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REPORT ON COMBINED HELICOPTER BORNE MAGNETIC, ELECTROMAGNETIC AND VLF SURVEY CADMAN LAKE AND KEEZHIK LAKE PROPERTIES FORT HOPE AREA, ONTARIO

> for **RECEIVED** NORAMCO EXPLORATIONS INC. by NOV 24 1987 AERODAT LIMITED MINING LANDS SECTION OCTOBER 28, 1987

> > R. J. de Carle Consulting Geophysicist

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LIST OF MAPS

(Scale 1:10,000)

- MAPS: (As listed under Appendix "B" of the Agreement)
- TOPOGRAPHIC BASE MAP; topographic base map enlarged from a 1:50,000 topographic map, showing registration crosses corresponding to NTS co-ordinates on survey maps.
- FLIGHT LINE MAP; showing all flight lines and fiducials.
- 3. AIRBORNE ELECTROMAGNETIC SURVEY INTERPRETATION MAP; showing flight lines, fiducials conductor axes and anomaly peaks along with inphase amplitudes and conductivity thickness ranges for the 4600 Hz coaxial coil system.
- TOTAL FIELD MAGNETIC CONTOURS; showing magnetic values contoured at 5 nanoTesla intervals, flight lines and fiducials.
- 5. VERTICAL MAGNETIC GRADIENT CONTOURS; showing magnetic gradient values contoured at 1 nanoTeslas per metre.
- 6. APPARENT RESISTIVITY CONTOURS; showing contoured resistivity values, flight lines and fiducials.
- 7. VLF-EM TOTAL FIELD CONTOURS; showing VLF-EM values contoured at 1% intervals, flight lines and fiducials.
- 8. ACETATE OVERLAY OF TOTAL FIELD MAGNETICS; showing magnetic values contoured at 5 nanoTesla intervals, flight lines and fiducials.

1. INTRODUCTION

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This report describes an airborne geophysical survey carried out on behalf of Noramco Explorations Inc. by Aerodat Limited. Equipment operated included a three frequency electromagnetic system, a high sensitivity cesium vapour magnetometer, a two frequency VLF-EM system, a film tracking camera, an altimeter and an electronic positioning system. Electromagnetic, magnetic and altimeter data were recorded both in digital and analog form. Positioning data were stored in digital form and recorded on film as well as being marked on the flight path mosaic by the operator while in flight.

The survey, comprised of two separate blocks of ground in the Fort Hope Area, Kenora Mining District of northern Ontario, are located in the general proximity of Keezhik Lake (Block B) and Cadman Lake (Block C). Four flights were required to complete the survey and were flown on September 21 and 22, 1987. Flight lines, for each block, were oriented 000-180 degrees with a nominal line spacing of 100 metres. Coverage and data quality were considered to be well within the specifications described in the contract.

The survey objective is the detection and location of mineralized zones which can be directly or indirectly related to precious or base metal exploration targets. Of importance, therefore, are poorly mineralized conductors, displaying weak conductivity, which may represent structural features which can sometimes play an essential role in the eventual location of primary minerals. Weak conductors associated with iron formations are also considered primary targets for precious metals. In regard to base metal targets, short, isolated or flanking conductors displaying good conductivity and having either magnetic correlation or no magnetic correlation, are all considered to be areas of extreme interest.

A total of 615 kilometres of the recorded data were compiled in map form and are presented as part of this report according to specifications outlined by Noramco Explorations Inc.

The following is a summary of the total mileage for each of the flown blocks:

Block	Area Name	Mileage (kms)
В	Keezhik Lake	430
С	Cadman Lake	185

2. SURVEY AREA LOCATION

2 - 1

The survey areas are depicted on the index map as shown. All blocks are located to the north of the Albany River, with the two blocks being some 20 kilometres north-northeast of Miminiska Lake. They are also located approximately 40 kilometres northwest of Fort Hope, Ontario. The following is a brief summary for each area location:

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Block B Keezhik Lake
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Latitude 51 degrees 47' north NTS 52P9, 15, 16 Longitude 88 degrees 32' west

Cadman Lake Block C NTS 52P16

Latitude 51 degrees 46' north Longitude 88 degrees 23' west



3. AIRCRAFT AND EQUIPMENT

3.1 Aircraft

An Aerospatiale A-Star 350D helicopter, (C-GJIX), owned and operated by Ranger Helicopters Limited, was used for the survey. Installation of the geophysical and ancillary equipment was carried out by Aerodat. The survey aircraft was flown at a mean terrain clearance of 60 metres.

3.2 Equipment

3.2.1 Electromagnetic System

The electromagnetic system was an Aerodat 3-frequency system. Two vertical coaxial coil pairs were operated at 935 Hz and 4600 Hz and a horizontal coplanar coil pair at 4175 Hz. The transmitter-receiver separation was 7 metres. Inphase and quadrature signals were measured simultaneously for the 3 frequencies with a time constant of 0.1 seconds. The electromagnetic bird was towed 30 metres below the helicopter.

3.2.2 VLF-EM System

The VLF-EM System was a Herz Totem 2A. This instrument measures the total field and quadrature components of two selected transmitters, preferably oriented at right angles to one another. The sensor

was towed in a bird 12 metres below the helicopter. The transmitters monitored were Jim Creek, Washington, broadcasting at 24.8 kHz, and Annapolis, Maryland, broadcasting at 21.4 kHz

3.2.3 Magnetometer

The magnetometer employed a Scintrex Model VIW-2321 H8 cesium, optically pumped magnetometer sensor. The sensitivity of this instrument was 0.1 nanoTeslas at a 0.2 second sampling rate. The sensor was towed in a bird 12 metres below the helicopter.

3.2.4 <u>Magnetic Base Station</u>

An IFG-2 proton precession magnetometer was operated at the base of operations to record diurnal variations of the earth's magnetic field. The clock of the base station was synchronized with that of the airborne system to facilitate later correlation.

3.2.5 Radar Altimeter

A King Air radar altimeter was used to record terrain clearance. The output from the instrument is a linear function of altitude for maximum accuracy.

3.2.6 Tracking Camera

A Sony video tracking camera was used to record flight path on VHS video tape. The camera was operated in continuous mode. Fiducial numbers and time reference marks, for cross reference to the analog and digital data, were encoded on the tape.

3.2.7 Analog Recorder

An RMS dot-matrix recorder was used to display the data during the survey. In addition to manual and time fiducials, the following data were recorded:

Channel	Input	Scale
CXII	Low Frequency Inphase	2.0 ppm/mm
CXQ1	Low Frequency Quadrature	2.0 ppm/mm
CXI2	High Frequency Inphase	2.0 ppm/mm
CXQ2	High Frequency Quadrature	2.0 ppm/mm
CPI1	Mid Frequency Inphase	8.0 ppm/mm
CPQ1	Mid Frequency Quadrature	8.0 ppm/mm
VLT	VLF-EM Total Field, Line	2.5%/mm
VLQ	VLF-EM Quadrature, Line	2.5%/mm
VOT	VLF-EM Total Field, Ortho	2.5%/mm
VOQ	VLF-EM Quadrature, Ortho	2.5%/mm

Channel	Input	Scale	
ALT	Altimeter	10 ft/mm	
MAGF	Magnetometer, fine	2.5 nT/mm	
MAGC	Magnetometer, coarse	25 nT/mm	
MAGN	Magnetometer, noise	0.025 nT/mm	

3.2.8 Digital Recorder

A DGR 33 data system recorded the survey on magnetictape. Information recorded was as follows:EquipmentRecording IntervalEM system0.1 secondsVLF-EM0.5 secondsMagnetometer0.2 secondsAltimeter0.5 secondsNav System1.0 seconds

Positional information was recorded at 1.0 second intervals on a DAC/NAV I.

4. DATA PRESENTATION

4.1 Base Map

A topographic base at a scale of 1:10,000 was prepared from an enlargement of a 1:50,000 topographic map.

4.2 Flight Path Map

The flight path for all blocks was derived from the Mini-Ranger radar positioning system. The distance from the helicopter to two established reference locations was measured several times per second and the position of the helicopter calculated by triangulation. It is estimated that the flight path is generally accurate to about 10 metres with respect to the topographic detail of the base map.

The flight path map showing all flight lines, are presented on a Cronaflex copy of the topographic base map, with camera frame and navigator's manual fiducials for cross reference to both the analog and digital data.

4.3 Airborne Electromagnetic Survey Interpretation Map

The electromagnetic data were recorded digitally at a sample rate of 10 per second with a time constant of 0.1 seconds. A two stage digital filtering process was carried out to reject major sferic events and to reduce system noise.

Local sferic activity can produce sharp, large amplitude events that cannot be removed by conventional filtering procedures. Smoothing or stacking will reduce their amplitude but leave a broader residual response that can be confused with geological phenomena. To avoid this possibility, a computer algorithm searches out and rejects the major sferic events.

The signal to noise ratio was further enhanced by the application of a low pass digital filter. It has zero phase shift which prevents any lag or peak displacement from occurring, and it suppresses only variations with a wavelength less than about 0.25 seconds. This low effective time constant permits maximum profile shape resolution.

Following the filtering process, a base level correction was made. The correction applied is a linear function of time that ensures the corrected amplitude of the various inphase and quadrature components is zero when no conductive or permeable source is present. The filtered and levelled data were used in the interpretation of the electromagnetics.

An interpretation map was prepared showing peak locations of anomalies and conductivity thickness ranges along with the

Inphase amplitudes (computed from the 4600 Hz coaxial response) and conductor axes. The anomalous responses of the three coil configurations along with the interpreted conductor axes were plotted on a Cronaflex copy of the topographic base map.

4.4 Total Field Magnetic Contours

The aeromagnetic data were corrected for diurnal variations by adjustment with the digitally recorded base station magnetic values. No correction for regional variation was applied. The corrected profile data were interpolated onto a regular grid at a 25 metre true scale interval using a cubic spline technique. The grid provided the basis for threading the presented contours at a 5 nanoTesla interval.

The contoured aeromagnetic data have been presented on a Cronaflex copy of the topographic base map.

4.5 Vertical Magnetic Gradient Contours

The vertical magnetic gradient was calculated from the gridded total field magnetic data. Contoured at a 1 nT/m interval, the gradient data were presented on a Cronaflex copy of the topographic base map.

4.6 Apparent Resistivity Contours

The electromagnetic information was processed to yield a map of the apparent resistivity of the ground.

The approach taken in computing apparent resistivity was to assume a model of a 200 metre thick conductive layer (i.e., effectively a half space) over a resistive bedrock. The computer then generated, from nomograms for this model, the resistivity that would be consistent with the bird elevation and recorded amplitude for the 4600 Hz coaxial frequency pair used. The apparent resistivity profile data were interpolated onto a regular grid at a 25 metres true scale interval using a cubic spline technique.

The contoured apparent resistivity data were presented on a Cronaflex copy of the topographic base map with the flight path.

4.7 VLF-EM Total Field Contours

The VLF-EM signals from NLK, Jim Creek, Washington, broadcasting at 24.8 kHz were compiled. The VLF data were compiled in contour map form and presented on a Cronaflex copy of the topographic base map.

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5. INTERPRETATION

5.1 Geology

The map area lies within the Uchi Subprovince, a predominately metavolcanic-metasedimentary east trending belt in the Superior Province of the Canadian Shield. With the exception of a few wide, north trending dikes of Middle Precambrian diabase, all the rocks in the area are Early Precambrian in age. Quaternary deposits of glacial till, and glaciolacustrine and glaciofluvial sand and gravel now cover much of the bedrock.

Towards the northwest portion of the Cadman Lake property, there exists a porphyritic flow complex as well as a guartzfeldspar porphyry package of rocks. Traversing in a northwestsoutheast direction, through the middle of the East Arm, is a mafic intrusive body which has been described as being anorthositic gabbro to gabbro. The remainder of the Cadman Lake block, according to those geology maps available to the writer, would appear to be underlain with massive to foliated basalt to andesite (Fort Hope-Lansdowne House Sheet, Map 2237).

However, referring to Map 55-1963, Miminiska Area, Ontario, it will be noted that towards the extreme northwest corner of the Cadman Lake block, there exists an acidic volcanic rock unit, in contact with the aforementioned gabbro complex. As well, it will be seen that a banded iron formation has been mapped towards the extreme northeast corner of the block. In fact, it is located just outside of the survey boundary.

The Keezhik Lake block is underlain with much the same rock as those for the Cadman Lake block. The western half of the block is underlain with pillowed basalt to andesite while towards the east, the rocks are mainly massive to foliated basalt to andesite. Along the northern boundary of the survey block, areas of rhyolite to dacite rocks have been mapped. The same gabbroic rocks that were indicated within the Cadman Lake block, also extend into the eastern portion of the Keezhik Lake block.

Porphyritic flows or quartz-feldspar porphyry have also been mapped towards the eastern section of the block. It is also the same package of rocks which extend into the Cadman Lake block.

5.2 Magnetics

The magnetic data presentation for the Keezhik Lake block has shown an approximate northeast-southwest trending lithology.

Individual magnetic trends are interpreted to be interlayering of basalt to andesitic bedding. Towards the northwest boundary, the higher intensity magnetic trends may be related to banded iron formation. As well, the higher intensity portions towards the northeast corner of the block are probably related to the anorthositic gabbro that has been mentioned previously.

There would appear to be one diabase dyke within the survey block and it is located towards the north-central portion of the block. Its extent to the south may be limited, but upon further examination in the field, the diabase dyke may be found to extend well beyond the southern boundary. In fact, the writer believes this to be the case.

The lower intensity magnetic areas are perhaps related to the felsic volcanics, especially towards the eastern portion of the Keezhik Lake block. It is quite a large area, somewhat circular, just to the west of the assumed gabbroic intrusive rock unit.

Some of the northeast-southwest trending lower intensity magnetic features may be related to metasedimentary rocks as this rock is known to exist within the survey block.

The attitude of the metavolcanic-metasedimentary package of rocks would appear to be, for the most part, towards the south, with some areas being steeply dipping or near vertical.

The high intensity magnetic feature traversing across the northeastern portion of the Cadman Lake block is related to a banded iron formation which has been indicated on geology map 54-1963. Some of the other higher intensity, elongated magnetic features within the East Arm of Keezhik Lake are thought to be related to anorthositic gabbro. Lower intensity areas may be related to massive to foliated basalt and andesite.

5.3 Vertical Magnetic Gradient Contours

The vertical gradient data has clearly defined the northeastsouthwest trending lithology within the Keezhik Lake block. It has separated these trends into unique horizons and actually, can be interpreted to correspond with a particular rock unit.

The areas of high intensity magnetics have been clearly "broken up" into unique trends as a result of the computation of the vertical gradient. This interpretation is not as readily obvious when one refers to the magnetic total field map.

It should also be noted that the zero contour interval coincides directly or very close to geological contacts. It is because of this phenomenon that the calculated vertical gradient map can be compared to a pseudo-geological map. By using known or accurate geological information and combining this data with the vertical gradient data, one can use the presented maps as a pseudo-geological map. Obviously, the more that is known about an area geologically, the closer this type of presentation is to what the rock types are.

This type of presentation is an invaluable tool in helping to define complex geology, especially in drift covered areas. Not only in areas of complex geology but in areas of closely spaced geologic formations, has the calculated vertical gradient computation been of exceptional value. Since a good portion of the survey blocks are overlain with Quaternary sand and gravel, this particular presentation will be very useful.

The writer has indicated several fault zones on the interpretation map. Because of the nature of the computation of the vertical gradient data, magnetic anomalies produced by near surface features are emphasized with respect to those resulting from more deeply buried rock formations. As a result, much more detail is obtained, providing a better op-

portunity to recognize fault zones. As mentioned, some fault zones have been interpreted by the writer, however, it will become more apparent to the client as more field geological information is obtained, that other fault zones do exist.

This presentation will also, perhaps, change the clients mind about certain geologic horizons and especially the location of contacts.

5.4 Electromagnetics

The electromagnetic data was first checked by a line-by-line examination of the analog records. Record quality was good with minor noise levels on the low frequency coaxial trace. This was readily removed by an appropriate smoothing filter. Instrument noise was well within specifications. Geologic noise, in the form of surficial conductors, is present, in some areas of the survey, on the higher frequency responses and to a minor extent, on both the low frequency inphase and quadrature response.

Anomalies were picked off the analog traces of the low and high frequency coaxial responses and then validated on the coplanar profile data. These selections were then checked with a proprietary computerized selection program which can be adjusted for ambient and instrumental noise. The data were then edited and re-plotted on a copy of the profile map. This procedure ensured that every anomalous response spotted on the analog data was plotted on the final map and allowed for the rejection - or inclusion if warranted - of obvious surficial conductors. Each conductor or group of conductors was evaluated on the bases of magnetic (and lithologic, where applicable) correlations apparent on the analog data and man made or surficial features not obvious on the analog charts.

RESULTS

As a result of this airborne survey being carried out, there were a number of bedrock conductors intercepted in both the Keezhik Lake and Cadman Lake blocks. Most display good electromagnetic responses with some having magnetic association while others seem to be flanking magnetic trends. Formational trends are quite apparent with most of these showing variable conductivity values along their strike lengths. These areas may be locations for accumulations of massive sulphides, of which, economic sulphides may exist. There are several conductors that are correlating with magnetic lows indicating that pyrite and/or graphite is the probable cause. There are a number of isolated one, two or three line conductive trends which the writer has outlined on the interpretation map. These are areas that have base metal potential. Also, note how a few of them have been cut off by inferred fault zones.

Referring to the high frequency quadrature trace, it will be seen that lake bottom sediments are quite conductive. As well, there are areas that reflect a thick layer of conductive overburden. However, it is felt that both of these conductive horizons did not act as a masking layer in preventing the detection of any weak bedrock conductors.

It is also interesting to note that the inphase responses for all frequencies are negative over horizons which display high intensity magnetic features. This is a reflection of the magnetite content. The higher the magnetite content, the more pronounced would be the negative electromagnetic response. Also, as can be seen from the results, there are no electrical conductors associated with this geological horizon, with the exception of ZONES K16 and C-10, suggesting the absence of any sulphides within these assumed highly magnetic banded iron formation.

The writer has outlined on the map, selected targets which have been assigned a number. It is recommended that each zone be given a thorough investigation in regards to geology and previous work carried out. A brief comment is given for each of these zones along with a priority rating, 1-high, 2-medium, 3-low.

ZONE K-1

The conductor displays a reasonable electromagnetic response and one that, for the most part, has magnetic correlation. The trend no doubt extends to the west, beyond the western boundary of the Keezhik Lake block. However, it appears to have been pinched out towards the east near line 11700. A dip to the south is interpreted. The rock types in the area are thought to be pillowed basalt to andesite.

The target may be at depth because it is known that a layer of Quaternary sand and gravel exists in the area, as well, the conductor is located within Keezhik Lake. Priority 2.

ZONE K-2

The short trend would appear to be on the south flank of a magnetic feature, which is located approximately 50 metres north of K-2. A wide, vertical dyke-like conductor is

interpreted for K-2, as well as being located at depth. The latter could be due to the thick lake bottom sediments as well as the layer of sand and gravel. Pillowed basalt and andesite are thought to be the rock types. Priority 3.

ZONE K-3

The long conductor, which is dipping to the south, displays reasonably good conductivity and is flanking a magnetic feature which is located approximately 50 metres to the south. It is thought that the conductive trend is associated with a geological contact. It is also felt that K-3 may be related to the same bedrock source as that for K-6, K-9, K-10 and K-11, all being related to the same magnetic flank. Pillowed basalt and andesite are the rock types. Priority 3.

ZONE K-4

This short trend displays a weak electromagnetic response but it is still felt that the cause of this conductive response is related to a bedrock source. Its relationship with a magnetic feature may suggest pyrrhotite as the source. Priority 2.

ZONE K-5

This one line conductor is definitely an isolated, flanking anomaly to K-3. Its EM response is reasonable and it would appear to be correlating with the zero contour interval from the calculated vertical gradient data. The latter suggests a relationship with a geological contact. There may also be a fault zone just to the east of K-5. Pillowed basalt and andesite are thought to be the rock types. Priority 1.

ZONE K-6

This indicated trend displays an extremely weak electromagnetic response, and as suggested previously, may be associated with the same geological environment as that for K-3, K-9, K-10 and K-11. Priority 3.

ZONE K-7

The trend displays a very strong electromagnetic response and a preliminary indication is that K-7 is not related to the same source as that for K-8, primarily because of its relationship with a magnetic feature. The latter zone does not have any magnetic association. It is also felt that K-7 is close to a metasedimentary quartzite and conglomerate horizon. Priority 1.

ZONE K-8

This is an extremely long conductor displaying fair to poor conductivity along most of its strike length. As well, there

is no magnetic correlation. Pyrite is the probable cause. Areas in the vicinity of lines 11480, 11400, 11320 and 11280, however, display fair to good conductivity and perhaps, should be areas to be looked at. Any proximity to fault structures are locations to be investigated. Priority 3.

ZONE K-9

The outlined target displays a weak EM response and is correlating with the flank of a magnetic trend. As mentioned previously, it may be associated with the same geological horizon as K-3, K-6, K-10 and K-11. Priority 3.

ZONE K-10

This zone is thought to be related to the same source as that for K-11, however this one, has been faulted off. A dip to the south is interpreted. Priority 1.

ZONE K-11

The long conductor displays a very strong electromagnetic response and would seem to have little or no magnetic association, except for the extreme northern and southern ends of the trend. A dip to the south is interpreted. As mentioned previously, the extreme west end of the trend may have been faulted off. It is perhaps, in this area, that further work

may be considered. Towards the east end, where the writer has outlined ZONES K-11, K-12 and K-13, it is felt that further work in the field, in the form of a ground EM survey, should be carried out in order to accurately delineate the conductors. It is suggested, by the writer, that K-12 may be the eastern extent of K-11 with the present eastern extent of K-11 being an isolated conductor. Priority 2.

ZONES K-12 and K-13

The writer has combined these two for discussion because of the previously mentioned possible change in the interpretation. It should also be said that K-12 may extend well to the west. K-13 is probably isolated and as such, may turn out to be an interesting target. Referring to geology map 54-1963, it will be noted that acidic volcanic rocks have been mapped in the vicinity of the western extent of ZONE K-12, at the base of the peninsula. Priority 1.

ZONE K-14

This two line conductor is interpreted as a bedrock source which may be at depth. It is also correlating with a magnetic low suggesting an association with either graphite or pyrite. A ground survey is suggested. Priority 2.

ZONE K-15

This two line conductor displays a very weak electromagnetic response that may be related to a bedrock source. It is extremely weak. The trend is correlating with a magnetic low indicating that either pyrite or graphite may be the source. Pillowed basalt or andesite may be the rock type. Priority 3.

ZONE K-16

The zone displays a very good electromagnetic response as well as having good magnetic correlation. In fact, this may be the situation where sulphides is involved with a banded iron formation. It has a short strike length and interestingly enough, the sulphides do not seem to correlate with the magnetics along the remainder of the iron formation. Priority 1.

ZONES K17, K18 and K-19

All are long, linear trends displaying fair to good conductivity. As indicated on the interpretation map, the trends have been faulted off towards the west end and it may be in this area that further work is warranted. The EM responses are somewhat broad, suggesting that the conductors may be at depth. ZONES K-17 and K-18 are correlating with a magnetic trend suggesting pyrrhotite as the source while K-19



is correlating with a magnetic low indicating that either pyrite or graphite is the source. Priority 2.

ZONES K-20 and K-21

Both are extremely poor conductors. The two reasonable responses, which suggests that the responses may be bedrock related, are on line 11260. It is in this area that any further work should be concentrated. There does not seem to be any relationship with magnetics. The possibility exists that the interpreted fault zone, to the east, extends further to the south, to cut off the east end of both conductors K-20 and K-21. Priority 3.

ZONE K-22

The electromagnetic responses for this conductor are very poor and the writer interprets them as being possibly due to conductive lake bottom sediments. In fact, the trend may be related to an edge effect. Priority 3.

ZONE K-23

This lone intercept, in all probability, has a west extention to it, whereas it is probably limited, as to strike extent, to the east. It displays a fair EM response but does not have any magnetic correlation. The profile is somewhat broad, indicating perhaps a deep source. There is an esker nearby and this may have something to do with it. Priority 1.

ZONE K-24

The western extent of this conductor seems to be somewhat better defined than the east end and this could be related to the depth to the top of the conductor. It is also quite apparent from the electromagnetic traces that towards the east, the overburden as well as the lake bottom sediments, are quite conductive. This has certainly had a masking effect on the detection of the bedrock conductor. Any preliminary work on this zone should be carried out in the vicinity of intercept 10860A. There is also good magnetic correlation. Priority 1.

ZONE K-25

This lone intercept displays a fair EM response but one that is definitely due to a bedrock source. It also has good magnetic correlation. Referring to the topographic base map, it will be noted that the intercept would appear to be located within a swamp. Basalt and andesite may be the rock type. Priority 1.

ZONE K-26

The western extent of this trend may be related to conductive lake bottom sediments whereas the eastern portion is definitely due to a bedrock source. A northerly dip is interpreted. There is also magnetic correlation which suggests that pyrrhotite may be the source. Priority 1.

ZONE C-1

This isolated conductor has an extremely short strike length and would appear to be dipping towards the northwest. It displays a reasonably good electromagnetic response but has no magnetic association. Pyrite and/or graphite is the probable source. Basalt and andesite are thought to be the rock types. Priority 1.

ZONE C-2

The anomaly displays a rather broad electromagnetic response, one that is indicative of a deep target. Because of its location at the end of the flight line, it is not known whether or not the isolated response extends to the west. It is felt, however, that its eastern extent is limited. There is fair magnetic association. Priority 1.

ZONE C-3

The trend is definitely due to a bedrock source, which also has good magnetic correlation. It is interesting to note that even though there is a lengthy magnetic trend, the resultant conductivity is rather short. A dip to the north-northwest is interpreted. Priority 1.

ZONE C-4

This trend displays a good EM response but has only a subtle magnetic feature associated with it. A dip to the northeast is interpreted. There is every possibility that the fault zone interpreted to the south, may extend northward to cut off the east end of C-4. There is an esker in close proximity to C-4 so it may be found that the conductor is at depth. Priority 2.

ZONE C-5

The lone anomaly may be correlating with the banded iron formation which has been interpreted by the writer. It is also quite possible that the source for C-5 is the same as that for C-9. Priority 1.

ZONES C-6, C-7 and C-10

All three conductors are correlating with magnetic lows which flank the interpreted banded iron formation. ZONE C-6 is the



electromagnetic response. Priority 2.

ZONE C-8

This is an extremely weak electromagnetic response but one that is related to a poorly mineralized bedrock source. Its association with the flank of a magnetic feature suggests a relationship with a geological contact. Priority 2.

ZONE C-9

As mentioned previously, this conductor is associated with a banded iron formation. Its conductivity is quite good, as, of course, is its magnetic association. A dip to the north is interpreted. Sulphides within the iron formation is the cause. Although there seems to be a limited western extent, the conductor is thought to extend well to the east. Priority 1.

5.5 Apparent Resistivity

There are subtle similarities between the total field magnetics and the apparent resistivity data indicating a possible relationship with the bedrock. It does not appear, for the most part, that the apparent resistivity data is solely outlining conductive lake bottom sediments or conductive overburden. With this in mind, it is perhaps correct in suggesting a probable relationship with the basement rocks.

There is also good correlation between the selected targets and the apparent resistivity data. With the latter presentation, strike extent of the conductors is usually longer.

The background apparent resistivity for both survey blocks is generally in the 501 to 1000 ohm-metre range, with a few areas being somewhat less.

5.6 VLF-EM Total Field

Referring to the Keezhik Lake block, it will be noted that there are no similarities with the aeromagnetic data. The VLF tends to strike east-west to northwest-southeast, whereas the aeromagnetic data tend to strike northeast-southwest. Obviously, the VLF is not related to the basement but rather to possible overlying overburden. In the Cadman Lake block, however, there are similarities and thus, a possible relationship with the basement rocks.

Any structural information that may be forthcoming from the VLF data over the Keezhik Lake block could only be gained after a closer examination of the two sets of data. Much the

same synopsis can be made for the Cadman Lake block. There seems, however, to be signs of faulting within the Cadman Lake block.

In comparing the 3-frequency EM data with the VLF data, again it will be seen that there are no similarities between the two sets of data, in regards to the selected EM targets. However, if one refers to the quadrature responses of the 3-frequency EM and compare it to the VLF-EM data, then there does appear to be some correlation. The suggestion here is that the VLF may, in fact, be giving a representation of the conductive overburden.

5.7 <u>Recommendations</u>

On the basis of the results of this airborne survey, ground follow-up work is recommended for the selected targets as outlined by the writer on the interpretation map. Most of these zones would be primarily base metal targets because of their shorter strike lengths.

Because of the unobvious for the much longer conductors, in that conductances are similar, selecting areas for further follow up is difficult. Some of the conductive trends have magnetic association while others do not. As well, the geological picture is not as clear in order to give a geological-geophysical synopsis. It is, therefore, suggested that a geological reconnaissance survey of the areas be carried out, where possible, in order to establish a relationship between each of the intercepted bedrock conductors and the basement rocks. As mentioned previously, there is a thin layer of conductive overburden over most of the survey blocks, but outcrops do exist.

Over the more favourable areas geologically, till or soil sampling for gold is recommended with any correlation of subsequent anomalous areas and intercepted bedrock conductors being prime targets for drilling. Areas which may give promising results are those areas in close proximity to the interpreted fault zones as well as areas which are correlating with the banded iron formation.

In regards to a follow-up geophysical programme, any of the horizontal loop EM systems can be used. It would seem that detectability should be easy for any of the types of conductors intercepted within either of the two survey blocks. It is not
recommended, however, that a VLF-EM survey be carried out because of the apparent lack of detectability of the conductors with the airborne system. An induced polarization survey could be carried out if the area is overlain with a layer of highly conductive overburden or if the ground EM methods have not defined the conductors fully or if disseminated sulphides are suspected.

Some of the more interesting targets to investigate in the field include K-5, K-7, K-10, K-12 to K-14, K-16, K-24, K-25, C-1, C-3, C-4 and C-9.

Robert J. de Carle

Robert J. de Carle Consulting Geophysicist

for

AERODAT LIMITED October 28, 1987

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APPENDIX I

GENERAL INTERPRETIVE CONSIDERATIONS

Electromagnetic

The Aerodat three frequency system utilizes two different transmitter-receiver coil geometries. The traditional coaxial coil configuration is operated at two widely separated frequencies and the horizontal coplanar coil pair is operated at a frequency approximately aligned with one of the coaxial frequencies.

The electromagnetic response measured by the helicopter system is a function of the "electrical" and "geometrical" properties of the conductor. The "electrical" property of a conductor is determined largely by its electrical conductivity, magnetic susceptibility and its size and shape; the "geometrical" property of the response is largely a function of the conductor's shape and orientation with respect to the measuring transmitter and receiver.

Electrical Considerations

For a given conductive body the measure of its conductivity or conductance is closely related to the measured phase shift between the received and transmitted electromagnetic field. A small phase shift indicates a relatively high conductance, a large phase shift lower conductance. A small phase shift results in a large inphase to quadrature ratio and a large phase shift a low ratio. This relationship is shown quantitatively for a nonmagnetic vertical half-plane model on the accompanying phasor diagram. Other physical models will show the same trend but different quantitative relationships.

The phasor diagram for the vertical half-plane model, as presented, is for the coaxial coil configuration with the amplitudes in parts per million (ppm) of the primary field as measured at the response peak over the conductor. To assist the interpretation of the survey results the computer is used to identify the apparent conductance and depth at selected anomalies. The results of this calculation are presented in table form in Appendix II and the conductance and inphase amplitude are presented in symbolized form on the map presentation.

The conductance and depth values as presented are correct only as far as the model approximates the real geological situation. The actual geological source may be of limited length, have significant dip, may be strongly magnetic, its conductivity and thickness may vary with depth and/or strike and adjacent bodies and overburden may have modified the response. In general the conductance estimate is less affected by these limitations than is the

- 2 -

depth estimate, but both should be considered as relative rather than absolute guides to the anomaly's properties.

Conductance in mhos is the reciprocal of resistance in ohms and in the case of narrow slab-like bodies is the product of electrical conductivity and thickness.

Most overburden will have an indicated conductance of less than 2 mhos; however, more conductive clays may have an apparent conductance of say 2 to 4 mhos. Also in the low conductance range will be electrolytic conductors in faults and shears.

The higher ranges of conductance, greater than 4 mhos, indicate that a significant fraction of the electrical conduction is electronic rather than electrolytic in nature. Materials that conduct electronically are limited to certain metallic sulphides and to graphite. High conductance anomalies, roughly 10 mhos or greater, are generally limited to sulphide or graphite bearing rocks.

Sulphide minerals, with the exception of such ore minerals as sphalerite, cinnabar and stibnite, are good conductors; sulphides may occur in a disseminated manner that inhibits electrical

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conduction through the rock mass. In this case the apparent conductance can seriously underrate the quality of the conductor in geological terms. In a similar sense the relatively nonconducting sulphide minerals noted above may be present in significant consideration in association with minor conductive sulphides, and the electromagnetic response only relate to the minor associated mineralization. Indicated conductance is also of little direct significance for the identification of gold mineralization. Although gold is highly conductive, it would not be expected to exist in sufficient quantity to create a recognizable anomaly, but minor accessory sulphide mineralization could provide a useful indirect indication.

In summary, the estimated conductance of a conductor can provide a relatively positive identification of significant sulphide or graphite mineralization; however, a moderate to low conductance value does not rule out the possibility of significant economic mineralization.

Geometrical Considerations

Geometrical information about the geologic conductor can often be interpreted from the profile shape of the anomaly. The change in shape is primarily related to the change in inductive coupling among the transmitter, the target, and the receiver.

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In the case of a thin, steeply dipping, sheet-like conductor, the coaxial coil pair will yield a near symmetric peak over the conductor. On the other hand, the coplanar coil pair will pass through a null couple relationship and yield a minimum over the conductor, flanked by positive side lobes. As the dip of the conductor decreased from vertical, the coaxial anomaly shape changes only slightly, but in the case of the coplanar coil pair the side lobe on the down dip side strengthens relative to that on the up dip side.

As the thickness of the conductor increases, induced current flow across the thickness of the conductor becomes relatively significant and complete null coupling with the coplanar coils is no longer possible. As a result, the apparent minimum of the coplanar response over the conductor diminishes with increasing thickness, and in the limiting case of a fully 3 dimensional body or a horizontal layer or half-space, the minimum disappears completely.

A horizontal conducting layer such as overburden will produce a response in the coaxial and coplanar coils that is a function of altitude (and conductivity if not uniform). The profile shape will be similar in both coil configurations with an amplitude ratio (coplanar:coaxial) of about 4:1*.

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In the case of a spherical conductor, the induced currents are confined to the volume of the sphere, but not relatively restricted to any arbitrary plane as in the case of a sheet-like form. The response of the coplanar coil pair directly over the sphere may be up to 8* times greater than that of the coaxial pair.

In summary, a steeply dipping, sheet-like conductor will display a decrease in the coplanar response coincident with the peak of the coaxial response. The relative strength of this coplanar null is related inversely to the thickness of the conductor; a pronounced null indicates a relatively thin conductor. The dip of such a conductor can be inferred from the relative amplitudes of the side-lobes.

Massive conductors that could be approximated by a conducting sphere will display a simple single peak profile form on both coaxial and coplanar coils, with a ratio between the coplanar to coaxial response amplitudes as high as 8*.

Overburden anomalies often produce broad poorly defined anomaly profiles. In most cases, the response of the coplanar coils closely follows that of the coaxial coils with a relative amplitude ratio of 4*.

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Occasionally, if the edge of an overburden zone is sharply defined with some significant depth extent, an edge effect will occur in the coaxial coils. In the case of a horizontal conductive ring or ribbon, the coaxial response will consist of two peaks, one over each edge; whereas the coplanar coil will yield a single peak.

* It should be noted at this point that Aerodat's definition of the measured ppm unit is related to the primary field sensed in the receiving coil without normalization to the maximum coupled (coaxial configuration). If such normalization were applied to the Aerodat units, the amplitude of the coplanar coil pair would be halved.

Magnetics

The Total Field Magnetic Map shows contours of the total magnetic field, uncorrected for regional variation. Whether an EM anomaly with a magnetic correlation is more likely to be caused by a sulphide deposit than one without depends on the type of mineralization. An apparent coincidence between an EM and a magnetic anomaly may be caused by a conductor which is also magnetic, or by a conductor which lies in close proximity to a magnetic body. The majority of conductors which are also magnetic are sulphides containing pyrrhotite and/or magnetite. Conductive and magnetic

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bodies in close association can be, and often are, graphite and magnetite. It is often very difficult to distinguish between these cases. If the conductor is also magnetic, it will usually produce an EM anomaly whose general pattern resembles that of the magnetics. Depending on the magnetic permeability of the conducting body, the amplitude of the inphase EM anomaly will be weakened, and if the conductivity is also weak, the inphase EM anomaly may even be reversed in sign.

VLF Electromagnetics

The VLF-EM method employs the radiation from powerful military radio transmitters as the primary signals. The magnetic field associated with the primary field is elliptically polarized in the vicinity of electrical conductors. The Herz Totem uses three coils in the X, Y, Z configuration to measure the total field and vertical quadrature component of the polarization ellipse.

The relatively high frequency of VLF (15-25) kHz provides high response factors for bodies of low conductance. Relatively "disconnected" sulphide ores have been found to produce measureable VLF signals. For the same reason, poor conductors such as sheared contacts, breccia zones, narrow faults, alteration zones and porous flow tops normally produce VLF anomalies. The method can therefore be used effectively for geological mapping. The only

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relative disadvantage of the method lies in its sensitivity to conductive overburden. In conductive ground the depth of exploration is severely limited.

The effect of strike direction is important in the sense of the relation of the conductor axis relative to the energizing electromagnetic field. A conductor aligned along a radius drawn from a transmitting station will be in a maximum coupled orientation and thereby produce a stronger response than a similar conductor at a different strike angle. Theoretically, it would be possible for a conductor, oriented tangentially to the transmitter to produce no signal. The most obvious effect of the strike angle consideration is that conductors favourably oriented with respect to the transmitter location and also near perpendicular to the flight direction are most clearly rendered and usually dominate the map presentation.

The total field response is an indicator of the existence and position of a conductivity anomaly. The response will be a maximum over the conductor, without any special filtering, and strongly favour the upper edge of the conductor even in the case of a relatively shallow dip.

The vertical quadrature component over steeply dipping sheet-like

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conductor will be a cross-over type response with the cross-over closely associated with the upper edge of the conductor.

The response is a cross-over type due to the fact that it is the vertical rather than total field quadrature component that is measured. The response shape is due largely to geometrical rather than conductivity considerations and the distance between the maximum and minimum on either side of the cross-over is related to target depth. For a given target geometry, the larger this distance the greater the depth.

The amplitude of the quadrature response, as opposed to shape is function of target conductance and depth as well as the conductivity of the overburden and host rock. As the primary field travels down to the conductor through conductive material it is both attenuated and phase shifted in a negative sense. The secondary field produced by this altered field at the target also has an associated phase shift. This phase shift is positive and is larger for relatively poor conductors. This secondary field is attenuated and phase shifted in a negative sense during return travel to the surface. The net effect of these 3 phase shifts determine the phase of the secondary field sensed at the receiver.

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A relatively poor conductor in resistive ground will yield a net positive phase shift. A relatively good conductor in more conductive ground will yield a net negative phase shift. A combination is possible whereby the net phase shift is zero and the response is purely in-phase with no guadrature component.

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A net positive phase shift combined with the geometrical crossover shape will lead to a positive quadrature response on the side of approach and a negative on the side of departure. A net negative phase shift would produce the reverse. A further sign reversal occurs with a 180 degree change in instrument orientation as occurs on reciprocal line headings. During digital processing of the quadrature data for map presentation this is corrected for by normalizing the sign to one of the flight line headings. APPENDIX II

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ANOMALY LIST

LIGHT LINE ANOMALY CATEGORY AMPLITUDE (PPM) CTP DEPTH HEIGI 5 10021 A 0 1.7 6.5 0.0 0 80 5 10021 B 1 14.4 14.8 1.1 0 62 5 10030 A 0 20.5 35.9 0.6 0 48 5 10030 B 0 -0.4 18.6 0.0 0 62 5 10040 A 0 -0.4 18.6 0.0 0 46 5 10040 B 0 4.0 15.5 0.0 0 62 5 10040 C 0 2.4 8.4 0.0 0 54 5 10050 A 0 1.9 13.2 0.0 0 47 5 10050 B 0 -2.7 6.5 0.1 0 52	۱D
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5 10160 A 0 1.0 5.7 0.0 0 59)
5 10170 A 0 4.1 9.5 0.2 0 48	3
5 10180 A 0 5.5 7.3 0.5 0 59)
5 10190 A 1 18.2 20.1 1.1 0 46	;
5 10200 A 0 8.7 14.8 0.4 0 59 5 10200 B 0 13 0 44 5 0 2 0 40)
5 10200 B 0 13.9 44.5 0.2 0 49	,
5 10210 A 0 26.3 62.2 0.4 0 39)
5 10210 B 0 3.6 11.8 0.1 0 52	2
5 10220 A 0 3.3 6.7 0.2 0 71	L
5 10220 в 0 30.4 50.6 0.7 0 44	i
5 10230 A 0 13.2 51.3 0.1 0 42	2

					CONI	BIRD		
				AMPLITUD	E (PPM)	CTP	DEPTH	HEIGHT
LIGHT	LINE	ANOMALY	CATEGORY	INPHASE	QUAD.	MHOS	MTRS	MTRS
5	10230	В	0	12.2	19.9	0.5	0	55
5	10240	A	1	20.7	23.0	1.1	0	57
5	10250	A	1	42.0	43.2	1.6	0	48
5	10260	A	0	10.3	25.4	0.2	0	58
5	10280	A	0	4.3	12.0	0.1	0	51
5	10450	A	0	4.7	12.9	0.1	0	52
5	10460	A	0	9.9	15.0	0.5	0	57
5	10470	A	0	3.9	14.6	0.0	0	45
5	10510	A	0	8.2	18.8	0.2	0	57
5	10580	A	0	13.1	17.7	0.7	1	40
6	10740	A	0	18.9	34.9	0.5	0	43
6	10750	A	0	18.7	46.0	0.3	0	39
6	10760	A	0	9.1	28.4	0.2	0	45
6	10790	A	0	9.8	33.3	0.1	0	47
6	10790	В	0	7.4	54.5	0.0	0	37
6	10800	A	n	6.4	33.7	0.0	0	47
6	10800	В	õ	8.0	25.2	0.1	ŏ	50
6	10810	A	0	11.6	53.5	0.1	0	40
. 6	10820	A	0	6.1	32.9	0.0	0	48
6	10830	A	0	21.9	81.7	0.2	0	43
6	10840	A	0	10.3	40.9	0.1	0	49
6	10850	A	0	7.9	16.0	0.3	0	48
6	10860	A	0	7.8	13.4	0.4	0	53
6	10890	A	0	1.0	8.7	0.0	0	47

					CONI	BIRD		
	7 7 11 17		CAME CODY	AMPLITUD	E (PPM)	CTP	DEPTH	HEIGHT
LIGHT	LINE	ANOMALY	CATEGORY	INPHASE	QUAD.	MHOS	MTRS	MTRS
r	10000		0		16.2	• •	•	. 1
6	10900	A	0	1.1	16.2	0.0	0	41
6	10910	A	0	10.1	63.9	0.0	0	36
6	10920	A	0	8.8	53.5	0.0	0	41
6	10930	A	0	9.0	14.2	0.5	0	50
7	11071	A	0	9.3	45.4	0.1	0	43
7	11080	A	0	9.9	62.8	0.0	0	35
7	11090	A	0	8.1	30.2	0.1	0	54
7	11100	A	0	7.3	20.3	0.2	0	45
7	11100	в	0	9.6	34.3	0.1	0	51
7	11110	A	0	12.2	36.3	0.2	0	48
7	11110	В	õ	19.8	25.1	0.9	õ	48
7	11120	λ.	0	12 /	21 6	0 5	0	4.0
7	11120	B	0	13.4 13.2	35.5	0.5	0	40
-		-	•				•	
7	11130	A B	0	10.2	21.0	0.3	0	48 53
·		2	Ū	2010	2010	••••	v	00
7	11140	A	0	8.9	17.2	0.3	0	42
,	11140	Б	U	11.0	<i>22.2</i>	0.4	U	41
7	11150	A	0	11.0	17.5	0.5	0	49
7	11150	В	0	6.8	16.1	0.2	0	48
7	11160	A	0	5.4	21.7	0.1	0	48
7	11160	В	0	10.7	23.4	0.3	0	46
7	11170	A	0	8.4	16.2	0.3	0	49
7	11170	В	0	3.9	11.5	0.1	0	51
7	11180	A	0	7.3	26.6	0.1	0	44
7	11190	А	0	10.6	24-5	0.3	0	48
*			Ū.		2.10		Ŭ	
7	11200	A	0	3.5	11.0	0.1	0	41
1	TT200	ß	U	0./	42.4	0.0	U	51

Estimated depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or overburden effects.

1

						CONDUCTOR		
				AMPLITUD	E (PPM)	CTP	DEPTH	HEIGHT
LIGHT	LINE	ANOMALY	CATEGORY	INPHASE	QUAD.	MHOS	MTRS	MTRS
	• • • •							
7	11210	A	0	25.9	83.7	0.3	0	40
7	11210	B	Ō	13.5	57.6	0.1	Ō	41
7	11210	С	0	13.9	23.2	0.5	0	50
7	11220	A	0	7.5	19.4	0.2	0	49
7	11220	B	0	16.5	75.8	0.1	0	37
7	11220	С	0	20.4	81.1	0.2	0	39
7	11230	A	0	19.6	68.5	0.2	0	42
7	11230	B	0	12.4	28.5	0.3	0	45
7	11240	A	0	9.1	42.3	0.1	0	39
7	11240	В	0	5.5	48.8	0.0	0	38
7	11240	С	0	11.9	71.2	0.0	0	37
7	11240	D	0	17.2	65.1	0.2	0	42
7	11250	A	0	21.4	64.0	0.3	0	44
7	11250	В	0	17.8	58.2	0.2	0	44
7	11250	С	0	12.8	56.0	0.1	0	41
7	11250	D	0	-3.6	21.9	0.0	0	48
7	11260	A	0	-10.7	42.7	0.0	0	37
7	11260	В	0	12.2	70.6	0.1	0	38
7	11260	С	0	23.1	89.7	0.2	0	38
7	11260	D	0	25.3	88.4	0.2	0	39
7	11270	A	0	17.5	57.7	0.2	0	45
7	11270	В	0	13.8	55.8	0.1	0	44
7	11270	с	0	12.6	54.3	0.1	0	44
7	11280	A	0	18.0	49.3	0.3	0	41
7	11280	В	0	18.2	63.5	0.2	0	41
7	11290	A	0	16.9	49.2	0.2	0	40
7	11300	A	0	21.6	46.4	0.4	0	42
, 7	11300	B	õ	12.8	40.1	0.2	õ	43
7	11310	۵	٥	12.4	43.5	0.2	0	41
, 7	11310	B	õ	22.3	46.0	0.5	Ď	42
, ,	11310	č	1	41.9	55.6	1.1	õ	41
7	11310	D	ō	7.4	56.4	0.0	Õ	43
7	11320	A	0	24.2	50.4	0.5	0	42

IGHT LINE ANOMALY CATEGORY IMPLITUDE (PFM) INPHASE QUAD. CTT DEFTH HEIGHT HHOS MTRS MTRS 7 11320 C 1 47.7 55.5 1.4 0 38 7 11320 C 1 47.7 55.5 1.4 0 38 7 11331 A 0 14.1 48.2 0.2 0 44 7 11331 B 2 63.0 57.1 2.2 0 41 7 11340 A 0 19.0 41.1 0.4 0 43 7 11340 B 1 31.1 39.3 1.1 0 45 7 11340 C 0 14.8 45.9 0.2 0 47 7 11350 A 0 21.1 60.3 0.3 0 47 7 11350 C 0 34.1 99.0 0.4 0 37 7 </th <th></th> <th></th> <th></th> <th></th> <th></th> <th>CONI</th> <th>BIRD</th>						CONI	BIRD		
7 11320 B 2 53.8 50.1 2.0 0 41 7 11320 D 0 18.8 56.4 0.3 0 39 7 11331 A 0 14.1 48.2 0.2 0 44 7 11331 B 2 83.6 69.2 2.7 0 42 7 11331 D 0 6.4 36.3 0.0 0 41 7 11330 D 0 6.4 36.3 0.0 0 41 7 11340 A 0 19.0 41.1 0.4 0 43 7 11340 C 0 14.8 45.9 0.2 0 47 7 11350 A 0 21.1 60.3 0.3 0 47 7 11360 A 0 33.7 51.4 0.9 0 38 7 11360 B 0 34.1 99.0 0.4 0 37	IGHT	LINE	ANOMALY	CATEGORY	AMPLITUD INPHASE	E (PPM) QUAD.	CTP MHOS	DEPTH MTRS	HEIGHT MTRS
7 11320 B 2 53.8 50.1 2.0 0 41 7 11320 D 0 18.8 56.4 0.3 0 39 7 11331 A 0 14.1 48.2 0.2 0 44 7 11331 B 2 63.0 57.1 2.2 0 41 7 11331 D 0 6.4 36.3 0.0 0 41 7 11331 D 0 6.4 36.3 0.0 0 41 7 11340 A 0 19.0 41.1 0.4 0 43 7 11340 C 0 14.8 45.9 0.2 0 47 7 11350 A 0 21.1 60.3 0.3 0 47 7 11360 A 0 33.7 51.4 0.9 0 38 7 11360 B 0 27.5 76.1 0.3 0 40									• • • •
7 11320 B 2 33.6 50.1 2.0 0 41 7 11320 D 0 16.8 56.4 0.3 0 39 7 11331 B 0 14.1 48.2 0.2 0 44 7 11331 B 2 83.6 69.2 2.7 0 42 7 11331 D 0 6.4 36.3 0.0 0 41 7 11340 A 0 19.0 41.1 0.4 0 43 7 11340 B 0 13.1 39.3 1.1 0 47 7 11350 B 0 21.1 60.3 0.3 0 47 7 11350 B 0 21.1 60.3 0.3 0 47 7 11350 B 0 33.7 51.4 0.9 0 38 7 <	7	11220	P	2	53 O -	E 0 1	2 0	•	4.5
7 11320 D 1 <th1< td="" th<=""><td>7</td><td>11220</td><td>B</td><td>2</td><td>23.0</td><td>50.1 55 5</td><td>2.0</td><td>0</td><td>41</td></th1<>	7	11220	B	2	23.0	50.1 55 5	2.0	0	41
7 11320 B 0 11.0 50.4 0.3 0 33 7 11331 B 0 14.1 48.2 0.2 0 44 7 11331 B 2 63.0 57.1 2.2 0 41 7 11331 D 0 6.4 36.3 0.0 0 41 7 11340 A 0 19.0 41.1 0.4 0 43 7 11340 B 1 19.0 41.1 0.4 0 43 7 11340 C 0 14.8 45.9 0.2 0 47 7 11350 A 0 21.1 60.3 0.3 0 47 7 11360 A 0 33.7 51.4 0.9 0 38 7 11360 B 0 34.1 99.0 0.4 0 37 7 11370 B 0 27.5 76.1 0.3 0 45	7	11220		<u>,</u>	4/./	55.5	1.4	Ŏ	20
7 11331 A 0 14.1 48.2 0.2 0 44 7 11331 C 2 83.6 69.2 2.7 0 42 7 11331 D 0 6.4 36.3 0.0 0 41 7 11340 A 0 19.0 41.1 0.4 0 43 7 11340 B 1 31.1 39.3 1.1 0 45 7 11350 A 0 21.1 60.3 0.3 0 47 7 11350 A 0 21.1 60.3 0.3 0 47 7 11350 B 0 21.1 60.3 0 46 7 11360 A 0 33.7 51.4 0.9 0 38 7 11370 A 0 27.5 76.1 0.3 0 40 7 11380 A 1 35.4 38.4 1.4 0 45 <td< td=""><td>1</td><td>11320</td><td>D</td><td>v</td><td>10.0</td><td>30.4</td><td>0.5</td><td>v</td><td>39</td></td<>	1	11320	D	v	10.0	30.4	0.5	v	39
7 11331 B 2 83.6 69.2 2.7 0 42 7 11331 D 0 63.0 57.1 2.2 0 41 7 11331 D 0 6.4 36.3 0.0 0 41 7 11340 A 0 19.0 41.1 0.4 0.43 7 11340 B 1 31.1 39.3 1.1 0.45 7 11350 A 0 21.1 60.3 0.3 0.47 7 11350 B 0 21.1 60.3 0.3 0.47 7 11350 C 0 15.4 37.0 0.3 0.47 7 11360 A 0 33.7 51.4 0.6 37 7 11370 B 0 34.0 55.1 0.8 39 7 11380 B 0 11.2 42.4 0.1 0.42 7 <td< td=""><td>7</td><td>11331</td><td>А</td><td>0</td><td>14.1</td><td>48.2</td><td>0.2</td><td>0</td><td>44</td></td<>	7	11331	А	0	14.1	48.2	0.2	0	44
7 11331 C 2 63.0 57.1 2.2 0 41 7 11340 A 0 19.0 41.1 0.4 0 43 7 11340 B 1 31.1 39.3 1.1 0 45 7 11350 A 0 21.1 60.3 0.3 0 47 7 11350 A 0 21.1 60.3 0.3 0 47 7 11350 B 0 21.1 60.3 0.3 0 47 7 11350 B 0 21.1 60.3 0.3 0 47 7 11360 A 0 33.7 51.4 0.9 0 38 7 11360 B 0 27.5 76.1 0.3 0 40 7 11370 A 0 27.5 76.1 0.3 0 45 7 11380 A 1 35.4 </td <td>7</td> <td>11331</td> <td>В</td> <td>2</td> <td>83.6</td> <td>69.2</td> <td>2.7</td> <td>0</td> <td>42</td>	7	11331	В	2	83.6	69.2	2.7	0	42
7 11331 D 0 6.4 36.3 0.0 0 41 7 11340 A 0 19.0 41.1 0.4 0 43 7 11340 B 1 31.1 39.3 1.1 0 45 7 11350 A 0 21.1 60.3 0.3 0 47 7 11350 B 0 21.1 60.3 0.3 0 47 7 11350 C 0 15.4 37.0 0.3 0 47 7 11360 A 0 33.7 51.4 0.9 0.38 7 11360 B 0 34.1 99.0 0.4 0.37 7 11370 B 0 27.5 76.1 0.3 0.40 7 11380 A 1 35.4 38.4 1.4 0.42 7 11390 A 0 11.2 42.4 0.1 0.42	7	11331	С	2	63.0	57.1	2.2	0	41
7 11340 A 0 19.0 41.1 0.4 0 43 7 11340 C 0 14.8 45.9 0.2 0 47 7 11350 A 0 21.1 60.3 0.3 0 47 7 11350 B 0 21.1 60.3 0.3 0 47 7 11350 C 0 15.4 37.0 0.3 0 47 7 11360 A 0 23.7 51.4 0.9 0 38 7 11360 B 0 34.1 99.0 0.4 0 37 7 11370 B 0 27.5 76.1 0.8 0 39 7 11380 A 1 35.4 38.4 1.4 0 45 7 11380 B 1 14.8 38.9 0.3 0 42 7 11390 B 2 75.3 66.6 2.4 0 38 <td>7</td> <td>11331</td> <td>D</td> <td>0</td> <td>6.4</td> <td>36.3</td> <td>0.0</td> <td>0</td> <td>41</td>	7	11331	D	0	6.4	36.3	0.0	0	41
7 11340 B 1 31.1 39.3 1.1 0 45 7 11340 C 0 14.8 45.9 0.2 0 47 7 11350 A 0 21.1 60.3 0.3 0 47 7 11350 B 0 20.9 34.4 0.6 0 46 7 11350 C 0 15.4 37.0 0.3 0 47 7 11360 A 0 33.7 51.4 0.9 0 38 7 11360 B 0 27.5 76.1 0.3 0 40 7 11370 B 0 27.5 76.1 0.8 0 39 7 11380 A 1 35.4 38.4 1.4 0 45 7 11380 B 0 11.2 42.4 0.1 0 42 7 11390 B 2 75.3 66.6 2.4 0 38 <td>7</td> <td>11340</td> <td>Δ</td> <td>n</td> <td>19 0</td> <td>41.1</td> <td>04</td> <td>0</td> <td>43</td>	7	11340	Δ	n	19 0	41.1	04	0	43
7 11340 c 0 14.8 45.9 0.2 0 47 7 11350 A 0 21.1 60.3 0.3 0 47 7 11350 B 0 20.9 34.4 0.6 0 46 7 11350 C 0 15.4 37.0 0.3 0 47 7 11360 A 0 33.7 51.4 0.9 0 38 7 11360 B 0 37.7 51.4 0.9 0 38 7 11370 A 0 27.5 76.1 0.3 0 40 7 11380 A 1 35.4 38.4 1.4 0 45 7 11380 B 0 11.2 42.4 0.1 0 42 7 11390 A 2 75.3 66.6 2.4 0 38 7 11400 A 2 25.4 18.8 2.1 0 59 <td>7</td> <td>11340</td> <td>B</td> <td>1</td> <td>31.1</td> <td>39.3</td> <td>1.1</td> <td>ň</td> <td>45</td>	7	11340	B	1	31.1	39.3	1.1	ň	45
7 11350 A 0 21.1 60.3 0.3 0 47 7 11350 C 0 20.9 34.4 0.6 0 46 7 11350 C 0 15.4 37.0 0.3 0 47 7 11360 A 0 33.7 51.4 0.9 0 38 7 11360 B 0 34.1 99.0 0.4 0 37 7 11370 B 0 27.5 76.1 0.3 0 40 7 11380 A 1 35.4 38.4 1.4 0 45 7 11380 B 0 14.8 38.9 0.3 0 45 7 11390 B 2 75.3 66.6 2.4 0 38 7 11390 B 2 75.3 66.6 2.4 0 38 7 11400 B 2 25.4 18.8 2.1 0 59	ż	11340	c	ō	14.8	45.9	0.2	ŏ	47
7 11350 A 0 21.1 60.3 0.3 0 47 7 11350 C 0 15.4 37.0 0.3 0 47 7 11350 C 0 15.4 37.0 0.3 0 47 7 11360 A 0 33.7 51.4 0.9 0 38 7 11360 B 0 34.1 99.0 0.4 0 37 7 11370 A 0 27.5 76.1 0.3 0 40 7 11380 A 1 35.4 38.4 1.4 0 45 7 11380 B 0 11.2 42.4 0.1 0 42 7 11390 A 2 75.3 66.6 2.4 0 38 7 11400 B 2 25.4 18.8 2.1 0 59 7 11410 B 0 5.8 9.8 0.3 0 54	-		-	-				-	
7 11350 B 0 20.9 34.4 0.6 0 46 7 11350 C 0 15.4 37.0 0.3 0 47 7 11360 A 0 33.7 51.4 0.9 0 38 7 11360 B 0 37.7 51.4 0.9 0 38 7 11370 A 0 27.5 76.1 0.3 0 40 7 11370 B 0 34.0 55.1 0.8 0 39 7 11380 A 1 35.4 38.4 1.4 0 45 7 11380 B 0 11.2 42.4 0.1 0 42 7 11390 B 2 75.3 66.6 2.4 0 38 7 11400 B 2 25.4 18.8 2.1 0 59 7 11400 B 2 25.2 14.4 2.9 0 48 <td>7</td> <td>11350</td> <td>A</td> <td>0</td> <td>21.1</td> <td>60.3</td> <td>0.3</td> <td>0</td> <td>47</td>	7	11350	A	0	21.1	60.3	0.3	0	47
7 11350 C 0 15.4 37.0 0.3 0 47 7 11360 A 0 33.7 51.4 0.9 0 38 7 11360 B 0 34.1 99.0 0.4 0 37 7 11370 A 0 27.5 76.1 0.3 0 40 7 11370 B 0 34.0 55.1 0.8 0 39 7 11380 A 1 35.4 38.4 1.4 0 45 7 11380 B 0 11.2 42.4 0.1 0 42 7 11390 B 0 11.2 42.4 0.1 0 42 7 11400 A 2 75.3 66.6 2.4 0 38 7 11400 B 2 25.4 18.8 2.1 0 59 7 11420 A 2 25.2 14.4 2.9 0 48 <td>7</td> <td>11350</td> <td>В</td> <td>0</td> <td>20.9</td> <td>34.4</td> <td>0.6</td> <td>0</td> <td>46</td>	7	11350	В	0	20.9	34.4	0.6	0	46
7 11360 A 0 33.7 51.4 0.9 0 38 7 11370 A 0 27.5 76.1 0.3 0 40 7 11370 B 0 27.5 76.1 0.3 0 40 7 11370 B 0 34.0 55.1 0.8 0 39 7 11380 A 1 35.4 38.4 1.4 0.45 7 11380 B 0 11.2 42.4 0.1 0.42 7 11390 B 0 11.2 42.4 0.1 0.42 7 11400 A 2 75.3 66.6 2.4 0.38 7 11400 B 2 25.4 18.8 2.1 0.59 7 11420 A 2 25.2 14.4 2.9 0.48 7 11420 B 0 7.3 13.1 0.3 0.54 7	7	11350	С	0	15.4	37.0	0.3	0	47
7 11360 B 0 34.1 99.0 0.4 0 37 7 11370 A 0 27.5 76.1 0.3 0 40 7 11370 B 0 34.0 55.1 0.8 0 39 7 11380 A 1 35.4 38.4 1.4 0 45 7 11380 B 0 11.2 42.4 0.1 0 42 7 11390 B 0 11.2 42.4 0.1 0 42 7 11390 B 0 11.2 42.4 0.1 0 42 7 11400 B 0 10.6 30.4 0.2 0 42 7 11400 B 0 5.8 9.8 0.3 0 56 7 11420 A 2 25.2 14.4 2.9 0 48	7	11360	А	0	33.7	51.4	0.9	0	38
7 11370 A 0 27.5 76.1 0.3 0 40 7 11370 B 0 34.0 55.1 0.8 0 39 7 11380 A 1 35.4 38.4 1.4 0 45 7 11380 B 0 11.2 42.4 0.1 0 42 7 11390 B 2 93.7 72.3 3.0 0 37 7 11390 B 2 75.3 66.6 2.4 0 38 7 11400 A 2 75.3 66.6 2.4 0 38 7 11400 B 2 25.4 18.8 2.1 0 59 7 11410 B 2 25.2 14.4 2.9 0 48 7 11420 B 0 7.3 13.1 0.3 0 54 7 11420 B 0 7.3 13.1 0.3 7 47	7	11360	B	õ	34.1	99.0	0.4	õ	37
711370A027.576.10.3040711370B0 34.0 55.1 0.8 0 39 711380A1 35.4 38.4 1.4 0 45 711390A0 11.2 42.4 0.1 0 42 711390B2 93.7 72.3 3.0 0 37 711400A2 75.3 66.6 2.4 0 38 711410B2 25.4 18.8 2.1 0 59 711420A2 25.2 14.4 2.9 0 48 711420A2 25.2 14.4 2.9 0 48 711430A1 13.0 10.7 1.4 0 55 7 11440 B0 7.3 13.1 0.3 0 47 7 11440 A0 7.3 13.1 0.3 0 47 7 11440 A0 7.3 13.1 0.3 0 47 7 11450 A0 5.7 8.6 0.4 0 53 7 11460 A0 4.8 21.9 0.0 0 46			_	•				-	• •
7 11370 B 0 34.0 55.1 0.8 0 39 7 11380 A 1 35.4 38.4 1.4 0 45 7 11380 B 0 11.2 42.4 0.1 0 42 7 11390 A 0 11.2 42.4 0.1 0 42 7 11390 B 2 75.3 66.6 2.4 0 37 7 11400 A 2 75.3 66.6 2.4 0.3 38 7 11410 A 0 5.8 9.8 0.3 0 56 7 11410 B 2 25.4 18.8 2.1 0 59 7 11420 A 2 25.2 14.4 2.9 0 48 7 11420 B 0 7.3 13.1 0.3 0 54 7 11430 A 1 13.0	7	11370	A	0	27.5	76.1	0.3	0	40
711380 11380 7A1 35.4 14.8 38.4 38.9 1.4 0.30 45 45711390 11390 7A011.2 93.742.4 72.30.1 3.0042 42 3.0711400 11400 BA275.3 10.666.6 30.42.4 0.2038 42711400 11400 BA05.8 29.8 25.40.3 18.8056 	7	11370	В	0	34.0	55.1	0.8	0	39
7 11380 B 0 14.8 38.9 0.3 0 43 7 11380 B 0 14.8 38.9 0.3 0 45 7 11390 A 0 11.2 42.4 0.1 0 42 7 11390 B 2 93.7 72.3 3.0 0 37 7 11400 A 2 75.3 66.6 2.4 0 38 7 11400 B 0 10.6 30.4 0.2 0 42 7 11410 B 0 5.8 9.8 0.3 0 56 7 11420 A 2 25.4 18.8 2.1 0 59 7 11420 B 0 4.3 7.2 0.3 0 54 7 11420 B 0 7.3 13.1 0.3 0 47 7 11430 A 1 13.0 10.7 1.4 0 55	7	11290		1	25 A	20 1	1 /	0	15
711300B0111050130.5013711390B293.772.33.0037711400A275.366.62.4038711400B010.630.40.2042711410A05.89.80.3056711410B225.418.82.1059711420A225.214.42.9048711420B04.37.20.3054711430A113.010.71.4055711440B07.313.10.3047711450A05.78.60.4053711460A04.821.90.0046	7	11380	R	1 0	14.8	38.9	0.3	0	45
7 11390 A 0 11.2 42.4 0.1 0 42 7 11390 B 2 93.7 72.3 3.0 0 37 7 11400 A 2 75.3 66.6 2.4 0 38 7 11400 B 0 10.6 30.4 0.2 0 42 7 11410 A 0 5.8 9.8 0.3 0 56 7 11410 B 2 25.4 18.8 2.1 0 59 7 11420 A 2 25.2 14.4 2.9 0 48 7 11430 A 1 13.0 10.7 1.4 0 55 7 11440 A 0 7.3 13.1 0.3 0 47 7 11440 B 0 5.7 8.6 0.4 0 53 7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46	•		-	·				•	
711390B2 93.7 72.3 3.0 0 37 711400A2 75.3 66.6 2.4 0 38 711400B0 10.6 30.4 0.2 0 42 711410A0 5.8 9.8 0.3 0 56 711420A2 25.4 18.8 2.1 0 59 711420A2 25.2 14.4 2.9 0 48 711430A1 13.0 10.7 1.4 0 55 711440A0 7.3 13.1 0.3 0 47 711450A0 5.7 8.6 0.4 0 53 711460A0 4.8 21.9 0.0 0 46	7	11390	A	0	11.2	42.4	0.1	0	42
7 11400 A 2 75.3 66.6 2.4 0 38 7 11400 B 0 10.6 30.4 0.2 0 42 7 11410 A 0 5.8 9.8 0.3 0 56 7 11410 B 2 25.4 18.8 2.1 0 59 7 11420 A 2 25.2 14.4 2.9 0 48 7 11420 B 0 4.3 7.2 0.3 0 54 7 11430 A 1 13.0 10.7 1.4 0 55 7 11440 B 0 7.3 13.1 0.3 0 47 7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46	7	11390	В	2	93.7	72.3	3.0	0	37
7 11400 A 2 73.3 00.0 2.4 0 30 7 11400 B 0 10.6 30.4 0.2 0 42 7 11410 A 0 5.8 9.8 0.3 0 56 7 11410 B 2 25.4 18.8 2.1 0 59 7 11420 A 2 25.2 14.4 2.9 0 48 7 11420 B 0 4.3 7.2 0.3 0 54 7 11430 A 1 13.0 10.7 1.4 0 55 7 11440 A 0 7.3 13.1 0.3 0 47 7 11440 B 0 7.3 13.1 0.3 7.47 7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9	7	11400		`	75.2	66 6	2 4	0	20
7 11400 B 0 10.0 30.4 0.2 0 42 7 11410 B 2 25.4 18.8 2.1 0 56 7 11420 A 2 25.2 14.4 2.9 0 48 7 11420 B 0 4.3 7.2 0.3 0 54 7 11420 B 0 7.3 12.0 0.3 0 54 7 11430 A 1 13.0 10.7 1.4 0 55 7 11440 A 0 7.3 13.1 0.3 0 47 7 11440 B 0 7.3 13.1 0.3 0 47 7 11440 B 0 5.7 8.6 0.4 0 53 7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46 <td>י ד</td> <td>11400</td> <td>R</td> <td>2</td> <td>10 6</td> <td>30.4</td> <td>2.4 0 2</td> <td>0</td> <td>20</td>	י ד	11400	R	2	10 6	30.4	2.4 0 2	0	20
711410A0 5.8 9.8 0.3 0 56 7 11410B2 25.4 18.8 2.1 0 59 7 11420A2 25.2 14.4 2.9 0 48 7 11420B0 4.3 7.2 0.3 0 54 7 11430A113.0 10.7 1.4 0 55 7 11440A0 7.3 13.1 0.3 0 47 7 11440B0 5.7 8.6 0.4 0 53 7 11450A0 4.8 21.9 0.0 0 46	,	11400	Ð	v	10.0	30.4	0.2	0	42
7 11410 B 2 25.4 18.8 2.1 0 59 7 11420 A 2 25.2 14.4 2.9 0 48 7 11420 B 0 4.3 7.2 0.3 0 54 7 11430 A 1 13.0 10.7 1.4 0 55 7 11440 A 0 7.3 13.1 0.3 0 47 7 11440 B 0 7.3 13.1 0.3 7 47 7 11440 B 0 5.7 8.6 0.4 0 53 7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46	7	11410	А	0	5.8	9.8	0.3	0	56
7 11420 A 2 25.2 14.4 2.9 0 48 7 11420 B 0 4.3 7.2 0.3 0 54 7 11430 A 1 13.0 10.7 1.4 0 55 7 11440 A 0 7.3 13.1 0.3 0 47 7 11440 B 0 7.3 13.1 0.3 7 47 7 11440 B 0 5.7 8.6 0.4 0 53 7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46	7	11410	В	2	25.4	18.8	2.1	0	59
7 11420 A 2 25.2 14.4 2.9 0 48 7 11420 B 0 4.3 7.2 0.3 0 54 7 11430 A 1 13.0 10.7 1.4 0 55 7 11430 A 0 7.3 13.1 0.3 0 47 7 11440 A 0 7.3 13.1 0.3 0 47 7 11440 B 0 5.7 8.6 0.4 0 53 7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46	_			_				_	
7 11420 B 0 4.3 7.2 0.3 0 54 7 11430 A 1 13.0 10.7 1.4 0 55 7 11440 A 0 7.3 13.1 0.3 0 47 7 11440 B 0 7.3 13.1 0.3 0 47 7 11440 B 0 5.7 8.6 0.4 0 53 7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46	7	11420	A	2	25.2	14.4	2.9	0	48
7 11430 A 1 13.0 10.7 1.4 0 55 7 11440 A 0 7.3 13.1 0.3 0 47 7 11440 B 0 4.1 7.0 0.3 7 47 7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46	7	11420	В	0	4.3	7.2	0.3	0	54
7 11440 A 0 7.3 13.1 0.3 0 47 7 11440 B 0 4.1 7.0 0.3 7 47 7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46	7	11430	А	1	13.0	10.7	1.4	0	55
7 11440 A 0 7.3 13.1 0.3 0 47 7 11440 B 0 4.1 7.0 0.3 7 47 7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46	•			-				•	
7 11440 B 0 4.1 7.0 0.3 7 47 7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46	7	11440	А	0	7.3	13.1	0.3	0	47
7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46	7	11440	B	0	4.1	7.0	0.3	7	47
7 11450 A 0 5.7 8.6 0.4 0 53 7 11460 A 0 4.8 21.9 0.0 0 46	-	11450		^	г э	0 (A 4	^	E 5
7 11460 A 0 4.8 21.9 0.0 0 46	/	11450	A	U	5./	0.0	0.4	U	23
	7	11460	A	0	4.8	21.9	0.0	0	46

					CONI	BIRD		
IGHT	LINE	ANOMALY	CATEGORY	AMPLITUD INPHASE	E (PPM) QUAD.	CTP MHOS	DEPTH MTRS	HEIGHT MTRS
	* • • •				• • • • •			
7	11460	В	0	8.8	16.0	0.4	0	48
7	11470	A	0	10.8	26.2	0.3	0	45
7	11480	A	0	12.6	27.0	0.3	0	44
7	11490	A	0	28.1	39.3	0.9	0	41
7	11490	В	0	3.6	27.8	0.0	0	45
7	11500	A	0	2.1	22.9	0.0	0	44
7	11500	В	2	51.7	31.2	3.5	0	46
7	11510	A	2	36.8	26.4	2.5	0	50
7	11520	A	0	19.4	26.1	0.8	0	50
7	11530	A	0	18.8	30.4	0.6	0	38
/	11230	В	0	10.1	31.0	0.2	0	57
7	11540	A	0	4.2	30.9	0.0	0	43
7	11540	В	1	30.5	33.1	1.3	0	44
7	11550	A	1	16.6	19.1	1.0	0	53
7	11550	В	0	3.5	41.0	0.0	0	40
7	11561	A	0	7.7	12.2	0.4	0	50
7	11561	В	0	7.4	10.4	0.5	3	45
8	11570	A	0	8.3	8.8	0.8	0	54
8	11570	В	0	5.0	10.4	0.2	0	54
8	11580	A	0	11.1	24.7	0.3	0	46
8	11580	В	0	5.7	16.3	0.1	0	49
8	11590	A	0	5.8	18.8	0.1	0	53
8	11600	A	0	9.8	35.2	0.1	0	44
8	11610	A	0	7.8	40.2	0.0	0	44
8	11620	A	0	7.6	33.5	0.1	0	45
8	11630	A	0	13.6	57.2	0.1	0	46
8	11640	A	0	12.1	56.5	0.1	0	44

						CONI	DUCTOR	BIRD
IGHT	LINE	ANOMALY	CATEGORY	AMPLITUD INPHASE	DE (PPM) QUAD.	CTP MHOS	DEPTH MTRS	HEIGHT MTRS
8	11650	A	0	6.9	46.3	0.0	0	44
8	11700	A	0	4.8	20.3	0.0	0	47
8	11710	A	0	7.1	20.1	0.2	0	52
8	11720	A	0	15.8	28.6	0.5	0	48
8	11730	A	0	20.2	37.9	0.5	0	43
8	11740	А	0	17.7	44.7	0.3	0	42

Estimated depth may be unreliable because the stronger part of the conductor may be deeper or to one side of the flight line, or because of a shallow dip or overburden effects.

APPENDIX III

CERTIFICATE OF QUALIFICATIONS

I, ROBERT J. DE CARLE, certify that: -

- 1. I hold a B. A. Sc. in Applied Geophysics with a minor in geology from Michigan Technological University, having graduated in 1970.
- 2. I reside at 28 Westview Crescent in the town of Palgrave, Ontario.
- 3. I have been continuously engaged in both professional and managerial roles in the minerals industry in Canada and abroad for the past eighteen years.
- 4. I have been an active member of the Society of Exploration Geophysicists since 1967 and hold memberships on other professional societies involved in the minerals extraction and exploration industry.
- 5. The accompanying report was prepared from information published by government agencies, materials supplied by Noramco Explorations Inc. and from a review of the proprietary airborne geophysical survey flown by Aerodat Limited for Noramco Explorations Inc. I have not personally visited the property.
- I have no interest, direct or indirect, in the property described nor do I hold securities in Noramco Explorations Inc.

Signed,

Robert J. de Carle

Robert J. de Carle Consulting Geophysicist

Palgrave, Ontario

October 28, 1987

Vpe of Survey (s)	ik Lake Prio?	enty						
Augborne (sephysical &	Survey.	52F	P165W9489 2, 1056	5 KEE7HIK	AKE (EAST A		
Pure Gold	Resources Ju	۱ د.					-7689 -7689	20
ddress	St val	North	2. 10	Jutavia			······	
urvey Company			say-, c	Date of Survey	(from & to) 87 22	09 87	otal Miles of line	Cut
ame and Address of Author (o	f Geo-Technical report)			Day Mo.	Yr. Day	Mo. Yr.	430 line	km5
3883 Nashua	DRIVE Mis	56155	augy, (Ontakio	L4V 17	<u>थ्<u>उ.</u></u>		
pecial Provisions	Geophysical	Days per		laims (raversed (lining Claim	Expend.	erical sequer	1CE) ning Claim	Expens
For first survey:	- Electromagnetic	Claim	Prefix	Number	Days Cr.	Prefix	Number	Days C
Enter 40 days. (This includes line cutting)	Magnetometer	l	D B	913016		TB	919491	
	- Badiometric			. 913017	·		919492	+
For each additional survey: using the same grid:	Other			9/3018	·		919493	
Enter 20 days (for each)	Gaalogiaal			913019	 		919494	
ι.	Geological	d		913020	łł		919495	
lan Days	Geochemical	Days per		913021	} {		919 502	
Complete reverse side	Geophysical	Claim		913022	+		919509	
and enter total(s) here	Electromagnetic			913023			919516	
RECEIV	- Magnetometer	l		913024			919523	
	Radiometric			9130 25			919545	
NOV 2 0 19	87 - Other		had Carl	913026			919546	
	Geological		and the second	913027		in the second	919541	
MINING LANDS S	ECIdONical			913185			919548	_
irborne Gredits		Days per Claim		913186	·		919549	
Note: Special provisions credits do not apply	Electromagnetic	40		913187			919550	
to Airborne Surveys.	Magnetometer	40		913188			919557	
	Radiometric	1		913/89			919558	
cpenditures (excludes powe	er stripping)	$\frac{1}{1}$		913/90			919581	
DE	GEIVE			913191			919582	
rformed on Claim(s)	NUV U 9 1981			919491			9195 83	
				9/94PR			9:9:58+	-
17.8.9	Condition of the section	· · · • •	the state	919489			919584	- ,
Total Expenditures		otal Credits		919491	11		919:566	
\$	+ 15 =				-d	Total numi	ber of mining	
Lstructions	L L					claims cove report of w	red by this /	208.
Total Days Credits may be ap choice. Enter number of days	portioned at the claim h credits per claim selecte	older's d		For Office Use C	Dnly			
in columns at right.			Total Days Recorded	Cr. Date Recorded	0 int	Mining Rec	order	ч. Дания в
te Rec	orded Holder or Agent (S	ignaturel	1. LHO	DencApproved	as Hecorded	Brench Dir	77-5	4
NOV 4, 1987 M	lichelle Dubrio	<u> </u>	101.	JC6 De	81	W	Loute	
titication Verifying Repo	rt of Work	Audadaa of	•ho foot f	Arth in the Dancet		¥K		

1. g. Ø					Tred !	Marag	remeat	Jac. 29
Ministry of Northern Developme and Mines	Report of We (Geophysical, (ork Geological,	Cada	ion in	structions:	 Please type If number exceeds spa Only days 	or print, of mining claims ce on this form, a	a traverses ttach a lich
Ontario	Geochemical a	nd Expend	litures)	#5	0	"Expenditu in the "E	res" section may xpend. Days Cr."	be enterer: columns.
Type of Survey(s)	cx 10	565	Wining	Act	Township	Do not use or Area	shaded areas below	<u>.</u>]
Claim Holder(s)	Geophysical:	Euroei	45		GAST	AAM Prospecto	schik Lak	cGar
Address Pure Gold R	esources_In	<u>c.</u>					4689	
Survey Company	str. 22. No	Rth Br	ry Or	Date of Survey	P182	مدن ۱۱	Total Miles of line (Cut
Acrodat Ltd		•		09 Day Mo.	87 Yr. Day	09 87 Mo. Yr.	185 km	15.
3883 NAShua	DRIVE His	5]55AU	GA ON	tarin	LAV IR	3.		
Credits Requested per Each (Claim in Columns at r	ight	Mining Cl	aims Traversed (I	List in num	erical sequer	nce)	
For first surprise	Geophysical	Claim	Prefix	Number	Expend. Days Cr.	Prefix	Number	Days Cr.
Enter 40 days. (This	- Electromagnetic		TB	919496		TB	919522	<u></u>
Includes line cutting)	Magnetometer	l		919497		THE AND	- 919 524	
For each additional survey:	- Radiometric			919498			919525	4
Enter 20 days (for each)	- Other			919499			919526	
	Geological			919500			919 527	
· · · · · · · · · · · · · · · · · · ·	Geochemical			919501			919528	
Man Days	Geophysical	Days per Claim		919503			919529	
Complete reverse side and enter total(s) here	- Electromagnetic			919504			919 530	
REC	EI Mg EcDeter			919505			919531	
NOW	D - Badiometric		5357675	919501			9195527	
, str.A	2 () 1307 - Other			910			010002	1 1
MINING LA	NDS-SECTION						01052J	
	Geochemical			9:95.			71/207	
Airborne Credits		Days per		01051			<u></u>	
Note: Special provisions	Electromagnetic			919311			919236	·
credits do not apply to Airborne Surveys	Magnetometer	-70		919512			919251	1
	Radiometric			919515			919228	
Expenditures (excludes powe	er strippingla.un	<u></u>		919514			919539	
Type of Work Performed)	EBEIVEI			919515			919540	
Performed on Claim(s)		₩ ₩		919517	 		919541	
		 		919518			919542	
189	1611 周3-2-3-5	• 0		919519	·		919543	
Calculation of Expenditure Days	Credits	otal		919 520	<u> </u>		919544	4
Total Expenditures		Credits		919521			919551	<u> </u>
\$	÷15 =					Total num claims cov	ber of mining ered by this	73
Instructions Total Days Credits may be ap	oportioned at the claim h	older's	1	For Office Hea	nly		···· L	J
choice. Enter number of days in columns at right.	s credits per claim selecte	d	Total Days Becorded	Cr. Date Recorded		Mining Rec	order	
Date Ra	corded Holder or Asent (Joh C	Dancapproved	N 9 AR	Branchall	in hi th	yed of
Nov. 4 1987 9	michelle Dube	au I	28.			Securit	antement .	
Certification Verifying Repo	rt of Work					Jo ph	N JU	
I hereby certify that I have a or witnessed same during and	personal and intimate kr l/or after its completion a	nowledge of and the ann	the facts set f exed report is	orth in the Report true.	of Work ann	exea hereto, h	aving performed th	ie work
Name and Postal Address of Peri	son Certifying		<u>.</u>	· .		~	, .	
NORAMED EXPLOR	ATIONS 9 nc.	121	D Hau	1 St. (1) Date Certified	North B	Certified b	nt, PIBZU v (Signature)	26
				Noil 4	1007	om.	chall M. h	<u></u>



Ministry of Northern Development and Mines

Geophysical-Geological-Geochemical Technical Data Statement

File_

Ontario		Cadman Lake	PROP.	r lle
TE	TO BE AT FACTS SI CHNICAL REPO	FACHED AS AN APPE HOWN HERE NEED N RT MUST CONTAIN I	NDIX TO TECHNI OT BE REPEATED NTERPRETATION	CAL REPORT IN REPORT , CONCLUSIONS ETC.
Type of Survey(s)	Licheance G	cophysical Su	aney st	
Township or Area	aci ARM	Keezhik Lake	1	MINUNG OF A DAG TO A UDDODD
Claim Holder(s). Ru	Cold Resa	ukers Inc.		List numerically
_/2/1	Man At	W. North Ba	y Ontario	
Survey Company	Acridat L	ld.		
Author of Report	Bobert J.	de Carte		(prefix) (number)
Address of Author	3883 Nashu	a DR. Hasis	auga Ont.	
Covering Dates of Su	rvey <u>. Scipil é</u>	(linecutting to office)	0 '	
Total Miles of Line C	ut	os kmg	e and to define a second and the extension of the	
1				lee List attacked
SPECIAL PROVIS CREDITS REQUE	IONS STED	Geophysical	DAYS per claim	
ENTER 40 dave (i	aludaa	Electromagnetic		
line cutting) for fir	st	-Magnetometer_		
survey.		-Radiometric		
ENTER 20 days fo	r each	–Other		
additional survey u	sing	Geological		
same grid.		Geochemical		
AIRBORNE CREDIT	S (Special provisio	on credits do not apply to	airborne surveys)	
Magnetometer <u>40</u>	Electromagne (enter day	etic <u>40</u> Radior vs per claim)	netric	
DATE: New 4.19		TURE: Aniche	16 Dubran	
		Author of F	leport or Agent	RECEIVED
				NOV 23 1987
Res. Geol	Qualific	cations		
Previous Surveys	Dete		3	
riie No. Type		Claim Hol	der	
	••••		••••••	
	••••		••••••	
•••••	•••			
	••••			
	•••			
				TOTAL CLAIMS 73.

OFFICE USE ONLY

		GEOPHYSIC	AL TECHNICAL DA	TA	
2	ROUND SURVEYS – If mo	re than one survey, sp	ecify data for c ach ty	pe of survey	•
N	umber of Stations		Number of	of Readings	
S	tation interval		Line space	ing	
P	rofile scale	······			
С	ontour interval			······································	
<i>r</i> N	Instrument				
H	Accuracy – Scale constant _	·····			
N	Diurnal correction method _				
MAC	Base Station check-in interva	al (hours)			
	Base Station location and va	lue			
	••••••••••••••••••••••••••••••••••••••				
g	Instrument				:
ET	Coil configuration			· · · · · · · · · · · · · · · · · · ·	
NGN	Coil separation				
WC	Accuracy	······			
TRC	Method:	Fixed transmitter	Shoot back	🗔 In line	🖾 Parallel line
EC	Frequency		(marify VI F station)		
E	Parameters measured		(specify v.1 station)		
	Instrument				
	Scale constant				
Z	Corrections made				
VL					
GRA	Base station value and locati	on			
•					
	Elevation accuracy				
	Instrument				
	Method Time Domain		□ F	requency Domain	
	Parameters – On time		F	requency	
~	- Off time		R	ange	
E	– Delay time				
E	– Integration tin	ne			
SIS	Power				
R	Electrode array				
	Electrode spacing				
d	-r -o				

INDUCED POLARIZATION

Type of electrode _



SELF POTENTIAL Instrument_____ _____ Range _____ Survey Method Corrections made RADIOMETRIC Instrument____ Values measured Energy windows (levels)_____ Height of instrument______Background Count ______ Size of detector_____ Overburden____ (type, depth - include outcrop map) **OTHERS (SEISMIC, DRILL WELL LOGGING ETC.)** Type of survey_____ Instrument Accuracy_____ Parameters measured _____ Additional information (for understanding results)_____ AIRBORNE SURVEYS Type of survey(s) <u>Aubounc</u> <u>Hagnetic</u> <u>EH</u> Instrument(s) <u>IH</u> <u>Accodat</u> <u>5</u> <u>frequency</u> <u>34</u> <u>(specify for each type of survey)</u> VLF- Totem 2 A. Mag = Scintrey Accuracy Mag = O.1 0400 Telsas. (specify for each type of survey) Aircraft used Accosponiate 4-Star 350 d helicuptor Sensor altitude. VLF - 18 m. Mag = 48 m. Navigation and flight path recovery method Mini Ranger radar positioning system Aircraft altitude______ (co_m______ Line Spacing_______

Miles flown over total area 615 km3. Over claims only

GEOCHEMICAL SURVEY – PROCEDURE RECORD

Numbers of claims from which samples taken_____

Total Number of Samples		L METHOD	S
Type of Sample(Nature of Material)		per cent	
Average Sample Weight	·	p.p.m. p.p.b.	
Method of Collection		P.P.Z.	
	Cu, Pb, Zn, Ni, Co,	Ag, Mo,	As,-(circle)
Soil Horizon Sampled	Others		· · · · · · · · · · · · · · · · · · ·
Horizon Development	Field Analysis (tests)
Sample Depth	Extraction Method		
Terrain	Analytical Method		
	Reagents Used		
Drainage Development	Field Laboratory Analysis		
Estimated Range of Overburden Thickness	No. (<u> </u>	tests)
	Extraction Method		
	Analytical Method	· · · · · · · · · · · · · · · · · · ·	
	Reagents Used		<u></u> <u>_</u>
SAMPLE PREPARATION	Commercial Laboratory (_		tests)
(Includes drying, screening, crushing, ashing)	Name of Laboratory.		
Mesh size of fraction used for analysis	Extraction Method		
	Analytical Method		
	Reagents Used		
	General		
General			
			·····-
· · · · · · · · · · · · · · · · · · ·			<u></u>

м	ining Claim	Expend.		N	Aining Claim	Expend.	1	
Prefix	Number	Days Cr.		Prefix	Number	Days Cr.	-	
TB	919496			TB	919522			
	919497				019524			
	9.998				919525	1		
	919499				919526			
	919500				919527		DMAN	
	919501				919528			TROPERTY CLAIMS
	0.0502				010579		В	919552
			1				B	919553
	919504		4		919 530	·	B	919554
	919505		1		919531		β	919555
9			1	1			E	919556
	919506		-		219532		μ. Έ	919559
	919507				919533		B	919560
]		019524		5	919561
к. К. 75	919508_	- 4	-		70237		5	919562
	919510			1	919535	1	ľ	919563
	91951		ł		919536			919064 910565
	212011-	-+		ł				919560 919577
	919512				91953	/		919567
	919513				919538	5		919568
	0.00			}	019 629	3		919569
			-			1	1	919570
5	919515				919540			919571
	010511				919541			919572
			-	1				919573
	919518		-		919 542	2		919574
	919519				91954	3		919575
		1			ALC AL	1		919576
	919 520	· }		1	212.54	7		919577
	919521	1	1		91955	[] 	5	919578
						ן (דיד		919579
						11	5	919580



Ministry of Northern Development and Mines

Geophysical-Geological-Geochemical Technical Data Statement

File___

Keezhik				
TO BE ATTACHED AS AN APPENDIX TO TECHNICAL REPORT FACTS SHOWN HERE NEED NOT BE REPEATED IN REPORT TECHNICAL REPORT MUST CONTAIN INTERPRETATION, CONCLUSIONS ETC.				
Type of Survey(s) Lichorne Heaphysical Surveys				
Township or Area Last ann - Kerzhik Lake	MINING CLAIMS TRAVERSED			
1210 Falara (t. 14) Month Ban (Dat				
Survey Company Ger Mat 14d.	(magin)			
Author of Report Robert J. de Carle.	(prenx) (number)			
Address of Author 3883 Mashua Dr. Mississauga, Unt				
Covering Dates of Survey Sept 21 23 1987	<i>/</i> .			
Total Miles of Line Cut	See LIST ATTAChed			
SPECIAL PROVISIONSDAYSCREDITS REQUESTEDGeophysical	tast. List			
Electromagnetic				
ENTER 40 days (includes Magnetometer	tic. Literature			
line cutting) for first	iresul			
ENTER 20 days for each —Other				
additional survey using Geological				
same grid.				
Geochemical				
<u>AIRBORNE CREDITS</u> (Special provision credits do not apply to airborne surveys)				
(enter days per claim)	RECEIVED			
DATE: Now 4,128 7 SIGNATURE: Anuly Ve Aubean				
Author of Report or Agent	any 2 ⊈ 1987			
	MINING LANDS SECTION			
Res. GeolQualifications				
Previous Surveys				
File No. Type Date Claim Holder				
	TOTAL CLAIMS 208.			

OFFICE USE ONLY

GEOPHYSICAL TECHNICAL DATA

2	<u>GROUND SURVEYS</u> – If more than one survey,	, specify data for each	type of survey	••
N	lumber of Stations	Numbe	r of Readings	
s	tation interval	Line sn	acing	<u>, , , , , , , , , , , , , , , , , , , </u>
P	rofile scale	Init sp	acing	
C	ontour interval		******	
C				·
	Instrument			
AGNETIC	Accuracy – Scale constant			₩ <u>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</u>
	Diurnal correction method	·····		
	Base Station check-in interval (hours)			······································
2	Base Station location and value			
	base station location and value	балайлана. — — — — — — — — — — — — — — — — — — —		
r N	Instrument			
STIC	Coil configuration			
UN	Coil separation			
MA				
RO	Method: Fixed transmitter	🖾 Shoot back	🗆 In line	Parallel line
S	Frequency			
EL	Parameters measured	(specify V.L.F. station)		
		· · · · · · · · · · · · · · · · · · ·		
	Instrument			
	Scale constant			
건	Corrections made			
IV				
GR	Base station value and location			
0.				
	Elevation accuracy			
	Instrument			
1	Method [] Time Domain		Frequency Domain	
	Parameters On time		Frequency	
X	Off time		Range	
LI V	Delay time			
STI	- Integration time			
ESI	Power			
	Electrode array			
	Electrode spacing			
•	Type of electrode			

INDUCED POLARIZATION



SELF POTENTIAL Instrument_____ Range Survey Method Corrections made_____ RADIOMETRIC Instrument_____ Values measured _____ Energy windows (levels) Height of instrument_____Background Count _____ Size of detector_____ Overburden_____ (type, depth - include outcrop map) **OTHERS (SEISMIC, DRILL WELL LOGGING ETC.)** Type of survey_____ Instrument _____ Accuracy_____ Parameters measured Additional information (for understanding results)_____ AIRBORNE SURVEYS Type of survey(s) <u>Magnetic</u>, EN & VLF. Instrument(s) F.M. Amodel 3 Frequency System VIF = Herg Totem 3A Hag · Scintrey VIW 2331 (specify for each type of survey) Accuracy Hag O.1 nanoteless (specify for each type of survey) Aircraft used Aerospostiale A-Stor 350d helicopter Sensor altitude Ext 30m, VLF- 48m Mag 18m Navigation and flight path recovery method Aini Ranger rodar positioning system. Aircraft altitude______ (0.0 m)______Line Spacing____/0.0 m. Miles flown over total area 615 km Over claims only

GEOCHEMICAL SURVEY -- PROCEDURE RECORD

Numbers of claims from which samples taken_____

Total Number of Samples	ANALYTICA	L METHODS				
Type of Sample(Nature of Material)	Values expressed in:	per cent				
Average Sample Weight		p.p.m.				
Method of Collection	Cu, Pb, Zn, Ni, Co,	Ag, Mo, As,-(circle)				
Soil Horizon Sampled	Others					
Horizon Development	Field Analysis (tests)				
Sample Depth	Extraction Method					
Terrain	Analytical Method					
	Reagents Used					
Drainage Development	Field Laboratory Analysis					
Estimated Range of Overburden Thickness	No. (tests)				
~	Extraction Method	·				
	Analytical Method					
	Reagents Used					
SAMPLE PREPARATION	Commercial Laboratory (_	tests)				
(Includes drying, screening, crushing, ashing)	Name of Laboratory	,				
Mesh size of fraction used for analysis	Extraction Method					
	Analytical Method					
	Reagents Used					
General	General					

Mining Claim		Expend.	Mining Claim		Expend.
Prefix	. Number	Days Cr.	Prefix	Number	Days Cr.
TB	913016		T.B.	917491	4
	213 017			919492	
	213018			919493	
	213019			919494	
	213000			919495	· · · · · · · · · · · · · · · · · · ·
	913021			919562	
	913022			919507	
	913003			212514	
	213024				•• ••• • • • •
. •	913035			919545	
۰.	9130.26			219546	
, . .	913027			919541	
	913185				
	913166			919:49	
	9/3187			919550	
	. 913186			319:557	
	912189			915558	
	913190			919581	
	913151			919562	
	91 9 481			919513	
	919488			919584	
	919489			919585	
	912490			919586	

KEEZHIK LAKE CLAIMS CONTINUED

CLAIM #	CLAIM #	CLAIM #	CLAIM #
919587	934905	934947	968321
919588	934906	934948	968322
919589	934907	934949	968323
919590	934908	934950	968324
919591	934909	934951	968325
919592	934910	934952	968326
919593	934911	934953	968327
919594	934912	934954	968328
919595	934913	934955	968329
919596	934914	934956	968330
919597	934915	934957	968331
919598	934916	934958	968332
919600	934917	934959	968333
920181	934918	934960	968334
920182	934919	968238	968335
920183	934920	968239	968336
920184	934921	968240	968337
920185	934922	968241	968338
920186	934923	968242	968339
920187	934924	968243	968340
920188	934925	968244	968341
920189	934926	968245	968342
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920195	934932	968306	968348
920196	934933	968307	968349
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934902	934938	968312	968354
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December 15, 1987

Your File: 560 Our File: 2.10565

Mining Recorder Ministry of Northern Development and Mines 435 James Street South P.O. Box 5000 Thunder Bay, Ontario P7C 5G6

Dear Madam:

RE: Notice of Intent dated November 26, 1987 Geophysical (Electromagnetic and Magnetometer) Survey on Mining Claims TB 919496 et al in the Areas of Keezhik Lake (East Arm) and Ferguson Lake

The assessment work credits, as listed with the above-mentioned Notice of Intent, have been approved as of the above date.

Please inform the recorded holder of these mining claims and so indicate on your records.

Yours sincerely,

W.R. Cowan, Manager Mining Lands Section Mines and Minerals Division

Whitney Block, Room 6610 Queen's Park Toronto, Ontario M7A 1W3

Telephone: (416) 965-4888

DM:pl Enclosure: Technical Assessment Work Credits

cc: Mr. G.H. Ferguson Mining & Lands Commissioner Toronto, Ontario Resident Geologist Thunder Bay, Ontario

Pure Gold Resources Inc. 1210 Main Street W. North Bay, Ontario P1B 2W6



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Ministry of Northern Development **Technical Assessment** Work Credits

	2.10565
November 26,1987	Mining Recorder's Report of Work No. 560

Descended Unidae	·
Pure Gold Resource	s Inc.
XXXXXXXX Area Keezhik Lake (East	Arm) and Ferguson Lake
Type of survey and number of Assessment days credit per claim	Mining Claims Assessed
Geophysical 40 days	TB-919496 to 501 inclusive
Magnetometer 40 days	919503 to 08 inclusive 919510 to 15 inclusive 919517 to 22 inclusive
Radiometric days	919524 to 44 inclusive 919551 to 56 inclusive
	919559 to 75 inclusive
Other days	
Section 77 (19) See "Mining Claims Assessed" column	
Geological days	
Geochemical days	
Man days 🗌 🛛 Airborne 🗶	
Special provision	
Credits have been reduced because of partial coverage of claims.	
Credits have been reduced because of corrections to work dates and figures of applicant.	
Special credits under section 77 (16) for the following	mining claims
No credits have been allowed for the following mining	claims
X not sufficiently covered by the survey	insufficient technical data filed
TB-919576 to 80 inclusive	

The Mining Recorder may reduce the above credits if necessary in order that the total number of approved assessment days recorded on each claim does not exceed the maximum allowed as follows: Geophysical - 80; Geologocal - 40; Geochemical - 40; Section 77(19) - 60.
KEEZHIK LAKE CLAIMS CONTINUED

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CLAIM #	CLAIM #	CLAIM #	CLAIM #
919587	934905	934947	968321
919588	934906	934948	968322
919589	934907	934949	968323
919590	934908	934950	968324
919591	934909	934951	968325
919592	934910	934952	968326
919593	934911	934953	968327
919594	934912	934954	968328
919595	934913	934955	968329
919596	934914	934956	968330
919597	934915	934957	968331
919598	934916	934958	968332
919600	934917	934959	968333
920181	934918	934960	968334
920182	934919	968238	968335
920183	934920	968239	968336
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