

2006SW0050 42C03NW0012 ABBIE LAKE

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REPORT ON

COMBINED HELICOPTER-BORNE

MAGNETIC, ELECTROMAGNETIC,

AND VLF-EM SURVEY

KABENUNG CLAIMS

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MINING LANDS SECTIO

for
TUNDRA GOLD MINES LTD.
by
AERODAT LIMITED
JUNE 1983



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LIST OF MAPS

(Scale: 1/15,840)

Map	1	Interpreted Conductive Units
Map	2	Airborne Electromagnetic Survey Profile Mar (955 Hz. coaxial)
Map	3	Total Field Magnetic Map
Map	4	VLF-EM Total Field Contours

Data provided but not included in report:

- 1 master map (2 colour) of coaxial and coplanar profiles with flight path
- 2 anomaly list providing estimates of depth and conductivity thickness
- 3 analogue records of data obtained in flight

1. INTRODUCTION

This report describes an airborne geophysical survey carried out on behalf of Tundra Gold Mines Ltd. by Aerodat Limited. Equipment operated included a 3 frequency electromagnetic system, a VLF-EM system, and a magnetometer.

The survey was flown on March 6 to March 22, 1983 from an operations base at Wawa Ontario. A total of 563 line miles were flown, at a nominal line spacing of 660 feet.

Of the total flown, this report describes 462 line miles.

2. SURVEY AREA/CLAIM NUMBERS AND LOCATIONS

The mining claim numbers and locations covered by this survey are indicated on the map in the following pocket.

3. AIRCRAFT EQUIPMENT

3.1 Aircraft

The helicopter used for the survey was an Aerospatial Astar 350D owned and operated by North Star Helicopters. Installation of the geophysical and ancillary equipment was carried out by Aerodat. The survey aircraft was flown at a nominal altitude at 60 meters.

3.2 Equipment

3.2.1 Electromagnetic System

The electromagnetic system was an Aerodat/
Geonics 3 frequency system. Two vertical
coaxial coil pairs were operated at 955 and
4130 Hz and a horizontal coplanar coil pair
at 4500 Hz. The transmitter-receiver separation was 7 meters. In-phase and quadrature
signals were measured simultaneously for the
3 frequencies with a time-constant of 0.1
seconds. The electromagnetic bird was towed
30 meters below the helicopter.

3.2.2 VLF-EM System

The VLF-EM System was a Herz 2A. This instrument measures the total field and vertical

quadrature component of two selected frequencies.

The sensor was towed in a bird 15 meters below
the helicopter.

The sensor aligned with the flight direction is designated as "LINE", and the sensor perpendicular to the line direction as "ORTHO".

The "LINE" station used was NAA, Cutler Maine,

17.8 KHz or NLK, Jim Creek Washington, 24.8 KHz.

The "ORTHO" station was NSS, Annapolis Maryland,

21.4 KHz. The NSS transmitter was operating on a very limited schedule and was not available during a large part of the survey.

3.2.3 Magnetometer

The magnetometer was a Geometrics G-803 proton pracession type. The sensitivity of the instrument was 1 gamma at a 1.0 second sample rate. The sensor was towed in a bird 15 meters below the helicopter.

3.2.4 Magnetic Base Station

An IFG proton precession type magnetometer was operated at the base of operations to record diurnal variations of the earths magnetic field. The clock of the base station was synchronized with that of the airborne system

to facilitate later correlation.

3.2.5 Radar Altimeter

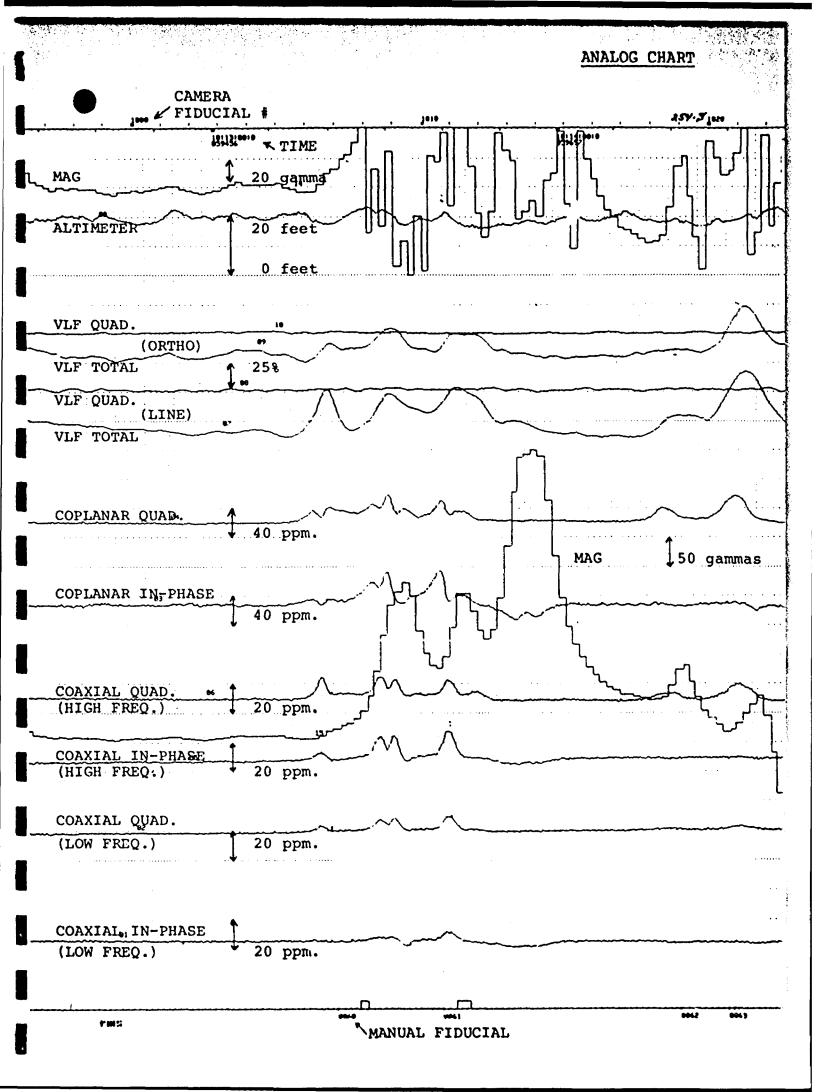
A Hoffman HRA-100 radar altimeter was used to record terrain clearance. The output from the instrument is a linear function of altitude for maximum accuracy.

3.2.6 Tracking Camera

A Geocam tracking camera was used to record flight path on 35 mm film. The camera was operated in strip mode and the fiducial numbers for cross reference to the analog and digital data were imprinted on the margin of the film.

3.2.7 Analog Recorder

A RMS dot-matrix recorder was used to display the data during the survey. A sample record with channel identification and scales is presented on the following page.



3.2.8 Digital Recorder

A Perle DAC/NAV data system recorded the survey data on cassette magnetic tape. Information recorded was as follows:

Equipment	Interval	
EM	0.1 second	
VLF-EM	0.5 second	
magnetometer	0.5 second	
altimeter	1.0 second	
fiducial (time)	1.0 second	
fiducial (manual)	0.2 second	

4. DATA PRESENTATION

4.1 Base Map and Flight Path Recovery

The base map photomosaic at a scale of 1/15,840 was constructed from available aerial photography. The flight path was plotted manually on this base and digitized for use in the computer compilation of the maps. The flight path is presented with fiducials for cross reference to both the analog and digital data.

4.2 Electromagnetic Profile Maps

The electromagnetic data was recorded digitally at a high sample rate of 10/second with a small time constant of 0.1 second. A two stage digital filtering process was carried out to reject major sferic events, and reduce system noise.

Local atmospheric activity can produce sharp, large amplitude events that cannot be removed by conventional filtering procedures. Smoothing or stacking will reduce their amplitude but leave a broader residual response that can be confused with a geological phenomenon. To avoid this possibility, a computer algorithm searches out and rejects the major "sferic" events.

The signal to noise was further enhanced by the application of a low pass filter. The filter was applied digitally. It has zero phase shift which prevents any lag or peak displacement from occurring and it suppresses only variation with a wavelength less than about 0.25 seconds. This low effective time constant permits maximum profile shape resolution.

Following the filtering processes, a base level correction was made. The correction applied is a linear function of time that ensures that the corrected amplitude of the various inphase and quadrature components

is zero when no conductive or permeable source is present. This filtered and levelled data was then presented in profile map form.

The in-phase and quadrature responses of the coaxial 955 Hz configuration are plotted with the flight path and presented on the photomosaic base.

The in-phase and quadrature responses of the coaxial 4500 Hz and the coplanar 4130 Hz configuration are plotted with flight path and are available as a two colour overlay.

4.3 Magnetic Contour Maps

The aeromagnetic data was corrected for diurnal variations by subtraction of the digitally recorded base station magnetic profile. No correction for regional variation is applied.

The corrected profile data was interpolated onto a regular grid at a 2.5 mm interval using a cubic spline technique. The grid provided the basis for threading the presented contours at a 10 gamma interval.

4.4 VLF-EM Contour and Profile Maps

The VLF-EM "LINE" signal, was compiled in map form. The mean response level of the total field signal was removed and the data was gridded and contoured at an interval of 2%. When the "ORTHO" signal was available it was compiled in a similar fashion.

4.5 Electromagnetic Conductor Symbolization

The electromagnetic profile maps were used to identify those anomalies with characteristics typical of bedrock conductors. The in-phase and quadrature response amplitudes at 4130 Hz were digitally applied to a phasor diagram for the vertical half-plane model and estimates of conductance (conductivity thickness) were made. The conductance levels were divided into categories as indicated in the map legend; the higher the number, the higher the estimated conductivity thickness product.

As discussed in Appendix I the conductance should be used as a relative rather than absolute guide to conductor quality. A conductance value of less than 2 mhos is typical for conductive overburden material and electrolytic conductors in faults and shears. Values greater than 4 mhos generally indicate some electronic conduction by certain metallic sulphides and/or graphite. Gold, although highly conductive, is not expected to occur in sufficient concentration to directly produce an electromagnetic anomaly; however, accessory mineralization such as pyrite or

graphite can produce a measurable response.

With the aid of the profile maps, responses of similar characteristics may be followed from line to line and conductor axes identified.

The distinction between conductive bedrock and overburden anomalies is not always clear and some of
the symbolized anomalies may not be of bedrock origin.

It is also possible that a response may have been
mistakenly attributed to overburden and therefore not
included in the symbolization process. For this reason,
as geological and other geophysical information becomes
available, reassessment of the significance of the
various conductors is recommended.

4.6 INTERPRETATION MAPS

The conductive trends are shown and discriminated for descriptive purposes.

These conductors are described below.

- 1 A weak conductor in volcanics length 1000'
- 2 Multiple poor conductors associated with iron formation
- A weak formational trend, south flank of iron formation, extends intermittently for four miles, may continue southwest as 22
- Moderate to fair conductor, coincides with magnetic high. One and one-quarter miles plus.
- 5 Weak conductor in sediments
- Isolated poor conductor mapped as sedimentvolcanic contact.
- 7 Fair conductor in volcanics.
- Short moderate conductor at sediment-volcanic contact
- 9 Short isolated conductor in volcanics.

- Weak conductor in sediments, on trend from 5.
- 11 Formational weak conductor two miles long, higher conductivity at west end.
- 12 Isolated, moderate conductor at sedimentvolcanic contact
- Weak conductor on north flank of iron formation. May be stratigraphic equivalent of 3.
- Short, fair magnetic conductor next to diabase dyke.
- Weak conductor next to diabase dyke. May be overburden.
- Moderate conductor at sediment-volcanic contact. May be extension of 12 west of diabase dyke.
- 17 Short, isolated conductor in volcanics.

 Magnetic low higher priority.
- Moderate conductor, magnetic, one-half mile long.
- 19 Weak, cross-cutting conductive trend.

- 20 Fair conductor, magnetic, 4000 feet long may be repetition of 18.
- 21 Isolated sharp conductor, near magnetic peak.
- 22 Formational, weak conductor on south flank of magnetic high, may be extension of 3.
- 23 Strong conductor with variable magnetic properties, roughly two miles long.
- 24 Shorter, fair conductor, magnetic.
- 25 Fair conductor in magnetic low, sediments
- Weak conductor on crosscutting magnetic trend.
- 27 Moderate conductor
- Short, fair conductor, may be on trend with 25
- 29 Strong conductor, seven miles in length may be on trend with 23 Bibis copper
 showing at western tip.
 - NOTE: The interpretation above suggests considerable structural disturbance in the vicinity of 19 and 26.

Interesting.

to diabase dyke.	ctor in vorcanies next
31 Isolated, short, weal	k conductor, magnetic
32 Moderate conductor or	n trend of magnetic low.
33 Isolated, short, pos	sibly overburden
34 Moderate conductor of	n magnetic high, sediment
35 Strong conductor, floore and half miles.	anking magnetics, length
36 Short, moderate, mag	netic, sediments
37 Fair conductor in se	dimentary trend
38 Moderate conductor o magnetics	ne mile long, flanking
39 Shorter, weak conduct	tor on volcanic-sediment
40 On volcanic-sediment conductor. Burrey s	contact. Weak definite
41 Isolated conductor o	n magnetic trend.
42, 43 Isolated definite co	

Short, magnetic conductor north of 29 trend

Short, weak conductor

Moderate conductor on north flank of magnetic high

Two mile long. Moderate to fair magnetic conductor.

Two mile magnetic conductor similar to 47

Short fair conductor in volcanic mapped as granite contact - investigate

Isolated definite conductor on intrusive

In addition to the fifty conductive features described above, there are an additional 13 weak indications of conductivity which lie in a range of weak bedrock or conductive overburden contrasts. These are designated by the letter "C" on the interpretation maps. They should be investigated if their locations are enhanced by geological favourability or other locational factors.

Respectfully submitted,

July 11, 1983.

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contact.

Fenton Scott, P. Eng.

APPENDIX I

GENERAL INTERPRETIVE CONSIDERATIONS

Electromagnetic

The Aerodat 3 frequency system utilizes 2 different transmitter-receiver coil geometries. The traditional coaxial coil configuration is operated at 2 widely separated frequencies and the horizontal coplanar coil pair is operated at a frequency approximately aligned with one of the coaxial frequencies.

The electromagnetic response measured by the helicopter system is a function of the "electrical" and "geometrical" properties of the conductor. The "electrical" property of a conductor is determined largely by its conductivity and its size and shape; the "geometrical" property of the response is largely a function of the conductors shape and orientation with respect to the measuring transmitter and receiver.

Electrical Considerations

For a given conductive body the measure of its conductivity or conductance is closely related to the measured phase shift between the received and transmitted electromagnetic field. A small phase shift indicates a relatively high conductance, a large phase shift lower conductance. A small phase shift results in a large in-phase to quadrature

ratio and a large phase shift a low ratio. This relationship is shown quantitatively for a vertical half-plane model on the accompanying phasor diagram. Other physical models will show the same trend but different quantitative relationships.

The phasor diagram for the vertical half-plane model, as presented, is for the coaxial coil configuration with the amplitudes in ppm as measured at the response peak over the conductor. To assist the interpretation of the survey results the computer is used to identify the apparent conductance and depth at selected anomalies. The results of this calculation are presented in table form in Appendix I and the conductance and in-phase amplitude are presented in symbolized form on the map presentation.

The conductance and depth values as presented are correct only as far as the model approximates the real geological situation. The actual geological source may be of limited length, have significant dip, its conductivity and thickness may vary with depth and/or strike and adjacent bodies and overburden may have modified the response. In general the conductance estimate is less affected by these limitations than the depth estimate but both should be considered a relative rather than absolute guide to the anomalies properties.

Conductance in mhos is the reciprocal of resistance in ohms and in the case of narrow slab like bodies is the product of electrical conductivity and thickness.

Most overburden will have an indicated conductance of less than 2 mhos; however, more conductive clays may have an apparent conductance of say 2 to 4 mhos. Also in the low conductance range will be electrolytic conductors in faults and shears.

The higher ranges of conductance, greater than 4 mhos, indicate that a significant fraction of the electrical conduction is electronic rather than electrolytic in nature. Materials that conduct electronically are limited to certain metallic sulphides and to graphite. High conductance anomalies, roughly 10 mhos or greater are generally limited to sulphide or graphite bearing rocks.

Sulphide minerals with the exception of sphalerite, cinnabar and stibnite are good conductors; however, they may occur in a disseminated manner that inhibits electrical conduction through the rock mass. In this case the apparent conductance can seriously under rate the quality of the conductor in geological terms. In a similar sense the relatively non-conducting sulphide minerals noted above may be present in significant concentration in association with minor conductive

sulphides, and the electromagnetic response only relate to the minor associate mineralization. Indicated conductance is also of little direct significance for the identification of gold mineralization. Although gold is highly conductive it would not be expected to exist in sufficient quantity to create a recognizable anomaly but minor accessory sulphide mineralization could provide a useful indirect indication.

In summary the estimated conductance of a conductor can provide a relatively positive identification of significant sulphide or graphite mineralization; however, a moderate to low conductance value does not rule out the possibility of significant economic mineralization.

Geometrical Considerations

Geometrical information about the geologic conductor can often be interpreted from the profile shape of the anomaly. The change in shape is primarily related to the change in inductive coupling among the transmitter, the target, and the receiver.

In the case of a thin, steeply dipping, sheet-like conductor, the coaxial coil pair will yield a near symmetric peak over the conductor. On the other hand the coplanar coil pair will pass through a null couple relationship and yield a minimum over the conductor, flanked by positive side lobes. As the dip of the conductor decreases from vertical, the coaxial

anomaly shape changes only slightly, but in the case of the coplanar coil pair the side lobe on the down dip side strengthens relative to that on the up dip side.

As the thickness of the conductor increases, induced current flow across the thickness of the conductor becomes relatively significant and complete null coupling with the coplanar coils is no longer possible. As a result, the apparent minimum of the coplanar response over the conductor diminishes with increasing thickness, and in the limiting case of a fully 3 dimensional body or a horizontal layer or half-space, the minimum disappears completely.

A horizontal conducting layer such as overburden will produce a response in the coaxial and coplanar coils that is a function of altitude (and conductivity if not uniform). The process the process of the process of the configurations with an amplitude ratio (coplanar/coaxial) of about 4/1.

In the case of a spherical conductor, the induced currents are confined to the volume of the sphere, but not relatively restricted to any arbitrary plane as in the case of a sheet-like form. The response of the coplanar coil pair directly over the sphere may be up to 8 times greater than that of the coaxial coil pair.

In summary a steeply dipping, sheet-like conductor will display a decrease in the coplanar response coincident with the peak of the coaxial response. The relative strength of this coplanar null is related inversely to the thickness of the conductor; a pronounced null indicates a relatively thin conductor. The dip of such a conductor can be infered from the relative amplitudes of the side-lobes.

Massive conductors that could be approximated by a conducting sphere will display a simple single peak profile form on both coaxial and coplanar coils, with a ratio between the coplanar to coaxial response amplitudes as high as 8.*

Overburden anomalies often produce broad poorly defined anomaly profiles. In most cases the response of the coplanar coils closely follow that of the coaxial coils with a relative amplitude ratio of 4.*

Occas anally if the edge of an overburden zone is sharply defined with some significant depth extent, an edge effect will occur in the coaxial coils. In the case of a horizontal conductive ring or ribbon, the coaxial response will consist of two peaks, one over each edge; whereas the coplanar coil will yield a single peak.

* It should be noted at this point that Aerodat's definition of the measured ppm unit is related to the primary field sensed in the receiving coil without normalization to the maximum coupled (coaxial configuration). If such normalization were applied to the Aerodat units, the amplitude of the coplanar coil pair would be halved.

Magnetics

The Total Field Magnetic Map shows contours of the total magnetic field, uncorrected for regional variation. Whether an EM anomaly with a magnetic correlation is more likely to be caused by a sulphide deposit than one without depends on the type of mineralization. An apparent coincidence between an EM and a magnetic anomaly may be caused by a conductor which is also magnetic, or by a conductor which lies in close proximity to a magnetic body. The majority of conductors which are also magnetic are sulphides containing pyrrhotite and/or magnetite. Conductive and magnetic bodies in close association can be, and often are, graphite and magnetite. It is often very difficult to distinguish between these If the conductor is also magnetic, it will usually produce an EM anomaly whose general pattern resembles that of the magnetics. Depending on the magnetic permeability of the conducting body, the amplitude of the inphase EM anomaly will be weake ed, and if the conductivity is also weak, the inphase EM anomaly may even be reversed in sign.

VLF Electromagnetics

The VLF-EM method employs the radiation from powerful military radio transmitters as the primary signals. The magnetic field associated with the primary field is elliptically polarized in the vicinity of electrical conductors. The Herz Totem uses three coils in the X. Y. Z. configuration to measure the total field and vertical quadrature component of the polarization ellipse.

The relatively high frequency of VLF 15-25 KHz provides high response factors for bodies of low conductance.

Relatively "disconnected" sulphide ores have been found to produce measurable VLF signals. For the same reason, poor conductors such as sheared contacts, breccia zones, narrow faults, alteration zones and porous flow tops normally produce VLF anomalies. The method can therefore be used effectively for geological mapping. The only relative disadvantage of the method lies in its sensitivity to conductive overburden. In conductive ground the depth of exploration is severely limited.

The effect of strike direction is important in the sense of the relation of the conductor axis relative to the energizing electromagnetic field. A conductor aligned along a radius drawn from a transmitting station will be

in a maximum coupled orientation and thereby produce a stronger response than a similar conductor at a different strike angle. Theoretically it would be possible for a conductor, oriented tangentially to the transmitter to produce no signal. The most obvious effect of the strike angle consideration is that conductors favourably oriented with respect to the transmitter location and also near perpendicular to the flight direction are most clearly rewired and usually dominate the map presentation.

The total field response is an indicator of the existence and position of a conductivity anomaly. The response will be a maximum over the conductor, without any special filtering, and strongly favour the upper edge of the conductor even in the case of a relatively shallow dip.

The vertical quadrature component over steeply dipping sheet like conductor will be a cross-over type response with the cross-over closely associated with the upper edge of the conductor.

The response is a cross-over type due to the fact that it is the vertical rather than total field quadrature component that is measured. The response shape is due largely to geometrical rather than conductivity considerations and the distance between the maximum and minimum on either side of the cross-over is related to target depth. For a given target geometry, the larger this distance the greater the

depth.

The amplitude of the quadrature response, as opposed to shape is function of target conductance and depth as well as the conductivity of the overburden and host rock. As the primary field travels down to the conductor through conductive material it is both attenuated and phase shifted in a negative sense. The secondary field produced by this altered field at the target also has an associated phase shift. This phase shift is positive and is larger for relatively poor conductors. This secondary field is attenuated and phase shifted in a negative sense during return travel to the surface. The net effect of these 3 phase shifts determine the phase of the secondary field sensed at the receiver.

A relatively poor conductor in resistive ground will yield a net positive phase shift. A relatively good conductor in more conductive ground will yield a net negative phase shift. A combination is possible whereby the net phase shift is zero and the response is purely in-phase with no quadrature component.

A net positive phase shift combined with the geometrical cross-over shape will lead to a positive quadrature response on the side of approach and a negative on the side of departure. A net negative phase shift would produce the reverse. A further sign reversal occurs with a 180 degree

change in instrument orientation as occurs on reciprocal line headings. During digital processing of the quadrature data for map presentation this is corrected for by normalizing the sign to one of the flight line headings.



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Ministry of Natural Resources

GEOPHYSICAL — GEOLOGICAL — GEOCHEMICAL TECHNICAL DATA STATEMENT

TO BE ATTACHED AS AN APPENDIX TO TECHNICAL REPORT FACTS SHOWN HERE NEED NOT PE REPEATED IN REPORT TECHNICAL REPORT MUST CONTAIN IN EXPRETATION, CONCLUSIONS ETC.

Type of Survey(s) Airborn	ne Electromagnetic, Magnet	cic, VLF-EM
Township or Area Pukaskwa		MINING CLAIMS TRAVERSED
Claim Holder(s) Tundra	List numerically	
Survey Company Aeroc	dat Limited	SSM_61590_et_al
Author of ReportFent	on Scott	(prefix) (number) List attched
Address of Author 17 M	alabar Place, Don Mills, (<u>On</u> t
Covering Dates of Survey M.	arch 6 to 22, 1983	
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Total Wiles of Line Out.		
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ENTER 20 days for each additional survey using	-Other	Dren
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AIRBORNE SURVEYS	
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Total Days Credits may be apportioned at the claim holder's choice. Enter number of days credits per claim selected In columns at right.

Total Expenditures

Calculation of Expenditure Days Credits

Recorded Holder of Agent (Signature) OCT. 29/83

ertification Verifying Report of Work TUNDAR GOLD

15

Total

Days Credits

I hereby certify that I have a personal and intimate knowledge of the facts set forth in the Report of Work annexed hereto, having performed the work or witnessed same during and/or after its completion and the annexed report is true.

me and Postal Address of Person Certifying

Se477 FENTUN 17 MALABAR PLACE DON MILLS Date Certified

OCT 23

M3B 144

Total number of mining

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62 (81/9)

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Technical Assessment Work Credits

2,597/

Recorded Holder	Tundra	Gold	Mines	Limite	ŀ		
Towards or fees	PUKAS						

Type of survey and number of Assessment days credit per claim	Mining Claims Assessed
Geophysical	SSM 619590 to 663 incl.
Electromagnetic	619665 to 89 incl.
Magnetometer 20.9 days	662001 to 10 incl. 662013 to 22 incl.
Radiometric V.L.F. 20.9 days	662027 to 44 incl.
Induced polarizationdays	662048 to 55 incl. 662057
Section 86 (18) days	662066 to 70 incl.
Geologicaldays	666538 to 99 incl.
Geochemical days	666638 to 71 incl. 666738 to 840 incl.
Man days Airborne	666842 to 92 indi
_	691398 to 457 incl.
Special provision Ground Ground	691518 to 637 ind.
Credits have been reduced because of partial	691737 to 57 ind.
coverage of claims.	692803 to 17 ind.
Credits have been reduced because of corrections	692868 to 928 incl.
to work dates and figures of applicant.	692968 to 99 ind.
	693001 to 15 incl.
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No credits have been allowed for the following mining of	
not sufficiently covered by the survey	Insufficient technical data filed

The Mining Recorder may reduce the above credits if necessary in order that the total number of approved assessment days recorded on each claim does not exceed the maximum allowed as follows: Geophysical — 80; Geological — 40; Geochemical — 40; Section 86(18)-60:



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Approval

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「o: Geophysics ∧	Mr. R. Barlow.			
Comments				

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Dec. 19,1983 Mary Ellen Anderson

Approved Reports of Work sent out

Notice of Intent filed

Approval after Notice of Intent sent out

Duplicate sent to Resident Geologist

Duplicate sent to A.F.R.O.

1983 11 08 2.5971

Mrs. M.V. St. Jules
Mining Recorder
Ministry of Natural Resources
875 Queen Street East
P.O. Box 669
Sault Ste. Marie, Ontario
P6A 5N2

Dear Madam:

He have received reports and maps for an Airborne Geophysical (Electromagnetic and Magnetometer and VLF) survey subsitted on mining claims SSM619590 et al in the Areas of Pukaskwa River and Abbie Lake.

This material will be examined and assessed and a statement of assessment work credits will be issued.

We do not have a copy of the report of work which is normally filed with you prior to the submission of this technical data. Please forward a copy as soon as possible.

Yours very truly,

E.F. Anderson Director Land Management Branch

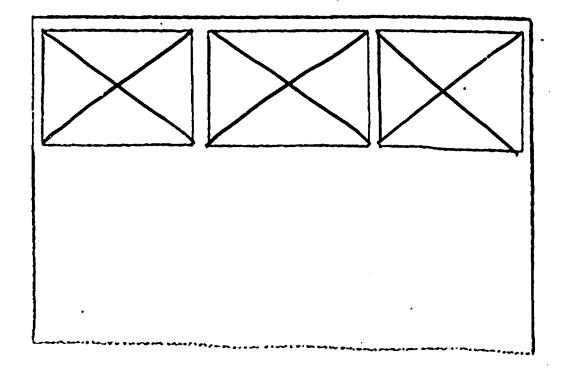
Whitney Block, Room 6643 Queen's Park Toronto, Ontario M7A 1W3 Phone: (416)965-1380

A. Barr: mc

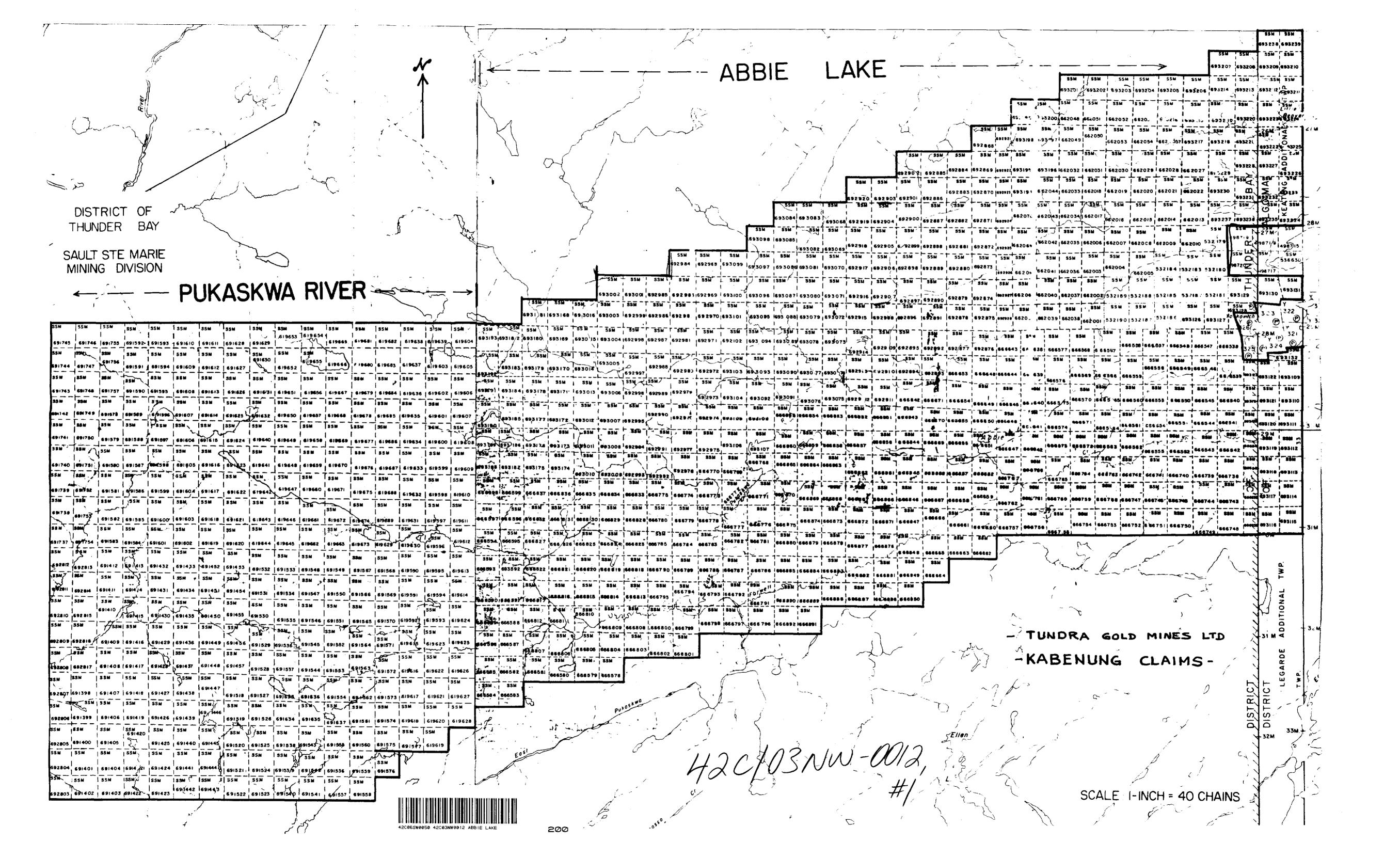
cc: Tundra Gold Mines Limited c/o H.I. Miller Suite 1205 45 Richmond Street West Toronto, Ontario M5H 1Z2

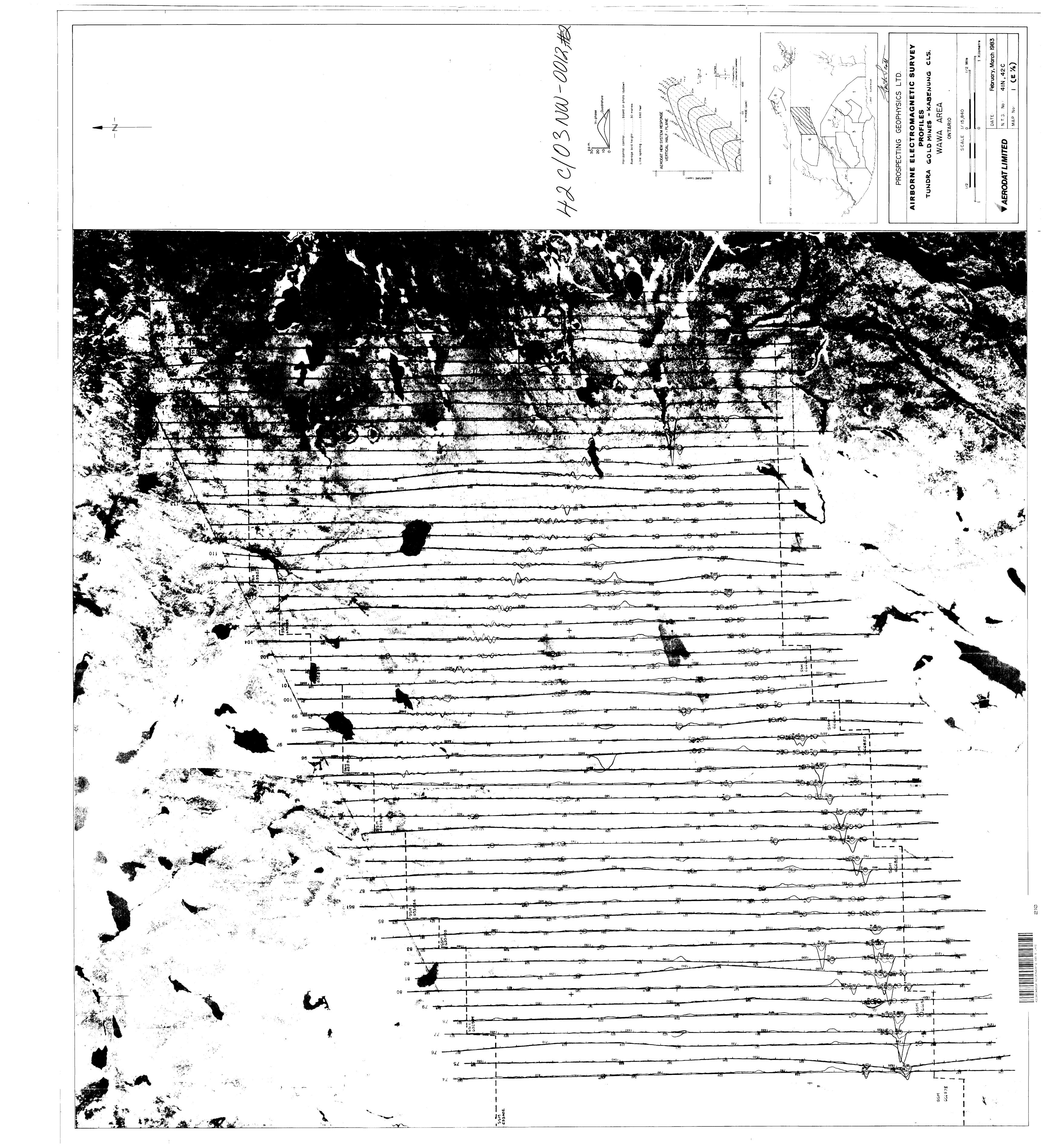
cc: Fenton Scott 17 Malabar Place Don Mills, Ontario M3B 1A4 SEE ACCOMPANYING
MAP(S) IDENTIFIED AS
420/03 NW-00/2

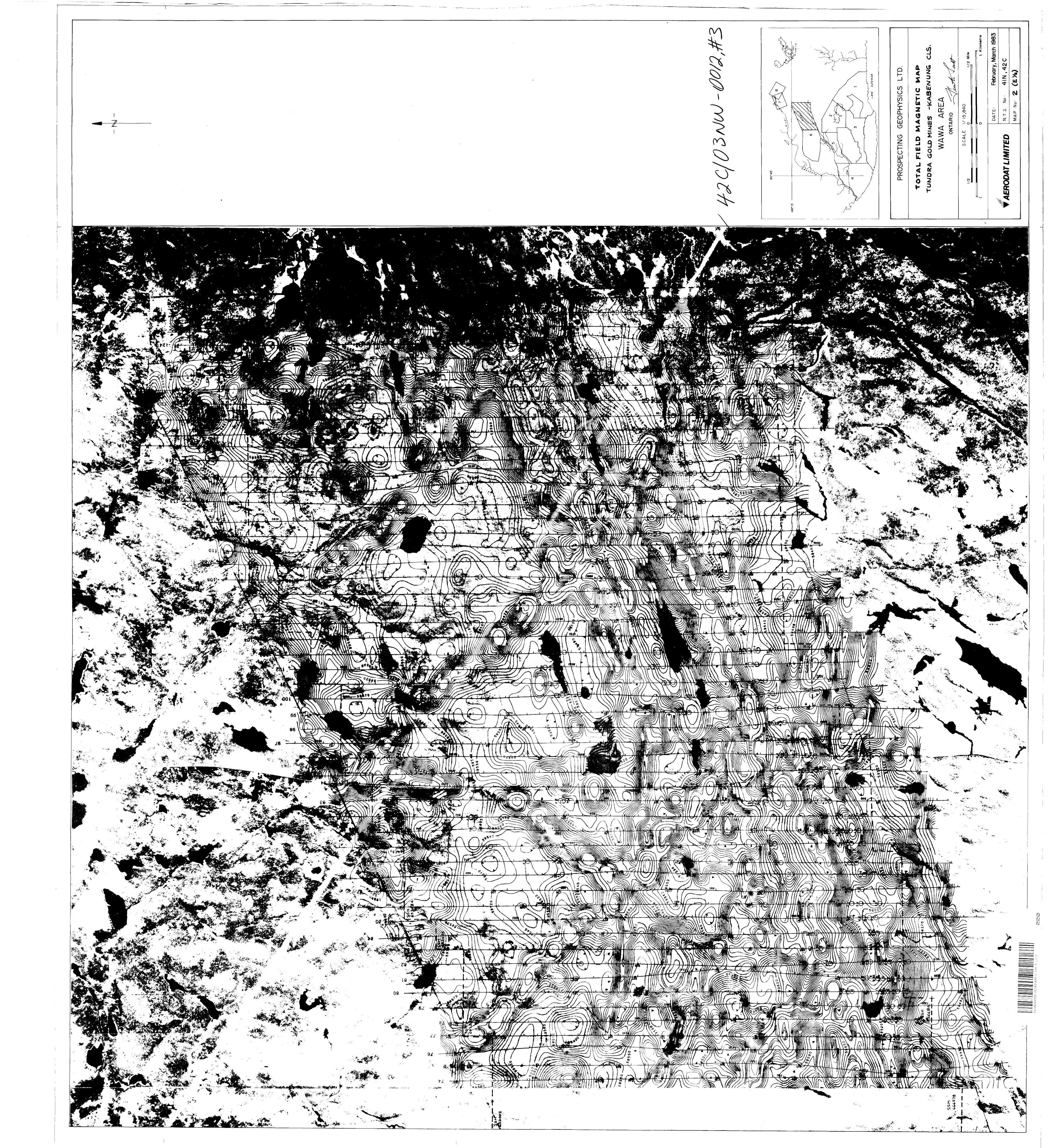
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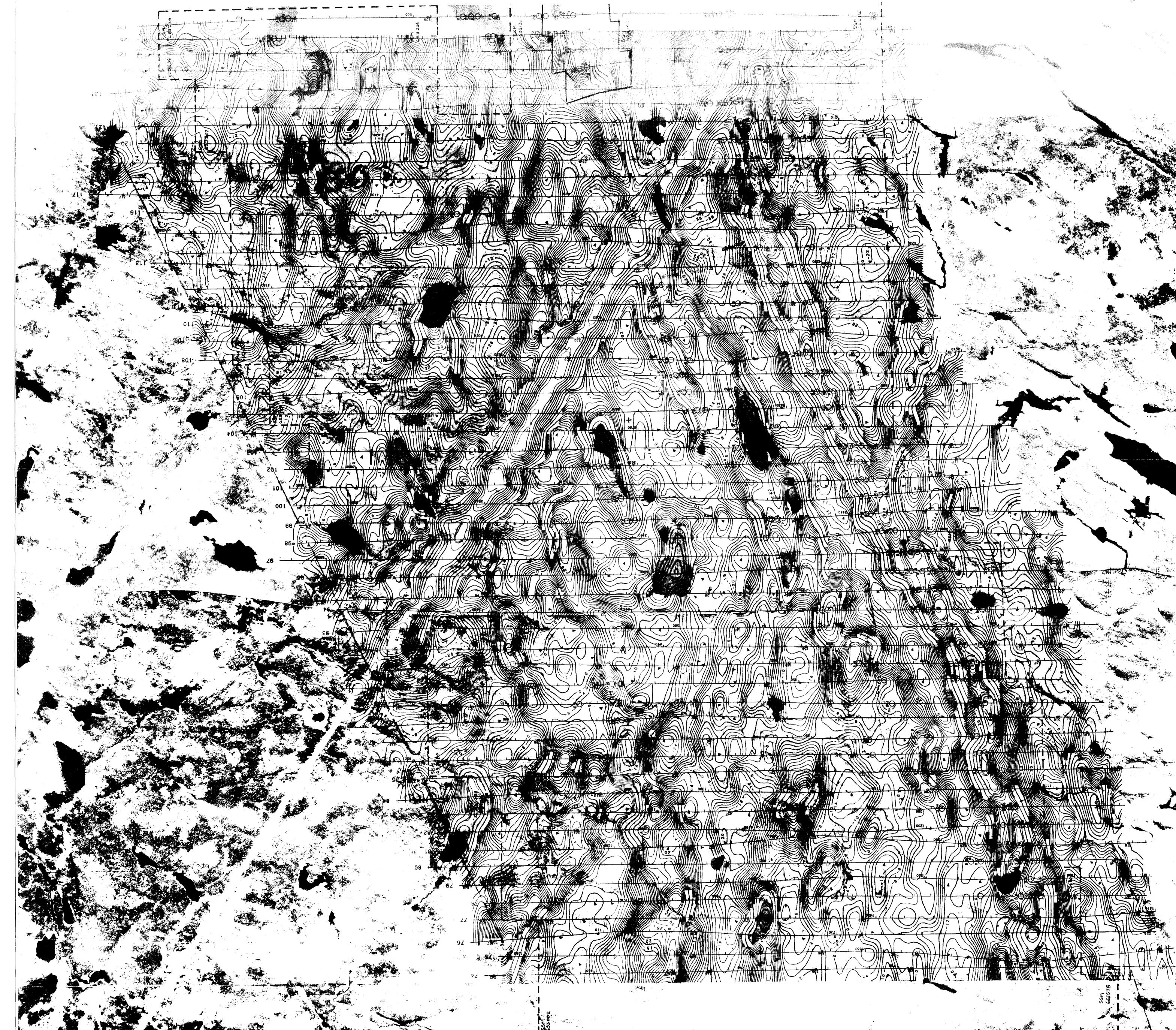
FOR ADDITIONAL INFORMATION SEE MAPS: 420/03 NW-00/2 #4-9

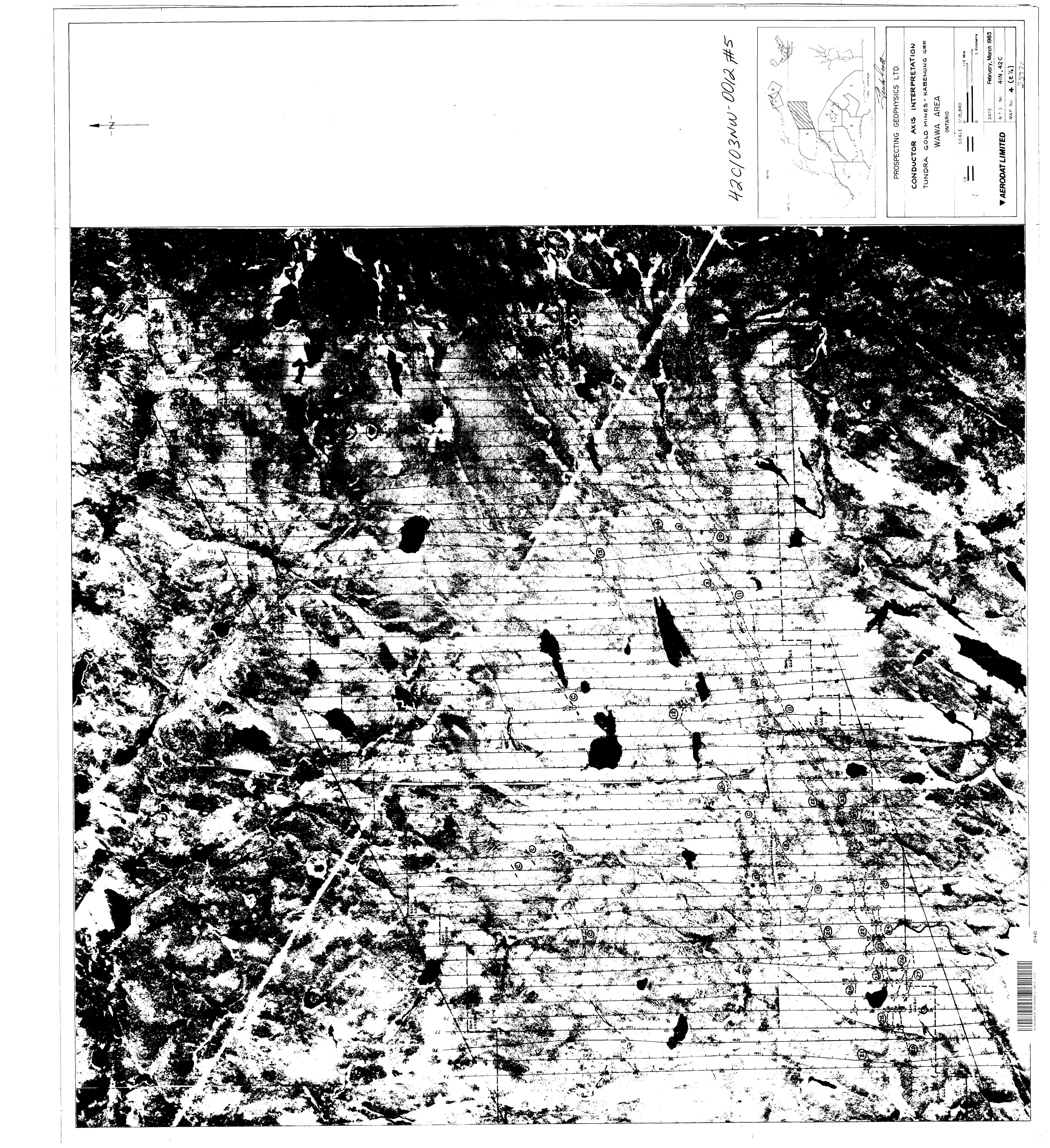






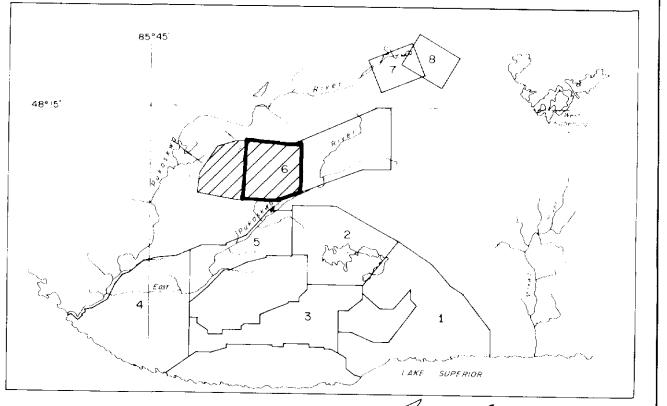
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PROSPECTING GEOPHYSICS LTD.

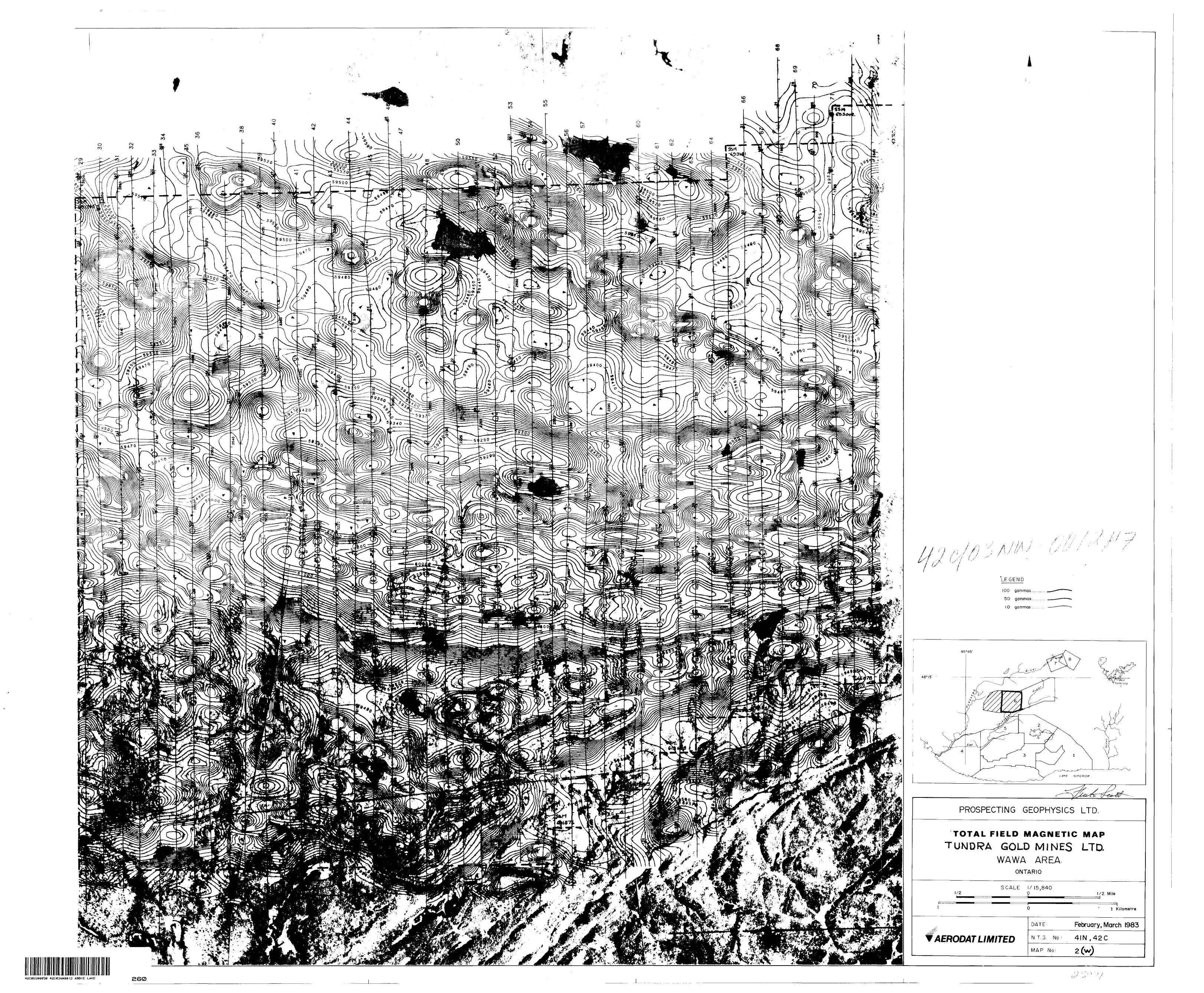
TUNDRA GOLD MINES LTD.

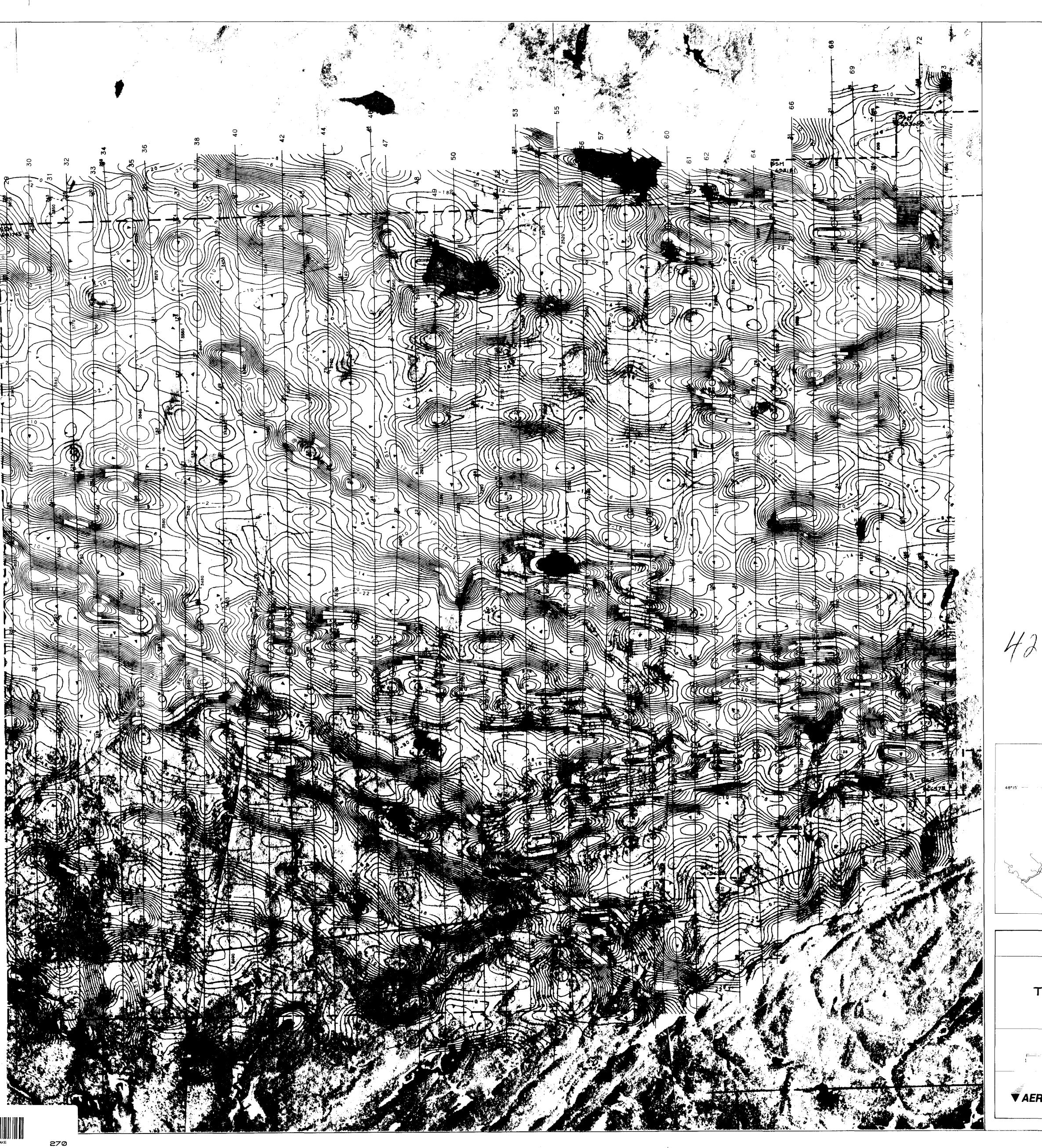
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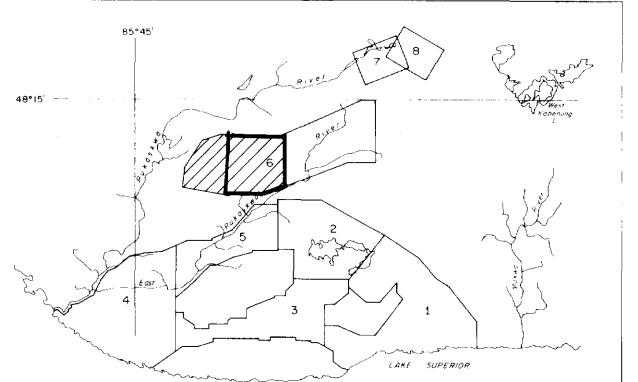
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PROSPECTING GEOPHYSICS LTD.

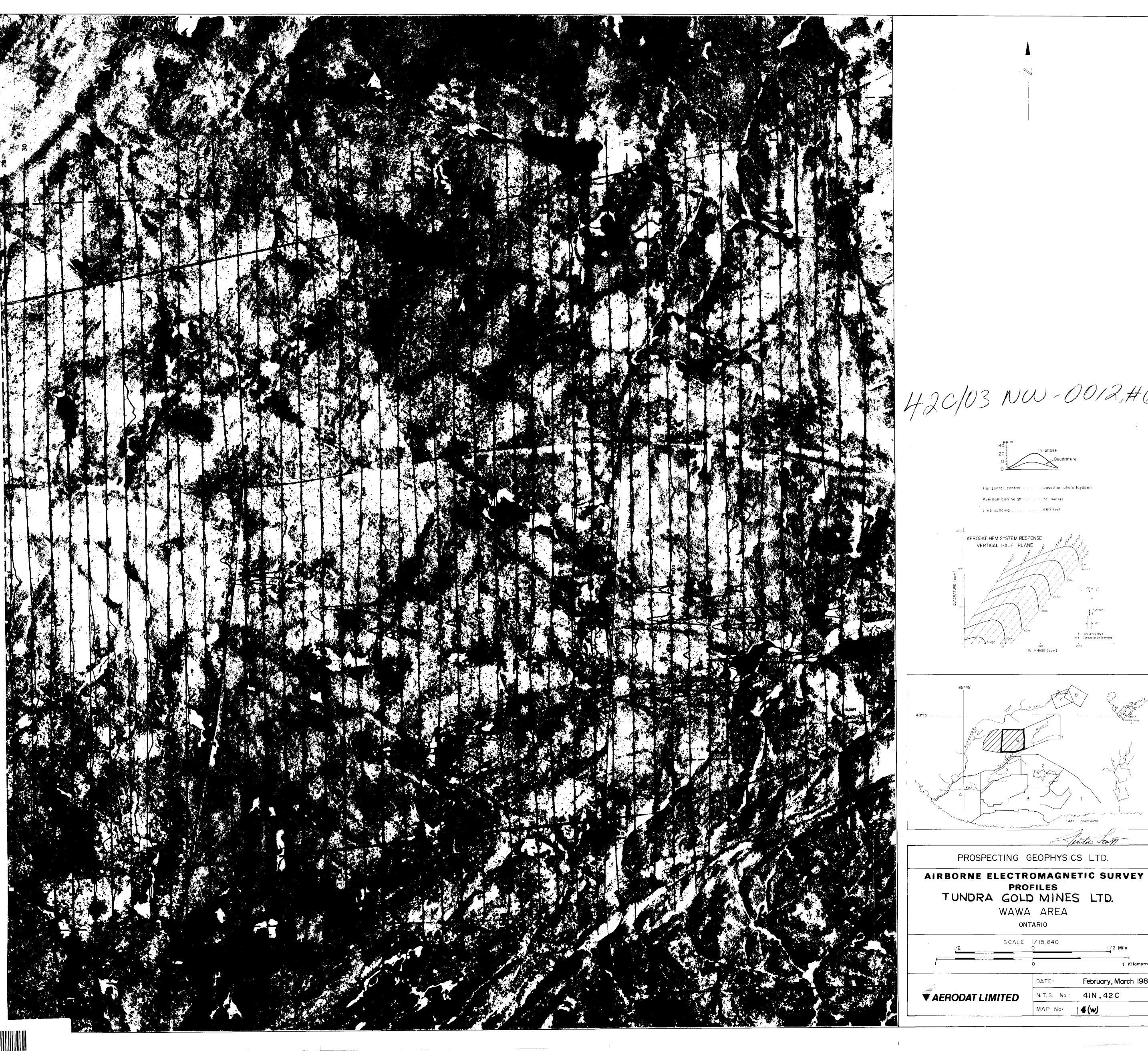
VLF-EM NAA (MAINE) 17.8 KHz.

TUNDRA GOLD MINES LTD. WAWA AREA

SCALE 1/15,840 0

▼ AERODAT LIMITED

February, March 1983 3(w) MAP No:



Jento Fox

February, March 1983

41N,42C

