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EXPLORATION ACTIVITIES ON LANDS GRANTED UNDER LICENCE OF OCCUPATION NO. 14888 ( 1981 - 1982 )

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An interim report Prepared by: Harish M. Verma, Ph. D., Consulting Geologist, for SELCO INC.

May, 1982



A REPORT ON EXPLORATION ACTIVITIES ON LANDS GRANTED UNDER LICENCE OF OCCUPATION NO 14888

#### Introduction:

This report describes the exploration and related activities on lands granted under Licence of Occupation No. 14888. Under this exploration program, drilling was carried out by Selco Inc.

### Objectives:

The objectives of the exploration program were:

- i) to determine the continuity of the silica sand kaolin deposits eastwards and northwards from the claims held by Mr. Bruce Douglas.
- ii) to determine the thickness of overburden in the area of Licence of Occupation; and
- iii) to obtain uncontaminated and undisturbed samples of silica sand

kaolin deposits in order to determine their commercial qualities.

### Location of Drillholes:

Two drillholes located roughly in a north south line in the middle third of the area east of the patented claims, were drilled during the winter of 1981-82. The location of the drillholes is shown on Figure 1. The location may be more properly described as follows:

DRILLHOLE NO. SDT-1: About 3 kilometres NNE of Kipling Dam, Kipling Township.

Longitude: 82<sup>0</sup> 10' 30" West Latitude: 50<sup>0</sup> 09' 15" North

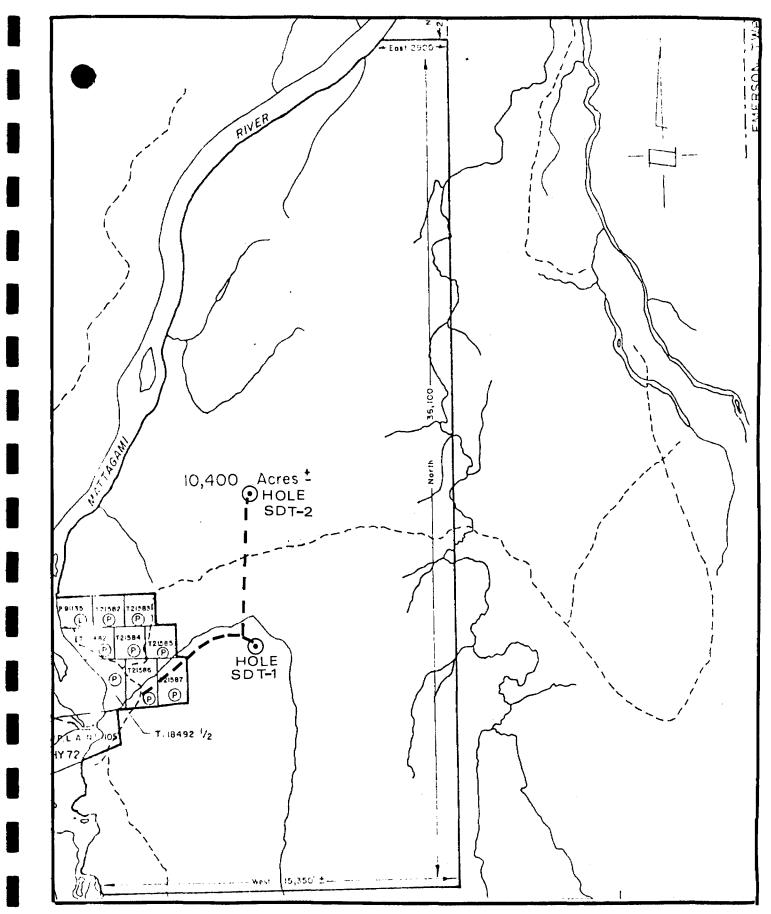


Fig. 1: Map showing the location of Drillholes SDT-1 and SDT-2 in the area of Licence of Occupation No. 14888. Scale 1: 100,000

DRILLHOLE NO. SDT-2: About 5 kilometres NE of Kipling Dam, Kipling Township. Longitude: 82<sup>0</sup> 10' 30" West Latitude: 50<sup>0</sup> 10' 30" North

#### Drilling Technique:

Drilling was carried out by Midwest Drilling by using a new drilling technique called Resonant Drilling or Sonic Drilling. In this technique, the rotatory motion of the drill rods is accompanied by a vibratory motion imparted to the drillhead by a pair of rotating drums. This new technique, although somewhat more expensive than conventional techniques, has the advantage of providing an uncontaminated and relatively undisturbed sample of unconsolidated sediments. It is the first time that this technique has been used in the investigation of silica sand-kaolin deposits of the James Bay Lowland.

The drill rig is mounted on a Nodwell. The sonic drill rig is equipped with a RDU 150 drillhead (called "the tub") and hydraulic power is provided by a Deutz 240 HP motor. The tower is 20' long, pull down type. The down hole tooling consists of 4<sup>1</sup>/<sub>4</sub>" outer diameter AOH rods with PW casing. Since the depth of penetration of the sonic drill is limited to about 330 feet ( 100 metres) an improvisation was made to accomplish deeper penetration. This improvisation consisted ot attaching a HC 150 Longyear diamond drill head to the sonic head. After the required penetration was achieved with the sonic technique, the Longyear drill head was moved into place and drilling continued with NQ wire line system using the sonic rods as the casing for the diamond drill rods. It was the first time that this dual system was tested and, with some minor modifications, has also proved to be quite successful.

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#### Logistics and Access:

Base camp was established in an open area on the west side of the road about 9 kilometres north of the Hydro Community of Smoky Falls. Originally, it was planned to move the drill rig along an old east-west winter road running through the area. However, this road was found to be unserviceable because of absence of frost on the ground prior to heavy accumulation of snow during November and December, 1981. New winter roads, therefore, had to be made along ground away from the muskeg terrain. The drill crew were ferried to and from the site by Helicopter. Drilling was carried out on a 24 hour, 2 shift basis. For emergencies during the night, snowmobiles were available as means of transport. Road work commenced on February 24, 1982 and drilling was carried out between February 28 and March 15, 1982.

#### GEOLOGY AND DRILLING RESULTS:

The area is covered by a thick sequence of quaternary deposits consisting mainly of tills underlain by clays and interbedded till and intertill sediments. Underneath the Quaternary deposits, the most prominent feature of the area is a Precambrian Escarpment (? Fault Scarp ) running in an east-west direction about 1.5 to 2 kms from the southern boundary of the area of the Licence. North of this escarpment, underneath the Quaternary deposits, are the Cretaceous deposits consisting of sands, clays and lignite. These Cretaceous deposits, known as the Mattagami Formation were the main focus of interest in the present program.

Drill logs of the two holes are given in Appendix 1. The following is a summary of the drill logs of the two holes: <u>Drillhole SDT-1</u>: This hole was drilled to a depth of 373 feet (113 m ). Quaternary deposits were encountered from 0 to 35.75 metres. These consist

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of the Adam and the Kipling Tills, underlain by greyish green clays of the Quaternary Missinaibi Formation. Below the Quaternary-Cretaceous Contact (35.75 m), the sediments are non-calcareous and consist of (from the top) silica sand - kaolin matrix, with minor interbeds of grey and brown fireclays, followed by black to brown dense carbonaceous clays. The commercially attractive silica sand - kaolin deposits occur from 35.75 metres to 93 metres. The black clays occur from 93 m to 105 m. From 105 m to the bottom of the hole are fine grained grey sands.

<u>DRILLHOLE SDT-2</u>: This hole, located about 3 km north of hole SDT-1, was drilled to a depth of 86 metres. Only quaternary sediments occur to the bottom of this hole. These consist of the Kipling and Adam Tills to a depth of 33 m. From 33 m to the bottom of the hole is a continuous succession of greyish green plastic calcareous lacustrine clays. In view of the fact that this hole went down to 68 metres without reaching the Cretaceous deposits, drilling was terminated at this depth. It appears that, in the vicinity of drillhole SDT-2, the Cretaceous deposits lie much deeper and are covered by a vast thickness of Quaternary deposits. Conclusions and Recommendations:

Pending a detailed laboratory examination and analysis of the samples obtained from the drillholes, the following conclusions and recommendations emerge from the exploration program:

1. Sonic drilling is an excellent technique for obtaining large, uncontaminated and undisturbed samples of unconsolidated sediments. Core recovery is 100%. Any future exploration program dealing with unconsolidated sediments should give serious consideration to using this technique. The weight of the drill rig ( 17 tons excluding the weight of the Nodwell) lends itself to drilling only in the winter. The drill rig has to be moved along specially prepared winter roads. The rig can also be moved on skids, pulled by a small tractor.

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2. Considerable planning is required ahead of time to prepare the roads so that the rig can be moved in and out quickly.

3. The Quaternary overburden continues to be thick eastwards from the boundary of the Douglas Claims. Thicker overburden lies in the area of the drillhole SDT-2.

4. In order to fully assess the potential of the entire area of the Licence, it is necessary to carry out further exploratory drilling in the northern part of the area as well in the area to the east of drillhole SDT-2.

5. The silica sand-kaolin samples obtained from drillhole SDT-1 are the best samples of this material obtained so far and should be carefully analysed for their commercial qualities.

Harish M. Verma, Ph. D., Consulting Geologist 2394, Rushbury Court, Burlington, Ontario L7P 3V8

Encl: Appendix 1 -Drill Logs of Drillholes SDT-1 and SDT-2 SELLO INC. -DOUGLAS TAYLOR PERMIT 1982 joint Venture DrillingProgramme James Bay Lowland Drilling - Midwest Drilling Googy - Harish M. Verma

DRILL LOG. DRILLHOLE NO: SDT- 1 LOCATION: Kipling Township, about 3 km NE of Kipling Dam Long. 82°10'30" W; Lat. 50°09' 15" N. Started Feb. 28, Finished March 5,1982 Sheet 1 of 5.

| Dep <b>th</b><br>(Ft.) | Lith.<br>Log                            | Sample        | Field Description and Remarks  |
|------------------------|---|---------------|--|
| 0 -                    | * *                                     | SONIC<br>CORE | 0'-8' Muskeg with some clay at the bottom  |
| 10                     |   |               | 8'-16' Alluvial sand   |
|                        |   |               | 16'-16.5' Clay<br>16.5'-20.5' Soft clay till with a few pebbles  |
| 20                     |   |               | 20.5'-25' Same as above with more clasts   |
|                        |   |               | 25'-29.5' Dense, grey to brown silty clay  |
| 30                     |   |               | 29.5'-40'Dense brownish clay till with very few clasts   |
| 40                     |   |               | 40'-42.5' Fine grained grey calcareous clay with more clasts   |
|                        |   |               | 42.5'-50' Same as above with increasing clasts towards the top of the section.                           |
| 50                     |   |               | 50'-60' Same as above grey calcareous clay with slight<br>more silt content                              |
| 60                     |   |               | 60'-65' Same as above with lesser number of clasts   |
|                        |   |               | 65'-70' Same as above with brownish tinge  |
| 70                     | 2 4 4 5 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 |               | 70'-77.5' Same as above- no obvious clasts   |
| 80                     |   |               | 77.5'-81' Dense, grey, clay till. A few small clasts,<br>some grit. More clasts in the bottom 1' interva |

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DRILLHOLE NO. SDT - 1 Sheet 2 of 5

| Depth<br>(Ft.) | Lith.<br>Log | Sample        | Field  | d Description and Remarks  |
|----------------|--------------|---------------|--|--|
| 81 -           |              | Sonic<br>Core | 81'-89'  | Dense, grey clay with brownish tinge,<br>no obvious clasts.  |
| -<br>90        |              |               |  | Dense grey brown calcareous clay with a<br>few very small clasts. At 100 feet, patches<br>of lenses of grey clay in grey, brownish clay.   |
| 100            |              |               |  | Same grey calcareous clay as above, few<br>clasts. At 116', more sandy   |
| 110            |              |               |  |  |
| 120            |              |               |  | QUATERNARY-CRETACEOUS CONTACT AT 118'<br>Fine grained, white to grey white, non-<br>calcareous, silica sand-kaolin matrix, coarsening<br>at 120'.<br>Coarse, white to greyish white silica sand.                                     |
| 130            |              |               |  | Transition zone- mixture of fine sand and brown clay.  |
|                |              |               | 134'-135'<br>135'-138'<br>138'-139'                                  | Light to dark brown, dense, non calcareous<br>fireclay.<br>Pure white quartzitic sand - appears to be<br>very little kaolin.<br>Quartz sand with dark heavy minerals (about<br>10%). Magnet picked up crystals of magnetite          |
|                |              |               | 140.5'-144<br>144.5'-145'<br>145'-150'<br>150'-151' (<br>151'-155' ( | and/or ilmenite.<br>'Brownish sand with a little kaolin.<br>.5'Dark brown clay<br>' Fine, brownish sand<br>Highly kaolinitic, very white quartz sand.<br>Coarser grained kaolinitic quartz sand<br>Same as above but getting coarser |
| 160            |              |               |  | Same as above, very highly kaolinized, getting<br>finer.   |

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DRILLHOLE NO.<u>SDT-1</u>. Sheet\_3\_\_\_of\_\_5\_\_\_.

| Depth<br>(Ft.) | Lith.<br>Log | Sample        | Field Description and Remarks   |
|----------------|--------------|---------------|---|
| 160 -          |              | Sonic<br>Core | 160'-165' Finer grained kaolinitic quartz sand  |
| -              |              | tore          | 165'-170' Pure white, medium grained, highly<br>kaolinitic quartz sand  |
| 170            |              |               | 170'-172.5' Grey, medium grained quartz sand with<br>reduced kaolin and increased heavy minerals<br>172,5'-180' Medium grained white quartz sand with<br>high kaolin content  |
| 180            |              |               | 180'-185' Medium grained quarts sand with grey rim around<br>the edge of the sonic core. The grey rim is<br>probably clay contamination from above or<br>leaching of quartz sand around the rim of the<br>core.   |
| 190            |              |               | 185'-191' Same as above<br>191'-193' Greyish white silica sand-kaolin matrix<br>193'-198.5' Quartz sand with varying amounts of kaolin.   |
| 200            |              |               | 198.5'-204' Fine grained greyish white quartz sand<br>with kaolin<br>204'-206' Brown fireclay   |
| 210            |              |               | 206'-211' Medium to fine grained white silica sand-<br>kaolin matrix<br>211'-222' Brown fireclay  |
| 220            |              |               | 222'-224' Grey sand with very little kaolin   |
| 230            |              |               | 222 -224 drey sand with very fittere kaofin<br>224'-230' Grey to whitish grey silica sand-kaolin matrix<br>getting coarser towards the bottom, with<br>large subangular quartz grains<br>230'-231' Fine grained grey silica sand-kaolin matrix<br>231'-233.5' Coarse grained white silica sand-kaolin matrix<br>233.5'-238' Fine grained silica sand kaolin matrix<br>with grey edges around the rim of the core<br>238'-240' Same as above but getting coarser grained |
|                | ;            |               | •   |

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DRILLHOLE NO. SDT-1 Sheet <u>4</u> of <u>5</u>.

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| Depth<br>(Ft.)  | Lith.<br>Log | Sample        | Fiel                     | d Description and Remarks  |
|-----------------|--------------|---------------|--------------------------|--|
| 240-            |              | Sonic<br>Core | 240'-241'                | Very coarse, angular grey sand with minor<br>amounts of kaolin. Abundant black heavy<br>minerals   |
| 25 <del>0</del> |              |               | 241'-258'                | Very fine grey sand with abundant kaolin   |
| -<br>           |              |               | 258'-260'                | Same as above enading into mono candy costion  |
| 26 <del>0</del> |              |               | 260'-262'<br>262'-265'   | Same as above grading into more sandy section<br>and then to fine to medium grained white sand<br>Same as above but getting coarser<br>Yellowish grey sand with kaolin         |
| 270             |              |               | 266.5-267.5              | Medium to coarse grained greyish white<br>silica sand kaolin matrix<br>'Same as above but getting coarser with<br>pebbles upto 2.5 cm across                                   |
| -               |              |               | 267.5'-275'<br>275'-300' | Medium to coarse grained greyish white<br>kaolinitic sand.<br>Medium to coarse grained grey white kaolinitic<br>sand   |
| 280-            |              | • •           |                          |  |
| 290             |              |               |                          |  |
|                 |              |               |                          |  |
| 300             |              |               | 300'-310'                | Medium to coarse grained silica sand-<br>kaolin matrix with large (upto 1 cm) rounded<br>pebbles. Probably high kaolin content.<br>Transition zone mixture of grey silica sand |
| 310             |              |               | 310.5-320'               | kaolin matrix and black carbonaceous clay.<br>Very dense, black carbonaceous clay with some<br>brownish inclusions. No lamination. slight<br>smell of organics.                |
|                 |              |               |                          |  |
| 320-            |              |               |                          |  |
| ł               | ]            |               |                          |  |

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DRILLHOLE NO.<u>SDT-1</u>. Sheet<u>5</u>of<u>5</u>.

| Dep <b>th</b><br>(Ft.) | Lith.<br>Log | Sample | Field Description and Remarks  |
|------------------------|--------------|--------|--|
| 320-<br><br><br><br>   |              | SONIC  | 320'-330' Dense, black, carbonaceous clay.<br>330-335' Same clay as above  |
| 340                    |              |        | <ul> <li>335'-339' Less dense light brown to grey carbonaceous clay.</li> <li>339'-341' Light brown to grey, more sandy plastic clay 0nly one foot of core recovered - same as above.<br/>Note: The NQ drilling rods, owing to excessive note: The NQ drilling rods, owing to excessive note: The NQ drilling rods.</li> </ul> |
| 350                    |              |        | vibration and the play between the NQ rods<br>and the sonic rods, broke at 3 placed while<br>going through the above dense clay.<br>346'-358' Only 4 feet recovered- grey fine sand<br>358'-373' No core recovery. Return water indicated same<br>material as above.<br>Drilling terminated at 373'                            |
| 360                    |              |        | PVC Pipe inserted to a depth of 250'.  |
| 375                    |              |        |  |
|                        |              |        |  |
|                        |              |        |  |

SELCO INC.- DOUGLAS TAYLOR PERMIT 1982 Joint Venture Drilling Programme James Bay Lowland

Drilling: Midwest Drilling

Geology: Harish M. Verma

DRILL LOG. DRILL HOLE NO. <u>SDT-2</u> Location: Kipling Township, about 5 km NE of Kipling Dam. Long. 82<sup>0</sup>10' 30" W; Lat. 50 10'30" N Started: March 13 Finished March 15, 1982 Sheet 1 of 3

| Dep <b>th</b><br>(Ft.) | Lith.<br>Log   | Sample        | Field Description and Remarks  |
|------------------------|----------------|---------------|--|
| -                      | *  *<br> *     | Sonic<br>Core | 0±14' Muskeg   |
|                        | *<br>*<br>*    |               |  |
| 10                     | भ <del>ग</del> |               | 14'-20' Calcareous grey plastic clay - no clasts   |
| 20                     |                |               | 20'-30' Grey clay with occasional pebbles  |
|                        |                |               |  |
| 30                     |                |               | 30'-35' Grey clay with large (2"-3") pebble at 34'   |
|                        |                |               | 35'-40' Greyish brown highly calcareous clay till  |
| 40                     |                |               | 40'-45' Grey to greyish brown hgihly calcareous clay   |
| -<br>-<br>-<br>-       |                |               | till- gritty with small clasts. harder and drier.<br>45'-50' Calcareous grey gritty till with small clasts.<br>Less clasts in the bottom 2 ft. |
| 50                     |                |               | 50'-60' Grey calcareous clay with some silt and occasional pebbles   |
|                        |                |               |  |
| 60                     |                |               | 60'-62' Same as above. Pebble at 60'.<br>62'-67' Coarse, hard grey till with small clasts  |
|                        |                |               | 67'-74' Grey, coarse calcareous till with numerous clasts.   |
| 70                     |                |               |  |
| -<br>                  |                |               | 74'-80' Grey, dense, highly calcareous clay till with<br>many clasts. Very hard from 74'-77'.  |
| 80-                    | * 1 R          |               | 80'-83.5' Same till as above, sandy, harder and with more clasts.  |
|                        |                |               | 83.5'-87' Grey, dense,highly calcareous sandy clay<br>till.<br>87'-90' Grey, dense calcareous clay till.                                       |
| -<br>10                | S D e          |               |  |

SELCO INC. - DOUGLAS TAYLOR PEPMIT P2 Joint Venture Drilling Programme JAMES BAY LOWLAND

DRILLHOLE NO. <u>SDT-2</u>. Sheet <u>2</u> of <u>3</u>.

| Depth<br>(Ft.)   | Lith.<br>Log | Sample        | Fie                            | eld Description and Remarks  |
|--|--------------|---------------|--------------------------------|--|
| 90 -<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>- |              | Sonic<br>Core | 90'-92'<br>92'-96'<br>96'-118' | Greenish grey, highly calcareous clay till<br>dense, somewhat plastic, a few clasts.<br>Same as above, harder, more gritty and more<br>clasts.<br>Greenish grey, highly calcareous dense clay till<br>with clasts - plastic in places. |
| 110  |              |               |                                |  |
| 120  | A. 9         |               |                                | Greenish grey plastic clay, few clasts, very<br>calcareous to 121'. Decrease in calcareous<br>nature from 121'-125'  |
| 130-   |              |               | 128'-133'                      | Greyish green, plastic, mildly calcareous clay<br>Dark brown, less calcareous clay, hard, less<br>plastic.<br>Greyish green, plastic calcareous clay - few<br>clasts.  |
| 140  |              |               | 135'-180'                      | Greenish grey calcareous plastic clay<br>uniform lithology   |
| 150  |              |               |                                |  |
| 160  |              |               |                                |  |
| 170  |              |               |                                |  |
| 180  |              |               |                                |  |

SECO INC. - Douglas, Taylor Permit 2 Joint Venture Drilling Programme JAMES BAY LOWLAND

DRILLHOLE NO. SDT-2 Sheet 3 of 3

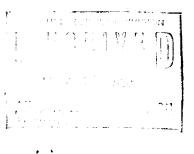
| Depth<br>(Ft.)             | Lith.<br>Log        | Sample        | Field Description and Remarks   |
|----------------------------|---------------------|---------------|---|
| 180 =                      |                     | Sonic<br>Core | 180'- 224' Same as above, greenish grey calcareous<br>plastic clay. No change in lithology. |
| 224                        |                     |               | Drilling terminated at 224'. No PVC pipe in the hole.                                       |
| -<br>                      |                     |               |   |
|                            |                     |               |   |
|                            |                     |               |   |
| -<br>                      |                     |               |   |
|                            |                     |               |   |
|                            |                     |               |   |
| -<br>-<br>                 |                     |               |   |
| -<br><br>                  |                     |               |   |
| -<br>-<br>-<br>-<br>-<br>- |                     |               |   |
|                            |                     |               |   |
|                            | • • •<br>- •<br>• • |               |   |



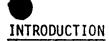
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EXPLORATION ACTIVITIES ON LANDS GRANTED UNDER LICENCE OF OCCUPATION NO. 14888 APRIL 1, 1982 TO MARCH 31, 1983

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J.A. Gribben March 23, 1983



During the period February 28th to March 15th, 1982 two holes totalling 182 metres were drilled on Licence of Occupation No. 14888. Results of this drilling were covered in a report by Dr. Harish Verma, Consulting Geologist, submitted in May, 1982.

In his report, Dr. Verma recommended that the silica-kaolin samples obtained from drill hole SDT-1 should be analysed for their commercial qualities. Under his direction and in conjunction with I.M.D. Laboratories a programme of testing was carried out. The section of Dr. Verma's final report that covers these tests forms the body of this report.

### **GEOPHYSICAL SURVEY**

An airborne magnetometer survey was carried out in June 1981 by Selco as part of a regional programme searching for kimberlite structures. A weak anomaly was detected near the south boundary of Licence of Occupation No. 14888. Subsequently a small grid J1-3 was cut and a ground magnetometer survey completed. The northern portion of this grid lies within Licence of Occupation No. 14888. The readings were obtained using a Geometrics G-816 total field proton magnetometer. The contoured results are shown on the accompanying plan ST-3383. There were no anomalies of interest located on the northern portion of grid J1-3.

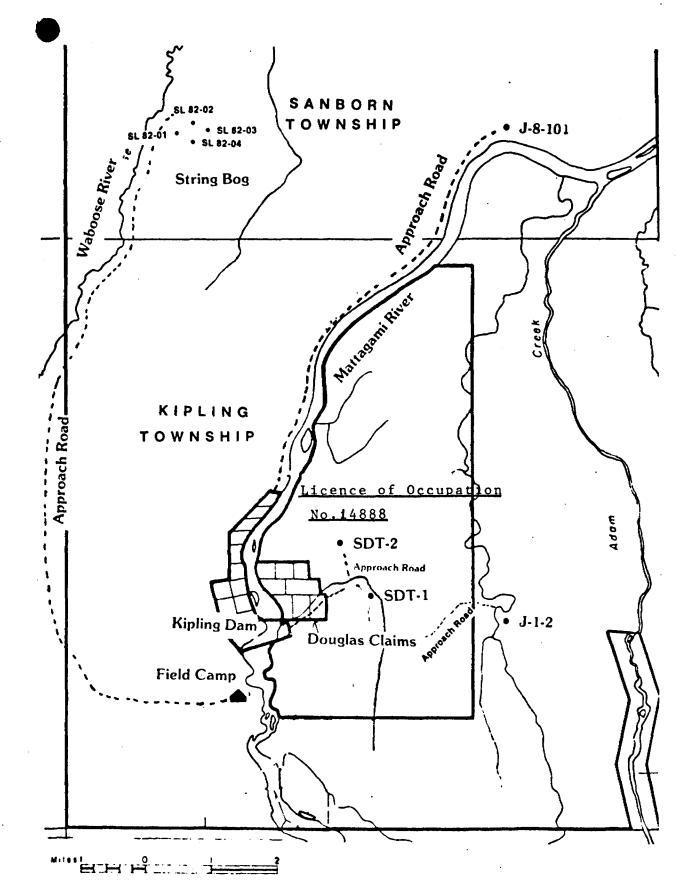
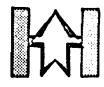


Figure 2. Map of parts of Kipling and Sanborn Townships showing the location of drillholes and the approach roads built.

## ANALYTICAL · RESULTS



## 4.1 INTRODUCTION

The present drilling has provided us with excellent quality samples of silica sand-kaolin mixtures from the upper Mattagami Formation in the following drillholes:

SDT-1, J-1-2, S1 82-01, SL 82-02, S1 82-03 and S1 82-04

The above holes have also provided us with excellent samples of high purity refractory clays (fireclays).

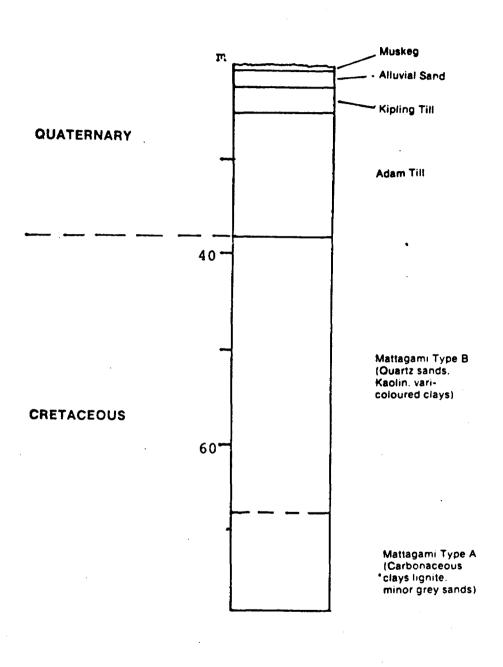
From an economic point of view Silica sand , kaolin and fireclays are attractive commercial targets. At present all of Canada's requirements of Kaolin are imported from the USA.

It was therefore proposed that some analytical work should be carried out on some of these samples in order to determine the commercial qualities of these products. Owing to time constraints and costs of such work, only a limited number of such samples could be subjected to this type of testing. Attention was focussed on drillhole SDT-1 which yielded an almost continuous 61 metre core of various grades of silica sand kaolin mixtures. It was therefore decided that a few samples from this hole be analysed.

## 4.2 OBJECTIVES

The objectives of the proposed analytical work were:

 a) to determine the proportions of silica sand and kaolin in the silica sand-kaolin mixtures in different parts of the sampled section.







- b) to determine the amounts of different size fractions in both the silica sand and the kaolin components of the samples.
- c) to determine the chemical composition, mineralogy and physical characteristics of the silica sand as well and the kaolin particularly in relation to their commercial usage.

In order to achieve the above objectives, it was proposed to

make the following determinations:

- 1. The amounts of minor constituents (Iron, Chromium, Titanium and Cobalt minerals) in the silica sands.
- 2. The chemical composition of the clay fraction as well as its free silica content.
- 3. The mineralogical composition of the clay fraction
- 4. The particle size distribution of the sand as well as the clay fraction and
- 5. The brightness of the clay fraction.
- If the above determinations appear encouraging for commercial

usage, the following additional determinations are warranted:

- 6. Fractionation of the clay fraction to 10 microns to determine what proportions are suitable for paper coating and filling applications.
- 7. Bleaching tests, if required.
- 8. Determine whether the free silica is distributed in all size ranges or only in the clay size fraction.
- 9. Determine the solution rheology (flow characteristics) of the clay fraction.
- 10. Determine the particle shape of the clay minerals.
- 11. Carry out paper coating and paper filling tests on the clay fraction

As the analytical work progressed, it became apparent that all the determinations could not be carried out without resolving problems posed



by some of the earlier determinations (see below). In practice items 1, 2, 4, 6, and 8 could be given attention.as the other items depended on these.

### Laboratories

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All the industrial mineral laboratories that could perform the type of work desired by us were contacted. Finally the choice fell on I.M.D. Laboratories on account of this firm's extensive previous experience with this type of material. I.M.D Laboratories was made responsible for doing the initial separations as well as for subcontracting the chemical and analytical work to other specialty labs. Chemical determinations were carried out by X-RAY ASSAY LABS. Particle size distribution and free silica content determinations were carried out by INDUSMIN Ltd. All the laboratories were advised to incorporate suitable standards in all analytical work. In the final stages of the work, when it appeared that the free silica content in a composite sample was beyond tolerable levels I. M. D Labs undertook limited work aimed at investigating ways in which the free silica levels in the Kaolin can be reduced.

## 4.3. SAMPLE SELECTION

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Fourteen samples of various grades of silica sand-kaolin mixtures were selected from the material of hole SDT-1. Sample numbers, the depth from which they were obtained, and their lithological characteristics are given in Table 3.



Photo te Frozen core of Silica Sand-Kaolin matrix.

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TABLE 3. LIST OF SAMPLES SELECTED FOR ANALYTICAL WORK



| <u>Sample No</u> . | •             | Lithological Description   |
|--------------------|---------------|--|
| SDT-1-3            | 36.89 - 37.80 | <b>Coarse</b> grained greyish white silica<br><b>sand-kaolin</b> mixture (SSK)             |
| SDT-1-4            | 38.41 - 39.02 | - Same as above -  |
| SDT-1-6            | 44.51 - 45.73 | Fine grained, white, highly kaolinitic SSK   |
| SDT-1-7            | 48.17 - 48.78 | Same as above, somewhat finer.   |
| SDT-1-8            | 49.69 - 50.30 | Fine grained white SSK   |
| SDT+1-9            | 50.60 - 50.91 | Pure white medium grained SSK  |
| SDT-1-10           | 56.70 - 57.31 | Medium grained SSK   |
| SDT-1-11           | 60.51 - 60.97 | Fine grained greyish white SSK   |
| SDT-1-13           | 69.51 - 70.12 | Grey to whitish grey SSK getting coarser towards the bottom with subangular quartz grains. |
| SDT-1-14           | 71.64 - 71.95 | Fine grained SSK   |
| SDT-1-15           | 74.39 -76-69  | Very fine grained SSK with abundant Kaolin.  |
| SDT-1-16           | 83.23 -83.84  | Medium to coarse grained greyish white SSK   |
| SDT-1-17           | 88.41 - 89.02 | Same as above  |
| <b>SDT-1-</b> 18   | 92.07 - 92.68 | Medium to coarse grained SSK with large pebbles.   |

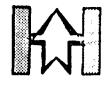
## 4.4 TEST RESULTS

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The following is a concise account of the testing procedures and results:

### SAMPLE DISPERSION AND DETERMINATION OF MOISTURE CONTENT

A small portion was weighed, dried and weighed again. This gave an estimate of moisture content. Results are given in table 4.



#### TABLE 4

### MOISTURE CONTENT OF SILICA + KAOLIN SAMPLES <sup>8Н</sup>2<sup>0</sup> STD - 3 9.4 9.8 STD - 4STD - 615.8 13.2 STD - 7 13.8 STD - 811.4 STD - 9 10.6 STD - 1016.3 STD - 11 8.2 STD - 13STD - 1410.0 15.8 STD - 15 STD - 169.2 10.8 STD - 17 9.5 STD - 18

STD - 5 and STD - 12 were sections of dark gray plastic ball or fire clay and were not sampled.

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The moisture content varies from 8.2% to 16.3 %. The mean value is 11.7%.

#### **INITIAL SEPARATIONS**

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Using 8, 30, 200 and 325 mesh screens the samples were separated into the following size fractions:

| Major                 | <b>Co</b> mponent:<br>r | s<br>Minor |
|-----------------------|-------------------------|------------|
| + 8 mesh Silica       | a .                     |            |
| -8 + 30 mesh Silica   | 3                       |            |
| -30+ 200 mesh Silica  | a +                     | Mica       |
| -200+ 325 mesh Silica | a <b>+</b> ,            | Mica       |
| -325 mesh Kaolir      | n . +                   | Silica     |

Table 5 gives the results of the above separation.

From a commercial point of view the more important fractions are:

| - 30 + 200 mesh | - Glass Grade Fraction  |
|-----------------|-------------------------|
| - 325 mesh      | - Kaolin sized fraction |

In our samples the glass grade fraction varies from 25% to 87%, with a mean value of 53%.

The kaolin sized sample ( - 325 mesh) is mixed with very fine silica and varies from a minimum of 6% to a maximum of 37%. The mean value is 13%.

SILICA DETERMINATIONS

-8 +.30 mesh silica fraction of 11 samples (untreated) was subjected to chemical analyses as follow:

| Whole Rock Major   | %   | XRF |
|--------------------|-----|-----|
| Whole Rock Minor   | ppm | XRF |
| Fe <sub>2</sub> 03 | ppm | AAA |

### TABLE 5

PERCENTAGE OF INDIVIDUAL SIZE FRACTIONS IN EACH SAMPLE

|         | ¥<br>+ 8 Mesh | -8 + 30<br> | -30 + 200<br> | <b>%</b><br>-200 + 325<br> | <b>%</b><br>- 325<br> |
|---------|---------------|-------------|---------------|----------------------------|-----------------------|
| STD - 3 | <b>4</b> ·    | 50          | 39            | 2                          | 5                     |
| 4       | 6             | 55          | 30            | 1                          | 8                     |
| 6       | 3             | <b>38</b> · | 47            | 1                          | 11                    |
| 7       | 1             | 5           | 79 :          | 1                          | 14                    |
| 8       | 0             | 4           | <b>87</b>     | 1                          | 8                     |
| 9       | 1             | 46          | 45            | 1                          | 7                     |
| 10      | 1             | 50          | 36            | 0                          | 13                    |
| 11      | 0             | 1.          | 78            | 1                          | 20                    |
| 13      | 11            | 34          | 48            | 1                          | 6                     |
| 14      | 0             | l           | 79            | 0                          | 20                    |
| 15      | 0             | 0           | · 55 ·        | 8                          | 37                    |
| 16      | 8             | 34          | 46            | 1                          | 11                    |
| 17      | 7             | 29          | 52            | 1                          | 11                    |
| 18      | 27            | 36          | 25:           | 1                          | 11                    |

All fractions from 8 mesh to 200 mesh are silica. The -200 + 325 mesh is a mixture of mica and silica while the -325 mesh is kaolin, containing fine silica.

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Table 6 gives the results of whole rock major analyses of

-8 + 30 mesh fraction.

Whole rock minor elements for the above fraction are as follows:

| Sample   | CR | RB | SR | Zr   |
|----------|----|----|----|------|
| SDT-1-3  | 30 | 0  | 0  | 20   |
| SDT-1-4  | 30 | 0  | 0  | 10   |
| SDT-1-6  | 30 | 0  | 0  | 40   |
| SDT-1-7  | 30 | 0  | 0  | 20   |
| SDT-1-8  | 30 | 0  | 0  | 20   |
| SDT-1-9  | 30 | 0  | 0  | 20   |
| SDT-1-10 | 30 | 0  | 0  | 10   |
| SDT-1-13 | 30 | 0  | 0  | 10   |
| SDT-1-16 | 30 | 0  | 0  | 20   |
| SDT-1-17 | 30 | 0  | 0  | . 30 |
| SDT-1-18 | 30 | 10 | 0  | 10   |

 $Fe_20_3$  (ppm) results with AAA technique are as follows:

| Sample   | Fe203 ppm |  |  |  |  |
|----------|-----------|--|--|--|--|
| SDT-1-3  | 150       |  |  |  |  |
| SDT-1-4  | 150       |  |  |  |  |
| SDT-1-6  | 130       |  |  |  |  |
| SDT-1-7  | 170       |  |  |  |  |
| SDT-1-8  | 320       |  |  |  |  |
| SDT-1-9  | 120       |  |  |  |  |
| SDT-1-10 | 170       |  |  |  |  |
| SDT-1-13 | 200       |  |  |  |  |
| SDT-1-16 | 170       |  |  |  |  |
| SDT-1-17 | 140       |  |  |  |  |
| SDT-1-18 | 230       |  |  |  |  |

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|----------|------|-------|-------|------|-------------------|------------------|--------------------------------|------|------|------|--------|------|
| SAMPLE   | SiO2 | AL203 | CaO   | MgO  | Na <sub>2</sub> O | к <sub>2</sub> 0 | Fe <sub>2</sub> 0 <sub>3</sub> | MnO  | TiO2 | P205 | L.O.I. | SUM  |
| SDT-1-3  | 99.3 | 0.09  | 0.01  | 0.00 | 0.00              | 0.01             | 0.04                           | 0.00 | 0.02 | 0.01 | 0.16   | 99.6 |
| SDT-1-4  | 99.3 | 0.09  | 0.01  | 0.00 | 0.00              | 0.01             | 0.06                           | 0.00 | 0.01 | 0.01 | 0.31   | 99.8 |
| SDT-1-6  | 99.1 | 0.07  | 0.01  | 0.00 | 0.00              | 0.01             | 0.04                           | 0.00 | 0.02 | 0.01 | 0.08   | 99.3 |
| SDT-1-7  | 99.6 | 0.09  | 0.02  | 0.00 | 0.00              | 0.01             | 0.07                           | 0.00 | 0.01 | 0.01 | 0.08   | 99.8 |
| SDT-1-8  | 99.5 | 0.17  | 0.02  | 0.01 | 0.00              | 0.01             | 0.05                           | 0.00 | 0.02 | 0.01 | 0.08   | 99.9 |
| SDT-1-9  | 99.5 | 0.10  | 0.02  | 0.00 | 0.00              | 0.01             | 0.04                           | 0.00 | 0.01 | 0.01 | 0.16   | 99.9 |
| SDT-1-10 | 99.5 | 0.10  | 0.02  | 0.00 | 0.00              | 0.01             | 0.02                           | 0.00 | 0.02 | 0.01 | 0.16   | 99.8 |
| SDT-1-13 | 99.3 | 0.08  | 0.02  | 0.00 | 0.00              | 0.01             | 0.03                           | 0.00 | 0.01 | 0.01 | 0.16   | 99.6 |
| SDT-1-16 | 99.2 | 0.15  | 0.02  | 0.01 | 0.00              | 0.01             | 0.02                           | 0.00 | 0.02 | 0.01 | 0.16   | 99.6 |
| SDT-1-17 | 99.5 | 0.11  | 0.02  | 0.00 | 0.00              | 0.01             | 0.03                           | 0.00 | 0.01 | 0.01 | 0.08   | 99.8 |
| SDT-1-18 | 99.2 | 0.16  | 0.02  | 0.00 | 0.02              | 0.01             | 0.02                           | 0.00 | 0.02 | 0.01 | 0.15   | 99.6 |

These analysis are for the washed, but otherwise untreated silica sand.

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## TABLE 6

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CHEMICAL ANALYSIS OF 8 + 30 MESH SILICA FRACTION

Thus the results on this untreated -8 + 30 mesh fraction show silica concentrations from 99.1% to 99.5%. Fe<sub>2</sub>O<sub>3</sub> concentrations in the same samples with XRF techniques varied from 0.02% to 0.07%. With the AAA techniques the concentrations were 140 ppm (0.014%) to 320 ppm (0.032%).

The - 30 + 150 mesh fraction was subjected to high intensity magnetic separation. The magnetic components of this fraction varied from 0.06% to 2.6% (Table 7).

The non-magnetic components of the above fraction were subjected to the following analyses:

| Whole Rock | Major. | %   | XRF |
|------------|--------|-----|-----|
| Whole Rock | Minor  | ppm | XRF |
| Fe203      |        | ppm | AAA |
| Co         |        | ppm | DCP |
| Cr         |        | ppm | DCP |

Whole rock major analyses of -30 + 150 faction are given in table 8. The Fe<sub>2</sub>O<sub>3</sub> content of this non-magnetic fraction varies from 0.013% to 0.032%. The Fe<sub>2</sub>O<sub>3</sub> value for the British Ceramic Standard (Glass Grade Sand) is 0.027%

The Cobalt and the Chromium values for this fraction are given below (following table 8)

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### TABLE 7

| <u>-30 + 20</u> | 0 MESH SIL | ICA - RECO       | VERY AFTER      | MAGNE | TIC SEPARATION      |      |
|-----------------|------------|------------------|-----------------|-------|---------------------|------|
|                 | Sample     | Total<br>Wt. (g) | Wt.<br>Mag. (g) | 8     | Wt.<br>Non-Mag. (g) | ج    |
| SDT-1 -         | 3          | 1000             | 11              | 1.1   | 989                 | 98.9 |
|                 | 4          | 1000             | 23              | 2.3   | 977                 | 97.7 |
|                 | 6          | 1000             | 10              | 1.0   | 990                 | 99   |
|                 | 7.         | 1000             | 8               | 0.8   | 992                 | 99.2 |
| •               | · 8        | 1000             | 8               | .0.8  | 992                 | 99.2 |
|                 | 9          | 1000             | 18              | 1.8   | 982                 | 98.2 |
|                 | 10         | 1000             | 16              | 1.6   | 984                 | 98.4 |
|                 | 11         | 1000             | 24              | 2.4   | 976                 | 97.6 |
|                 | 13         | 1000             | 19              | 1.9   | 981                 | 98.1 |
|                 | 14         | 1000             | 26              | 2.6   | 974                 | 97.4 |
|                 | 15         | 1000             | 22              | 2.2   | 978                 | 97.8 |
|                 | 16         | 1000             | 18 .            | 1.8   | 982                 | 98.2 |
|                 | 17         | 1000             | 16              | 1.6   | 984                 | 98.4 |
|                 | 18         | 1061             | 9               | 0.8   | 1052                | 99.2 |

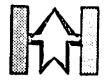
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|          |                  |       | EMICAL<br>TER HIG |      |                   |                  | + 150 MES<br>SEPARATI |      | CA SAND |      |        |                 |
|----------|------------------|-------|-------------------|------|-------------------|------------------|-----------------------|------|---------|------|--------|-----------------|
| SAMPLE   | sio <sub>2</sub> | AL203 | CaO               | MgO  | Na <sub>2</sub> 0 | к <sub>2</sub> 0 | Fe203                 | MnO  | TiO2    | P205 | L.O.I. | SUM             |
| SET-1-3  | 99.5             | 0.18  | 0.02              | 0.02 | 0.00              | 0.11             | 0.025                 | 0.00 | 0.02    | 0.01 | 0.08   | 100.0           |
| SDT-1-4  | 98.8             | 0.16  | 0.02              | 0.02 | 0.00              | 0.10             | 0.017                 | 0.00 | 0.01    | 0.01 | 0.08   | 99 <b>.2</b>    |
| SDT-1-6  | 99.4             | 0.11  | 0.02              | 0.01 | 0.00              | 0.10             | 0.014                 | 0.00 | 0.02    | 0.01 | 0.08   | 99.8            |
| SDT-1-7  | 99.6             | 0.14  | 0.02              | 0.00 | 0.00              | 0.00             | 0.013                 | 0.00 | 0.02    | 0.01 | 0.08   | 99.9            |
| SDT-1-8  | 98.6             | 0.18  | 0.02              | 0.01 | 0.00              | 0.01             | 0.013                 | 0.00 | 0.02    | 0.01 | 0.23   | 99.1            |
| SDT-1-9  | 99.0             | 0.19  | 0.02              | 0.01 | 0.00              | 0.00             | 0.018                 | 0.00 | 0.03    | 0.01 | 0.31   | 99.6            |
| SDT-1-10 | 99.4             | 0.14  | 0.02              | 0.01 | 0.00              | 0.00             | 0.017                 | 0.00 | 0.02    | 0.01 | 0.16   | 99 <b>.</b> 8 5 |
| SDT-1-11 | 99.3             | 0.31  | 0.02              | 0.02 | 0.00              | 0.01             | 0.023                 | 0.00 | 0.03    | 0.01 | 0.16   | 99.9            |
| SDT-1-13 | 98.8             | 0.11  | 0.02              | 0.02 | 0.00              | 0.01             | 6.019                 | 0.00 | 0.03    | 0.01 | 0.23   | 99.3            |
| SDT-1-14 | 99.3             | 0.35  | 0.02              | 0.02 | 0.00              | 0.03             | 0.027                 | 0.00 | 0.06    | 0.01 | 0.23   | 100.1           |
| SDT-1-15 | 98.8             | 0.48  | 0.02              | 0.01 | 0.00              | 0.02             | 0.032                 | 0.00 | 0.08    | 0.01 | 0.23   | 99.8            |
| SDT-1-16 | 99.8             | 0.19  | 0.02              | 0.01 | 0.00              | 0.02             | 0.017                 | 0.00 | 0.03    | 0.01 | 0.08   | 100.2           |
| SDT-1-17 | 99.3             | 0.19  | 0.02              | 0.01 | 0.00              | 0.02             | 0.014                 | 0.00 | 0.03    | 0.01 | 0.08   | 99.7            |
| SDT-1-18 | 99.4             | 0.26  | 0.02              | 0.01 | 0.00              | 0.08             | 0.024                 | 0.00 | 0.03    | 0.01 | 0.08   | 99.9            |
| BCS-313  | 99.5             | 0.15  | 0.02              | 0.00 | 0.00              | 0.04             | 0.027                 | 0.00 | 0.02    | 0.01 | 0.16   | 99.9            |

TABLE 8.

All results in percent (%) except for cobalt and chromium which are in parts per million.





| Cobalt and | Chromium in non-magneti | c fraction |
|------------|-------------------------|------------|
|            | of -30 + 150 fraction   |            |

| Sample   |      | Co   | ppm | Cr ppm |
|----------|------|------|-----|--------|
| SDT-1-3  |      |      | 1   | 3      |
| SDT-1-4  | less | than | 0.5 | 4      |
| SDT-1-6  | less | than | 0.5 | 2      |
| SDT-1-7  |      |      | 1.0 | 3.     |
| SDT-1-8  |      |      | 0.5 | 2      |
| SDT-1-9  |      |      | 0.5 | 5      |
| SDT-1-10 |      |      | 0.5 | 2      |
| SDT-1-11 |      |      | 0.5 | 4      |
| SDT-1-13 |      |      | 0.5 | 3      |
| SDT-1-14 |      |      | 1.5 | 7      |
| SDT-1-15 |      |      | 1.5 | 7      |
| SDT-1-16 |      |      | 0.5 | 3      |
| SDT-1-17 |      |      | 1.0 | 3      |
| SDT-1-18 |      |      | 1.0 | 6      |
| BCS 313  | Less | than | 0.5 | 2      |

Thus Cobalt varies from less than 0.05 ppm to 1.0 ppm. Chromium caries from 2 ppm to 8 ppm.

### KAOLIN CHEMICAL ANALYSES

The -325 mesh fraction dried and submitted for chemical analysis. Chemical analyses of the samples are given in table 9.

The same samples were also submitted for particle size distribution analyses. This was carried out by the Sedigraph Method. The Sedigraph

|                   |           | TABLE 9          |      |        |   |            |       |
|-------------------|-----------|------------------|------|--------|---|------------|-------|
| CHEMICAL ANALYSIS | OF CRUDE, | UNPROCESSED -325 | MESH | KAOLIN | - | SILICA MIX | TURES |

The control sample is a commercial quality coating clay.

| SAMPLE       | SiO2   | AL203 | CaO  | MgO  | Na <sub>2</sub> O | к <sub>2</sub> 0 | Fe203 | MnO  | TiO2 | P205 | L.O.I. | SUM          |   |
|--------------|--------|-------|------|------|-------------------|------------------|-------|------|------|------|--------|--------------|---|
| SDT-1-3      | 64.4   | 24.8  | 0.30 | 0.08 | 0.00              | 0.12             | 0.59  | 0.00 | 0.30 | 0.03 | 9.15   | 99 <b>.9</b> |   |
| SDT-1-4      | 63.3   | 26.3  | 0.11 | 0.02 | 0.00              | 0.10             | 0.37  | 0.00 | 0.25 | 0.03 | 9.54   | 100.1        |   |
| SDT-1-6      | 73.6   | 18.2  | 0.09 | 0.01 | 0.00              | 0.10             | 0.37  | 0.00 | 0.35 | 0.04 | 6.93   | 99.8         |   |
| SDT-1-7      | 52.7   | 32.0  | 0.14 | 0.07 | 0.02              | 0.23             | 0.81  | 0.00 | 0.86 | 0.04 | 12.5   | 99.4         | 5 |
| SDT-1-8      | 52.5   | 33.4  | 0.12 | 0.06 | 0.01              | 0.24             | 0.56  | 0.00 | 0.44 | 0.04 | 12.4   | 99.8         | ω |
| SDT-1-9      | 54.2   | 32.2  | 0.13 | 0.06 | 0.02              | 0.23             | 0.55  | 0.00 | 0.42 | 0.04 | 12.1   | 100.0        |   |
| SDT-1-10     | 57.5   | 29.1  | 0.16 | 0.09 | 0.00              | 0.30             | 0.84  | 0.00 | 0.62 | 0.04 | 11.0   | 99.8         |   |
| SDT-1-11     | 52.1   | 32.5  | 0.12 | 0.09 | 0.02              | 0.30             | 1.05  | 0.00 | 1.18 | 0.03 | 12.2   | 99.8         |   |
| SDT-1-13     | 68.6   | 20.5  | 0.16 | 0.05 | 0.01              | 0.18             | 1.15  | 0.01 | 1.03 | 0.04 | 8.08   | 99.9         |   |
| SDT-1-14     | 56.6   | 29.4  | 0.15 | 0.12 | 0.04              | 0.34             | 0.95  | 0.00 | 1.37 | 0.05 | 11.0   | 100.1        |   |
| SDT-1-15     | 56.1   | 28.7  | 0.17 | 0.17 | 0.Q2              | 0.45             | 1.16. | 0.00 | 1.39 | 0.05 | 11.3   | 99.6         |   |
| SDT-1-16     | 52.8   | 32.5  | 0.12 | 0.08 | 0.03              | 0.34             | 0.90  | 0.00 | 0.88 | 0.05 | 12.2   | 99.8         |   |
| SDT-1-17     | 57.5   | 29.1  | 0.10 | 0.06 | 0.02              | 0.61             | 0.84  | 0.00 | 0.75 | 0.04 | 10.8   | 99.9         | • |
| SDT-1-18     | 57.0   | 30.1  | 0.11 | 0.07 | 0.04              | 1.07             | 0.69  | 0.00 | 0.36 | 0.04 | 10.5   | 100.1        |   |
| NBS-97A      | 43.7 · | 38.9  | 0.10 | 0.16 | 0.04              | 0.50             | 0.47  | 0.00 | 1.90 | 0.36 | 13.5   | 100.0        |   |
| CONTROL SAMP | 45.9   | 39.0  | 0.01 | 0.07 | 0.21              | 0.21             | 0.70  | 0.00 | 0.51 | 0.10 | 13.7   | 100.4        |   |

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particle size distribution curves are given in Appendix.

Percentage of free silica present in kaolin samples were determined by XRD techniques. Results are given in table 10. The free silica values obtained were very high. Attention was therefore focussed on further treatment of kaolin in order to determine in what size fraction the silica is concentrated and what would be the best way to reduce it.

#### KAOLIN FRACTIONATION

A composite was prepared for preliminary fractionation test, by the sedimentation technique. The objective was two fold. The first was to determine if the silica level could be reduced to less than 1% by conducting separations at 10 micron and 5 micron. The second was to determine if the free silica, contained in the kaolin was coarser than 10 micron. It was hoped that by fractionating the kaolin at 10 micron size, the silica would be retained in the coarse, plus 10 micron fraction.

These tests were carried out by standard sedimentation techniques, whereby kaolin slurry is allowed to settle in a tall cylinder and the settling time for particles coarser than 10 micron was calculated using Stoke's Law. At the prescribed time, the supernatant slurry was withdrawn, filtered and dried. The dried kaolin was analyzed for free silica and particle size distribution. Four separate tests were conducted. None of these tests were successful in reducing the free silica content to the desired level. As shown in table 11, the best result obtained was on a sample fractionated at 5 micron whereby the free silica content was reduced to 5.2 % - still unacceptably high.

Since Kaolin and silica have nearly identical specific gravities, both appear to behave similarly in a fluid medium. Sedimentation techiques

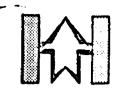
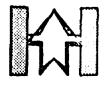


TABLE 10

# PERCENT "FREE SILICA" IN -325 MESH FRACTION

| Sample II | 2         | <pre>% Free -Quartz</pre> |
|-----------|-----------|---------------------------|
| SDT-1-3   |           | 35                        |
| -4        |           | 33                        |
| -6        |           | 55                        |
| -7        |           | 12                        |
| -8        |           | 12                        |
| -9        |           | 15                        |
| -10       |           | 19                        |
| -11       |           | 9                         |
| -13       |           | • 38                      |
| -14       |           | 19                        |
| -15       |           | 15                        |
| -16       |           | 12                        |
| -17       |           | 18                        |
| -18       |           | 16                        |
| SDT-1-20  | (Control) | 0                         |



#### TABLE 11

| PERCENTAGE | OF | "FREE | SILIC  | <u>A" II</u> | N SI | ZED  | FRACTI  | ONS |
|------------|----|-------|--------|--------------|------|------|---------|-----|
|            |    | 1     | Separa | ation        | !    | E Fi | cee Sil | ica |
| STD-15-2   |    |       | 10     | m            |      |      | 12.2    |     |
| 15-3       |    |       | 10     | m            |      |      | 7.0     |     |
| 15-4       |    |       | 5      | m            |      |      | 5.2     |     |

The free silica was determined using x-ray diffraction technique, comparing the samples against prepared samples of a commercial quality paper kaolin (containing no free silica) to which known quantities of -325 mesh ground quartz were added. A series of standards containing from 5 to 35% silica by weight were prepared.

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are therefore not very effective unless there is a significant difference in the particle size of the two minerals. Other techniques such as differential flocculation or microfloatation have been developed but are not commonly used in commercial kaolin processing.

It should be noted that the limited test work carried out was based upon a composite sample. Work on individual samples might have given different results.

#### SUMMARY OF ANALYTICAL STUDIES

The samples obtained from drillhole SDT-1 consist of silica, kaolin and other minor minerals such as chlorite, mica and some iron bearing minerals.

The <u>silica fraction</u> can be readily beneficiated to a quality consistent with the quality of silica sand used in the manufacture of flat, container or fiberglass. The silica is also suitable for blasting sand, filteration sand and as smelter flux.

Owing to the angularity of the silica grains, it is not suitable for foundary applications since foundary applications require a rounded sand.

<u>Kaolin</u>: Owing to contamination of kaolin with very fine silica, the quality of kaolin that can be extracted from the sample material is not up to the standards required for paper coating applications.

The kaolin may be suitable as a "paper filling"grade kaolin since higher levels of free silica can be tolerated in paper filling.

### CONCLUSIONS & RECOMMENTATIONS

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The following conclusions and recommendations emerge regarding the technical, geological and analytical aspects of the project:

#### **TECHNICAL ASPECTS**

1. Sonic drilling combined with NQ wire line drilling is a viable combination of techniques for obtaining high quality samples from unconsolidated sediments overlying bedrock. With the presently available equipment sonic drilling can be easily carried out upto a depth of about 100 metres. Probing any deeper is uneconomical and poses technical problems. Development of a wire line system may make it economical to drill deeper than 100 metres with the sonic drill.

2. The weight of the equipment imposes limitations on the mobility of the rig especially in muskeg terrain. Advance reconnaissance of the area and suitable preparation of access routes is recommended.

3. The alternation of highly compact clays and loose sands presents drilling problems in the subsurface. Such type of drilling requires great caution and skill.

#### GEOLOGICAL ASPECTS

Remarks about the geological aspects can be separated into those that apply to the area of drillholes J-1-2, SDT-1, and SDT-2 and those that apply to the area of holes SL 82-01 to 82-04.



#### Area of drillholes J-1-2, SDT-1 and SDT-2

 Area in the vicinity of drillholes SDT-1 and J-1-2 has a thick sequence of the upper Mattagami type B sediments containing impressive thicknesses of silica sand kaolin mixtures. These deposits are an almost unlimited source of silica sand and kaolin.

2. Quaternary overburden in the area of drillhole J-1-2 is only 17 metres offering encouraging possibilities for low cost open-pit mining of the silica sand and kaolin. The lateral extent of the shallow overburden in the vicinity of this hole may be determined by carrying out exploratory drilling on a small (100 m ) grid.

3. Quaternary overburden in the central part of the area of licence of Occupation No. 14888 appears to be very thick. Northern portions of this area have not been investigated. Area to the noth of hole SDT-2 may require some drilling.

4. Lignite seams encountered in hole J-1-2 combined with similar beds found in earlier drilling near the banks of Adam Creek warrant further exploratory work to determine if lignite in sufficient quantities occurs near the surface.

#### Area of drillholes SL 82-01. 82-02, 82-03, and 82-04

Within the Mattagami Formation, the occurrence of a lower,
 black clay-lignite association (type A lithology) and an upper,
 silica sand-clay association (type B lithology) is confirmed. Lignite
 can only be expected to occur where the lower association is well developed.



2. Thick lignite seams encountered earlier in drillhole 78-06 do not extend southeastwards from this hole. This may be partly due to the thinning of the Cretaceous sediments to the southeast or the lesser development of lignite bearing type A Mattagami sediments.

3. Any future efforts to find the continuity of lignite found in hole 78-06 should be directed to the north, west and northwest of hole 78-06. It is not necessary to carry out an expensive grid drilling program for this purpose - only one hole in each direction may suffice.

4. The Cretaceous sediments of the Mattagami Formation do not persist laterally to any great distances. Any future drilling program should be planned bearing this in mind.

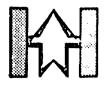
#### ANALYTICAL ASPECTS

Analysis of selected samples of silica sand-kaolin mixtures from a thick sequence of these deposits found in hole SDT-1 has revealed that:

1. The silica sand is of high quality and purity. Glass sand grade fraction is present in good proportion. The glass sand can be easily beneficiated with magnetic means.

The average percentage of kaolin in these mixtures is about
 13 %. Values as high as 20 percent were recorded.

3. The kaolin recovered from the samples may be suitable for paper filling applications.



4. The kaolin recovered from the samples has unacceptably high concentrations of fine free silica. For this reason it is not upto standards required for paper coating.

Limited separation tests on a composite sample employing conventional sedimentation techniques have failed to reduce the level of free silica to acceptable levels.

5. Further work is recommended to determine if the free silica can be effectively separated from the kaolin fraction. This work should utilize individual samples, not composites.

6. Depending upon the success of the above work efforts should be made to determine the optimum techniques for bleaching and for defining the rhelogical properties of the kaolin.



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Ministry of Natural Resources

60 Wilson Avenue Timmins, Ontario P4N 2S7

Our file number

| Your file | ASSECSMENT FILED<br>RESEARCH CARGE |
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Memorandum to:

Assessment Files Research Office 77 Grenville Street Room 802 Toronto, Ontario

Date: July 21, 1982

Subject: Geotechnical Report entitled:

Exploration Activities on Lands Granted Under

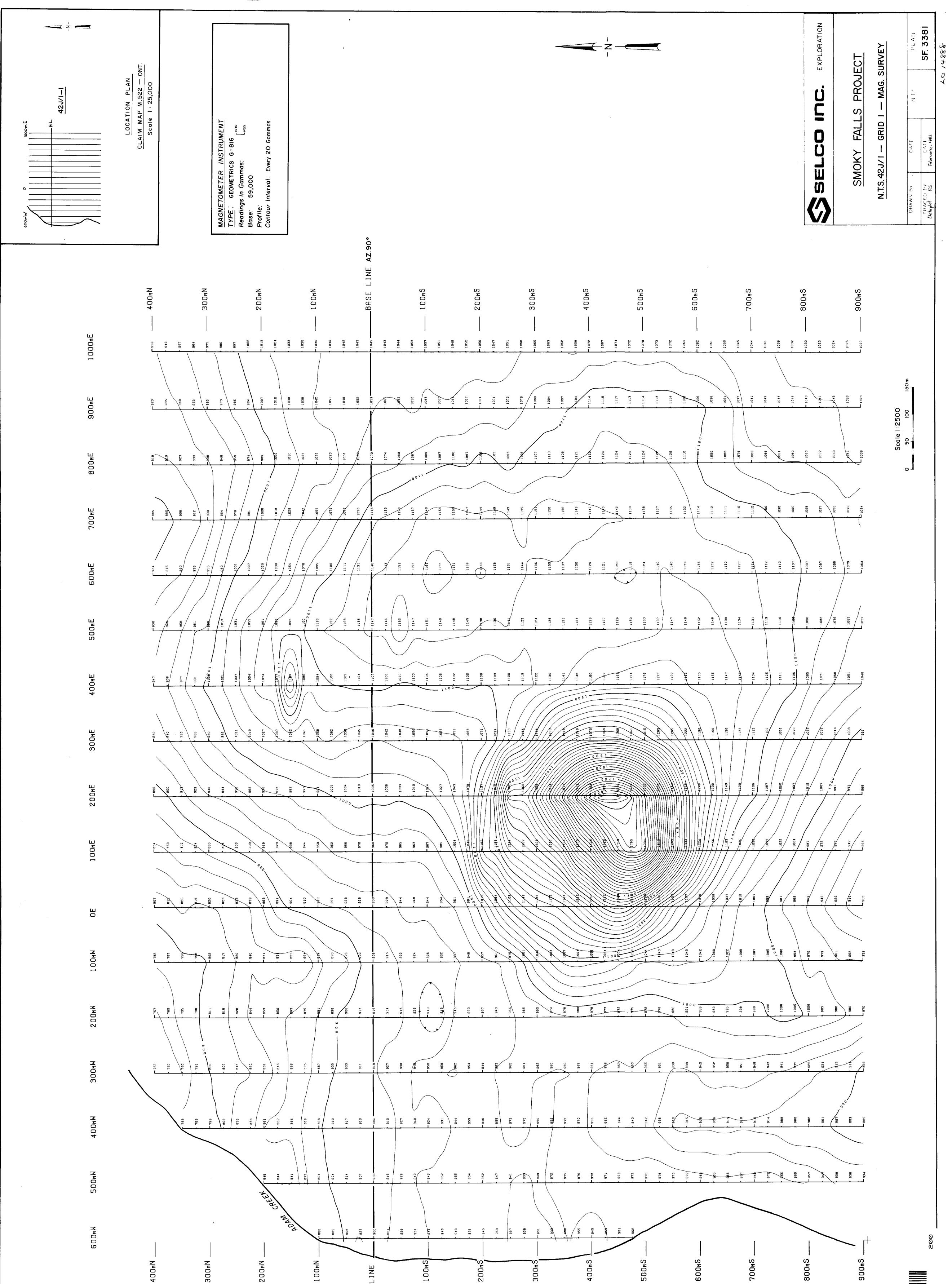
Licence of Occupation No. 14888 (1981-1982) The geotechnical report(s) attached hereto have been submitted by Selco Inc.

persuant to the terms of Exploratory Licence of Occupation Number 14888 . We have reviewed the report and approved it as a portion of the annual exploration obligation for the first term of this licence.

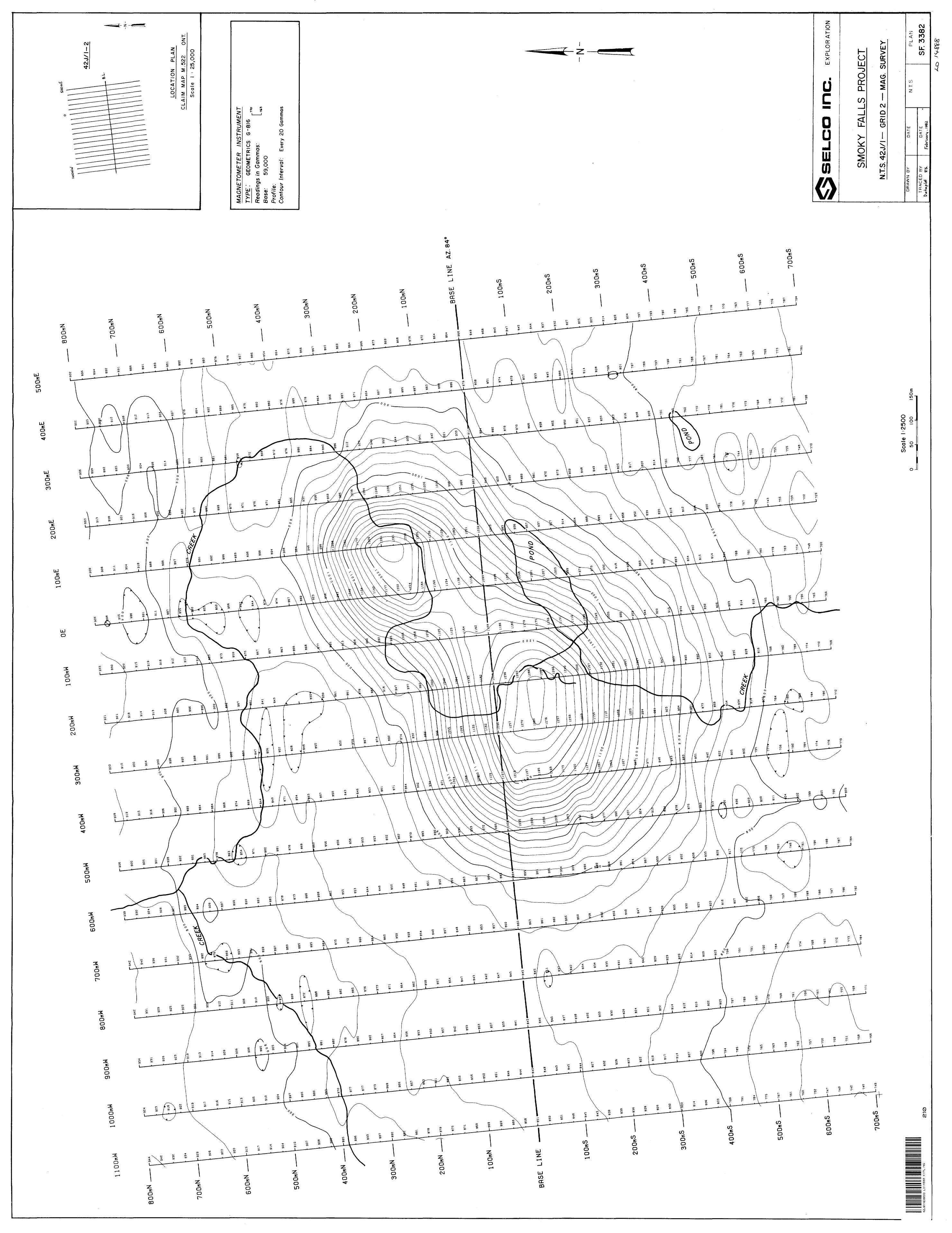
It is understood by the licencee that this assessment work, when approved, is to form part of the public record, and accordingly, may now be placed on file.

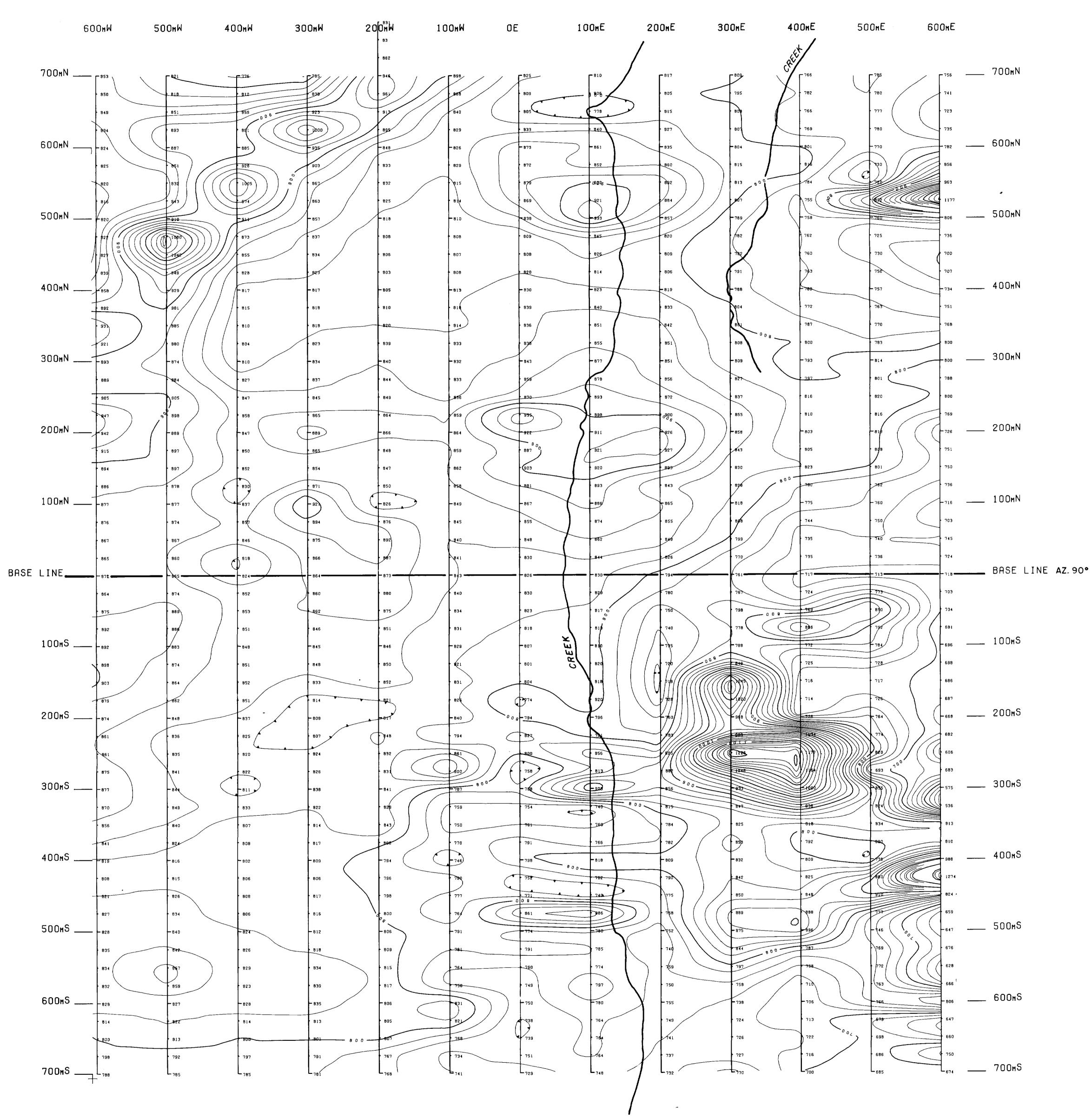
Resident Geologist Sub-Regional Office, Nothern Region Timmins, Ontario

c.c. Mining Recorders Office - Timmins



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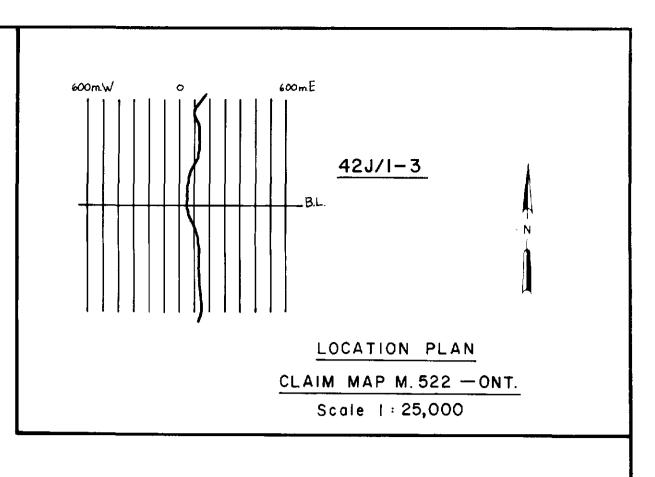




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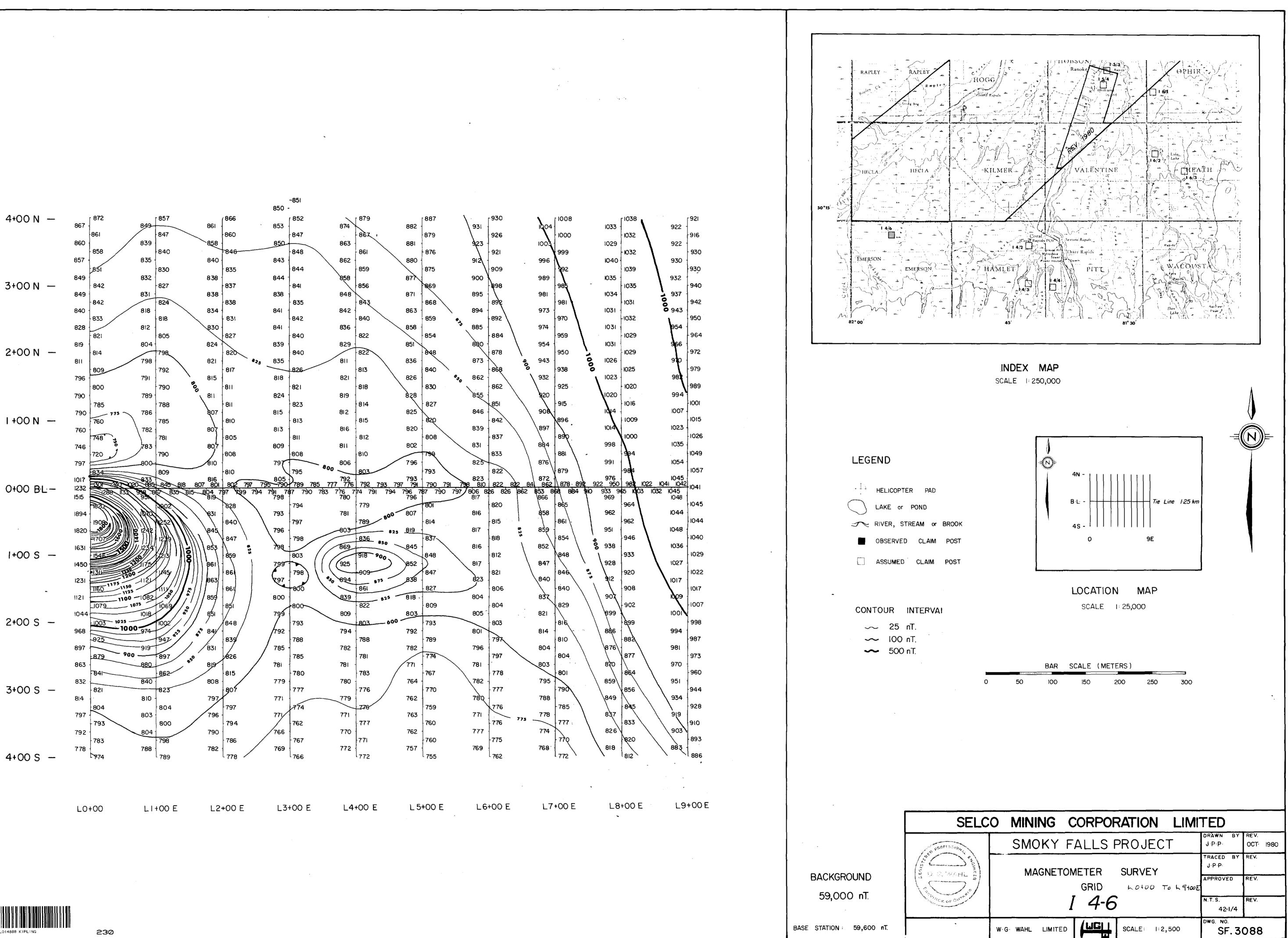
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# SMOKY FALLS PROJECT

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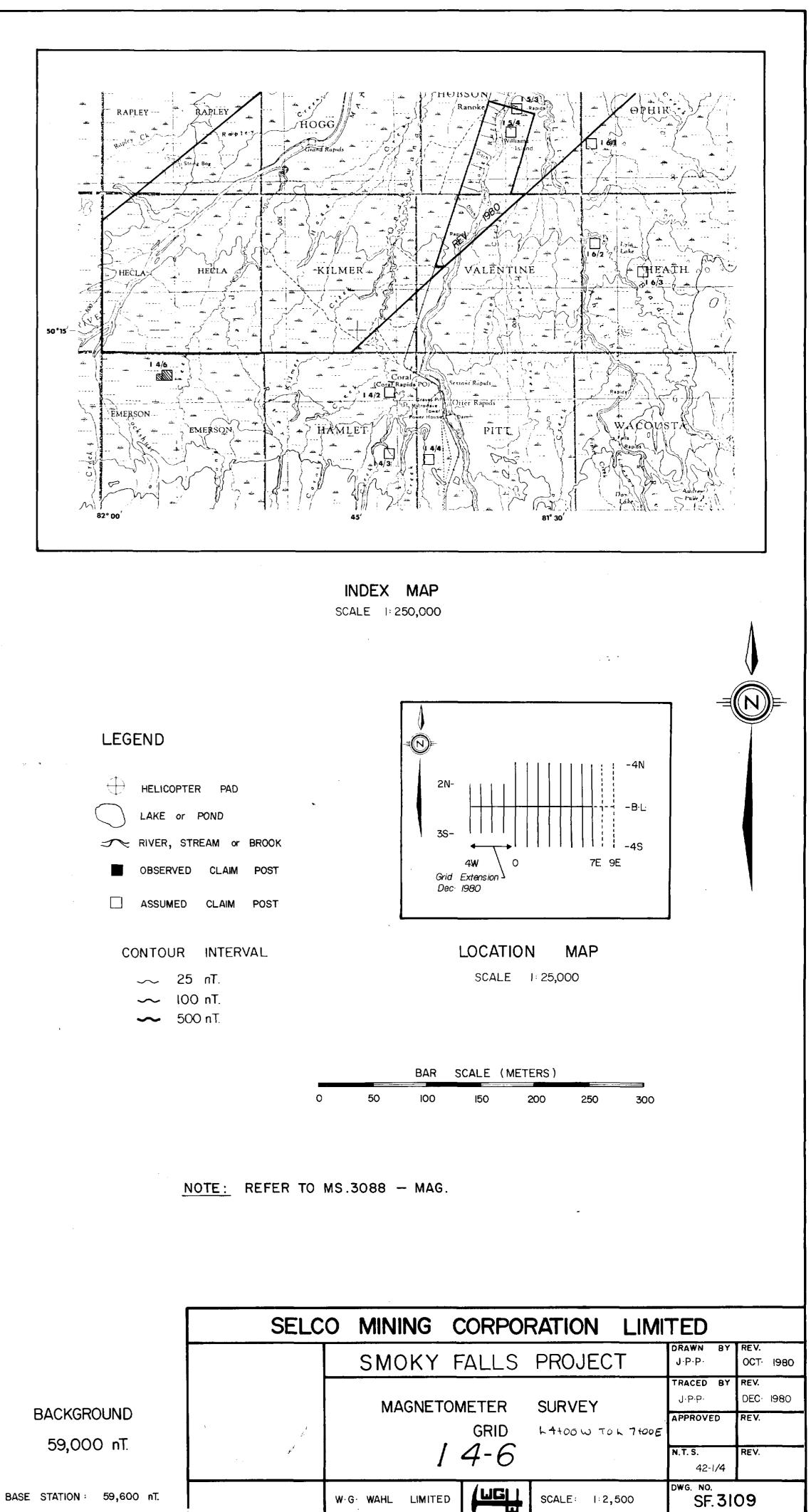




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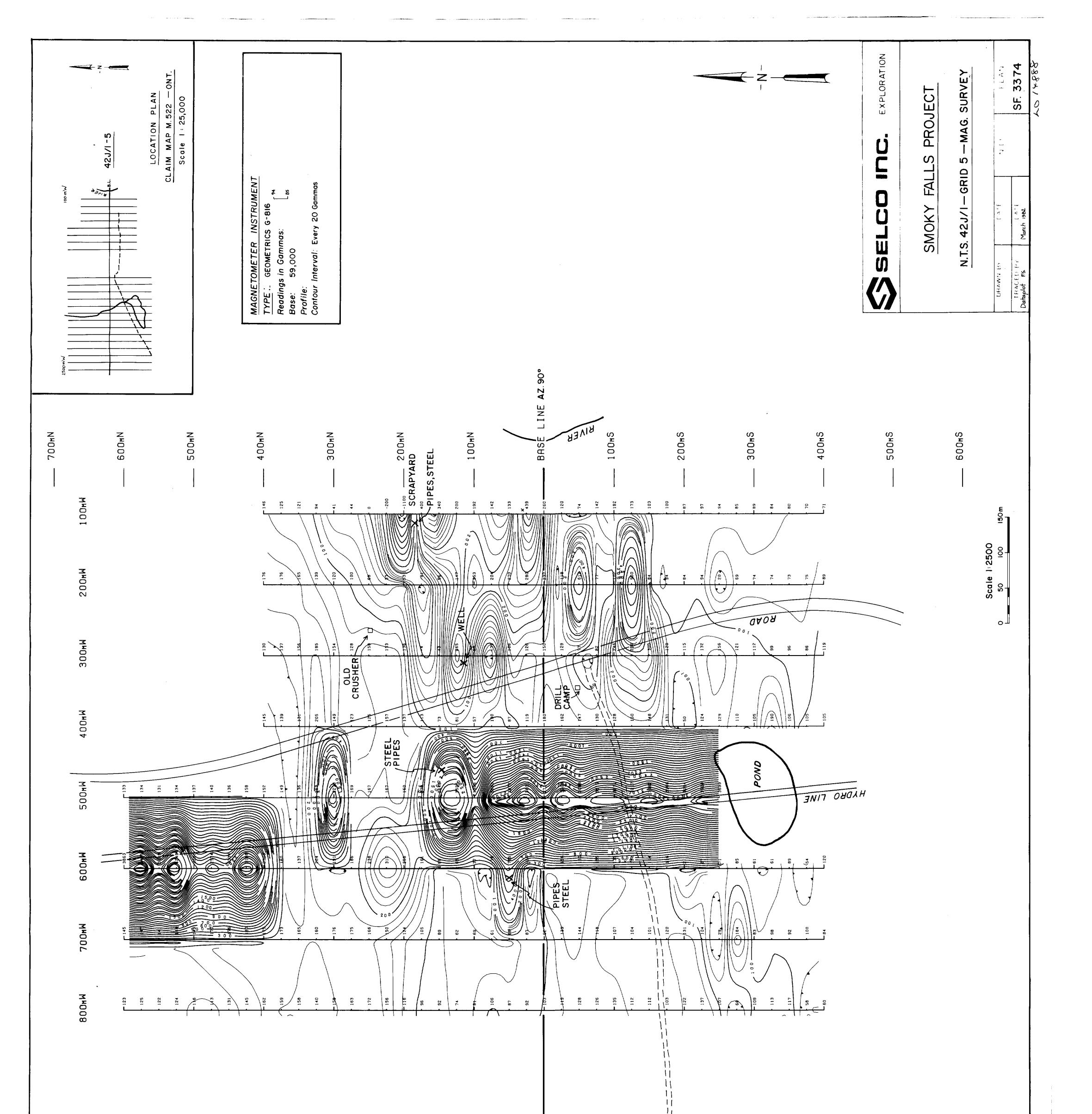
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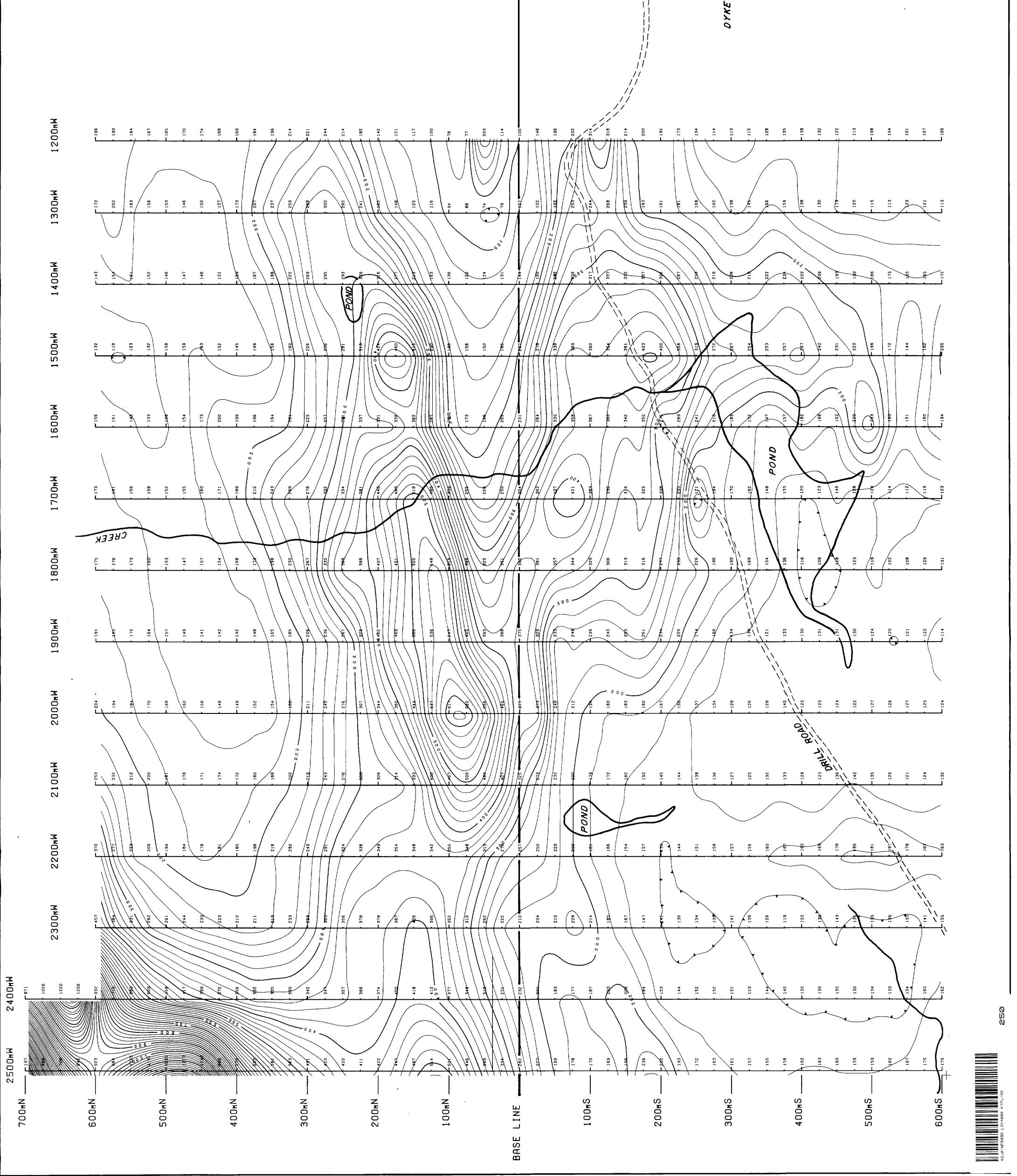
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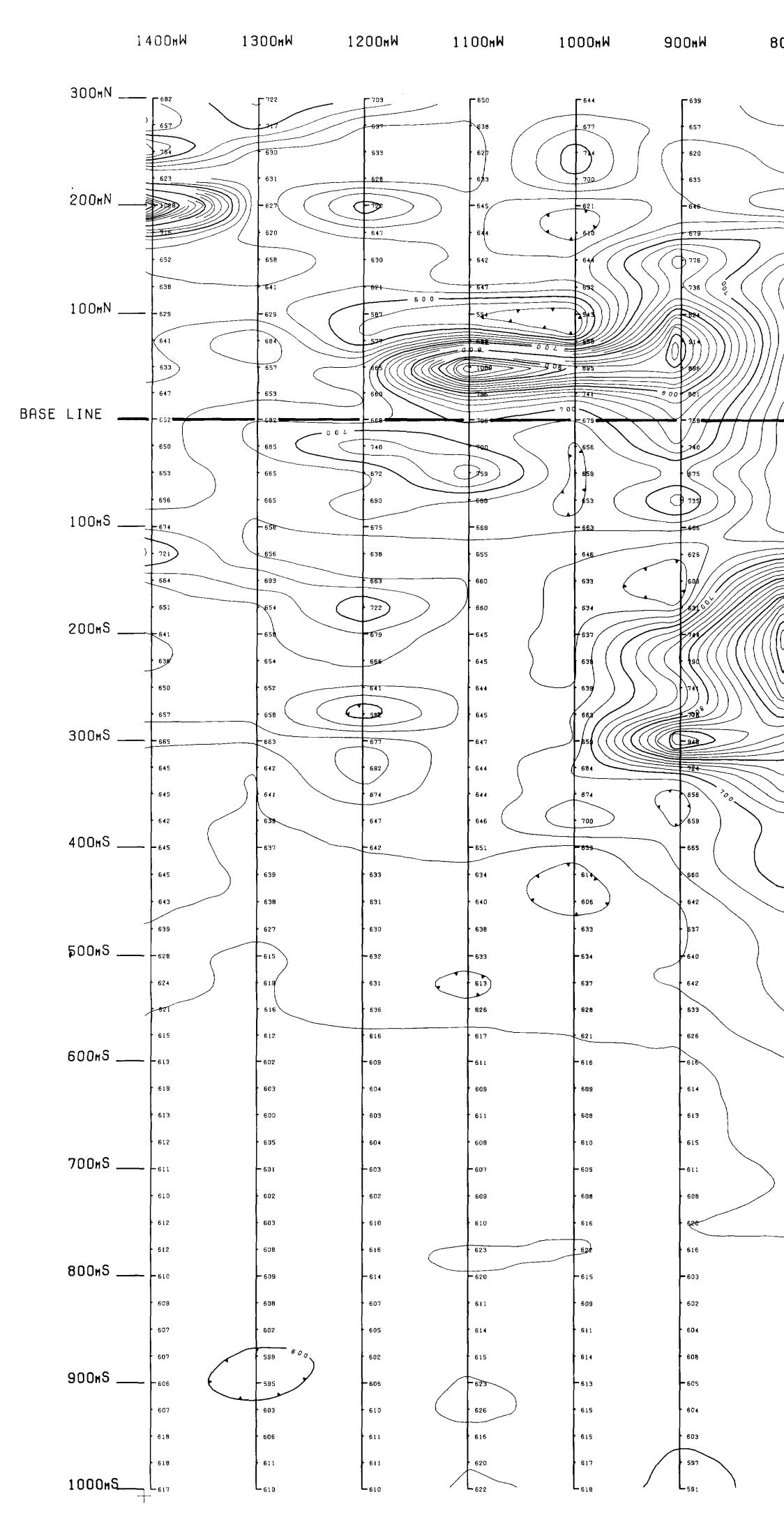


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