTAL VLF EM FIELD

FOR

DAVID J. MEUNIER