



42C10NW0001 NAMEIGOS0015 NAMEIGOS

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REPORT ON  
COMBINED HELICOPTER-BORNE  
MAGNETIC, ELECTROMAGNETIC,  
AND VLF-EM SURVEY  
OF  
JOSELIN LAKE CLAIMS

for  
SAXTON INDUSTRIES LIMITED  
by  
AERODAT LIMITED  
March 1983

11/10

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42C10NW0001 NAMEIGOS0015 NAMEIGOS

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1. INTRODUCTION

This report describes an airborne geophysical survey carried out on behalf of Saxton Industries Limited by Aerodat Limited. Equipment operated included a 3 frequency electromagnetic system, a VLF-EM system, and a magnetometer.

The survey was flown on March 25 and 26, 1983 from an operations base at Wawa Ontario. A total of 486 line miles were flown, at a nominal line spacing of 660 feet. Of the total flown, this report describes 63 line miles.

2. SURVEY AREA/CLAIM NUMBERS AND LOCATIONS

The mining claim numbers and locations covered by this survey are indicated on the map in the following pocket.



### 3. AIRCRAFT EQUIPMENT

#### 3.1 Aircraft

The helicopter used for the survey was an Aerospatial Astar 350D owned and operated by North Star Helicopters. Installation of the geophysical and ancillary equipment was carried out by Aerodat. The survey aircraft was flown at a nominal altitude at 60 meters.

#### 3.2 Equipment

##### 3.2.1 Electromagnetic System

The electromagnetic system was an Aerodat/Geonics 3 frequency system. Two vertical coaxial coil pairs were operated at 955 and 4130 Hz and a horizontal coplanar coil pair at 4500 Hz. The transmitter-receiver separation was 7 meters. In-phase and quadrature signals were measured simultaneously for the 3 frequencies with a time-constant of 0.1 seconds. The electromagnetic bird was towed 30 meters below the helicopter.

##### 3.2.2 VLF-EM System

The VLF-EM System was a Herz 2A. This instrument measures the total field and vertical

quadrature component of two selected frequencies. The sensor was towed in a bird 15 meters below the helicopter.

The sensor aligned with the flight direction is designated as "LINE", and the sensor perpendicular to the line direction as "ORTHO". The "LINE" station used was NAA, Cutler Maine, 17.8 KHz or NLK, Jim Creek Washington, 24.8 KHz. The "ORTHO" station was NSS, Annapolis Maryland, 21.4 KHz. The NSS transmitter was operating on a very limited schedule and was not available during a large part of the survey.

#### 3.2.3 Magnetometer

The magnetometer was a Geometrics G-803 proton precession type. The sensitivity of the instrument was 1 gamma at a 1.0 second sample rate. The sensor was towed in a bird 15 meters below the helicopter.

#### 3.2.4 Magnetic Base Station

An IFG proton precession type magnetometer was operated at the base of operations to record diurnal variations of the earths magnetic field. The clock of the base station was synchronized with that of the airborne system



to facilitate later correlation.

3.2.5 Radar Altimeter

A Hoffman HRA-100 radar altimeter was used to record terrain clearance. The output from the instrument is a linear function of altitude for maximum accuracy.

3.2.6 Tracking Camera

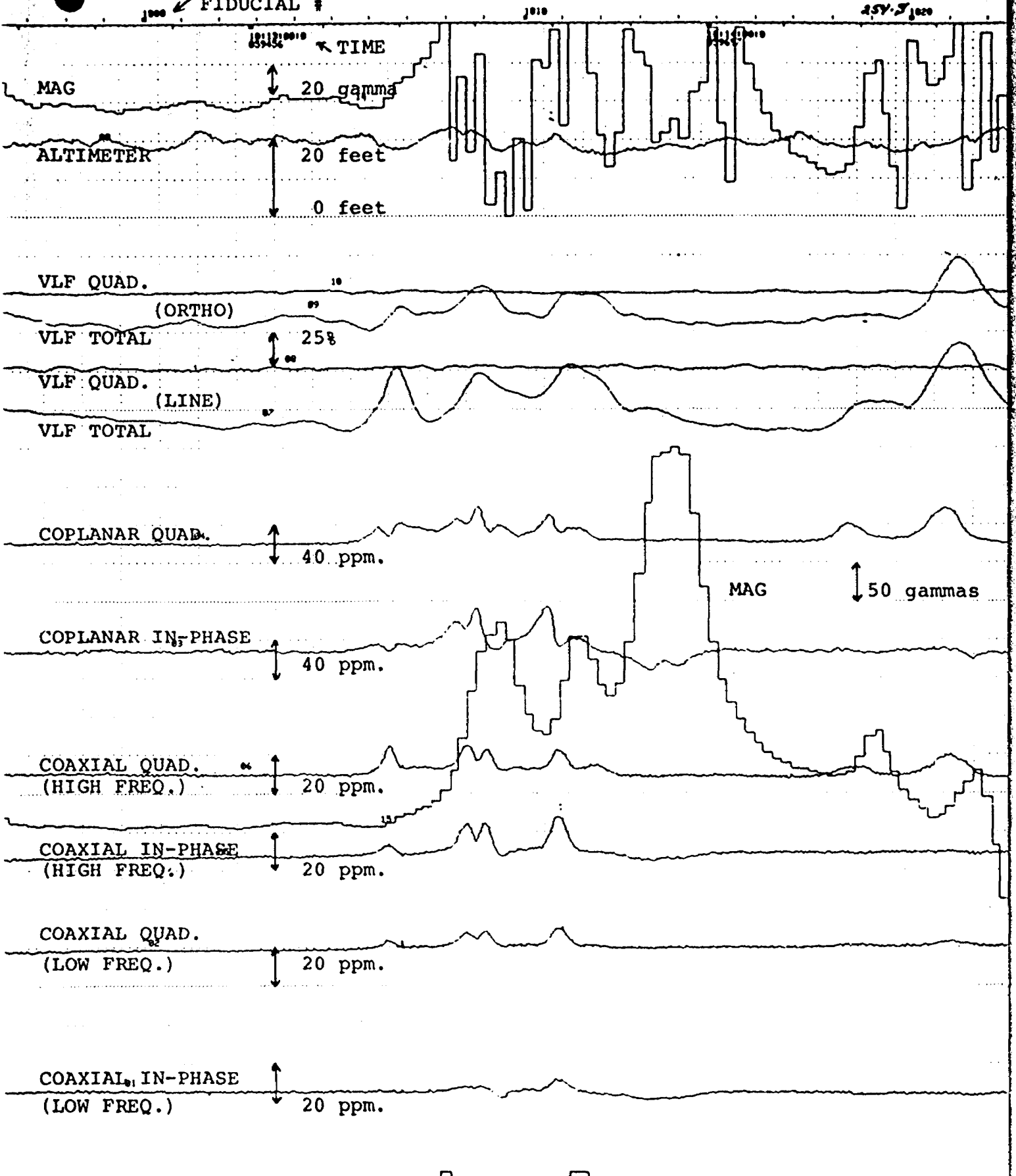
A Geocam tracking camera was used to record flight path on 35 mm film. The camera was operated in strip mode and the fiducial numbers for cross reference to the analog and digital data were imprinted on the margin of the film.

3.2.7 Analog Recorder

A RMS dot-matrix recorder was used to display the data during the survey. A sample record with channel identification and scales is presented on the following page.

ANALOG CHART

CAMERA  
FIDUCIAL #



FM2

MANUAL FIDUCIAL

FM2

FM1

3.2.8 Digital Recorder

A Perle DAC/NAV data system recorded the survey data on cassette magnetic tape. Information recorded was as follows:

<u>Equipment</u>	<u>Interval</u>
EM	0.1 second
VLF-EM	0.5 second
magnetometer	0.5 second
altimeter	1.0 second
fiducial (time)	1.0 second
fiducial (manual)	0.2 second

4. DATA PRESENTATION

4.1 Base Map and Flight Path Recovery

The base map photomosaic at a scale of 1/15,840 was constructed from available aerial photography. The flight path was plotted manually on this base and digitized for use in the computer compilation of the maps. The flight path is presented with fiducials for cross reference to both the analog and digital data.

#### 4.2 Electromagnetic Profile Maps

The electromagnetic data was recorded digitally at a high sample rate of 10/second with a small time constant of 0.1 second. A two stage digital filtering process was carried out to reject major sferic events, and reduce system noise.

Local atmospheric activity can produce sharp, large amplitude events that cannot be removed by conventional filtering procedures. Smoothing or stacking will reduce their amplitude but leave a broader residual response that can be confused with a geological phenomenon. To avoid this possibility, a computer algorithm searches out and rejects the major "sferic" events.

The signal to noise was further enhanced by the application of a low pass filter. The filter was applied digitally. It has zero phase shift which prevents any lag or peak displacement from occurring and it suppresses only variation with a wavelength less than about 0.25 seconds. This low effective time constant permits maximum profile shape resolution.

Following the filtering processes, a base level correction was made. The correction applied is a linear function of time that ensures that the corrected amplitude of the various inphase and quadrature components

is zero when no conductive or permeable source is present. This filtered and levelled data was then presented in profile map form.

The in-phase and quadrature responses of the coaxial 955 Hz configuration are plotted with the flight path and presented on the photomosaic base.

The in-phase and quadrature responses of the coaxial 4500 Hz and the coplanar 4130 Hz configuration are plotted with flight path and are available as a two colour overlay.

#### 4.3 Magnetic Contour Maps

The aeromagnetic data was corrected for diurnal variations by subtraction of the digitally recorded base station magnetic profile. No correction for regional variation is applied.

The corrected profile data was interpolated onto a regular grid at a 2.5 mm interval using a cubic spline technique. The grid provided the basis for threading the presented contours at a 10 gamma interval.

4.4 VLF-EM Contour and Profile Maps

The VLF-EM "LINE" signal, was compiled in map form. The mean response level of the total field signal was removed and the data was gridded and contoured at an interval of 2%. When the "ORTHO" signal was available it was compiled in a similar fashion.



#### 4.5 Electromagnetic Conductor Symbolization

The electromagnetic profile maps were used to identify those anomalies with characteristics typical of bedrock conductors. The in-phase and quadrature response amplitudes at 4130 Hz were digitally applied to a phasor diagram for the vertical half-plane model and estimates of conductance (conductivity thickness) were made. The conductance levels were divided into categories as indicated in the map legend; the higher the number, the higher the estimated conductivity thickness product.

As discussed in Appendix I the conductance should be used as a relative rather than absolute guide to conductor quality. A conductance value of less than 2 mhos is typical for conductive overburden material and electrolytic conductors in faults and shears. Values greater than 4 mhos generally indicate some electronic conduction by certain metallic sulphides and/or graphite. Gold, although highly conductive, is not expected to occur in sufficient concentration to directly produce an electromagnetic anomaly; however, accessory mineralization such as pyrite or

graphite can produce a measurable response.

With the aid of the profile maps, responses of similar characteristics may be followed from line to line and conductor axes identified.

The distinction between conductive bedrock and overburden anomalies is not always clear and some of the symbolized anomalies may not be of bedrock origin. It is also possible that a response may have been mistakenly attributed to overburden and therefore not included in the symbolization process. For this reason, as geological and other geophysical information becomes available, reassessment of the significance of the various conductors is recommended.

4.6 INTERPRETATION MAPS

The conductive trends are shown and discriminated for descriptive purposes.

These conductors are described below.

- 1 Weak bedrock conductor north flank of magnetic high-mapped as volcanics.
- 2 Possible bedrock conductor on north flank of magnetic high. No outcrop.
- 3 Weak, short conductor, may be overburden
- 4 Weak conductor, possibly bedrock
- 5 Good short conductor in volcanics next to diabase dyke.
- 6 Weak conductor trend, possibly overburden next to magnetic high. No outcrop, mapped as granite.
- 7 Weak conductor probably overburden, on strike with reported pyrite-molybdenum mineralization.

Respectfully submitted,



Fenton Scott, P.Eng.

August 11, 1983.

Anal 63.1263

## APPENDIX I

### GENERAL INTERPRETIVE CONSIDERATIONS

#### Electromagnetic

The Aerodat 3 frequency system utilizes 2 different transmitter-receiver coil geometries. The traditional coaxial coil configuration is operated at 2 widely separated frequencies and the horizontal coplanar coil pair is operated at a frequency approximately aligned with one of the coaxial frequencies.

The electromagnetic response measured by the helicopter system is a function of the "electrical" and "geometrical" properties of the conductor. The "electrical" property of a conductor is determined largely by its conductivity and its size and shape; the "geometrical" property of the response is largely a function of the conductors shape and orientation with respect to the measuring transmitter and receiver.

#### Electrical Considerations

For a given conductive body the measure of its conductivity or conductance is closely related to the measured phase shift between the received and transmitted electromagnetic field. A small phase shift indicates a relatively high conductance, a large phase shift lower conductance. A small phase shift results in a large in-phase to quadrature

ratio and a large phase shift a low ratio. This relationship is shown quantitatively for a vertical half-plane model on the accompanying phasor diagram. Other physical models will show the same trend but different quantitative relationships.

The phasor diagram for the vertical half-plane model, as presented, is for the coaxial coil configuration with the amplitudes in ppm as measured at the response peak over the conductor. To assist the interpretation of the survey results the computer is used to identify the apparent conductance and depth at selected anomalies. The results of this calculation are presented in table form in Appendix I and the conductance and in-phase amplitude are presented in symbolized form on the map presentation.

The conductance and depth values as presented are correct only as far as the model approximates the real geological situation. The actual geological source may be of limited length, have significant dip, its conductivity and thickness may vary with depth and/or strike and adjacent bodies and overburden may have modified the response. In general the conductance estimate is less affected by these limitations than the depth estimate but both should be considered a relative rather than absolute guide to the anomalies properties.

Conductance in mhos is the reciprocal of resistance in ohms and in the case of narrow slab like bodies is the product of electrical conductivity and thickness.

Most overburden will have an indicated conductance of less than 2 mhos; however, more conductive clays may have an apparent conductance of say 2 to 4 mhos. Also in the low conductance range will be electrolytic conductors in faults and shears.

The higher ranges of conductance, greater than 4 mhos, indicate that a significant fraction of the electrical conduction is electronic rather than electrolytic in nature. Materials that conduct electronically are limited to certain metallic sulphides and to graphite. High conductance anomalies, roughly 10 mhos or greater are generally limited to sulphide or graphite bearing rocks.

Sulphide minerals with the exception of sphalerite, cinnabar and stibnite are good conductors; however, they may occur in a disseminated manner that inhibits electrical conduction through the rock mass. In this case the apparent conductance can seriously under rate the quality of the conductor in geological terms. In a similar sense the relatively non-conducting sulphide minerals noted above may be present in significant concentration in association with minor conductive

sulphides, and the electromagnetic response only relate to the minor associate mineralization. Indicated conductance is also of little direct significance for the identification of gold mineralization. Although gold is highly conductive it would not be expected to exist in sufficient quantity to create a recognizable anomaly but minor accessory sulphide mineralization could provide a useful indirect indication.

In summary the estimated conductance of a conductor can provide a relatively positive identification of significant sulphide or graphite mineralization; however, a moderate to low conductance value does not rule out the possibility of significant economic mineralization.

#### Geometrical Considerations

Geometrical information about the geologic conductor can often be interpreted from the profile shape of the anomaly. The change in shape is primarily related to the change in inductive coupling among the transmitter, the target, and the receiver.

In the case of a thin, steeply dipping, sheet-like conductor, the coaxial coil pair will yield a near symmetric peak over the conductor. On the other hand the coplanar coil pair will pass through a null couple relationship and yield a minimum over the conductor, flanked by positive side lobes. As the dip of the conductor decreases from vertical, the coaxial

anomaly shape changes only slightly, but in the case of the coplanar coil pair the side lobe on the down dip side strengthens relative to that on the up dip side.

As the thickness of the conductor increases, induced current flow across the thickness of the conductor becomes relatively significant and complete null coupling with the coplanar coils is no longer possible. As a result, the apparent minimum of the coplanar response over the conductor diminishes with increasing thickness, and in the limiting case of a fully 3 dimensional body or a horizontal layer or half-space, the minimum disappears completely.

A horizontal conducting layer such as overburden will produce a response in the coaxial and coplanar coils that is a function of altitude (and conductivity if not uniform). The profile shape will be similar in both coil configurations with an amplitude ratio (coplanar/coaxial) of about 4/1.\*

In the case of a spherical conductor, the induced currents are confined to the volume of the sphere, but not relatively restricted to any arbitrary plane as in the case of a sheet-like form. The response of the coplanar coil pair directly over the sphere may be up to 8\* times greater than that of the coaxial coil pair.



In summary a steeply dipping, sheet-like conductor will display a decrease in the coplanar response coincident with the peak of the coaxial response. The relative strength of this coplanar null is related inversely to the thickness of the conductor; a pronounced null indicates a relatively thin conductor. The dip of such a conductor can be inferred from the relative amplitudes of the side-lobes.

Massive conductors that could be approximated by a conducting sphere will display a simple single peak profile form on both coaxial and coplanar coils, with a ratio between the coplanar to coaxial response amplitudes as high as 8.\*

Overburden anomalies often produce broad poorly defined anomaly profiles. In most cases the response of the coplanar coils closely follow that of the coaxial coils with a relative amplitude ratio of 4.\*

Occasionally if the edge of an overburden zone is sharply defined with some significant depth extent, an edge effect will occur in the coaxial coils. In the case of a horizontal conductive ring or ribbon, the coaxial response will consist of two peaks, one over each edge; whereas the coplanar coil will yield a single peak.

\* It should be noted at this point that Aerodat's definition of the measured ppm unit is related to the primary field sensed in the receiving coil without normalization to the maximum coupled (coaxial configuration). If such normalization were applied to the Aerodat units, the amplitude of the coplanar coil pair would be halved.

Magnetics

The Total Field Magnetic Map shows contours of the total magnetic field, uncorrected for regional variation. Whether an EM anomaly with a magnetic correlation is more likely to be caused by a sulphide deposit than one without depends on the type of mineralization.

An apparent coincidence between an EM and a magnetic anomaly may be caused by a conductor which is also magnetic, or by a conductor which lies in close proximity to a magnetic body. The majority of conductors which are also magnetic are sulphides containing pyrrhotite and/or magnetite. Conductive and magnetic bodies in close association can be, and often are, graphite and magnetite. It is often very difficult to distinguish between these cases. If the conductor is also magnetic, it will usually produce an EM anomaly whose general pattern resembles that of the magnetics. Depending on the magnetic permeability of the conducting body, the amplitude of the inphase EM anomaly will be weakened, and if the conductivity is also weak, the inphase EM anomaly may even be reversed in sign.

VLF Electromagnetics

The VLF-EM method employs the radiation from powerful military radio transmitters as the primary signals. The magnetic field associated with the primary field is elliptically polarized in the vicinity of electrical conductors. The Herz Totem uses three coils in the X. Y. Z. configuration to measure the total field and vertical quadrature component of the polarization ellipse.

The relatively high frequency of VLF 15-25 KHz provides high response factors for bodies of low conductance. Relatively "disconnected" sulphide ores have been found to produce measurable VLF signals. For the same reason, poor conductors such as sheared contacts, breccia zones, narrow faults, alteration zones and porous flow tops normally produce VLF anomalies. The method can therefore be used effectively for geological mapping. The only relative disadvantage of the method lies in its sensitivity to conductive overburden. In conductive ground the depth of exploration is severely limited.

The effect of strike direction is important in the sense of the relation of the conductor axis relative to the energizing electromagnetic field. A conductor aligned along a radius drawn from a transmitting station will be

in a maximum coupled orientation and thereby produce a stronger response than a similar conductor at a different strike angle. Theoretically it would be possible for a conductor, oriented tangentially to the transmitter to produce no signal. The most obvious effect of the strike angle consideration is that conductors favourably oriented with respect to the transmitter location and also near perpendicular to the flight direction are most clearly rendered and usually dominate the map presentation.

The total field response is an indicator of the existence and position of a conductivity anomaly. The response will be a maximum over the conductor, without any special filtering, and strongly favour the upper edge of the conductor even in the case of a relatively shallow dip.

The vertical quadrature component over steeply dipping sheet like conductor will be a cross-over type response with the cross-over closely associated with the upper edge of the conductor.

The response is a cross-over type due to the fact that it is the vertical rather than total field quadrature component that is measured. The response shape is due largely to geometrical rather than conductivity considerations and the distance between the maximum and minimum on either side of the cross-over is related to target depth. For a given target geometry, the larger this distance the greater the

depth.

The amplitude of the quadrature response, as opposed to shape is function of target conductance and depth as well as the conductivity of the overburden and host rock. As the primary field travels down to the conductor through conductive material it is both attenuated and phase shifted in a negative sense. The secondary field produced by this altered field at the target also has an associated phase shift. This phase shift is positive and is larger for relatively poor conductors. This secondary field is attenuated and phase shifted in a negative sense during return travel to the surface. The net effect of these 3 phase shifts determine the phase of the secondary field sensed at the receiver.

A relatively poor conductor in resistive ground will yield a net positive phase shift. A relatively good conductor in more conductive ground will yield a net negative phase shift. A combination is possible whereby the net phase shift is zero and the response is purely in-phase with no quadrature component.

A net positive phase shift combined with the geometrical cross-over shape will lead to a positive quadrature response on the side of approach and a negative on the side of departure. A net negative phase shift would produce the reverse. A further sign reversal occurs with a 180 degree

change in instrument orientation as occurs on reciprocal line headings. During digital processing of the quadrature data for map presentation this is corrected for by normalizing the sign to one of the flight line headings.







SELF POTENTIAL

Instrument \_\_\_\_\_ Range \_\_\_\_\_

Survey Method \_\_\_\_\_

Corrections made \_\_\_\_\_

RADIOMETRIC

Instrument \_\_\_\_\_

Values measured \_\_\_\_\_

Energy windows (levels) \_\_\_\_\_

Height of instrument \_\_\_\_\_ Background Count \_\_\_\_\_

Size of detector \_\_\_\_\_

Overburden \_\_\_\_\_  
(type, depth - include outcrop map)

OTHERS (SEISMIC, DRILL WELL LOGGING ETC.)

Type of survey \_\_\_\_\_

Instrument \_\_\_\_\_

Accuracy \_\_\_\_\_

Parameters measured \_\_\_\_\_

Additional information (for understanding results) \_\_\_\_\_

AIRBORNE SURVEYS

Type of survey(s) MAGNETIC EM VLF

Instrument(s) GEOMETRICS G-803 AERODAT 2EBER TOTEM 2A  
(specify for each type of survey)

Accuracy 0.5 GAMMAS 1 PPM 1% (1MM)  
(specify for each type of survey)

Aircraft used AERO SPATIAL - A-STAR HELICOPTER

Sensor altitude 150' 100' 150'

Navigation and flight path recovery method VISUAL NAVIGATION - MANUAL AND  
AUTOMATIC FIDUCIALS - ON BOARD CAMERA

Aircraft altitude 200' Line Spacing 660'

Miles flown over total area 486 Over claims only 63



Ministry of  
Natural  
Resources  
Ontario

Report of Work  
(Geophysical, Geological,  
Geochemical and Expenditures)

#154-83.

2.6068

The Mining Act

Instructions: - Please type or print.  
- If number of mining claims traversed exceeds space on this form, attach a list.  
Note: - Only days credits calculated in the "Expenditures" section may be entered in the "Expend. Days Cr." columns.  
- Do not use shaded areas below.

Jul 78

Type of Survey(s) **ELECTROMAGNETIC, MAGNETIC, VLF-EM** Township or Area **NAME 16DS**  
 Claim Holder(s) **SAXTON INDUSTRIES LTD.** Prospector's Licence No. **T 1341**  
 Address **4800 DUFFERIN ST. DOWNSVIEW ONTARIO**  
 Survey Company **AERODAT LIMITED** Date of Survey (from & to) **25 3 83 26 3 83** Total Miles of line Cut **63**  
 Name and Address of Author (of Geo-Technical report) **FENTON SCOTT 17 MALABAR PLACE DON MILLS ONTARIO**

Credits Requested per Each Claim in Columns at right

Mining Claims Traversed (List in numerical sequence)

Special Provisions	Geophysical	Days per Claim
For first survey: Enter 40 days. (This includes line cutting)	- Electromagnetic	
	- Magnetometer	
	- Radiometric	
	- Other	
For each additional survey: using the same grid: Enter 20 days (for each)	Geological	
	Geochemical	
Man Days Complete reverse side and enter total(s) here	Geophysical	Days per Claim
	- Electromagnetic	
	- Magnetometer	
	- Radiometric	
Airborne Credits Note: Special provisions credits do not apply to Airborne Surveys.	Electromagnetic	25.2
	Magnetometer	25.2
	VLF Radiometric	25.2

Mining Claim		Expend. Days Cr.	Mining Claim		Expend. Days Cr.
Prefix	Number		Prefix	Number	
SSM	684 100		SSM	684 123	
	01			24	
	02			25	
	03			26	
	04			27	
	05			28	
	06			29	
	07			30	
	08			31	
	09			32	
	10			33	
	11			34	
	12			35	
	13			36	
	14			37	
	15			38	
	16			39	
	17			40	
	18			41	
	19			684 294	
	20			95	
	21			96	
	22			97	

Expenditures (excludes power stripping)  
 Type of Work Performed **SAULT STE. MARIE MINING DIV.**  
 Performed on Claim(s) **RECEIVED**  
**DEC 9 1983**  
 A.M.  
 Calculation of Expenditure Days Credits  
 Total Expenditures \$  ÷ 15 =  Days Credits

Instructions  
 Total Days Credits may be apportioned at the claim holder's choice. Enter number of days credits per claim selected in columns at right.

Date **NOV 28/87** Recorded Holder or Agent (Signature) *[Signature]*

For Office Use Only  
 Total Days Cr. Recorded **7,560** Date Recorded **Nov. 9/83**  
 Mining Recorder *[Signature]*  
 Date Approved as Recorded **84.4.6** *[Signature]*

Certification Verifying Report of Work  
 I hereby certify that I have a personal and intimate knowledge of the facts set forth in the Report of Work annexed hereto, having performed the work or witnessed same during and/or after its completion and the annexed report is true.

Name and Postal Address of Person Certifying **FENTON SCOTT 17 MALABAR PLACE DON MILLS ONT**  
 Date Certified **NOV 27/87** Certified by (Signature) *[Signature]*

(SEE ATTACHED LIST)  
 Total number of mining claims covered by this report of work. **100**



Ministry of  
Natural  
Resources  
Ontario

Report of Work  
(Geophysical, Geological,  
Geochemical and Expenditures)

#154-83.

26068

The Mining Act

Instructions: - Please type or print.  
- If number of mining claims traversed exceeds space on this form, attach a list.  
Note: - Only days credits calculated in the "Expenditures" section may be entered in the "Expend. Days Cr." columns.  
- Do not use shaded areas below.

Jul 78

Type of Survey(s) **ELECTROMAGNETIC, MAGNETIC, VLF-EM** Township or Area **NAME 1605**  
 Claim Holder(s) **SAXTON INDUSTRIES LTD.** Proprietor's Licence No. **T 1341**  
 Address **4800 DUFFERIN ST. DOWNSVIEW ONTARIO**  
 Survey Company **AERODAY LIMITED** Date of Survey (from & to) **25 3 83 26 3 83** Total Miles of line Cut **63**  
 Name and Address of Author (of Geo-Technical report) **FENTON SCOTT 17 MALABAR PLACE DON MILLS ONTARIO**

Credits Requested per Each Claim in Columns at right Mining Claims Traversed (List in numerical sequence)

Special Provisions	Geophysical	Days per Claim
For first survey: Enter 40 days. (This includes line cutting)	- Electromagnetic	
	- Magnetometer	
For each additional survey: using the same grid: Enter 20 days (for each)	- Radiometric	
	- Other	
	Geological	
	Geochemical	
Man Days	Geophysical	Days per Claim
Complete reverse side and enter total(s) there	- Electromagnetic	
	- Magnetometer	
	- Radiometric	
	- Other	
	Geological	
	Geochemical	
Airborne Credits		Days per Claim
Note: Special provisions credits do not apply to Airborne Surveys.	Electromagnetic	25.2
	Magnetometer	25.2
	VLF	25.2
	Geometric	25.2

Mining Claim			Mining Claim		
Prefix	Number	Expend. Days Cr.	Prefix	Number	Expend. Days Cr.
SSM	684 100		SSM	684 123	
	01			24	
	02			25	
	03			26	
	04			27	
	05			28	
	06			29	
	07			30	
	08			31	
	09			32	
	10			33	
	11			34	
	12			35	
	13			36	
	14			37	
	15			38	
	16			39	
	17			40	
	18			41	
	19			684 294	
	20			95	
	21			96	
	22			97	

Expenditures (excludes power stripping)

Type of Work Performed **BAULY STE. MARIE MINING DIV.**

Performed on Claim(s) **RECEIVED**

Calculation of Expenditure Days Credits **DEC 9 1983**

Total Expenditures \$  + 15 =  Days Credits

(See attached list)  
Total number of mining claims covered by this report of work. **100**

Instructions  
Total Days Credits may be apportioned at the claim holder's choice. Enter number of days credits per claim selected in columns at right.

For Office Use Only

Total Days Cr. Recorded **7,560** Date Recorded **Aug. 9/83** Mining Recorder **[Signature]**

Date Approved as Recorded **87.4.6** Director **[Signature]**

Date **NOV 22/87** Recorded Holder or Agent (Signature) **[Signature]**

Certification Verifying Report of Work  
I hereby certify that I have a personal and intimate knowledge of the facts set forth in the Report of Work annexed hereto, having performed the work or witnessed same during and/or after its completion and the annexed report is true.

Name and Postal Address of Person Certifying **FENTON SCOTT 17 MALABAR PLACE, DON MILLS, ONT**

Date Certified **NOV. 27/85** Certified by (Signature) **[Signature]**



Ministry of  
Natural  
Resources

**Report of Work**  
(Geophysical, Geological,  
Geochemical and Expenditures)

- Instructions: - Please type or print.  
- If number of mining claims traversed exceeds space on this form, attach a list.  
Note: - Only days credits calculated in the "Expenditures" section may be entered in the "Expend. Days Cr." columns.  
- Do not use shaded areas below.

**The Mining Act**

Type of Survey(s)		Township or Area	
Claim Holder(s)		Prospector's Licence No.	
Address			
Survey Company		Date of Survey (from & to)	Total Miles of line Cut
		Day   Mo.   Yr.	Day   Mo.   Yr.
Name and Address of Author (of Geo-Technical report)			

**Credits Requested per Each Claim in Columns at right**

Special Provisions	Geophysical	Days per Claim
For first survey: Enter 40 days. (This includes line cutting)	- Electromagnetic	
	- Magnetometer	
	- Radiometric	
	- Other	
For each additional survey: using the same grid: Enter 20 days (for each)	Geological	
	Geochemical	
Man Days  Complete reverse side and enter total(s) here	Geophysical	Days per Claim
	- Electromagnetic	
	- Magnetometer	
	- Radiometric	
	- Other	
Airborne Credits  Note: Special provisions credits do not apply to Airborne Surveys.	Geological	
	Geochemical	
Electromagnetic	Days per Claim	
	Magnetometer	
	Radiometric	

**Mining Claims Traversed (List in numerical sequence)**

Mining Claim		Expend. Days Cr.	Mining Claim		Tend. # Cr.
Prefix	Number		Prefix	Number	
SSM	684 298		SSM	684 322	
	99			24	
	684 300			25	
	01			26	
	02			27	
	03			28	
	04			29	
	05			30	
	06			31	
	07			32	
	08			33	
	09			36	
	10			37	
	11			38	
	12			39	
	13			40	
	14			41	
	15		688	140	
	16			41	
	17			44	
	18			45	
	19			47	
	20			48	

RECEIVED

MINING LANDS SECTION

SAULT STE. MARIE MINING DIV.

RECEIVED

DEC 9 1983

A.M. 7:18:10

Expenditures (excludes power stripping)	
Type of Work Performed	
Performed on Claim(s)	

Calculation of Expenditure Days Credits	
Total Expenditures	Total Days Credits
\$	÷ 15 =

Instructions  
Total Days Credits may be apportioned at the claim holder's choice. Enter number of days credits per claim selected in columns at right.

Date	Recorded Holder or Agent (Signature)
------	--------------------------------------

For Office Use Only		
Total Days Cr. Recorded	Date Recorded	Mining Recorder
	Date Approved as Recorded	Branch Director

**Certification Verifying Report of Work**

I hereby certify that I have a personal and intimate knowledge of the facts set forth in the Report of Work annexed hereto, having performed the work or witnessed same during and/or after its completion and the annexed report is true.

Name and Postal Address of Person Certifying

Date Certified	Certified by (Signature)
----------------	--------------------------



1983 12 08

2.6068

Mrs. M.V. St. Jules  
Mining Recorder  
Ministry of Natural Resources  
875 Queen Street East  
P.O. Box 669  
Sault Ste. Marie, Ontario  
P6A 5N2

Dear Madam:

We have received reports and maps for an Airborne Geophysical (Electromagnetic, Magnetometer and V.L.F.) survey submitted on mining claims SSM 684100 et al in the Township of Nameigos.

This material will be examined and assessed and a statement of assessment work credits will be issued.

We do not have a copy of the report of work which is normally filed with you prior to the submission of this technical data. Please forward a copy as soon as possible.

Yours very truly,

E.F. Anderson  
Director  
Land Management Branch

Whitney Block, Room 6643  
Queen's Park  
Toronto, Ontario  
M7A 1W3  
Phone: (416)965-1380

A. Barr:mc

cc: Saxton Industries  
4800 Dufferin Street  
Downsview, Ontario  
M3H 5T3

cc: Fenton Scott  
17 Malabar Place  
Don Mills, Ontario  
M3B 1A4



Mining Lands Comments


To: Geophysics *Mr. R. Barlow*

Comments

*- May a VLF-EM maps need legend*

Approved

Wish to see again with corrections

Date

*Jan 21 84*

Signature

*R Barlow*

To: Geology - Expenditures

Comments

Approved

Wish to see again with corrections

Date

Signature

To: Geochemistry

Comments

*L.D.*

Approved

Wish to see again with corrections

Date

Signature

To: Mining Lands Section, Room 6462, Whitney Block.

(Tel: 5-1380)



February 28, 1984.

Saxton Industries  
4800 Dufferin Street  
Downsview, Ontario  
M3H 5T3

Dear Sirs:

RE: Airborne Geophysical (Electromagnetic, Magnetometer and  
V.L.F) survey submitted on mining claims SSM 684100  
et al in the Township of Nameigos.

Enclosed are the V.L.F and Magnetometer plans, in duplicate,  
for the above-mentioned survey. Please have the author of the  
report include a legend on each map detailing units measured  
and return all maps to this office as soon as possible.

For further information, please contact Mr. F.W. Matthews at  
(416) 965-1380.

Yours very truly,

J.R. Morton  
Acting Director  
Land Management Branch

Whitney Block, Room 6643  
Queen's Park  
Toronto, Ontario  
M7A 1W3  
Phone: 416/965-1380

M.E. Anderson:dg

cc: Fenton Scott  
17 Malabar Place  
Don Mills, Ontario  
M3B 1A4

cc: Mining Recorder  
Bault Ste. Marie, Ontario



Mining Lands Comments

*You wanted to see this file again.*

To: Geophysics

*Mr. Barlow.*

Comments

Approved

Wish to see again with corrections

Date

*March 19/89*

Signature

*R. Barlow*

To: Geology - Expenditures

Comments

Approved

Wish to see again with corrections

Date

Signature

To: Geochemistry

Comments

*L.D.*

Approved

Wish to see again with corrections

Date

Signature

To: Mining Lands Section, Room 6462, Whitney Block.

(Tel: 5-1380)

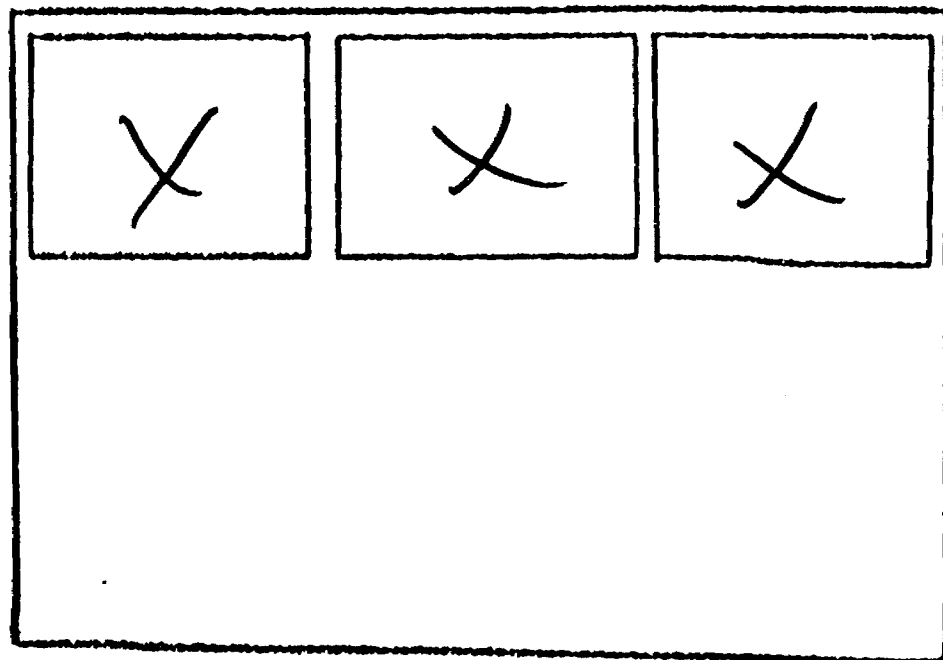
SEE ACCOMPANYING  
MAP(S) IDENTIFIED AS

NAMEIGOS - 0015 #1

2

3

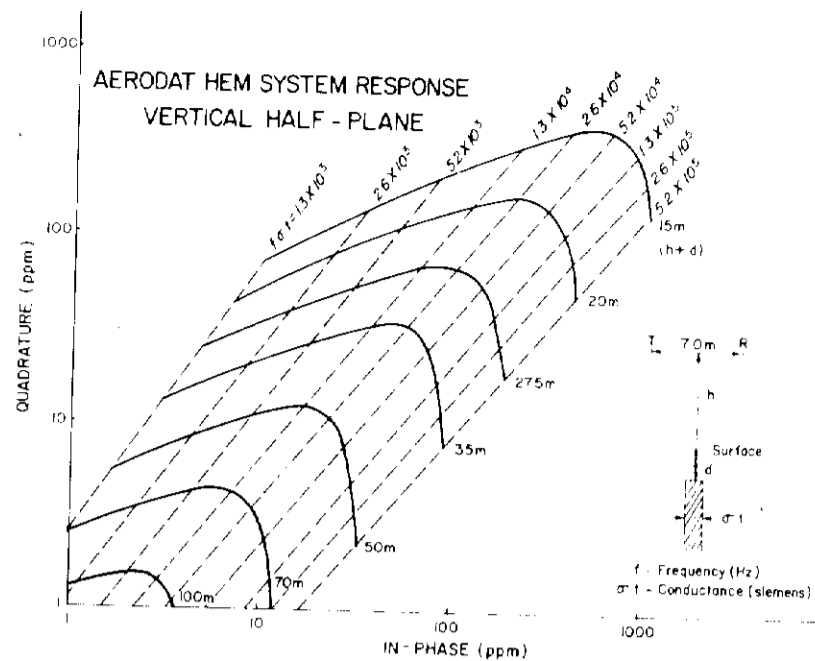
LOCATED IN THE MAP  
CHANNEL IN THE FOLLOWING  
SEQUENCE (X)



Horizontal control ..... based on photo laydown

Average bird height ..... 30 metres

Line spacing ..... 660 feet



**EM RESPONSE**

Conductivity thickness in mhos

- ⊙ > 500
- ⊙ 250 - 500
- ⊙ 125 - 250
- ⊙ 60 - 125
- ⊙ 30 - 60
- ⊙ 15 - 30
- ⊙ 8 - 15
- ⊙ 4 - 8
- ⊙ 2 - 4
- < 2
- 25 Inphase response

PROSPECTING GEOPHYSICS LTD.

**AIRBORNE ELECTROMAGNETIC SURVEY**

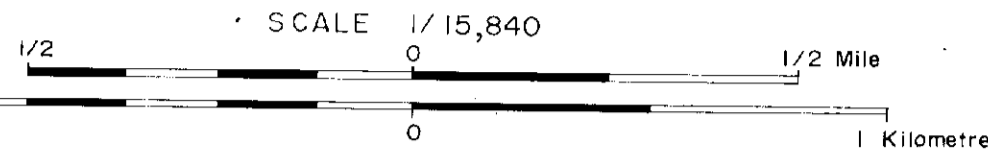
**PROFILES**

**SAXTON INDUSTRIES LTD:**

**HORNEPAYNE AREA**

ONTARIO

*Antas*

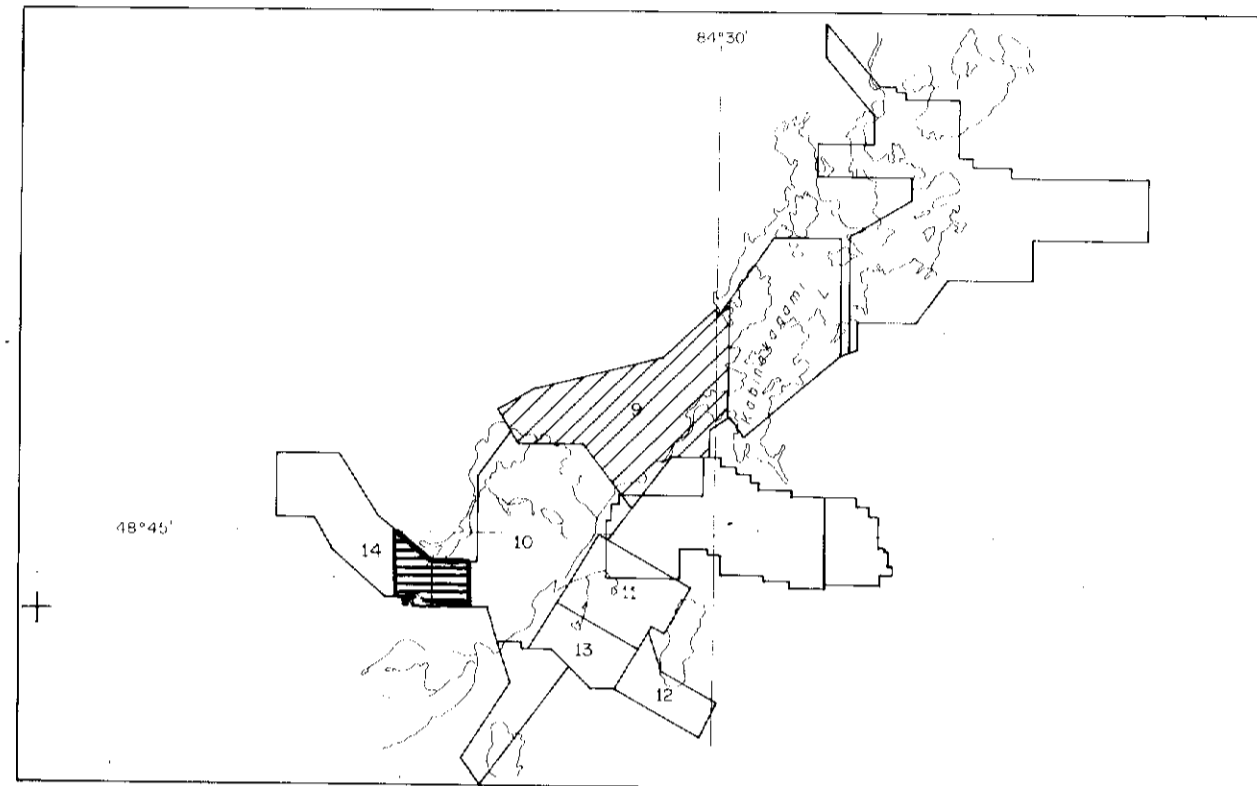


**AERODAT LIMITED**

DATE: March 1983

N.T.S. No: 42C, 42F

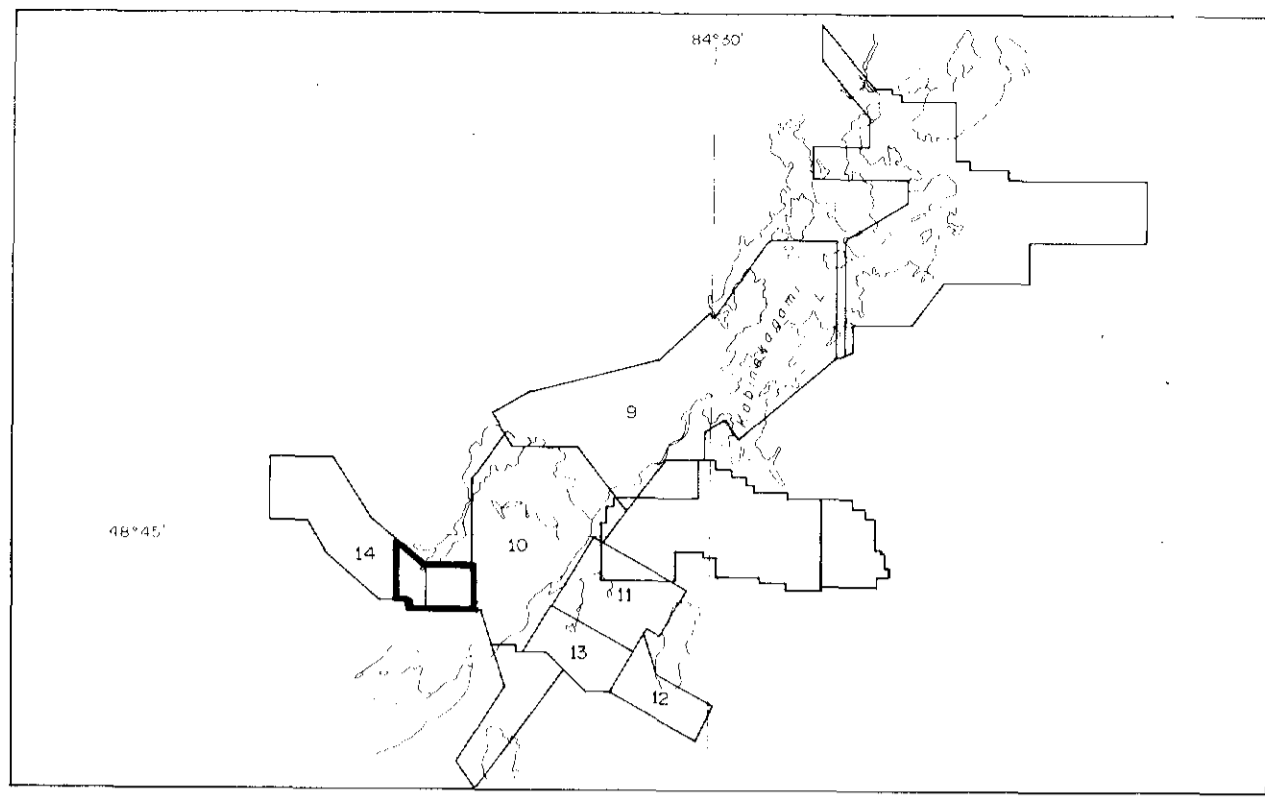
MAP No: 1



NAMEIGOS-0015 #1



42C10NW0001 NAMEIGOS0015 NAMEIGOS



2

PROSPECTING GEOPHYSICS LTD.

**TOTAL FIELD MAGNETIC MAP**  
**SAXTON INDUSTRIES LTD.**  
 HORNEPAYNE AREA  
 ONTARIO *John D. N.*

SCALE 1/15,840  
 1/2 Mile  
 1 Kilometre

<b>AERODAT LIMITED</b>	DATE: March 1983
	N.T.S. No: 42C, 42F
	MAP No:

**LEGEND**

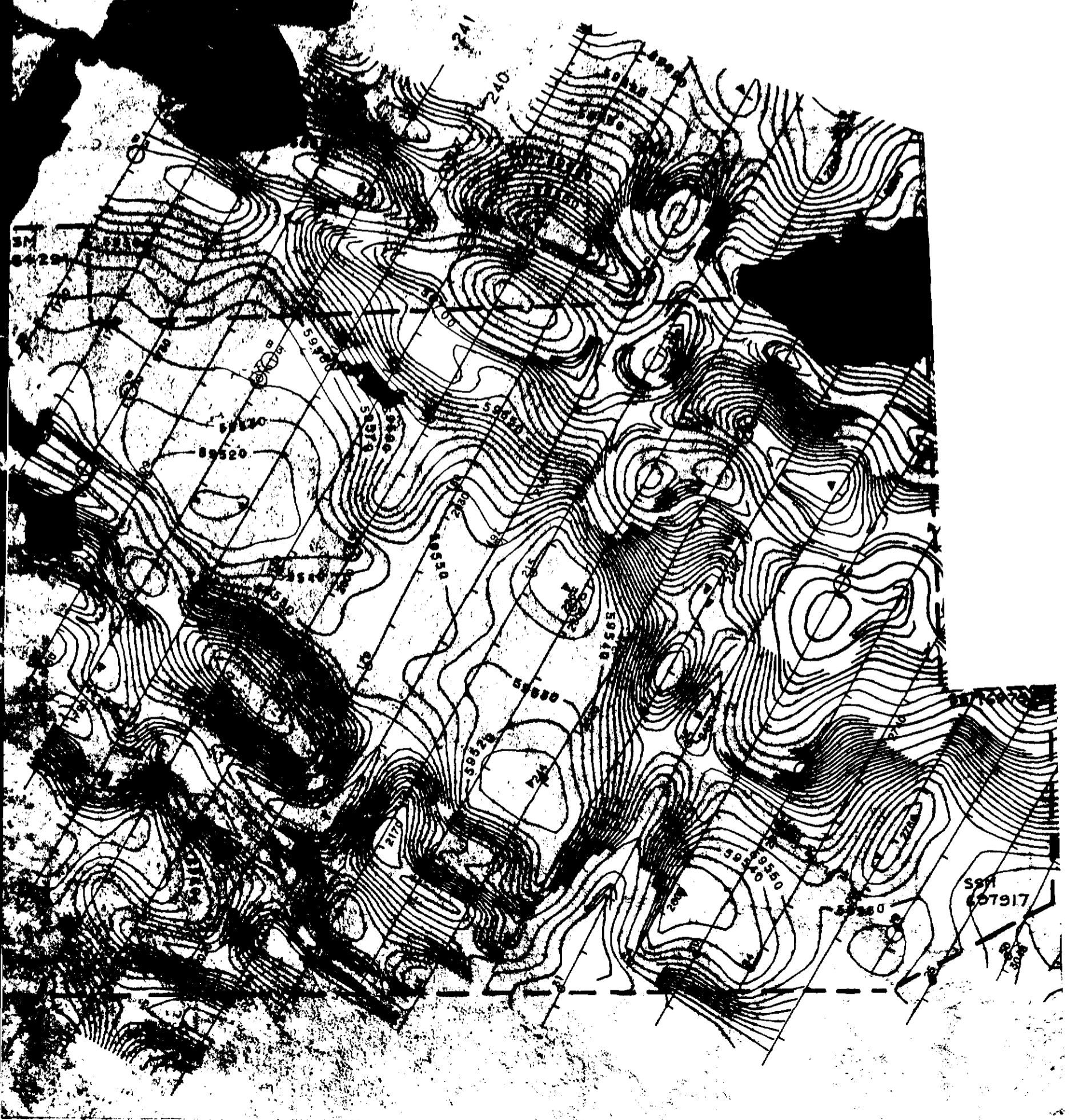
250 gammas

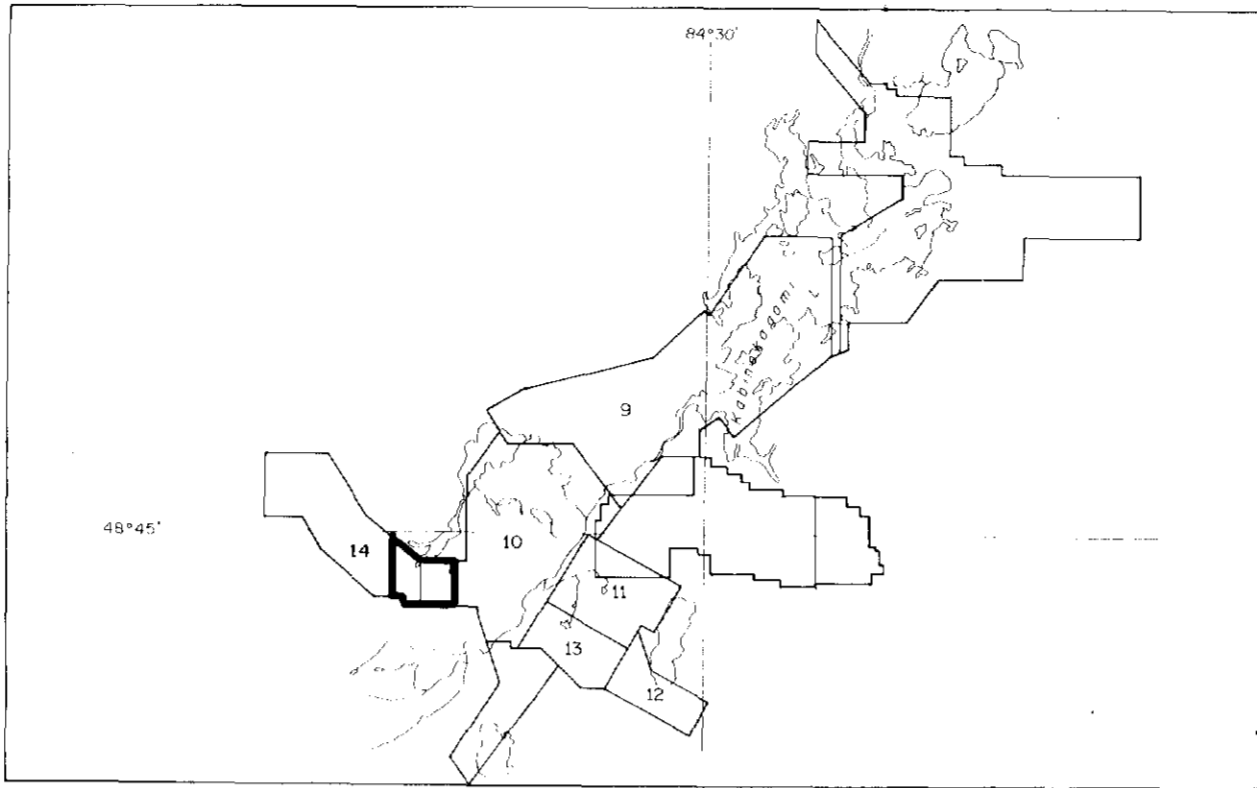
50 gammas

10 gammas



*NAME 1GOS-0015 #2*





**LEGEND**

50%   
 10%   
 2% 

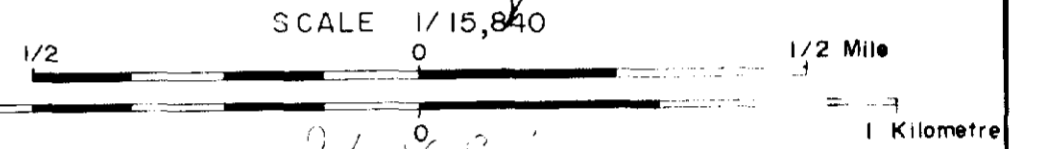
PROSPECTING GEOPHYSICS LTD.

VLF-EM NAA CUTLER 178 khz  
 SAXTON INDUSTRIES LTD.

HORNEPAYNE AREA

ONTARIO

*John Satt*



DATE: March 1983

**AERODAT LIMITED**

N.T.S. No: 42C, 42F

MAP No: 3



NAMEIGOS-0015 #3