Airborne Geophysical Survey

Lizar Property (Claim 1246624)

Lizar Township

Sault Ste Marie Mining Division

Hornepayne Area, Ontario

2.25102

Jari Paakki, MSc., PGeo

March 01, 2003
Thunder Bay, Ontario

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Hornepayne Area, Ontario

Introduction

At the request of Teck Cominco Limited, Fugro Airborne Systems conducted an airborne electromagnetic and magnetic survey over the Lizar property. The total survey consisted of 1,503 line kilometres with 40.7 line kilometres covering claim SSM 1246624 which is presented in this report.

Claim 1246624 is part of the Lizar property which is located some 100 kilometres east of the Hemlo mines, approximately 40 kilometres south of the town of Hornepayne (Fig. 1). Access to the property is via a network of logging roads south of Hornepayne, east from Highway 631.

Freewest Resources Canada Inc. is the recorded holder of claim 1246624 which Teck Cominco Limited has an option agreement. The claim consists of 15 units located in the central part of Lizar Township near Kabinakagami Lake (Fig. 2). The centre of the claim is at approximately UTM 685,300 mE and 5,419,200 mN (NAD 83, Zone 16).

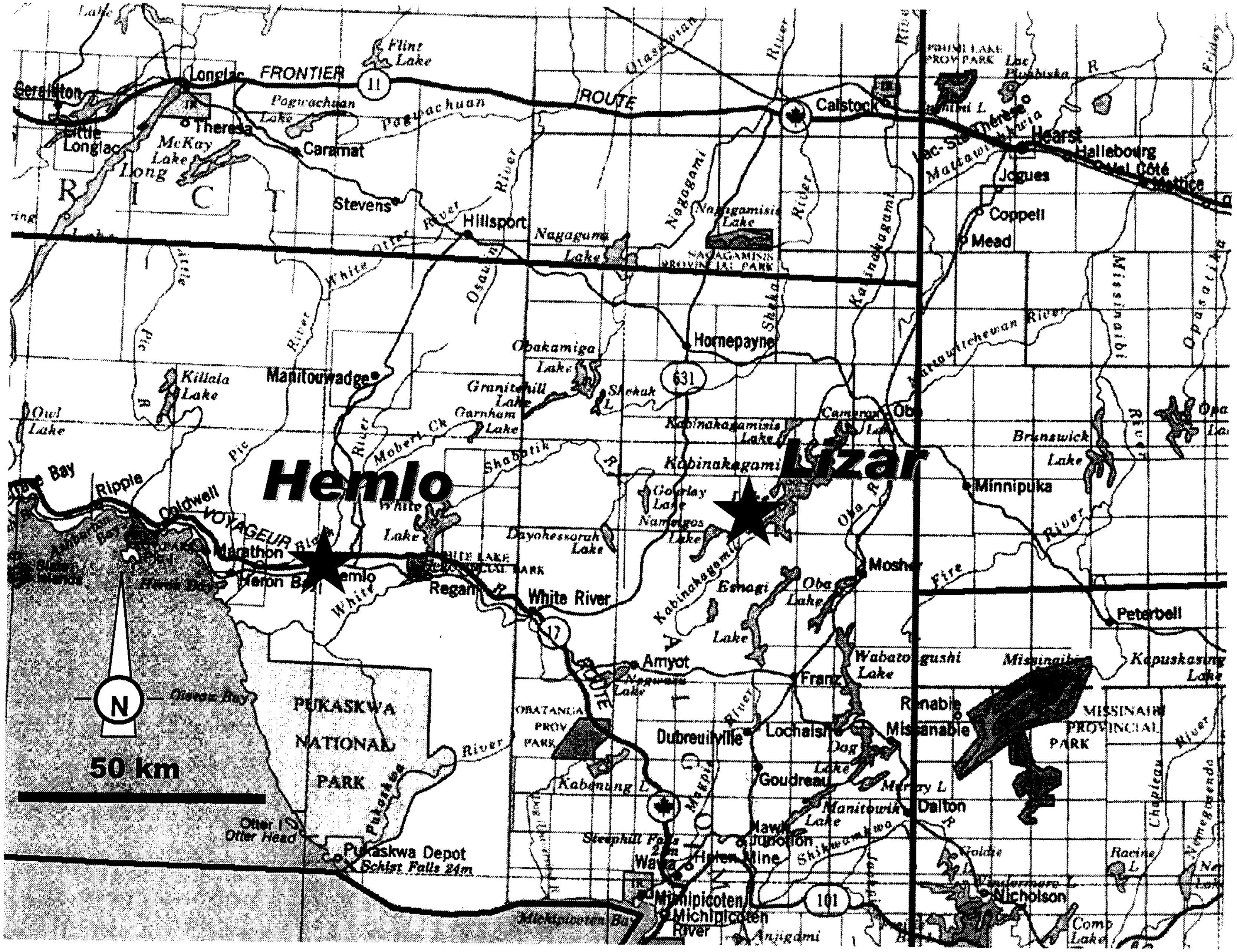

Figure 1: Location Map

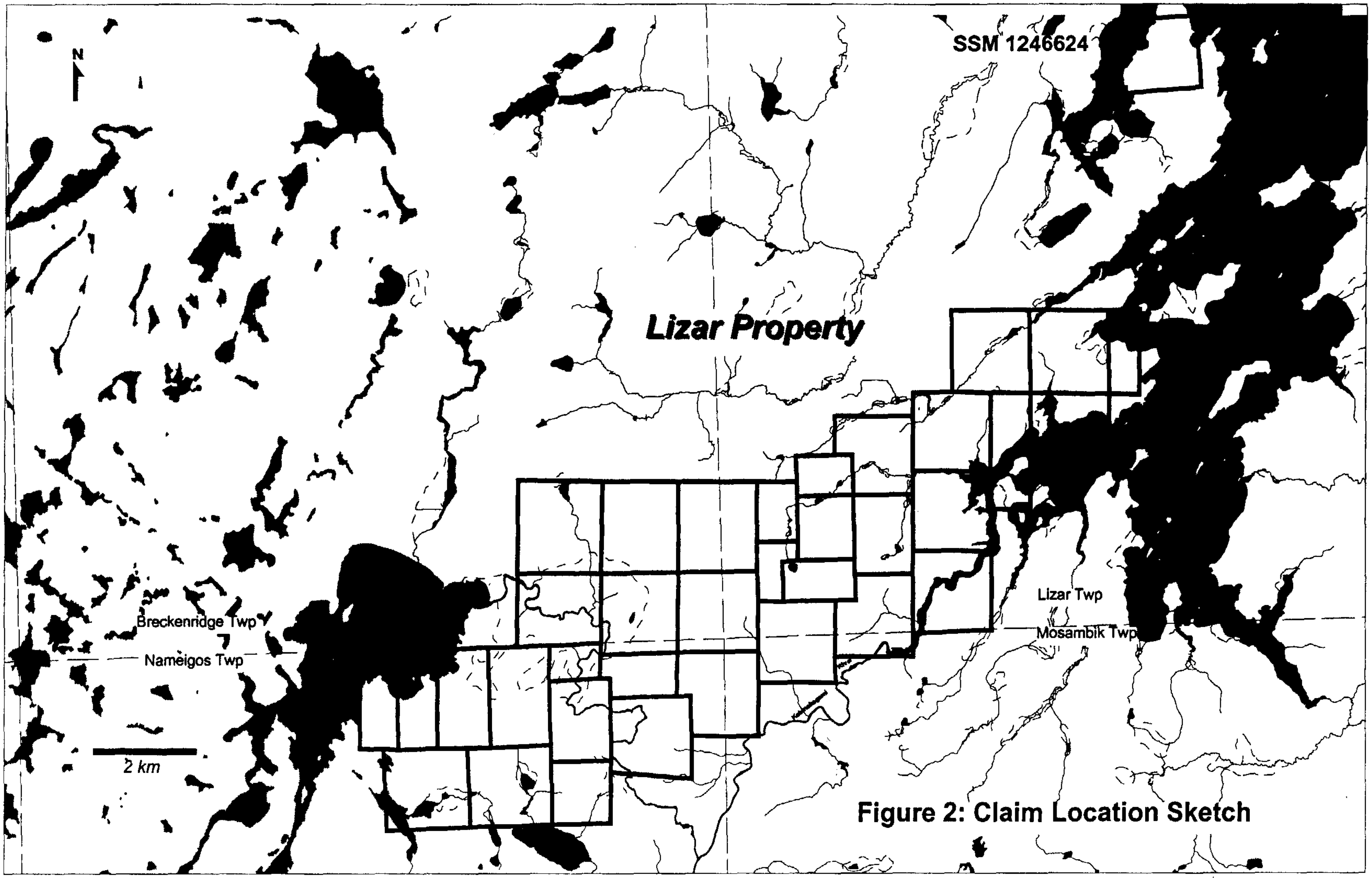

Figure 2: Claim Location Sketch

Geophysical Survey

From October 12 to October 23, 2002, an airborne electromagnetic and magnetic survey was completed on the Lizar Property. The survey was conducted by Fugro Airborne Surveys, 2060 Walkley Road, Ottawa, Ontario. The survey was designed to cover the entire property including claim 1246624 located to the northeast of the main block of claims. The Lizar property is underlain by mainly upper greenschist facies mafic volcanics and lesser sedimentary rocks, felsic lithologies and local gabbroic to ultramafic intrusions. Outcrop exposure is relatively poor comprising less than 1-2% in many parts of the property.

The aircraft used for this survey was a specially modified Casa-212 aircraft equipped with a magnetometer and a new GEOTEM 1000 Receiver capable of deeper ground penetration. The complete aircraft and survey specifications are appended (Appendix I). Fight lines were oriented north-south spaced 100 metres apart. Each flight line was 8 kilometres in length which is the minimum required for this specific survey for proper coupling. West-east oriented flight tie lines were positioned at approximately 2 kilometre spacings as control lines.

Results of the survey covering claim 1246624 are presented in Figures 3 and 4. Figure 3 shows flight lines with posted magnetic readings (in nT, nanotesla) along with contours of these values at a scale of 1:5 000. In Figure 4, also at a scale of 1:5 000, electromagnetic data is presented as posted values, profiles and anomaly picks.

Results of the survey over claim 1246624 indicate the presence of a larger magnetic high anomaly in the south central portion of the claim (see Fig. 4) This anomaly corresponds to an area where a gabbroic to ultramafic intrusion has been mapped. No significant electromagnetic anomalies are outlined.

Cost Statement

Airborne Magnetics and Electromagnetics Survey	$3,582
Plotting/Processing Data	$ 200
Aircraft Mobilization/Demobilization (pro rata)	$1,246
Aircraft Stand-By Due To Poor Weather (pro rata)	$ 278
TOTAL	**$5,306**

Statement of Qualifications

I, Jari Paakki, do certify that:

I am a registered Geoscientist (No. 0230) with the Association of Geoscientists of Ontario.

I graduated from Laurentian University in 1990 with a Bachelor of Science Degree and in 1992 with a Master of Science Degree, both in Geology.

I have been employed as a geologist continuously for the last 10 years.

The data contained in this report and conclusions drawn from it are true and accurate to the best of my knowledge.

March 01, 2005
Date

Jari Paakki
Senior Project Geologist
Teck Cominco Limited
Thunder Bay, Ontario

Appendix I

Airborne System and Survey Specifications

II

SURVEY OPERATIONS

Survey Coverage and Location

The survey area (Figure 2) was flown from Hornepayne, Ontario used as the base of operations.

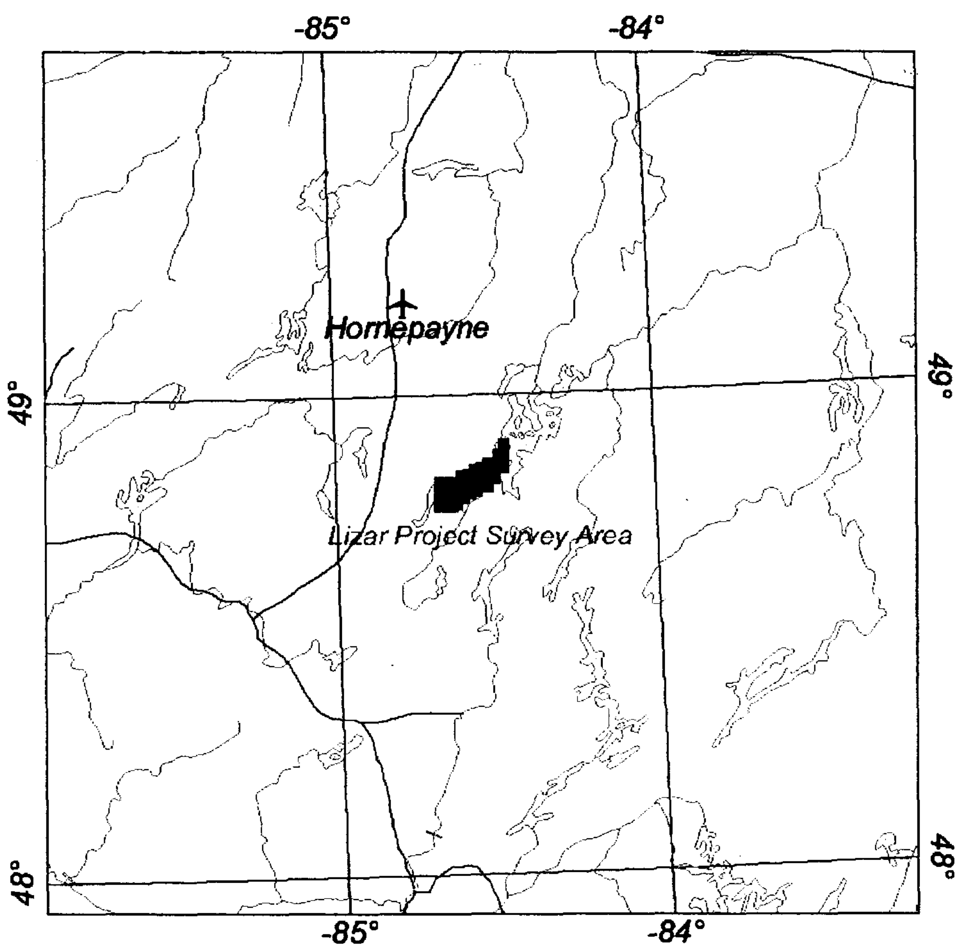

Figure 2. Survey Location.

Line direction, spacing, as well as size of the flown survey are shown in Table 1. In all, 1,503 line kilometres of data were collected.

Table 1

AREA	LINE DIRECTION	LINE SPACING	TIE-LINE DIRECTION	TIE-LINE SPACING	SIZE
Lizar Project	N-S	100 m	E-W	~ 2000 m	1,503 l km

Aircraft and Geophysical On-Board Equipment

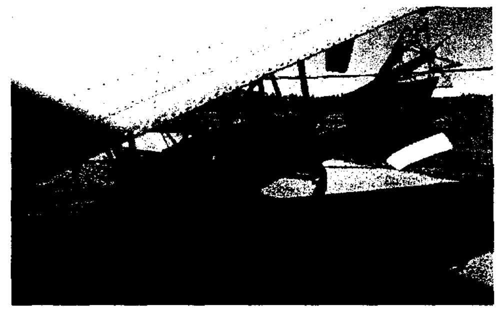

Figure 3. Magnetometer and GEOTEM® Receiver.

Aircraft	Casa-212 (Twin Turbo Propeller)
Operator	FUGRO AIRBORNE SURVEYS
Registration	C-GDPP
Survey speed	125 knots / 145 mph / 65 m/s
Magnetometer	Scintrex Cs-2 single cell cesium vapour, towed-bird installation, sensitivity = 0.01 nT[1], sampling rate = 0.1 s, ambient range 20,000 to 100,000 nT. The general noise envelope was kept below 0.5 nT. The nominal sensor height was ~73 m above ground.
Electromagnetic system	GEOTEM *1000*® 20 channel multicoil system
Transmitter:	Vertical axis loop mounted on aircraft of 231 m^2
	Number of turns: 6
	Nominal height above ground of 120 m
Receiver :	Multicoil system (X, Y and Z) with a final recording rate of 4 samples/second, for the recording of 20 channels of X, Y and Z-coil data. The nominal height above ground is ~70 m, placed ~130 m behind the centre of the transmitter loop.
Base frequency:	90 Hz
Pulse width:	2083 μs
Pulse delay:	130 μs
Off-time:	3385 μs
Point value:	43.4 μs
Transmitter current:	~500 A
Dipole moment:	~7 x $10^5 Am^2$

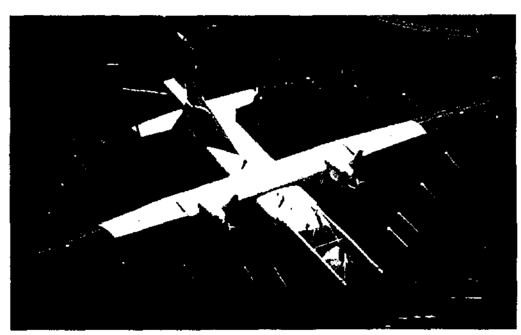

Figure 4. Modified CASA-212 on survey.

[1] One nanotesla (nT) is the S.I. equivalent of one gamma.

GEOTEM® 90 Hz frequency electromagnetic data windows:

Table 2

Channel	Start (p)	End (p)	Width (p)	Start (ms)	End (ms)	Mid (ms)
1	4	9	6	0.13	0. 391	0. 260
2	10	22	13	0. 391	0. 955	0. 673
3	23	36	14	0. 955	1.563	1.259
4	37	49	13	1.563	2.127	1.845
5	50	55	6	2.127	2.387	2.257
6	56	57	2	2.387	2.474	2.431
7	58	59	2	2.474	2.561	2.517
8	60	61	2	2.561	2.648	2.604
9	62	64	3	2.648	2.778	2.713
10	65	67	3	2.778	2.908	2.843
11	68	71	4	2.908	3.082	2.995
12	72	75	4	3.082	3.255	3.168
13	76	79	4	3.255	3.429	3.342
14	80	84	5	3.429	3.646	3.537
15	85	90	6	3.646	3.906	3.776
16	91	97	7	3.906	4.210	4.058
17	98	104	7	4.210	4.514	4.362
18	105	112	8	4.514	4.861	4.688
19	113	120	8	4.861	5.208	5.035
20	121	128	8	5.208	5.556	5.382

Digital Acquisition: FUGRO AIRBORNE SURVEYS GEODAS SYSTEM.

Analogue Recorder: RMS GR-33, showing the total magnetic field at 2 vertical scales, the radar and barometric altimeters, the time-constant filtered traces of dB/dt X-coil off-time channels 9-20 data and the on-time channel 1, the raw traces of both dB/dt and B-field X, Y and Z-coil channel 20, the EM X and Y-coils primary fields, the power line monitor, the 4th difference of the magnetics, the X-coil earth's field monitor and the fiducials.

Barometric Altimeter: Rosemount 1241M, sensitivity 1 ft, 1 s recording interval.

Radar Altimeter: King, accuracy 2%, sensitivity 1 ft, range 0 to 2500 ft, 1 sec recording interval.

Camera: Panasonic colour video, super VHS, model WV-CL302.

Electronic Navigation: NOVATEL Propak 4E-315R 12 channel GPS receiver, 1 sec recoding interval, with a resolution of 0.00001 degree and an accuracy of ±5 m.

Analogue recorder display setup:

Table 3

Name	Descirption	Scale	Unit
XF09	dB/dt X coil Time Filtered Channel 09	10000	pV/cm
XF10	dB/dt X coil Time Filtered Channel 10	10000	pV/cm
XF11	dB/dt X coil Time Filtered Channel 11	10000	pV/cm
XF12	dB/dt X coil Time Filtered Channel 12	10000	pV/cm
XF13	dB/dt X coil Time Filtered Channel 13	10000	pV/cm
XF14	dB/dt X coil Time Filtered Channel 14	10000	pV/cm
XF15	dB/dt X coil Time Filtered Channel 15	10000	pV/cm
XF16	dB/dt X coil Time Filtered Channel 16	10000	pV/cm
XF17	dB/dt X coil Time Filtered Channel 17	10000	pV/cm
XF18	dB/dt X coil Time Filtered Channel 18	10000	pV/cm
XF19	dB/dt X coil Time Filtered Channel 19	10000	pV/cm
XF20	dB/dt X coil Time Filtered Channel 20	10000	pV/cm
BZ20	B-Field Z coil Raw channel 20	80000	fT/cm
BX20	B-Field X coil Raw channel 20	80000	fT/cm
X20	dB/dt X coil Raw channel 20	20000	pV/cm
Z20	dB/dt X coil Raw channel 20	20000	pV/cm
X01	dB/dt X coil Raw channel 01	50000	pV/cm
XPL	Powerline Monitor	0.2	V/cm
XEFM	Earth Field Monitor	1	V/cm
XPRM	X Primary Field	0.4	V/cm
YPRM	Y Primary Field	13.3	V/cm
Y20	dB/dt Y coil Raw channel 20	20000	pV/cm
CMAG	Coarse Total Field Magnetics	300	nT/cm
FMAG	Fine Total Field Magnetics	100	nT/cm
RADR	Radar Altimieter	50	ft/cm
4DIF	Magnetic 4th Difference Filtered	1	nT/cm
BARO	Barometric Altimeter	100	ft/cm

Base Station Equipment

Magnetometer: Scintrex CS-2 single cell cesium vapour, mounted in a magnetically quiet area, measuring the total intensity of the earth's magnetic field in units of 0.01 nT at intervals of 1 s, within a noise envelope of 0.20 nT.

GPS Receiver: NOVATEL Propak 4E-315R 12 channel GPS receiver, 1 sec recoding interval, with a resolution of 0.00001 degree and an accuracy of ±5 m.

Computer: Laptop, Pentium II model, 220 Mhz.

Converter: Picodas, model MEP710 3/10901 GTS 780008.

Field Office Equipment

Computer:	Dell Inspiron 8000 Pentium III laptop with 30 GB hard drive.
Printer:	Hewlett Packard Deskjet 690C.
DAT Tape Drive:	DDS-90 4 mm.
Hard Drive:	8 GB Removable hard drive.

Survey Specifications

Traverse Line Direction:	See Table 1.
Traverse Line Spacing:	See Table 1.
Tie Line Direction:	See Table 1.
Tie Line Spacing:	See Table 1.
Navigation:	Differential GPS. Traverse and tie line deviation was not to exceed the theoretical flight path by 50 m over a distance >3 km.
Altitude:	The survey was flown at a mean terrain clearance of 120 m. Altitude was not to exceed 20 m from the nominal over 3 km.
Magnetic Noise Levels:	The noise envelope on the magnetic data was not to exceed ±0.25 nT over 3 km.
EM Noise Levels:	The noise envelope on the raw electromagnetic dB/dt X- and Z-coil channel 20 was not to exceed ±3500 pT/s over a distance greater than 3 km as displayed on the raw analogue traces.
Diurnal Variations:	Deviations were not to exceed 10 nT over a chord of 30 sec.

Survey Calibrations

EM System Calibration:	The EM system was calibrated at high altitude before and after every production flight. The effectiveness of the compensation was evaluated by checking the system response to the series of the survey aircraft "pitches". If necessary, calibration was repeated until satisfactory results were obtained.

Field Crew

Project Manager:	E. Aparicio
Geophysicist:	T. Carmichael
Data Processor:	M. Carriere
Pilots:	M. Williston, K. Wilson, L. Maike
Electronics Operator:	E. Aparicio
Engineer:	S. Erickson

Production Statistics

Flying dates:	October 14th – October 21st, 2002
Total production:	1,503 line kilometres
Number of production flights:	7
Hours of production flying:	22.8 hrs
Number of km/hour of production flying:	65.9 km/hour
Number of km/average production flight:	214.7 km/flight
Number of hours/average production flight:	3.3 hour/flight
Days lost due to weather:	1

III

QUALITY CONTROL AND COMPILATION PROCEDURES

In the field after each flight, all analogue records were examined as a preliminary assessment of the noise level of the recorded data. Altimeter deviations from the prescribed flying altitudes were also closely examined as well as the diurnal activity, as recorded on the base station.

All digital data were verified for validity and continuity. The data from the aircraft and base station was transferred to the PC's hard disk. Basic statistics were generated for each parameter recorded, these included: the minimum, maximum, and mean values; the standard deviation; and any null values located. All recorded parameters were edited for spikes or datum shifts, followed by final data verification via an interactive graphics screen with on-screen editing and interpolation routines.

The quality of the GPS navigation was controlled on a daily basis by recovering the flight path of the aircraft. The C^3NAVG^{2TM} (Combined Code and Carrier for NAVigation with GPS and GLONASS) correction programme employs the raw ranges from the base station to create improved models of clock error, atmospheric error, satellite orbit, and selective availability. These models are used to improve the conversion of aircraft raw ranges to aircraft position.

Checking all data for adherence to specifications was carried out in the field by the FUGRO AIRBORNE SURVEYS field geophysicist.

IV

DATA PROCESSING

Flight Path Recovery

GPS Recovery:	GPS positions recalculated from the recorded raw range data, and differentially corrected.
Projection:	Universal Transverse Mercator (UTM Zone 16N).
Datum:	NAD 83.
Ellipsoid:	GRS 1980.
Central meridian:	87° West.
False Easting:	500000 metres.
False Northing:	0 metres.
Scale factor:	0.99960.

Altitude Data

Noise editing:	Alfatrim median filter used to eliminate the two highest and two lowest values from the statistical distribution of a 9 point sample window for the radar altimeter. For the barometric altimeter the alfatrim median filter eliminated only the single highest and lowest points from the statistical distribution of a 5 point window.
Noise filtering:	Triangular filter set to remove radar, baro and GPS wavelengths less than 4 seconds.

Base Station Diurnal Magnetics

Noise editing:	Alfatrim median filter used to eliminate the two highest and two lowest values from the statistical distribution of a 9 point sample window.
Culture editing:	Polynomial interpolation via a graphic screen editor.
Noise filtering:	Running average filter set to remove wavelengths less than 2 seconds.

Extraction of long wavelength component:

Low pass filter set to retain only wavelengths greater than 75 seconds.

Airborne Magnetics

Lag correction:	3.7 seconds.

Noise editing: 4th difference editing routine set to remove spikes greater than 0.5 nT, followed by an alfatrim median filter eliminating the high and the low value from its calculation over a 5 point window.

Noise filtering: Triangular filter set to remove noise events having a wavelength less than 0.5 seconds and an amplitude less than 0.5 nT.

Diurnal substraction: The long wavelength component of the diurnal (greater than 75 seconds) was removed from the data, prior to the levelling analysis.

IGRF removal date: 2002.8.

Gridding: The data was gridded using an Akima routine with a grid cell size of 20 m.

Residual Magnetic Intensity:

The residual magnetic intensity (RMI) is derived from the total magnetic intensity (TMI), the diurnal, and the regional magnetic field. The total magnetic intensity is measured in the aircraft, the diurnal is measured from the ground station, and the regional magnetic field is calculated from the International Geomagnetic Reference Field (IGRF). The low frequency component of the diurnal is extracted from the filtered ground station data and removed from the TMI. The average of the diurnal is then added back in to obtain the resultant total magnetic intensity. The regional magnetic field, calculated for the specific survey location and the time of the survey, is then removed from the resultant total magnetic intensity. After levelling the residual magnetic intensity is completed.

Levelling:

The first stage of levelling of the magnetic data (correcting for residual diurnal effects, altitude differences and positioning errors) was done on the line data by automatically comparing the values of the total field at the intersection of each line and tie line. The differences were analyzed and a compensation was calculated at each intersection in order to provide a pattern of smoothly varying adjustments along each line and tie-line. Erratic differences, implying an error in the intersection location, were carefully checked and corrected.

The second step consisted of applying a micro-levelling routine to the gridded data in order to remove errors that are due to diurnal variations. During the micro-levelling routine a compensation grid was created and profile data was then extracted along the survey lines and stored in the final dataset as the levelling compensation.

The final Residual Magnetic Intensity was calculated in the following manner:

Filtered airborne Total Magnetic Intensity
- Low frequency component of the Diurnal data
+ Average diurnal data value
- IGRF
+ Levelling compensation
= Final Residual Magnetic Intensity

Electromagnetics

dB/dt Data

Lag correction: 4.2 seconds.

Data correction: The x, y and z-coil data were processed from the 20 raw channels recorded at 4 samples per second.

The following processing steps were applied to the dB/dt data from all coil sets:

a) The data from channels 1 to 5 (on-time) and 6 to 20 (off-time) were corrected for drift in flight form (prior to cutting the recorded data back to the correct line limits) by passing a low order polynomial function through the baseline minima along each channel, via a graphic screen display;

b) The data were edited for residual spheric spikes by examining the decay pattern of each individual EM transient. Bad decays (i.e. not fitting a normal exponential function) were deleted and replaced by interpolation;

c) Corrections were made in the x- and z-coil data for low frequency, incoherent noise elements (that do not correlate from channel to channel) in the data, by analysing the decay patterns of channels 10 to 20 (OMEGA process).

d) Noise filtering was done using an adaptive filter technique based on time domain triangular operators. Using a 2nd difference value to identify changes in gradient along each channel, minimal filtering (5 point convolution) is applied over the peaks of the anomalies, ranging in set increments up to a maximum amount of filtering in the resistive background areas (27 points for both the x-coil and the z-coil data).

e) This was followed by the application of a small running average filter.

f) The filtered data from the x, y and z-coils were then re-sampled to a rate of 5 samples/s and combined into a common file for archiving.

NOTE : *A fault developed with the transmitter controller board which affected the data from flights 6 to 11. This problem resulted in a slight shift in the group delay at the start of the waveform and the introduction of some spikes. This was remedied in processing by adjusting the gate positions, along the waveform, to compensate for the shift in the group delay and re-windowing the data from the halfwave files. Small irregularities in the on-time channels of the B-Field data may result.*

B-field Data

Processing steps: The processing of the B-Field data stream is essentially the same as that described above for the regular dB/dt stream. The lag adjustment used was the same, followed by: 1) drift adjustments; 2) spike editing for spheric events; 3) correction for low frequency, incoherent and non-decaying noise events; and 4) final noise filtering with an adaptive filter. The processing step 3 was applied in the B-field processing but not in the dB/dt processing. By nature, the B-Field data will contain a higher degree of coherency of the noise that automatically gets eliminated (or considerably attenuated) in the regular dB/dt, since this is the time derivative of the signal.

B-field Data Advantage:

The introduction of the B-Field data stream, as part of the GEOTEM system, provides the explorationist with a more effective tool for exploration in a broader range of geological environments and for a larger class of target priorities.

The advantage of the B-Field data compared with the normal voltage data (dB/dt) are as follows:

1. A broader range of target conductance that the system is sensitive to (the B-field is sensitive to bodies with conductance as great as 100,000 Siemens);
2. Enhancement of the slowly decaying response of good conductors;
3. Suppression of rapidly decaying response of less conductive overburden;
4. Reduction in the effect of spherics on the data;
5. An enhanced ability to interpret anomalies due to conductors below thick conductive overburden;
6. Reduced dynamic range of the measured response (easier data processing and display).

Figures 5 and 6 display the calculated vertical plate response for the GEOTEM signal for the dB/dt and B-field respectively. For the dB/dt response, you will note that the amplitude of the early channel peaks at about 25 Siemens, and the late channels at about 250 Siemens. As the conductance exceeds 1000 Siemens the response curves quickly roll back into the noise level. For the B-Field response, the early channel amplitude peaks at about 80 Siemens and the late channel at about 550 Siemens. The projected extension of the graph in the direction of increasing conductance, where the response would roll back into the noise level, would be close to 100,000 Siemens. Thus, a strong conductor, having a conductance of several thousand Siemens, would be difficult to interpret on the dB/dt data, since the response would be mixed in with the background noise. However, this strong conductor would stand out clearly on the B-Field data, although it would have an unusual character, being a moderate to high amplitude response, exhibiting almost no decay.

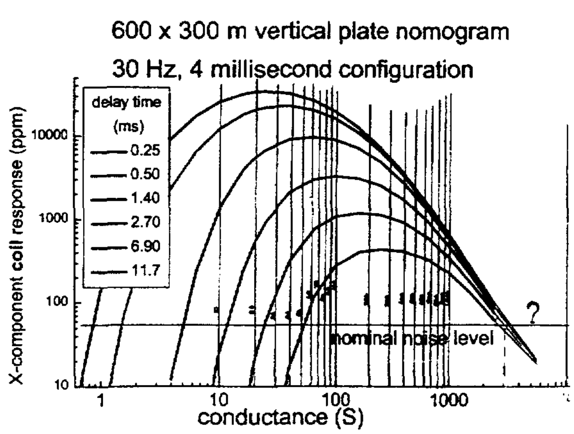

Figure 5. dB/dt vertical plate nomogram.

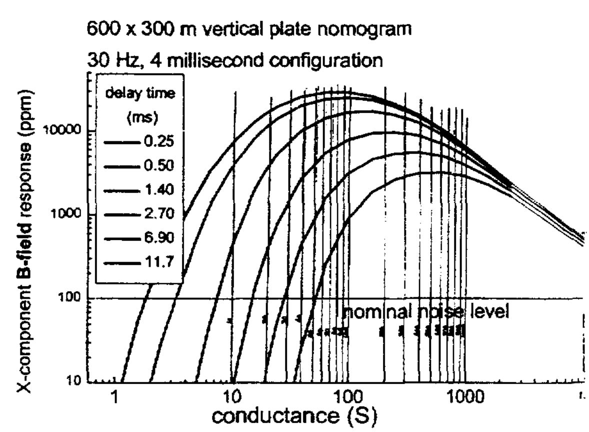

Figure 6. B-field vertical plate nomogram.

In theory, the response from a super conductor (50,000 to 100,000 Siemens) would be seen on the B-Field data as a low amplitude, non-decaying anomaly, not visible in the off-time channels of the dB/dt stream. Caution must be exercised here, as this signature can also reflect a residual noise event in the B-Field data. In this situation, careful examination of the dB/dt on-time (in-pulse) data is required to resolve the ambiguity. If the feature were strictly a noise event, it would be not be present in the dB/dt off-time data stream. This would locate the response at the resistive limit, and the mid in-pulse channel (normally identified as channel 3) would reflect little but background noise, or at best a weak negative peak. If, on the other hand, the feature does indeed reflect a superconductor, then this would locate the response at the inductive limit. In this situation, channel 3 of the dB/dt stream will be a mirror image of the transmitted pulse, i.e. a large negative.

EM Decay Constant:
The decay constant values are obtained by fitting the channel data to a single exponential function of the form:

$$Y=Ae^{-t/\tau},$$

where A = amplitude at time zero, t = time in microseconds and τ is the decay constant. A semi-log plot of this exponential function will be displayed as a straight line, the slope of which will reflect the rate of decay and therefore the strength of the conductor. A slow rate of decay, reflecting a high conductance, will be represented by a high decay constant value. As a single parameter, the decay constant provides more useful information than the amplitude data alone of any given single channel, as it indicates not only the peak position of the response but also the relative strength of the conductor.
For the present dataset, the decay constant was calculated by fitting the dB/dt X-coil data from channels 8 to 20 to the exponential function.

Anomaly Selection:
EM anomalies were selected by fitting the data from the dB/dt X-coil channels 9 to 20 to a vertical plate model, in order to extract conductance and depth information. Comparisons of the response from the X and Z coil data were made during the anomaly review for the final selection of the anomalies.
Refer to Appendix F for a full listing of the anomaly selections which provides the particulars of each selected anomaly, including the conductivity-thickness-product (CTP) and the depth of the conductor below surface. It is important to note that the derived values of CTP and depth associated with the anomaly selections are only valid if the geometry of the conductive source can be well approximated by a vertical plate of 300 by 600 m. A note is also included to guide the correct evaluation of the anomaly information.

Apparent Conductance Calculation:
The apparent conductance values were computed from the full waveform (all 20 channels) of the combined dB/dt X and Z-coils data by fitting to a thin sheet model. The results are stored in milliSiemens (mS).

Total Energy Envelope:
To combine the benefits of the measurements from both the X and Z coil data and reduce the asymmetry in the shape of the anomalies, the data from channel 9 of both the X and Z coils were used to compute the Total Energy Envelope. This was done through an Hilbert transform and essentially reflects the square root of the sum of the squares of each component. This parameter provides a good picture of the overall near-surface conductivity.

Gridding:
The EM data were gridded with a 20 m grid cell size, using a linear interpolation.

ONTARIO MINISTRY OF NORTHERN DEVELOPMENT AND MINES

Work Report Summary

Transaction No:	W0350.00344	**Status:**	APPROVED
Recording Date:	2003-MAR-05	**Work Done from:**	2002-OCT-12
Approval Date:	2003-MAR-05	**to:**	2002-OCT-23

Client(s):

300786 RESSOURCES FREEWEST CANADA INC., FREEWEST RESOURCES CANADA INC.

Survey Type(s):

AEM AMAG

Work Report Details:

Claim#	Perform	Perform Approve	Applied	Applied Approve	Assign	Assign Approve	Reserve	Reserve Approve	Due Date
SSM 1246624	$5,306	$5,306	$5,306	$5,306	$0	0	$0	$0	2003-MAR-19
	$5,306	$5,306	$5,306	$5,306	$0	$0	$0	$0	

External Credits: $0

Reserve:

$0 Reserve of Work Report#: W0350.00344

$0 Total Remaining

Status of claim is based on information currently on record.

42C16NW2001 2.25102 LIZAR 900

Ministry of
Northern Development
and Mines

Ministère du
Développement du Nord
et des Mines

Ontario

Date: 2003-MAR-06

GEOSCIENCE ASSESSMENT OFFICE
933 RAMSEY LAKE ROAD, 6th FLOOR
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FREEWEST RESOURCES CANADA INC.
800 BOUL. RENE LEVESQUE OUEST
BUREAU 1525
MONTREAL, QUEBEC
H3B 1X9 CANADA

Submission Number: 2.25102
Transaction Number(s): W0350.00344

Dear Sir or Madam

Subject: Approval of Assessment Work

We have approved your Assessment Work Submission with the above noted Transaction Number(s). The attached Work Report Summary indicates the results of the approval.

At the discretion of the Ministry, the assessment work performed on the mining lands noted in this work report may be subject to inspection and/or investigation at any time.

If you have any question regarding this correspondence, please contact BRUCE GATES by email at bruce.gates@ndm.gov.on.ca or by phone at (705) 670-5856.

Yours Sincerely,

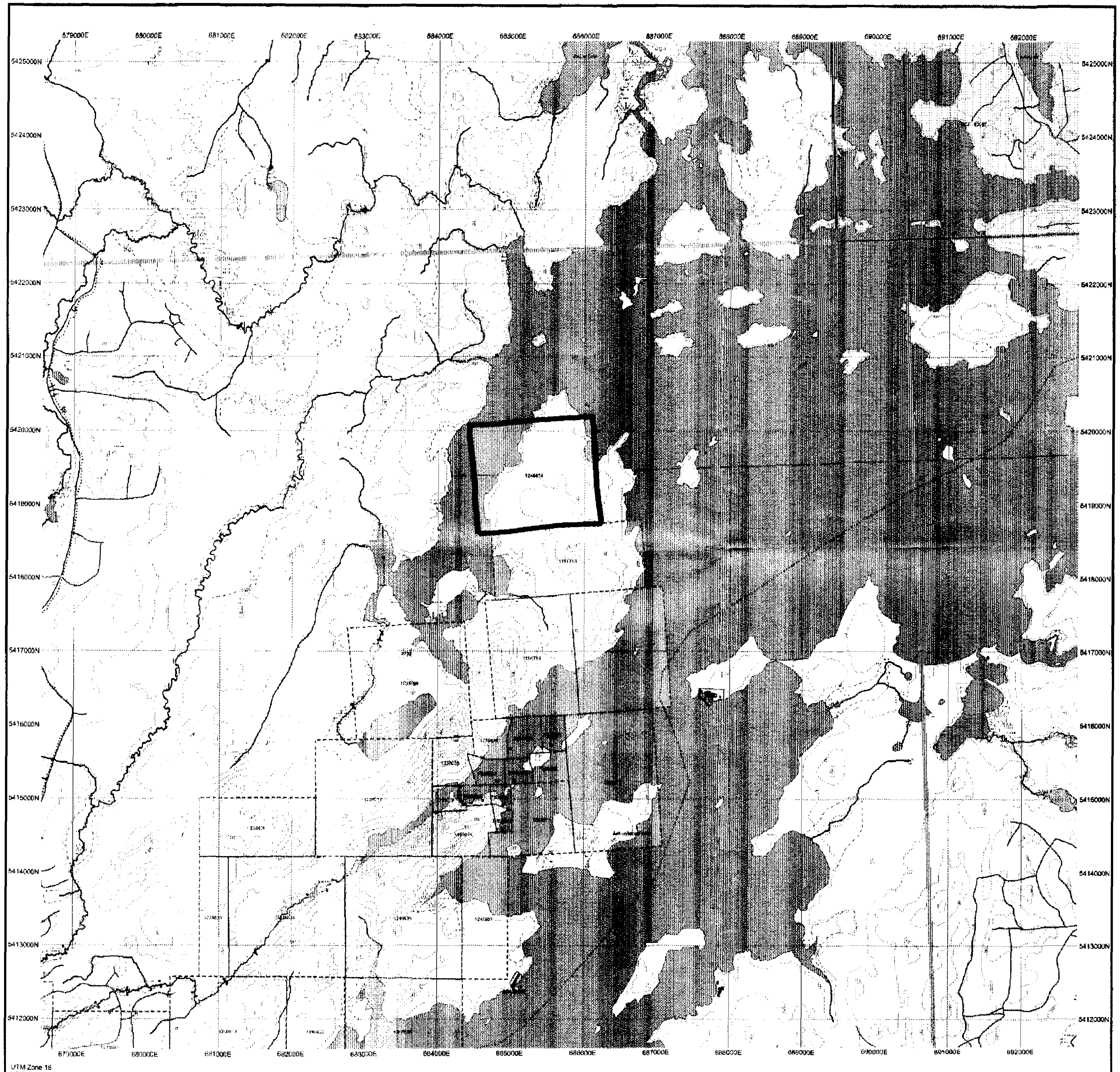
Ron Gashinski
Senior Manager, Mining Lands Section

Cc: Resident Geologist

Ressources Freewest Canada Inc., Freewest Resources Canada Inc.
(Claim Holder)

Assessment File Library

Ressources Freewest Canada Inc., Freewest Resources Canada Inc.
(Assessment Office)



ONTARIO CANADA
MINISTRY OF NORTHERN DEVELOPMENT AND MINES
PROVINCIAL MINING RECORDER'S OFFICE

Mining Land Tenure Map

Date / Time of Issue: Thu Mar 06 10:53:47 EST 2003

TOWNSHIP / AREA LIZAR

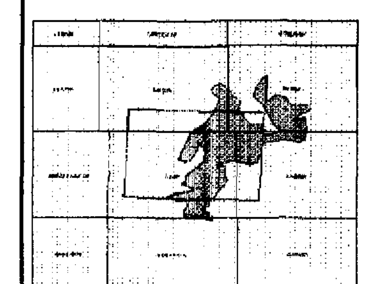
PLAN G-2328

ADMINISTRATIVE DISTRICTS / DIVISIONS

Mining Division	Sault Ste. Marie
Land Titles/Registry Division	ALGOMA
Ministry of Natural Resources District	WAWA

TOPOGRAPHIC

Land Tenure



LAND TENURE WITHDRAWALS

IMPORTANT NOTICES

LAND TENURE WITHDRAWAL DESCRIPTIONS

2.25102

AMAG

AEM

General Information and Limitations

42C16NW2001 2.25102 LIZAR

200

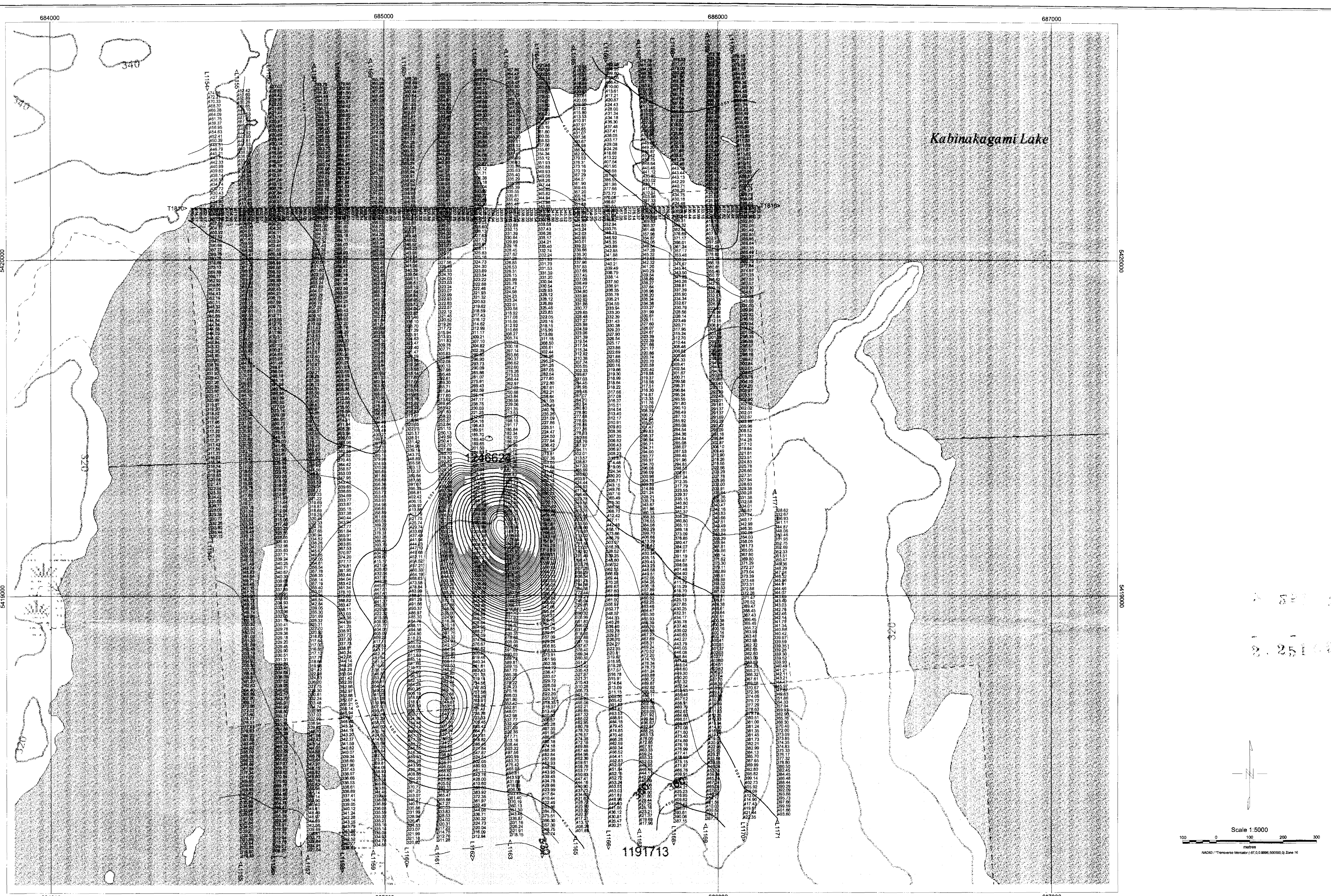


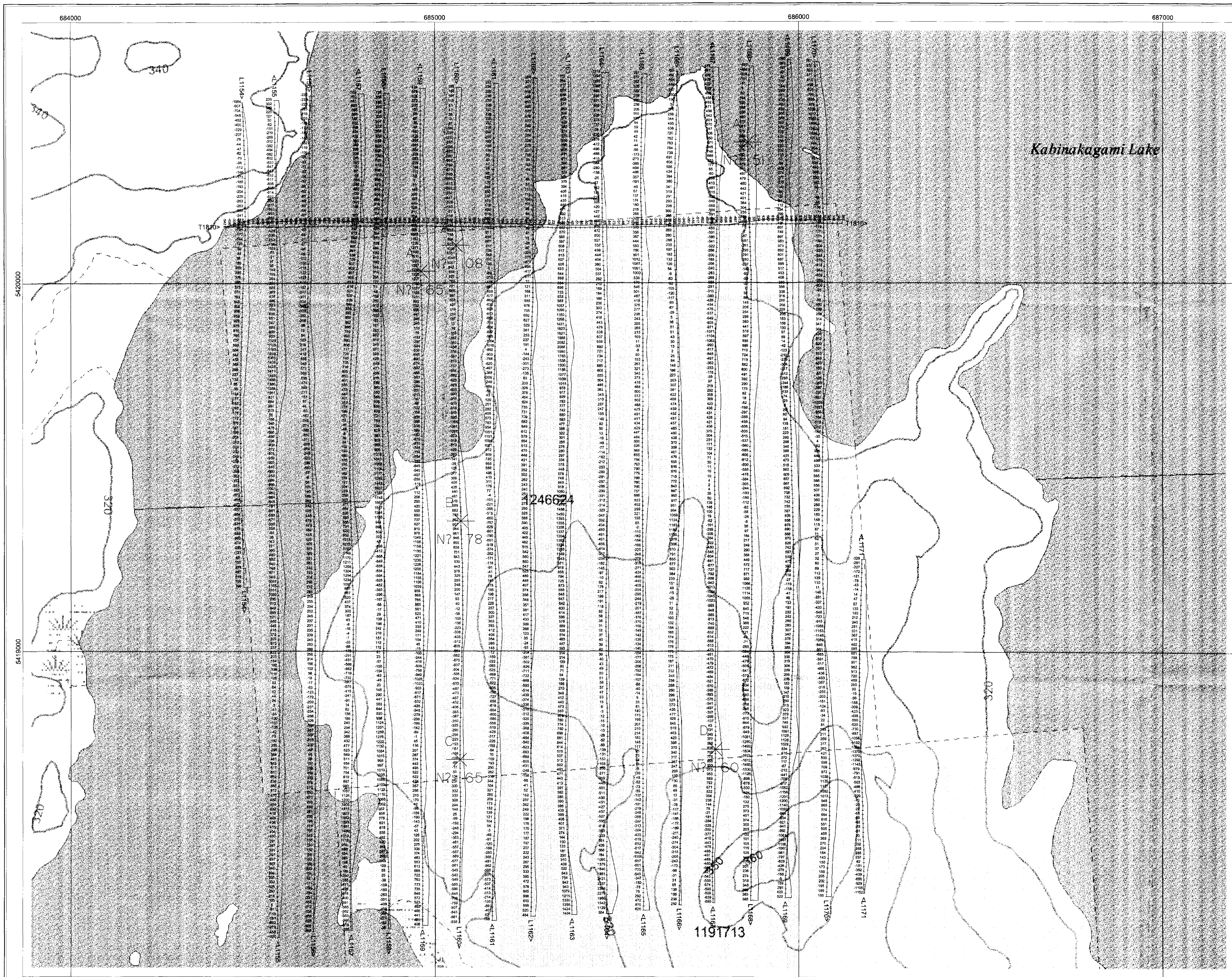
Figure 3

Teck Cominco Limited

Lizar Project
Lizar Township, Ontario

Airborne Electromagnetic Survey
Pole Reduced Magnetic Map
Contours with Mag Values

Tracy Campbell, January 10, 2003



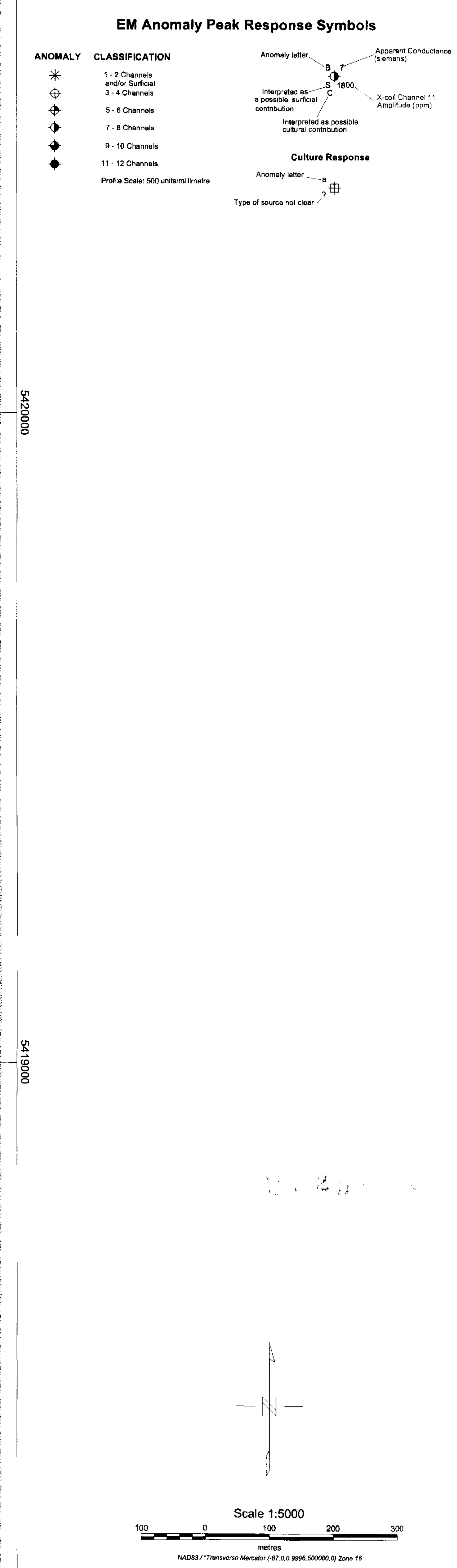


Figure 4

Teck Cominco Limited
Lizar Project **Lizar Township, Ontario**
Airborne Electromagnetic Survey Anomaly Picks with X Coil Channel 11 Profile
Tracy Campbell, January 10, 2003

42C16NW2001 2.25102 LIZAR

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